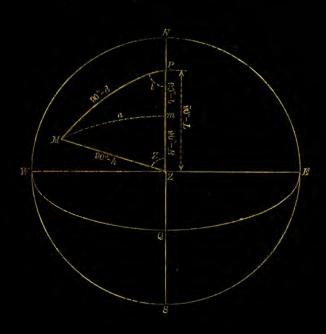
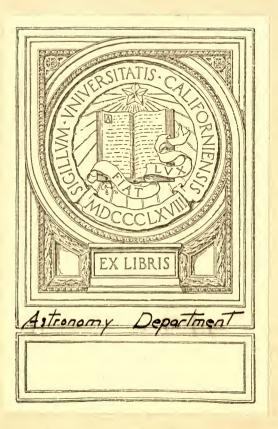


THE SIMPLEST AND READIEST IN SOLUTION

By Commander RADLER DE AQUINO BRAZILIAN NAVY

SECOND STEREOTYPED EDITION ENLARGED AND IMPROVED





Ready Reckoner and Altitude Correction Table

Number of minutes a, b, or Δd .

<i>x</i> +	0.'2	0.4	0.'6	0.'8	1'or	2'	3'	4'	5'	6'	7'	8'	9'	10'	II'	12'	13'	14'	15'	sec x	<i>x</i>
0 10 14 16 18	.20 .20 .19 .19	.40 .39 .39 .38	.60 ·59 ·58 ·58	.80 .79 .78 .77	1.00 0.93 ·97 .96 ·95	2.0 2.0 1.9 1.9	3.0 3.0 2.9 2.9 2.9	4.0 3.9 3.9 3.8 3.8	5.0 4.9 4.9 4.8 4.8	6.0 5.9 5.8 5.8 5.7	7.0 6.9 6.8 6.7 6.7	8.0 7.9 7.8 7.7 7.6	9.0 8.9 8.7 8.7 8.6	10.0 9.8 9.7 9.6 9.5	11.0 10.8 10.7 10.6 10.5	12.0 11.8 11.6 11.5	13.0 12.8 12.6 12.5 12.4	14.0 13.8 13.6 13.5 13.3	15.0 14.8 14.6 14.4 14.3	1.00 1.02 1.03 1.04 1.05	180 170 166 164 162
20 22 24 26 28	.19 .18 .18	·38 ·37 ·37 ·36 ·35	.56 .56 .55 .54 .53	·75 ·74 ·73 ·72 ·71	0.94 .93 .91 .90 .88	1.9 1.8 1.8	2.8 2.7 2.7 2.6	3.8 3.7 3.7 3.6 3.5	4.7 4.6 4.6 4.5 4.4	5.6 5.5 5.4 5.3	6.6 6-5 6.4 6.3 6.2	7·5 7·4 7·3 7·2 7·1	8.5 8.3 8.2 8.1 7.9	9.4 9.3 9.1 9.0 8.8	10.3 10.2 10.0 9.9 9.7	11.3 11.1 11.0 10.8 10.6	12.2 12.1 11.9 11.7 11.5	13.2 13.0 12.8 12.6 12.4	14.1 13.9 13.7 13.5 13.2	1.06 1.08 1.09 1.11	150 158 156 154 152
30 31 32 33 34 35 36 37 38 39	.17 .17 .17 .17 .16 .16 .16	.35 .34 .34 .33 .33 .32 .32 .32 .32	.52 .51 .50 .50 .49 .49 .48 .47	.69 .68 .67 .66 .66 .65 .64 .63	0.87 .86 .85 .84 .83 0.82 .81 .80 .79	I.7 I.7 I.7 I.7 I.6 I.6 I.6 I.6	2.6 2.5 2.5 2.5 2.5 2.4 2.4 2.4 2.3	3.5 3.4 3.4 3.3 3.3 3.2 3.2 3.2	4·3 4·3 4·2 4·2 4·1 4·1 4·0 4·0 3·9 3·9	5.2 5.1 5.0 5.0 4.9 4.9 4.8 4.7	6.1 6.0 5.9 5.8 5.7 5.6 5.5 5.4	6.9 6.8 6.7 6.6 6.6 6.5 6.4 6.3	7.8 7.7 7.6 7.5 7.5 7.4 7.3 7.2 7.1 7.0	8.7 8.6 8.5 8.4 8.3 8.2 8.1 8 0 7.8	9.5 9.4 9.3 9.2 9.1 9.0 8.9 8.8 8.5	10.4 10.3 10.2 10.1 9.9 9.8 9.7 9.6 9.5 9.3	11.3 11.1 11.0 10.9 10.8 10 6 10 5 10 4 10 2	12.1 12.0 11.9 11.7 11.6 11.5 11.3 11.2 11.0	13.0 12.9 12.7 12.6 12.4 12.3 12 1 12.0 11.8	I.15 I.17 I.18 I.19 I.21 I.22 I.24 I.25 I.27 I.29	150 149 148 147 146 145 144 143 142
40 41 42 43 44 45 46 47 48 49	.15 .15 .15 .14 .14 .14 .14	.31 .30 .30 .29 .29 .28 .28 .27 .27	.46 .45 .45 .44 .43 .42 .42 .41 .40	.61 .60 .59 .58 .57 .56 .55 .54	0.77 •75 •74 •73 •72 0.71 •69 •68 •67	I.5 I.5 I.5 I.4 I.4 I.4 I.4 I.3	2.3 2.2 2.2 2.2 2.1 2.1 2.0 2.0	3.1 3.0 3.0 2.9 2.9 2.8 2.8 2.7 2.7	3.8 3.7 3.7 3.6 3.5 3.4 3.3 3.3	4.6 4.5 4.5 4.4 4.3 4.2 4.2 4.1 4.0 3.9	5.4 5.3 5.2 5.1 5.0 4.9 4.8 4.7 4.6	6. I 6. o 5. 9 5. 9 5. 7 5. 6 5. 5 5. 4 5. 2	6.9 6.8 6.7 6.6 6.5 6.4 6.3 6.1 6.0 5.9	7.7 7.5 7.4 7.3 7.2 7.1 6.9 6.8 6.7 6.6	8.4 8.3 8.2 8.0 7.9 7.8 7.6 7.5 7.4 7.2	9.2 9.1 8.9 8.8 8.6 8.5 8.3 8.2 8.0 7.9	9.8 9.7 9.5 9.4 9.2 9.0 8.9 8.7 8.5	10.7 10.6 10.4 10.2 10.1 9.9 9.7 9.5 9.4 9.2	11.5 11.3 11.1 11.0 10.8 10.6 10.4 10.2 10.0 9.8	1.31 1.33 1.35 1.37 1.39 1.41 1.44 1.47	140 139 138 137 136 135 134 133 132
50 51 52 53 54 55 55 57 59	.13 .13 .12 .12 .11 .11 .11	.26 .25 .25 .24 .24 .23 .22 .22 .21	·39 ·38 ·37 ·36 ·35 ·34 ·34 ·33 ·32 ·31	.51 .50 .49 .48 .47 .46 .45 .44 .42	0.64 .63 .62 .60 .59 0.57 .56 .54 .53	I.3 I.2 I.2 I.2 I.1 I.1 I.1	1.9 1.8 1.8 1.7 1.7 1.6 1.6	2.6 2.5 2.4 2.4 2.3 2.2 2.2 2.1 2.1	3.2 3.1 3.0 2.9 2.9 2.8 2.7 2.6 2.6	3.9 3.8 3.7 3.6 3.5 3.4 3.4 3.3 3.2 3.1	4.5 4.4 4.3 4.2 4.1 4.0 3.9 3.8 3.7 3.6	5.1 5.0 4.9 4.8 4.7 4.6 4.5 4.4 4.2 4.1	5.8 5.7 5.5 5.4 5.3 5.2 5.0 4.9 4.8 4.6	6.4 6.3 6.2 6.0 5.9 5.7 5.6 5.4 5.3	7.1 6.9 6.8 6.6 6.5 6.3 6.2 6.0 5.8	7.7 7.6 7.4 7.2 7.1 6.9 6.7 6.5 6.4 6.2	8.4 8.2 8.0 7.8 7.6 7.5 7.3 7.1 6.9	9.0 8.8 8.6 8.4 8.2 8.0 7.8 7.6 7.4	9.6 9.4 9.2 9.0 8.8 8.6 8.4 8.2 7.9	1.56 1.59 1.62 1.66 1.70 1.74 1.79 1.84 1.89	130 129 128 127 126 125 124 123 122 121
60 61 62 63 64 65 66 67 68 69	.10 .09 .09 .09 .08 .08 .08	.20 .19 .19 .18 .17 .16 .16	.30 .29 .28 .27 .26 .25 .24 .23 .22	.40 .39 .38 .36 .35 .34 .33 .31 .30	0.50 .48 .47 .45 .44 0.42 .41 .39 .37	1.0 1.0 0.9 0.9 0.8 0.8 0.8	I.5 I.4 I.4 I.3 I.3 I.2 I.2 I.1	2.0 1.9 1.8 1.8 1.7 1.6 1.6 1.5	2.5 2.4 2.3 2.3 2.2 2.1 2.0 2.0 1.9	3.0 2.9 2.8 2.7 2.6 2.5 2.4 2.3 2.2 2.2	3.5 3.4 3.3 3.2 3.1 3.0 2.8 2.7 2.6 2.5	4.0 3.9 3.8 3.6 3.5 3.4 3.3 3.1 3.0 2.9	4.5 4.4 4.2 4.1 3.9 3.8 3.7 3.5 3.4 3.2	5.0 4.8 4.7 4.5 4.4 4.2 4.1 3.9 3.7 3.6	5.5 5.3 5.2 5.0 4.8 4.6 4.5 4.1 3.9	6.0 5.8 5.6 5.4 5.3 5.1 4.9 4.7 4.5 4.3	6.5 6.3 6.1 5.9 5.7 5.5 5.3 5.1 4.9 4.7	7.0 6.8 6.6 6.4 6.1 5.9 5.7 5.5 5.2 5.0	7.5 7.3 7.0 6.8 6.6 6.3 6.1 5.9 5.6	2.00 2.06 2.13 2.20 2.28 2.37 2.46 2.56 2.67 2.79	1120 119 118 117 116 115 114 113 112 111
70 71 72 73 74 75 76 77 78 79	.07 .07 .06 .06 .05 .05 .04 .04	.12 .11 .10 .10 .09		·22 ·21 ·19 ·18 ·17	0.34 .33 .31 .29 .28 0.26 .24 .22 .21	0.7 0.6 0.6 0.6 0.5 0.5 0.4 0.4	0.9	I.2 I.1 I.0 I.0 0.9 0.8	1.5 1.5 1.4 1.3 1.2	2. I 2. 0 1. 9 1. 8 1. 7 1. 6 1. 5 1. 3 1. 2	2.0	2.5 2.3 2.2 2.1 1.9 1.8 1.7	2.6 2.5 2.3 2.2 2.0 1.9	3.4 3.3 3.1 2.9 2.8 2.6 2.4 2.2 2.1	3.8 3.6 3.4 3.2 3.0 2.8 2.7 2.5 2.3 2.1	4. I 3. 9 3. 7 3. 5 3. 3 3. I 2. 9 2. 7 2. 5 2. 3	4.4 4.2 4.0 3.8 3.6 3.4 3.1 2.9 2.7 2.5	4.8 4.6 4.3 4.1 3.9 3.6 3.4 3.1 2.9 2.7	5.1 4.9 4.6 4.4 4.1 3.9 3.6 3.4 3.1 2.9	2.92 3.07 3.24 3.42 3.63 3.86 4.13 4.45 4.81 5.24	110 109 108 107 106 105 104 103 102 101
80 81 82 83 84 85 86 87 88 89	.03 .03 .02 .02 .02 .01 .01	.05 .04 .03 .03 .02 .01	.09 .08 .07 .06 .05 .04 .03 .02	.04	.02		0.1	0.5 0.4 0.3 0.3 0.2 0.1 0.1	0.6 0.5 0.4 0.3 0.3 0.2 0.1	0.6 0.5 0.4 0.3	0.9 0.7 0.6 0.5 0.4 0.2 0.1	1. I 1.0 0.8 0.7 0.6 0.4 0.3 0.1	1.1 0.9 0.8 0.6 0.5 0.3	1.7 1.6 1.4 1.2 1.0 0.9 0.7 0.5 0.3 0.2	1.9 1.7 1.5 1.3 1.1 1.0 0.8 0.6 0.4 0.2	2.1 1.9 1.7 1.5 1.3 1.0 0.8 0.6 0.4 0.2	2.3 2.0 1.8 1.6 1.4 1.1 0.9 0.7 0.5 0.2	2.4 2.2 1.9 1.7 1.5 1.2 1.0 0.7 0.5 0.2	2.6 2.3 2.1 1.8 1.6 1.3 1.0 0.8 0.5 0.3	57.3	99 98 97 96 95 94 93 92 91 90

Ready Reckoner and Altitude Correction Table

Number of minutes a, b, or Δd .

x +	cos x	16'	17'	18'	19'	20'	21'	22'	23'	24'	25'	26'	27'	28′	29'	30'	sec x	x
0 10 14 16 18	1.00 0.98 .97 .96 .95	16.0 15.8 15.5 15.4 15.2	17.0 16.7 16.5 16.3 16.2	18.0 17.7 17.5 17.3 17.1	19.0 18.7 18.4 18.3 18.1	20.0 19.7 19.4 19.2 19.0	21.0 20.7 20.4 20.2 20.0	22.0 21.7 21.3 21.1 20.9	23.0 22.7 22.3 22.1 21.9	24.0 23.6 23.3 23.1 22.8	24.0 23.8	26.0 25.6 25.2 25.0 24.7	27.0 26.6 26.2 26.0 25.7	28.0 27.6 27.2 26.9 26.6	29.0 28.6 28.1 27.9 27.6	30.0 29.5 29.1 28.8 28.5	I.00 I.02 I.03 I.04 I.05	180 170 166 164 162
20 22 24 26 28	0.94 .93 .91 .90 .88	15.0 14.8 14.6 14.4 14.1	16.0 15.8 15.5 15.3 15.0	15.9	17.1	18.8 18.5 18.3 18.0	19.7 19.5 19.2 18.9 18.5	20.7 20.4 20.1 19.8 19.4	21.6 21.3 21.0 20.7 20.3	22.6 22.3 21.9 21.6 21.2	22.8 22.5 22.1	24.4 24.1 23.8 23.4 23.0	25.4 25.0 24.7 24.3 23.8	26.3 26.0 25.6 25.2 24.7	27. 3 26. 9 26. 5 26. 1 25. 6	28.2 27.8 27.4 27.0 26.5	1.06 1.08 1.09 1.11 1.13	160 158 156 154 152
30 31 32 33 34 35 36 37 38 39	0.87 .86 .85 .84 .83 0.82 .81 .30 .79	13.9 13.7 13.6 13.4 13.3 13.1 12.9 12.8 12.6	14.7 14.6 14.4 14.3 14.1 13.9 13.8 13.6 13.4	14.7	16.5 16.3 16.1 15.9 15.8 15.6 15.4 15.2 15.0 14.8	17.3 17.1 17.0 16.8 16.6 16.4 16.2 16.0 15.8	18.2 18.0 17.8 17.6 17.4 17.2 17.0 16.8 16.5 16.3	19.1 18.9 18.7 18.5 18.2 18.0 17.8 17.6 17.3	19.9 19.7 19.5 19.3 19.1 18.8 18.6 18.4 18.1	20.4 20. I	21.7 21.4 21.2 21.0 20.7 20.5 20.2 20.0 19.7	22.5 22.3 22.0 21.8 21.6 21.3 21.0 20.8 20.5	23.4 23.1 22.9 22.6 22.4 22.1 21.8 21.6 21.3 21.0		25. I 24. 9 24. 6 24. 3 24. 0 23. 8 23. 5 23. 2 22. 9 22. 5	26.0 25.7 25.4 25.2 24.9 24.6 24.3 24.0 23.6	1.15 1.17 1.18 1.19 1.21 1.22 1.24 1.25 1.27	150 149 148 147 146 145 144 143 142 141
40 41 42 43 44 45 46 47 48 49	0.77 .75 .74 .73 .72 0.71 .69 .68 .67	12.3 12.1 11.9 11.7 11.5 11.3 11.1 10.9 10.7	13.0 12.8 12.6 12.4 12.2 12.0 11.8 11.6 11.4	13.4 13.2 12.9 12.7 12.5 12.3	13.4 13.2	15.3 15.1 14.9 14.6 14.4 14.1 13.9 13.6 13.4 13.1	16. 1 15.8 15.6 15.4 15.1 14.8 14.6 14.3 14.1	16.9 16.6 16.3 16.1 15.8 15.6 15.3 15.0 14.7	17.6 17.4 17.1 16.8 16.5 16.3 16.0 15.7 15.4	18.4 18.1 17.8 17.6 17.3 17.0 16.7 16.4 16.1	19.2 18.9 18.6 18.3 18.0 17.7 17.4 17.0 16.7	19.9 19.6 19.3 19.0 18.7 18.4 18.1 17.7 17.4	20.7 20.4 20.1 19.7 19.4 19.1 18.8 18.4 18.1	20.8 20.5 20.1 19.8 19.5	22.2 21.9 21.6 21.2 20.9 20.5 20.1 19.8 19.4	23.0 22.6 22.3 21.9 21.6 21.2 20.8 20.5 20.1	1.31 1.33 1.35 1.37 1.39 1.41 1.44 1.47 1.49 1.52	140 139 138 137 136 135 134 133 132 131
50 51 52 53 54 55 56 57 58 59	0.64 .63 .62 .60 .59 0.57 .56 .54 .53	10.3 10.1 9.9 9.6 9.4 9.2 8.9 8.7 8.5 8.2	10.9 10.7 10.5 10.2 10.0 9.8 9.5 9.3 9.0 8.8	11.6 11.3 11.1 10.8 10.6 10.3 10.1 9.8 9.5 9.3	12.0 11.7 11.4 11.2	12.9 12.6 12.3 12.0 11.8 11.5 11.2 10.9 10.6 10.3	13.5 13.2 12.9 12.6 12.3 12.0 11.7 11.4 11.1	14. I 13.8 13.5 13.2 12.9 12.6 12.3 12.0 11.7	14.8 14.5 14.2 13.8 13.5 13.2 12.9 12.5 12.2 11.8	15.4 15.1 14.8 14.4 14.1 13.8 13.4 13.1 12.7	16.1 15.7 15.4 15.0 14.7 14.3 14.0 13.6 13.2	16.7 16.4 16.0 15.6 15.3 14.9 14.5 14.2 13.8	16.2 15.9	18.0 17.6 17.2 16.9 16.5 16.1 15.7 15.2 14.8	17.5	19.3 18.9 18.5 18.1 17.6 17.2 16.8 16.3 15.9	1.56 1.59 1.62 1.66 1.70 1.74 1.79 1.84 1.89	130 129 128 127 126 125 124 123 122 121
60 61 62 63 64 65 66 67 68	0.42 .41 .39 .37	8.0 7.8 7.5 7.3 7.0 6.8 6.3 6.0 5.7	8.5 8.2 8.0 7.7 7.5 7.2 6.9 6.4 6.1	9.0 8.7 8.5 8.2 7.9 7.6 7.3 7.0 6.7 6.5	9.5 9.2 8.9 8.6 8.3 8.0 7.7 7.4 7.1 6.8	10.0 9.7 9.4 9.1 8.8 8.5 8.1 7.8 7.5 7.2	10.5 10.2 9.9 9.5 9.2 8.9 8.5 8.2 7.9	11.0 10.7 10.3 10.0 9.6 9.3 8.9 8.6 8.2 7.9	11.5 11.2 10.8 10.4 10.1 9.7 9.4 9.0 8.6 8.2	10.9 10.5 10.1 9.8 9.4 9.0	11.7 11.3 11.0 10.6 10.2 9.8 9.4	11.0 10.6 10.2 9.7	10.5	11.8 11.4 10.9 10.5	12.7 12.3 11.8 11.3 10.9	11.7	2.00 2.06 2.13 2.20 2.28 2.37 2.46 2.56 2.67 2.79	120 119 118 117 116 115 114 113 112
70 71 72 73 74 75 76 77	33 .31 .29 .28 0.26 .24 .22	3.3	5.3 5.0 4.7 4.4 4.1 3.8 3.5	5·3 5·0 4·7 4·4 4.0 3·7	5.6 5.2 4.9 4.6 4.3 4.0	4.5	5.8 5.4 5.1 4.7 4.4	6.8 6.4 6.1 5.7 5.3 4.9 4.6	6.3 6.0 5.6 5.2 4.8	7.8 7.4 7.0 6.6 6.2 5.8 5.4	8.1 7.7 7.3 6.9 6.5 6.0 5.6	8.5 8.0 7.6 7.2 6.7 6.3 5.8	8.8 8.3 7.9 7.4 7.0 6.5 6.1 5.6	8.7 8.2 7.7 7.2 6.8 6.3 5.8	9.4 9.0 8.5 8.0 7.5 7.0 6.5 6.0	9.8 9.3 8.8 8.3 7.8 7.3 6.7 6.2	3.24 3.42 3.63 3.86 4.13 4.45 4.81	110 109 108 107 106 105 104 103 102 101
80 81 82 83 83 84 85 86 86 86 86 86 86 86 86 86 86 86 86 86	0.17 .16 .14 .12 .10 0.09 .07 .05 .03	2.5 2.2 1.9 1.7 1.2 1.1 0.8 0.6	3 3.0 5 2.7 2 2.4 2 1.8 4 1.5 1 1.2 3 0.9 6 0.6 6 0.6	3.11 2.88 2.55 2.22 1.99 1.60 0.90 0.60 0.33	3·3 3.0 2.6 2·3 2.0 1.7 1.3 1.0 0.7 0.3	3·5 3·1 2·8 2·4 2·1 1·7 1·4 1·0 0·7 0·3	3.6 3.3 2.9 2.6 2.2 1.8 1.5 1.1	3.4 3.1 2.7 2.3 1.9 1.5 1.2 0.8	3.6 3.2 2.8 2.4 2.0 1.6 1.2 0.8	4.23 3.83 3.33 2.99 2.55 2.11 1.77 1.38 0.88	4·3 3·9 3·5 3.0 2.6 2.2 1.7 1.3 0.9 C.4	4.5 4.1 3.6 3.2 2.7 2.3 1.8 1.4 0.9 0.5	4.2 3.8 3.3 2.8 2.4 1.9 0.9 0.5	3.9 3.4 2.9 2.4 2.0 1.5 1.0	5.0 4.5 4.0 3.5 3.0 2.5 2.0 1.5 1.0 0.5	5.22 4.77 4.22 3.77 3.11 2.60 2.11 1.60 0.55	5.76 6.39 7.19 8.21 9.57 11.5 14.3 19.1 28.7 57.3	100 99 98 97 96 95 94 93 92 91

The "Newest" Navigation Altitude and Azimuth Tables, by Commander Radler de Aquino, Brazilian Navy, second edition, enlarged and improved, London, 1918. Published by J. D. Potter, 145 Minories, London, E. Price 12s. net.

A slightly improved method of finding the Altitude and Azimuth by means of my Tables has been developed recently whereby it is not necessary to *interpolate* and find the true values of b and t for the true value of declination d, as explained on pages xv, xxi, and xxv of my Tables. It is sufficient to find only in column a the values of b (generally a whole degree) and of t that correspond to an approximate value of d. This approximate value of d is always the tabular value nearest to the true value, provided t_A is near $t_{D.R.}$ b is combined in the usual way with L_A (also generally the whole degree nearest the dead-reckoning latitude) to find C, and h' and Z' are found corresponding to the a and a0. Now as a1 and a2 are for the tabular value of a3, we must correct them for the difference a2 between this tabular value and the true value of the declination. We know from page xvii that a change of altitude a2 and the angle of declination a3 is given by the formula: a4 and the angle a6 is the parallactic angle. If we call, in Fig. 2 on page xii, the angle a6.

The value of a is found on the same line with b, d, and t (a being practically the same for all three values of a). In the same way β is found on the same line opposite C, h, and C.

However, instead of finding C with L_A and b, it is in the great majority of cases better to find L_A from b and C, as explained below.

The working out of our typical example on page xix will show the great advantage of this improvement.

$$\frac{a = 52^{\circ} \text{ O'} \quad \text{G. A. T.} = 20^{\circ} \quad 50^{\circ} \quad 24^{\circ}}{L_{A.} = 37^{\circ} \quad \text{N}} \qquad d = 10^{\circ} \quad 27^{\circ} \quad \text{S}} \qquad \text{or } t_{G.} = 314^{\circ} \quad 51^{\prime} \quad \text{Pages 69 and 122, 2d. ed. 1912.}$$

$$\frac{b = 17^{\circ} \quad \dots \quad d' = 10^{\circ} \quad 22^{\prime} \quad \dots \quad t_{A.} = 53^{\circ} \quad 14^{\prime} \quad \text{E} \quad \dots \quad a = 76^{\circ} \cdot .5}{d - d' = + 5^{\prime}} \qquad G_{A.} = 8^{\circ} \quad 5^{\prime} \quad \text{W}$$

$$C = 54^{\circ} \quad \dots \quad h' = 21^{\circ} \quad 13^{\prime} \quad \dots \quad Z'_{A.} = \text{S} \quad 57^{\circ} \quad 42^{\prime} \quad \text{E} \quad \dots \quad \beta = 60^{\circ} \cdot .4$$

$$\Delta h = -3^{\prime} \cdot .7 \qquad \qquad M = 136^{\circ} \cdot .9$$

$$h_{A.} = 21^{\circ} \quad 9^{\prime} \cdot .3$$

$$h = 21 \quad .7$$

$$h - h_{A.} = -2^{\prime} \cdot .3$$

NOTE.—Numbers taken out of the Tables by Inspection are black-faced in order to distinguish them from data given or found.

In addition to the formulæ given on page xxviii for finding L_A , with b and C, we have added those for finding M with a and β .

$$d \text{ and } L_A \text{ same name } \begin{cases} t < 90^{\circ} & L_A < b : L_A = b - C \text{ and } M = a + \beta \\ L_A > b : L_A = b + C \text{ and } M = a - \beta \end{cases}$$

$$d \text{ and } L_A \text{ contrary names} \qquad : L_A = C + b \text{ and } M = \beta - a$$

$$d \text{ and } L_A \text{ contrary names} \qquad : L_A = C - b \text{ and } M = a + \beta$$

When $t > 90^{\circ}$ the sum $C + b > 90^{\circ}$ also, and we must subtract it from 180° to obtain L_{A} .

A simple inspection of these formulæ shows that no different rules are necessary with this new process. A knowledge of the approximate value of L_A is always known by dead-reckoning, and therefore, we can immediately find, in view of the fact that b and L_A are generally whole degrees, the value of C that combined with b will give us L_A . The tabular value h' nearest to the true altitude h shows us opposite it also the value of C.

The formulæ show also that when we *subtract* b and C to find L_A , we must add a and β to obtain M. When we *add* b and C to find L_A , we must *subtract* a and β from one another to obtain M.

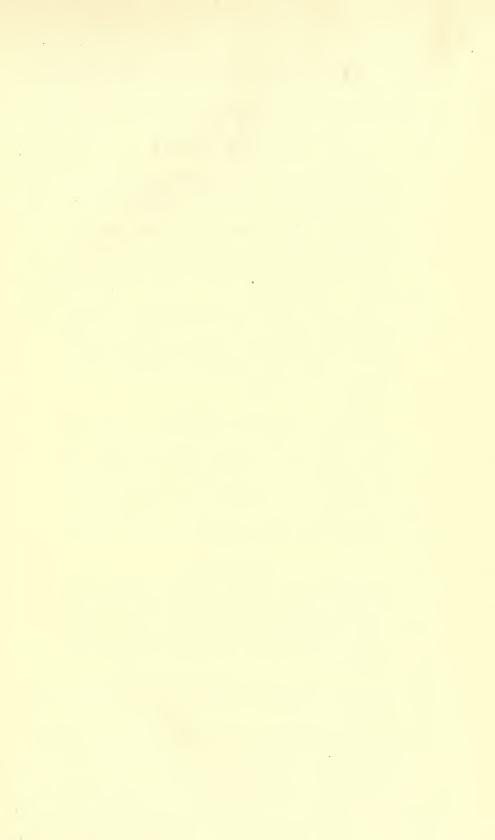
The "Altitude correction" $\Delta h = 3'.7$ is given immediately by our Table² on the back, where we enter at the top with $\Delta d = 5'$, and with $M = 137^{\circ}$ on the right hand side. If M is less than 90°, enter the Table on the left hand side. The correction has the same sign as d - d' or Δd when M is less than 90° and the contrary sign to d - d' or Δd when M is greater than 90°.

In this way Altitude and Azimuth from the assumed position are found by means of simple mnemonical rules without interpolating.

- ' As Δd is generally only a few minutes of arc, Z' does not need in practice any correction. The formula on page xvii: $\Delta Z = \sin M \sec h \Delta d$ shows us that ΔZ is always smaller than $\sec h \Delta d$. Under $h = 60^{\circ}$, ΔZ is always smaller than $2\Delta d$.
- ² Also by our Plane Traverse Tables in LAT. column if we enter them with Δd as D and with M or $180^{\circ} M$ as Course.

THE "NEWEST" NAVIGATION ALTITUDE AND AZIMUTH TABLES





ATTENTION!

Would you ever think of going to the trouble of calculating the elements of the NAUTICAL ALMANAC, viz. declination, right ascension, equation of time, &c., by means of formulæ and logarithms, when His Majesty's NAUTICAL ALMANAC Office tabulates these data every year? Certainly not.

Would you ever think of working out your dead-reckoning by means of formulæ and logarithms when the Plane Traverse Tables facilitate the direct solution of all problems related thereto? Not at all!

Why then go to the trouble to solve the astronomical triangle of position by means of complicated formulæ and logarithms when we have tabulated its elements in our "Altitude and Azimuth Tables" (Spherical Traverse Tables) and have given the simplest and readiest methods for solving all problems related thereto?

HOWEVER,

If you do not like the method for finding the altitude using an assumed position, use then the new Altitude Tables at the end of this book, and methods explained on page xxxviii for the azimuth.

They are also the "simplest and readiest in solution."

THE "NEWEST" NAVIGATION

ALTITUDE

AND

AZIMUTH TABLES

FOR FACILITATING THE DETERMINATION OF LINES OF POSITION AND GEOGRAPHICAL POSITION AT SEA

THE SIMPLEST AND READIEST IN SOLUTION

Plane and Spherical Traverse Tables for Solving all Problems of Navigation

By COMMANDER RADLER DE AQUINO BRAZILIAN NAVY

SECOND STEREOTYPED EDITION

ENLARGED AND IMPROVED

Sights "may be practically worked out so as to give the ship's place as accurately as it can be deduced from the observations, with hardly any calculation.

"One of the advantages in the use of this method is that no logarithmic work is required."

SIR WILLIAM THOMSON (LORD KELVIN). "Tables for Facilitating Sumner's Method at Sea." London, 1876. pp. iv. and v.

"È facile persuadersi che, dopo avere acquistata un po' di pratica, le operazioni descritte possono esser fatte con grande speditezza: l'uso della Tavola è facile e le regole da applicare sono indiscutibilmente semplici."

DOTT. ALBERTO ALESSIO, R.I.N. "Sulla Teoria e la Pratica della Nuova Navigazione Astronomica." Rivista Marittima for March 1909, Appendice, p. 59.

1918

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EXPRESSION OF OPINION

NAVY DEPARTMENT.

COPIA.

18111

WASHINGTON.

February 1, 1909.

SIR: Replying to your letter No. 17512, of the 21st ultimo, enclosing a copy of a letter from the Brazilian Ambassador, requesting an expression of the Department's opinion as to the scientific merit of the altitude and azimuth tables prepared by the Naval Attaché to his Embassy, of which you enclosed a copy and description, I have the honor to inform you that the Hydrographer of the U.S. Navy, to whom your letter and enclosures were referred, has submitted the following report, which is

quoted for your information:

"Existing tables give the distance and bearing, on the globe or the celestial sphere or any other sphere, of any place from every other place, and consequently the zenith distance and bearing, that any celestial body would have at any given time to an observer situated in any geographical position. So that, an observer in a geographical position as yet unknown, about to measure the altitude of a celestial body for position, may assume beforehand a geographical position in the region of his station and find from the tables the zenith distance and bearing which the celestial body would have if observed from the assumed position; and then, comparing the zenith distance, so taken from the tables, with the zenith distance shown by the measured altitude, may at once find the Sumner line by laying off from the assumed geographical position, in the direction of the bearing, an intercept equal to the difference of these zenith distances and drawing at right angles to the bearing through the point thus found. All cases of cœlo-navigation are thus brought under a single rule.

"Aquino's purpose is to abridge the extent of the existing tables by tabulating the solutions of the two right-angled spherical triangles, into which the astronomical triangle may always be divided, with values of the argument no nearer together than 30' in one case, and 1° in the other. To make this plan feasible, his purpose is to sacrifice the freedom of choice now existing with reference to the assumed geographical position, and, by short calculation, to find instead an auxiliary geographical position so placed that the proposed tables may be entered without interpolation between the tabular values of the arguments, which are, in fact, designedly spaced too far apart for successful interpolation. The advantage of having one simple rule for the solution of all cases is also somewhat disturbed by necessary variations from the singleness of the rule in order to adapt the proposed tables to varying combinations of data arising from different relative positions of the observer and the

observed celestial body.

"The plan of the proposed work, as outlined in the enclosed publications, is sound in principle and scientific in conception; and the tables will possess the merit of being compressed into a small book."

I have the honor to be, Sir,

Very respectfully,

TRUMAN H. NEWBERRY, Secretary.

THE HONORABLE
THE SECRETARY OF STATE.



Confere. E. L. CHERMONT. Conforme com o original no Archivo da Embaixada do Brazil em Washington. SYLVINO GURGEL DO AMARAL, Conselheiro de Embaixada.

NOTE.—This expression of opinion is made public by special permission of the Hon.

Secretary of the Navy. O.N.I. No. 9864 of 1909.

^{1 &}quot;A Navegação sem logarithmos." Imprensa Nacional, Rio de Janeiro, 1903, and "Altitude and Azimuth Tables for facilitating the Determination of Lines of Position and Geographical Position at Sea." Reprinted from the United States Naval Institute Proceedings for December, 1908.

BOOK NOTICES

Of the U.S. Naval Institute Proceedings, March, 1910

"ALTITUDE AND AZIMUTH TABLES," 1910. By Lieutenant Radler de Aquino, Brazilian Navy.

After a careful examination of this book and of the methods given for the solution of the astronomical triangle there can be no doubt of its practicability and of its claim, "The simplest and readiest in solution."

In the solution of the line of position for the sun, which is by far the most common of all sights, and employing all figures to get functions as closely as given in the Nautical Almanac, which in practice is not necessary, a comparison of the two methods is as follows:—

		Figures.	Book openings.	Time.
Common to both		. 177	8	9 ^m 30 ^s
Peculiar to each		∫ 101 Aquino	2	4 ^m 7 ^m 3Cs
Peculiar to each	•	. { 101 Aquino 138 St. Hilaire	2	4 ^m

Upon examination of the above table it can be immediately seen how much quicker in solution the Aquino is. In point of accuracy of results within the limits of 70 declination, and taking into consideration the errors of observation, there is no choice. There is less chance of making errors in working on account of the fact that only four functions have to be picked out accurately from the tables, whereas in the St. Hilaire eight have to be found. In comparing the two methods the part common to both is not considered.

In the case of the meridian altitudes the ordinary method of combining the zenith distance and declination is better than the method shown in this book, on account of it being necessary to remember one precept instead of four.

The method of finding latitude from a sight of Polaris presents no advantages over that given in the back of the Nautical Almanac for the current year, and has less advantage over that given in the Almanac of 1912.

The determination of the line of position without azimuths is to be commended and, if the altitude is to be determined by the tables of this book, is of great value.

The necessity of the rectification of lines of position occurs very rarely in practice, but when it does happen this method is an excellent one.

The identification of celestial bodies and the finding of the approximate altitude and azimuth before taking a sight are, under the present great interest in the use of stars for navigational purposes, of great value, and when the tables are once thoroughly understood, very easy to find.

Azimuths can be determined with ease and necessary accuracy by means of these tables

The use of these to find the Great Circle Course is not recommended. Lunar distances have been abandoned by navigators.

Taken as a whole, this book cannot be too highly recommended, and all navigators should possess a copy. It is to be hoped that the author will publish the larger book he is making out for his own use.

G. R. MARVELL,

INTRODUCTION

The determination of lines of position (from which geographical position—latitude and longitude—is deduced at sea), the identification of celestial bodies and the determination of distance and course in Great Circle Sailing are the three principal problems of Navigation depending upon the solution of a spherical triangle.

In each problem we have two sides and the included angle to find the third side and one of the other angles. This means that all the three problems can be solved in the same way, by the same formulæ,

by the same method, and by the same tables.

Most of the problems of celestial Navigation depend upon the solution of a right-angled spherical triangle, and as the three principal problems are solved by dividing the spherical triangle into two right-angled triangles, they *all* may be easily and readily solved *without logarithms* by aid of the appended tables, which, however, were especially arranged for facilitating the determination of lines of position and the identification of celestial bodies at sea.

The method used for determining lines of position is general, every sight is worked out the same way; no special classification needs to be made before trying to work it out. Whether the sight is a circummeridian, an ex-meridian, or a time-sight, it is always worked out the same way. At the same time, no signs or naming of auxiliary data comes in to confuse the navigator. The only calculations involved are two small multiplications (not always necessary), and the finding of C with C and C0, by the use of simple formulæ, without giving consideration to algebraic signs or arcs greater than 90°.

The tables will also enable the navigator in latitudes above 45° to

With the exception of the tables for rectifying lines of position, all the others are well known and need no explanation. In the tables for correcting altitudes, the corrections were calculated with data (mean refractions, mean dip of the horizon, parallax in altitude, &c.) tabulated in the *Connaissance des Temps*, published by the

Bureau des Longitudes, Paris.

¹ Besides these tables our volume contains tables for converting intervals of mean solar time into those of sidereal time (acceleration); for converting time into arc, and vice versa; for the total correction of altitudes of Stars and Planets, the Sun and the Moon; change of altitude per minute of arc of hour angle, change of azimuth per minute of arc of altitude; for controlling the coincidence of lines of position; azimuths of *Polaris*; change of altitude per minute of time, and for rectifying lines of position. Also Plane Traverse Tables, a Ready Reckoner, &c.

determine with great accuracy lines of position on Mercator's chart without azimuths.

Time-azimuths for compass correction and control are found without interpolation by the same method used for determining lines of position, which, of course, is a decided advantage.

Such questions as: Where are we? What star is that? &c., will receive a prompt and accurate reply when the problem is worked out by our methods and our tables.

Fortunately most of the problems do not require great approximation, and for this reason interpolations are practically unnecessary.

The omission of Lunar Distances from the Nautical Almanac, as "no longer of sufficient use to justify their retention," has forced upon navigators the necessity of knowing how to calculate them.

This problem is similar to the problem of determining distance in Great Circle Sailing, and we believe that from the sailor's point of view our method (and formulæ) will prove more satisfactory than the one given in the Nautical Almanac, because it does not involve the use of algebraic signs or arcs greater than 90°, always a cause of difficulty, confusion, and error.

Many valuable suggestions received from Dott. Giuseppe Pesci, of the Royal Italian Naval Academy, Livorno, Italy, have been embodied in this work, and it gives us great pleasure to acknowledge here our grateful thanks.

The author hopes that navigators will appreciate the great advantages these tables present. Indeed, we may safely say: They are "the simplest and readiest in solution."

On board the Brazilian battleship Minas Geraes, NEWCASTLE-UPON-TYNE, November 11, 1909.

INTRODUCTION TO SECOND EDITION

The addition of the complementary column c/C reducing to a minimum the work of combining L and b, of a Plane Traverse Table for distances up to 300 miles, of a Ready Reckoner, of the Sun's upper Limb Correction Table, of the Table giving the change of hour angle per minute of arc of altitude and a most careful and complete revision of the tables and text represent the improvements and further simplifications to be found in this new edition. A new set of Tables for calculating the Altitude have been added for use of those people who do not like to use the assumed position. They are also "the simplest and readiest in solution."

HYDROGRAPHIC OFFICE, RIO DE JANEIRO, November 11, 1911.

CIRCLES, CURVES, AND LINES OF POSITION

A line of position is just as valuable as the isolated knowledge of latitude or longitude, and represents the exact and only true interpretation of a sight.

When a navigator at a given instant of Greenwich (known by a chronometer regulated to mean or sidereal time) observes the altitude of a celestial body, he determines *ipso facto* on the celestial sphere a small circle passing through his zenith.¹

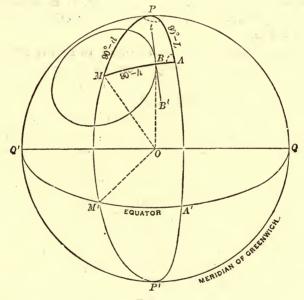


FIG. I.

This circle is determined by its centre and its radius. The centre of the circle is M, the centre of the celestial body at the moment of the observation, and is determined by the declination d or MM' (sometimes called Geographical Latitude) of the body, and by its

¹ This discovery was first made by Captain THOMAS H. SUMNER, an American shipmaster, in 1837, and was explained on page 42 of his work, "A New and Accurate Method of Finding a Ship's Position at Sea, by Projection on Mercator's Chart," Boston, 1843.

Vide also BARTHET, "Méthode graphique pour faire le point à la mer," published in the Annales maritimes et coloniales, Paris, 1847, for an account of Captain Sumner's discovery.

hour angle from Greenwich, QPM' (called its Geographical Longitude). The radius is the body's true zenith distance, MB (the complement of its true altitude). With these elements we could, if practical, draw the circle on a globe. This circle is known as the *circle of position*, because it contains the navigator's zenith corresponding to his position on the surface of the Earth.

The transformation affecting all spherical figures when we pass from the terrestrial globe to Mercator's chart also involves the circle of position, which is transformed into a curve of position, open or closed, according to the position of the poles in relation to the circle.

In order to know his position, it is not necessary for the navigator to draw the whole curve on the chart, and, in view of the difficulty of even drawing a small portion of it in the vicinity of the observer (always indicated by the D. R. position A), it is substituted by a straight line of position, BB', representing practically the necessary part of the curve.

This straight line of position, in order to secure the best results, ought to be always determined on the chart, or elsewhere, by the method invented thirty-five years ago by Admiral A. BLOND DE MARCQ SAINT-HILAIRE, French Navy.

"The great advantage of this method of obtaining a line of position," as Commander W. C. P. Muir, U.S. Navy, Head of the Department of Navigation of the U.S. Naval Academy, explicitly states in italics in his excellent treatise on "Navigation and Compass Deviations," second edition, 1908, p. 640, "lies in the fact, that since the formulæ make it available practically without limitations as to azimuth, altitude, or hour angle, it furnishes one method equally applicable to all conditions, whether these conditions would otherwise require the formulæ of a time-sight, a $\phi'' \phi'$ sight, or that of a body observed near the meridian."

It consists in determining a particular point B (known as the "computed point") of the circle of position—the intersection of AM, the vertical circle of the celestial body passing through the D. R. position A with the circle of position. These two circles intersect each other at right-angles, and therefore the straight line of position will be also perpendicular to the body's true bearing.

Thus the determination of the line of position, containing the observer's position, consists in constructing a straight line drawn through the computed point B at right-angles to the body's true bearing.

In order to determine the computed point B when the position by D. R. A is given, we lay off from this point, as shown in Fig. 1, a

² Published by the United States Naval Institute, Annapolis, Md., U.S.A., price

five dollars gold.

¹ Vide "Calcul du point observé," Revue maritime et coloniale, vol. xlvi., 1875, pages 341 and 714.

CIRCLES, CURVES, AND LINES OF POSITION

distance, AB, equal to the difference between the two zenith distances: the D. R. AM, and the *true* BM (or between the two altitudes: the *true* and the D. R. with opposite sign). The extremity of this length is the computed point B. This point is *always* nearer to the true position than the position by D. R., and represents the most probable position of the observer, when only one observation is available.

The difference between the two altitudes is called *altitude difference* or *intercept*.

The position by D. R. A, the altitude difference AB, and the body's azimuth PAM are the elements necessary and sufficient for determining a line of position at sea.

The position by D. R. is generally computed up to the time of observation, the true altitude is found by taking and correcting the observed altitude; the calculated altitude and azimuth (from which the true bearing is found) are easily and rapidly determined by our tables as explained hereafter.

In order, however, to do away with interpolations and corrections which otherwise would have had to be made before finding the altitude and azimuth, we take an assumed latitude and longitude instead of the latitude and longitude by D. R.¹ Referring to Fig. 4 on page xxvi, we consider A' (the assumed position) instead of A (the position by D. R.) for determining the line of position.

The advantages of using an assumed position instead of the position by D. R. have not been fully appreciated by the majority of navigators. No greater accuracy is gained by determining the line of position from A than from A', while the use of this position, as we will see further on, facilitates and reduces the computations very much, thus minimising the chances of error, &c.

Finally, the problem of determining a line of position at sea reduces itself to find how far (in miles) the line of position is from the ASSUMED position, and in what direction it lies.

^{1 &}quot;A Navegação sem Logarithmos" (Navigation without Logarithms). Imprensa Nacional. Rio de Janeiro, 1903. Published by order of the Minister of Marine. This work was preceded by an article by the author in the Revista Maritima Brazileira, Oct. 1902. "Taboas para achar alturas e azimuths, etc." The present tables represent an enlarged, improved, and very simplified edition of "A Navegação sem Logarithmos." Vide also "Resolução Nomographica do Triangulo de Posição" by DOTT. G. PESCI. Translated from the Italian into Portuguese by the author of these tables and reprinted from the Revista Maritima Brazileira, Nov. and Dec. 1907, and Feb. 1908, and DOTT. PESCI's recent "Studio critico": Sulle "Tables for facilitating Sumner's Method at Sea," di Lord Kelvin, in the Rivista Maritima for January 1909, page 43.

GENERAL PRINCIPLE AND EQUATIONS

In Fig. 2, P is the elevated pole and PMZ is the astronomical triangle of position projected on the plane of the horizon.

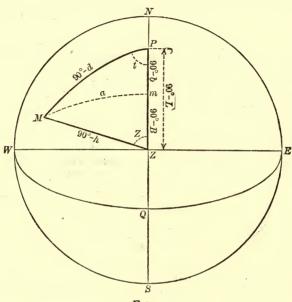


FIG. 2.

If we let fall a perpendicular from M on PZ, it will divide the triangle of position into two right-angled triangles. Let us call the perpendicular a and the two parts into which PZ is divided $90^{\circ}-b$ and $90^{\circ}-B$.

The perpendicular a is common to the two triangles and therefore to

$$\begin{cases} a \text{ and } 90^{\circ} - b \text{ in triangle } MPm \text{ correspond } 90^{\circ} - d \text{ and } t \\ a ,, 90^{\circ} - B ,, , MZm ,, 90^{\circ} - h ,, Z \end{cases}$$

and vice versa, or to

$$a \text{ and } \begin{cases} b \text{ correspond } d \text{ and } t, \\ B , h , Z \end{cases}$$

and vice versa.

¹ The principle upon which these tables are based is as old as Spherical Trigonometry itself, and naturally it was the only way of solving spherical triangles until, as DOTT. PESCI informs us, ALBATANI (880-928 A.D.) discovered the well-known relation (erroneously attributed to Euler) between the three sides and an angle of a spherical triangle

CONSTRUCTION OF THE TABLES

This correspondence is fundamental and must always be remembered.

By Napier's mnemonical rules we find the following equations binding together these elements:

(1)
$$\begin{cases} \sin d = \cos a \sin b \\ \sin h = \cos a \sin B \end{cases}$$
 (2)
$$\begin{cases} \cot t = \cot a \cos b \\ \cot Z = \cot a \cos B \end{cases}$$

and

(3)
$$\begin{cases} \sin a = \cos d \sin t \\ \sin a = \cos h \sin Z \end{cases}$$
 (4)
$$\begin{cases} \cot b = \cot d \cos t \\ \cot B = \cot h \cos Z \end{cases}$$

CONSTRUCTION OF THE TABLES

As a, b and B in groups of equations (1) and (2) can have values between 0° and 90°, we have tabulated the values of d and t corresponding to various values of a for every 30′ from 0° to 84° and for every 1° from 84° to 90° (88° 50′ being especially included on account of *Polaris*) and b for every 1° (and *ipso facto* the values of b and b corresponding to various values of b and b.

As groups of equations (3) and (4) are respectively similar to (1) and (2), we notice that we have also tabulated the values of a and b corresponding to various values of d and t (and *ipso facto* the values of a and b corresponding to various values of b and b0.

For this reason the tables have two entrances.

The upper one with a and b as arguments giving, by means of the upper equations of groups of equations (1) and (2), d and t (or with a and B as arguments giving, by means of the lower equations of groups (1) and (2), h and D).

The lower one with d and t as arguments giving, by means of the upper equations of groups of equations (3) and (4), a and b (or with b and b as arguments giving, by means of the lower equations of groups (3) and (4), a and b, but not considered for greater simplicity in dealing with the principal problem).

For convenience and greater simplicity a complementary column c/C to column b/B is given on each page where c stands for $90^{\circ}-b$ and C for $90^{\circ}-B$.

Therefore the tables can also be entered with a and c giving d and t, and also with a and C giving h and C.

Example I. Entering the tables on page 119 with $a=48^{\circ}$ o' and $b=59^{\circ}$ we find $d=35^{\circ}$ o' and $t=65^{\circ}$ 7'.

Example II. Entering the tables on page 63 with $a=6^{\circ}$ o' and $B=73^{\circ}$ or $C=17^{\circ}$, we find $h=72^{\circ}$ o' and $Z=19^{\circ}$ 46'.

Example III. Entering the tables on page 91 with $d=27^{\circ}$ o' and $t=60^{\circ}$ we find $a=50^{\circ}$ 30' and $b=45^{\circ}$ 32'.

In columns $\frac{60'}{\Delta}$ and $\frac{\Delta}{60'}$, Δ represents the difference between two

successive values and the factors $\frac{60'}{\Delta}$ and $\frac{\Delta}{60'}$ are given in order to facilitate interpolation.

All values designedly appear in our tables, and examples always reduced to the first quadrant with sign plus with further simplification in view.

CALLET'S 2 logarithms with seven decimal places were used in the calculations. In many cases VLACQ'S 3 ten decimal place logarithms were used.

EXAMINATION OF THE TABLES

A mere inspection of the tables shows at a glance how the elements vary in the astronomical triangle of position.

For a given value of a, d and t vary proportionately to b throughout the tables, except in a very few practical cases when the declination of the observed body d is higher than 70° . As long as the difference $\left(\frac{\Delta_2}{60'}\right)$ between two successive values of $\frac{\Delta}{60'}$ is equal to or smaller than 0.15, the maximum error in t due to second differences is equal to or smaller than t. Up to $d=60^{\circ}$ this maximum error is equal to or smaller than 0.5.

Careful examination, however, of these *Tables* has shown that the error of t when using simple interpolation for any declination has no practical effect upon the value of h determined by them.

² "Tables de logarithmes, suivies d'un recueil de Tables nautiques." Editeur Firmin-Didot et Cie, Paris, 1883.

³ "Trigonometria Artificialis sive Magnus Canon Triangulorum Logarithmicus," Gouda, 1633.

below magnitude 3.0. Of the 486 stars catalogued in the *Nautical Almanac* for 1910 only 24 have higher declinations than 77° 46′, and their magnitudes range between 4.3 and 8.4, being therefore unsuitable for navigation.

It is noticed that the influence of the second differences only begins to appear in a few cases above the extreme limit of declination (=60°) adopted by nearly all nautical tables, notwithstanding the existence of 36 stars (15 of which are of or above 3.0) above magnitude 4.1, with greater declinations than 60°.

¹ These tables were first described by the author in the *United States Naval Institute Proceedings* for December 1908, page 1299, and in the *Revista Maritima Brazileira* for March 1909, page 1577. A description of them by DOTT. A. ALESSIO, R.I.N., is also found in the *Rivista Maritima* for March 1909, Appendice, page 56.

The only relatively important star above 70° declination is β Ursæ Minoris with N 74° 31′ decreasing. Its magnitude is 2.2. Among the 316 stars above magnitude 4.1 (not including *Polaris*) catalogued in the *Nautical Almanac* for the year 1910, the highest declination is that of β Hydri, magnitude 2.9, with S 77° 46′ decreasing, and for this reason the differences $\frac{\Delta}{60'}$ only extend to this value of d. Of the 316 stars mentioned above there are only 6 with declinations higher than 70°, and 4 of them are below magnitude 3.0. Of the 486 stars catalogued in the *Nautical Almanac* for 1910

LINES OF POSITION

ALTITUDE AND AZIMUTH FOR LINES OF POSITION

The problem is: Given d, t and L, find h and Z.

DETERMINATION OF h AND Z.

Let us see now how altitude and azimuth can be easily and rapidly determined by these tables.

Entering the tables with d and t as arguments, we will find in

columns a and b approximate values of a and b.

Entering the tables again with a and b as arguments, we will find approximately the values of d and t given.¹ The true value of b is then determined for the *exact* value of d and a value of t is found corresponding to this b.

The values of h and Z will then be found in the same column a corresponding to B or to its complement C.

Example. $d=16^{\circ} 27'$, $t=61^{\circ} 10'$ and $L=23^{\circ} 39' \cdot 3$.

Entering the tables with $d=16^{\circ}$ 30' and $t=61^{\circ}$ we find $a=57^{\circ}$ 0' and $b=31^{\circ}$ 26'. Corresponding to $a=57^{\circ}$ 0' and $b=31^{\circ}$ we find $d=16^{\circ}$ 17' and $t=60^{\circ}$ 54'. The true value of b corresponding to $d=16^{\circ}$ 27' is 31° 20'.7 and the value of t corresponding to this value of b is 60° 59'.6.

If $B=35^{\circ}$ (or $C=55^{\circ}$) we will have $h=18^{\circ}$ 12' and $Z=61^{\circ}$ 59'.

DETERMINATION OF C.

We will now show how C is determined when L and b are known. When the perpendicular a falls between P and Z, as it does in Fig. 2 (d and L being of the same name and $t < 90^{\circ}$), we have

$$[90^{\circ} - B] + 90^{\circ} - b = 90^{\circ} - L$$

and therefore

$$C=b-L$$
: when $L < b$.

If the perpendicular fell between Z and Q (d and L being also of the same name and $t < 90^{\circ}$), we would have

$$[90^{\circ} - B] + 90^{\circ} - L = 90^{\circ} - b$$

and therefore

$$C=L-b$$
: when $L>b$.

¹ The value of a shows *immediately* on which two pages of the tables we have to work, and also in which of the three columns. The value of b shows on which of the two pages we have to begin, and also the line on which the approximate values of d and t are found. Although *not strictly necessary* this knowledge of the approximate value of b is convenient.

The value of a is also not strictly necessary as long as the values of d and t are found together in the same column a. After a little manipulation of the tables no difficulty will be experienced in finding them together in the same column a.

In case the perpendicular fell between P and N (which only happens when $t > 90^{\circ}$ and we enter the tables with $180^{\circ} - t$ instead of t), we would have

and therefore

$$[90^{\circ} - B] = 90^{\circ} - L + 90^{\circ} - b$$

 $C = 180^{\circ} - (L + b)$.

Finally, when the perpendicular falls between Q and S (d and L are then of contrary names), we have

$$[90^{\circ} - B] + 90^{\circ} - L = 90^{\circ} + b$$
$$C = L + b.$$

Thus when

d and L same name
$$\begin{cases} t < 90^{\circ} \begin{cases} L < b : C = b - L; \ Z < 90^{\circ} \\ L > b : C = L - b; \ Z > 90^{\circ} \end{cases} \\ t > 90^{\circ} \dots : C = L + b; \ Z < 90^{\circ} \end{cases}$$
d and L contrary names : $C = L + b; \ Z > 90^{\circ}$

By these formulæ C can be obtained from L and b with great simplicity and rapidity.

In the first two cases, the *smaller* of the two quantities L and b, is always subtracted from the *larger* of the two.

In the third and fourth cases L and b are always added together. When $t>90^{\circ}$ their sum is always greater than 90°, and it is subtracted from 180°. When d and L are of contrary names their sum is always smaller than 90°.

The quadrant in which the observed body is, is also shown for reference and by our method is always known a priori.

When d and L are of the same name and $t < 90^{\circ}$, Z is less or greater than 90° when L is less or greater than b.

When $t>90^{\circ}$, Z is always less than 90° ; finally when d and L are of contrary names Z is always greater than 90° .

When $Z < 90^{\circ}$ the value of Z given by the tables is reckoned from the *elevated* pole to East or West, and when $Z > 90^{\circ}$ from the *depressed* pole to East or West, since the tables only give values up to 90° .

VARIATIONS OF DATA.

A further inspection of the Tables shows that they are also available for determining at sight by inspection "what effect given variations of data will produce in quantities computed from them." 1

If we call Δh , ΔZ , Δd , Δt , and ΔL respectively the variations of altitude, azimuth, declination, hour angle and latitude the following formulæ will give us the errors Δh and ΔZ in the values of h and Z

CHANGES OF ALTITUDE AND AZIMUTH

computed, when d, t and L are affected by small errors Δd , Δt and ΔL respectively:—

$$\Delta h = \cos M \, \Delta d - \cos L \, \sin Z \, \Delta t + \cos Z \, \Delta L \tag{1}$$

and

$$\cos h \Delta Z = \sin M \Delta d + \cos M \cos d \Delta t - \sin h \sin Z \Delta L \qquad (2)$$

where M is the parallactic angle.

CHANGES OF ALTITUDE AND AZIMUTH.

If Δd and ΔL are *nil* we have by (1) $\Delta h = -\cos L \sin Z \Delta t$, or $\frac{\Delta h}{\Delta t} = -\cos L \sin Z$, which gives us the "Change of Altitude per Minute of Arc of Hour Angle" (Table on p. 170).

If Δt and ΔL are *nil* we have by (1) $\Delta h = \cos M \Delta d$, or $\frac{\Delta h}{\Delta d} = \cos M$, which gives us the "Change of Altitude per Minute of Arc of Declination."

If Δd and Δt are *nil* we have by (1) $\Delta h = \cos Z \Delta L$, or $\frac{\Delta h}{\Delta L} = \cos Z$, which gives us the "Change of Altitude per Minute of Arc of Latitude."

In the same way we would have by (2)

$$\Delta Z = \cos M \cos d \sec h \Delta t$$
, or $\frac{\Delta Z}{\Delta t} = \cos M \cos d \sec h$

$$\Delta Z = \tan h \sin Z \Delta L$$
 , $\frac{\Delta Z}{\Delta L} = \tan h \sin Z$

$$\Delta Z = \sin M \sec h \, \Delta d$$
 ,, $\frac{\Delta Z}{\Delta d} = \sin M \sec h$

The 1st expression of ΔZ is easily transformed into

$$\Delta Z = \sin L \Delta t - \tan h \cot Z \Delta h$$

as explained on page xxvii later on.

The value of ΔZ from the 2nd expression of ΔZ is given immediately by the Tables in column $\frac{\Delta}{60}$ alongside the value of Z.

Example. If $h=38^{\circ}$ and $Z=62^{\circ}$ we will find them approximately together in column $a=44^{\circ}$ on page 113, and therefore $\frac{\Delta Z}{\Delta L}=0'.70$ found in column $\frac{\Delta}{60'}$ alongside Z (=61° 56').

The 3rd expression of ΔZ has not any practical importance, as Δd is always smaller than o'.5.

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¹ and ² CHAUVENET, "A Manual of Spherical and Practical Astronomy," Philadelphia, 1890. Vol. I. pp. 50, 51.

THE PARALLACTIC ANGLE M.

By interchanging L and d in the tables we can find immediately in column Z the parallactic angle M.

THE LONGITUDE FACTOR, OR PAGEL'S COEFFICIENT.

If Δh and Δd in (1) are *nil* we can find immediately the longitude factor or PAGEL'S coefficient the most important of all, as it shows at once the change of hour angle or longitude due to a change of 1' in the latitude.

We find from (1) when $\Delta h = \Delta d = 0$

$$\cos L \sin Z \Delta t = \cos Z \Delta L$$

or

$$\cos L \cdot \frac{\Delta t}{\Delta L} = \cot Z$$

In our Tables

$$\cos B \cot a = \cot Z$$

and, therefore, if we enter the Tables with L in the place of B and Z in column Z, the cotangent of α in which Z stands is equal to $\frac{\Delta t}{\Delta L}$, the longitude factor, or PAGEL'S coefficient.

The blackfaced numbers at the head of each four columns represent the cot α above which they are.

- I. Example. If $L=24^{\circ}$ and $Z=73^{\circ}$ o' we will find on page 148 $\frac{\Delta t}{\Delta L}=\cot a=\cot 71^{\circ}$ 30'=0'.335.
- II. Example. If $L=55^{\circ}$ and $Z=60^{\circ}$ 10' we will find on page 115 $\frac{\Delta t}{\Delta L} = \cot a = \cot 45^{\circ} = 1'.000$.
- III. Example. If $L = 50^{\circ}$ and $Z = 42^{\circ}$ 30' we will find on page 95 $\frac{\Delta t}{\Delta L} = \cot \alpha = \cot 30^{\circ} 30' = 1'.698.$

For the sake of simplicity we will call $\frac{\Delta t}{\Delta L}$: p.

LATITUDE FACTOR.

The latitude factor or the change of latitude due to a change of \mathbf{I}' in the hour angle or longitude is found immediately by noticing that $\frac{\Delta L}{\Delta t}$ is the reciprocal of $\frac{\Delta t}{\Delta L}$ or of cot a, that is, cot $(90^{\circ} - a)$ or tan a.

- I. Example. If $L=24^{\circ}$ and $Z=73^{\circ}$ o' we will find on page 81 $\frac{\Delta L}{\Delta L} = \tan \alpha = \cot 19^{\circ} 30' = 2'.824$.
- II. Example. If $L=55^{\circ}$ and $Z=60^{\circ}$ 10' we will find on page 115 $\frac{\Delta L}{\Delta t} = \tan \alpha = \cot 45^{\circ} \text{ o'} = \text{1'.000.}$
- III. Example. If $L = 50^{\circ}$ and $Z = 42^{\circ}$ 30' we will find on page 133 $\frac{\Delta L}{\Delta t} = \tan \alpha = \cot 59^{\circ} \text{ 30'} = 0'.589.$

I. TYPICAL EXAMPLE FOR ALL SIGHTS

(Whether circummeridian, ex-meridian or time sights.)

The following typical example is given in order to illustrate the way in which all sights ought to be treated:

SIGHT OF THE SUN.

On February 21, 1910, about 8^h A.M., in Lat. by D. R. 36° 56′ N., and Long. by D. R. 8° 5′ W., the observed altitude of the Sun's lower limb, bearing southward and eastward, was 20° 59′.2 at 21^h 6^m 11^s of the chronometer, 6^m 59^s slow of G. M. T. Height of eye 36 ft. Required the line of position.

$$C.=21^{h} \quad 6^{m} \quad 11^{s}$$

$$C.C. = + \quad 6 \quad 59$$

$$G. \quad M. \quad T. = 21^{h} \quad 13^{m} \quad 10^{s}$$

$$Eq. \quad of \quad T. = - \quad 13 \quad 46$$

$$a=52^{\circ} \quad o' \quad G. \quad A. \quad T. = 20^{h} \quad 59^{m} \quad 24^{s} \quad or \quad t_{G} = 3^{h} \quad o^{m} \quad 36^{s} \quad E = 45^{\circ} \quad 9'.0 \quad E$$

$$b=17^{\circ} \quad 8'.4 \qquad d=10^{\circ} \quad 27' \quad S$$

$$t_{A} = 53 \quad 15 \cdot 3 \quad E$$

$$L_{A} = 36 \quad 51 \cdot .6 \quad N$$

$$G_{A} = 8^{\circ} \quad 6'.3 \quad W$$

$$C=54^{\circ} \qquad h_{A} = 21 \quad 13 \cdot .0$$

$$h = h_{A} = - 6'.0$$

$$k_{A} = 21 \quad 13 \cdot .0$$

Note. This calculation could have been made in advance before taking the sight if it had been decided to observe the Sun at 21^h 6^m 11^s of the chronometer.

Working out this example with 5 decimal place logarithms we would find, with $d=10^{\circ}$ 27', $t_{A}=53^{\circ}$ 15'.3 and $L_{A}=36^{\circ}$ 51'.6:

$$b=17^{\circ}$$
 8'.0, $h_{A}=21^{\circ}$ 13'.1 and $Z_{A}=57^{\circ}$ 42'.4

by means of groups of equations: (2) for Z and (4) for b and h.

When due to unknown currents or any other reason we have not a reliable D. R. position, a can be determined by means of h and Z. Z is found by compass observation or by the method indicated on page xxxv. Enter the tables with h in the place

of d and Z in the place of t.

¹ As in practice an assumed latitude is used instead of the latitude by D. R., it is better, in order to avoid mistakes, not to consider the latitude by D. R. at all, only the longitude by D. R., except when only one observation is available and the ship's most probable position has to be found. The longitude by D. R., itself is only used to find the approximate value of a.

Group (3) constitutes the *check* group, because it contains d and t given, and h and Z required.

This development shows the time and trouble our tables save, besides doing away with the turning of pages, lessening the chances of error, and simultaneously checking, *per se*, part of the results. In these calculations advantage has been taken of our precepts, and therefore no algebraic signs or arcs greater than 90° appear.

EXPLANATION.

After the correction is applied to the chronometer time and the equation of time to the G. M. T. we fibd G. A. T. also called the "Sun's geographical longitude" $(\odot$'s t_G), because it is the Sun's hour angle from Greenwich. This G. A. T. is *immediately converted* into arc^1 and combined apart with the Longitude by D. R. or $G_{D.R.}$, giving the Sun's hour angle from D. R. or $t_{D.R.}$ in arc:

$$\bigcirc$$
's $t_G = 45^{\circ}$ 9' E
 $G_{D.R.} = 8$ 5 W
 \bigcirc 's $t_{D.R.} = 53^{\circ}$ 14' E

The declination of the Sun, found in the *Nautical Almanac* at the same time as the Eq. of T., is taken to the nearest minute of arc. (It is noticed that no seconds of arc are used in our method nor are they necessary, and the quantities expressed in arc need only be taken within *one-tenth of one minute* when greater accuracy is desired).

Entering the tables on page 69 with $d=10^{\circ}$ 30' and $t_{D.R.}=53^{\circ}$ 14' as arguments, we find in column $a:52^{\circ}$, which is an approximate value of a, and in column $b:17^{\circ}$, which is an approximate value of b.

Entering the tables again on page 122 with $a=52^{\circ}$ o' and $b=17^{\circ}$ as arguments, we find that the Sun's declination 10° 27' is comprised between 10° 22' and 10° 58' respectively corresponding to $b=17^{\circ}$ and

¹ This procedure, not usually followed in the text books, has the *triple* advantage of simplifying the determination of *t*, abolishing the argument in time in the tables and the necessity of dealing with data expressed in time and in arc after G. A. T. is converted.

PLOTTING THE LINE OF POSITION

Interpolating (here the interpolation is reduced to the multiplication of the factor $\frac{60'}{\Lambda}$ =1.67, by the difference between 10° 27' and 10° 22', that is 5'), we find that $b=17^{\circ}$ 8'.4 and t_{A} corresponding to this value of b is 53° 15'.3. The ready reckoner on pp. 50 to 53 will save the trouble of doing these multiplications.

In order to do away with any corrections, this t_{A_n} which differs from $t_{D.R.}$ one minute and three-tenths, is taken as the hour angle. Combining it with the \odot 's $t_{g}=45^{\circ}$ 9'.0 W., we find a longitude which

may be called assumed: $G_A = 8^{\circ} 6'.3 \text{ W}.$

In order to do away with any further interpolations, C is made a whole number of degrees by assuming a latitude, nearly the same as the Lat. by D. R., that will make it so. In our particular case it will be seen that $L_{4}=36^{\circ}$ 51'.6 combined with $b=17^{\circ}$ 8'.4, according to the precepts given, d and L contrary names: C=L+b; $Z>00^{\circ}$, will make C just 54°.

Therefore in the same column $a=52^{\circ}$ o' with $C=54^{\circ}$, we will find

 $h_A = 21^{\circ} 13'$ and $Z_A = 57^{\circ} 42'$.

CHECK.

The necessary calculations to find h_A and Z_A are so simple and few, and, therefore, the liability to error so small, that we do not think a check is necessary.

However, the correctness of the calculations might be tested without new data by proceeding backwards, as explained further on

for "identifying celestial bodies" (vide page xxxv). To $h_{A}=21^{\circ}$ 13' and $Z_{A}=57^{\circ}$ 42' corresponds $B=36^{\circ}$ in column $a=52^{\circ}$ o'. If $L_{A}=36^{\circ}$ 51'.6, c will be found by the precepts on page xxxvi. As $Z > 90^{\circ}$, $c = L_A + B = 72^{\circ}$ 51'.6 < 90°, b will be 17° 8'.4, and we will find by interpolation (here it is reduced to the division of 8'.4 by the factor $\frac{60'}{\Lambda} = 1.67$ giving 5') $d = 10^{\circ} 27'$ and $t_{A} = 53^{\circ} 15'.3$, "d and L contrary names" and " $t < 90^{\circ}$ ".

Of course, if d and t_A were not the same as used before, the calculations would be in error.

PLOTTING THE LINE OF POSITION.

Fig. 3, representing a section of a chart of the coast of Portugal, shows A the assumed position from which the line of position is determined. The altitude difference is AB = -6'.o. It is + when the true altitude h is greater than the assumed altitude h_A and—when the true altitude is smaller than the assumed altitude. It is always taken in the direction of the observed body: towards, when + and in the opposite direction: away from, when -.

LG is the line of position perpendicular to AB. The foot of

the perpendicular dropped from the position by D. R. on the line of position is the ship's most probable position and *must* be taken as the ship's position when only one observation is available.

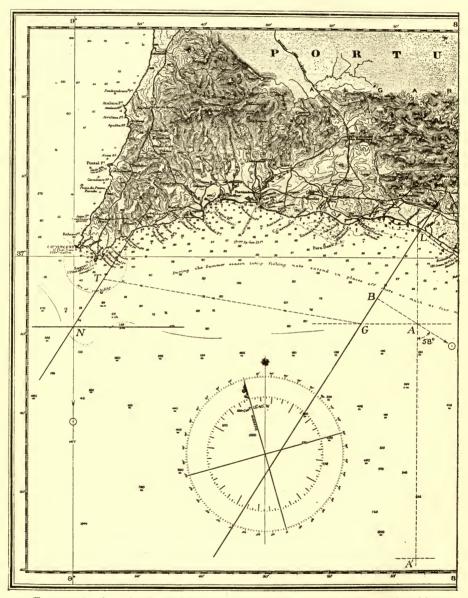


FIG. 3.—Section of a chart of the coast of Portugal showing how line of position is plotted and ship's position AT NOON is found.

This line of position is just as valuable as the isolated knowledge of latitude or longitude, and represents the exact and only true interpretation of the sight.

II. TYPICAL EXAMPLE FOR ALL SIGHTS

The following typical example is also given in order to illustrate the way in which all sights ought to be treated:

SIGHT OF THE SUN.

On August 21, 1908, about 11h A.M., in Lat. by D. R. 16° 16′ S.,¹ and Long. by D. R. 38° 18′ W., the observed altitude of the Sun's lower limb, bearing northward and eastward, was 59° o' at 1h 19m 40s of the chronometer, 26m 59s slow of G. M. T. Height of eye 28 ft. Required the line of position and the ship's most probable position.

$$C. = 1^{h} 19^{m} 40^{s}$$

$$C. C. = + 26 59$$

$$G. M. T. = 1^{h} 46^{m} 39^{s}$$

$$Eq. of T. = -3 3$$

$$\frac{a = 12^{\circ} \text{ o'}}{b = 12^{\circ} 26'.5} \qquad \frac{d = 12^{\circ} 10' \text{ N}}{d = 12^{\circ} 10' \text{ N}} \text{ or } t_{G.} = 25^{\circ} 54' \text{ W}$$

$$\frac{t_{A.} = 12 17}{G_{A.} = 38^{\circ} 11'} \text{ E}$$

$$\frac{h_{o} = 59^{\circ} \text{ o'}}{Corr. = + 10}$$

$$\frac{h_{A.} = 58 49}{h - h_{A.} = + 21'} \qquad Z_{A.} = \text{N } 23^{\circ} 41' \text{ E}$$

Note. This calculation could have been made in advance before taking the sight if it had been decided to observe the Sun at 1^h 19^m 40^s of the chronometer.

Working out this example with 5 decimal place logarithms we would find, with $d=12^{\circ}$ 10', $t_A=12^{\circ}$ 17' and $L_A=16^{\circ}$ 33'.5:

$$b = 12^{\circ} 26'.6$$
, $h_{A} = 58^{\circ} 48'.8$ and $Z_{A} = 23^{\circ} 40'.8$

by means of groups of equations: (2) for Z and (4) for b and h.

When due to unknown currents or any other reason we have not a reliable D.R. position, a can be determined by means of h and Z. Z is found by compass observation or by the method indicated on page xxxv. Enter the tables with h in the place of d and Z in the place of f.

¹ As in practice an assumed latitude is used instead of the latitude by D. R., it is better, in order to avoid mistakes, not to consider the latitude by D. R. at all, only the longitude by D. R., except when only one observation is available and the ship's most probable position has to be found. The longitude by D. R., itself is only used to find the approximate value of α .

Group (3) constitutes the *check* group, because it contains d and t given, and h and Z required.

This development shows the time and trouble our tables save, besides doing away with the turning of pages, lessening the chances of error, and simultaneously checking, per se, part of the results. In these calculations advantage has been taken of our precepts, and therefore no algebraic signs or arcs greater than 90° appear.

EXPLANATION.

After the correction is applied to the chronometer time and the equation of time to the G. M. T. we find G. A. T. also called the "Sun's geographical longitude" (\odot 's t_G), because it is the Sun's hour angle from Greenwich. This G. A. T. is *immediately converted into arc*¹ and combined apart with the Long. by D. R., giving the Sun's hour angle from D. R. or $t_{D.R.}$ in arc:

$$\odot$$
's $t_G = 25^{\circ} 54'$ W
 $G_{D.R.} = 38 \text{ 18}$ W
 \odot 's $t_{D.R.} = 12^{\circ} 24'$ E

The declination of the Sun, found in the Nautical Almanac at the same time as the Eq. of T., is taken to the nearest minute of arc. (It is noticed that no seconds of arc are used in our method nor are they necessary, and the quantities expressed in arc need only be taken within one-tenth of one minute when greater accuracy is desired).

Entering the tables with $d=12^{\circ}$ o' and $t_{D.R.}=12^{\circ}$ 24' as arguments, we find in column $a:12^{\circ}$, which is an approximate value of a, and in column $b:12^{\circ}$, which is an approximate value of b.

Entering the tables again with $a=12^{\circ}$ o' and $b=12^{\circ}$ as arguments,

¹ This procedure, not usually followed in the text books, has the *triple* advantage of simplifying the determination of *t*, abolishing the argument in time in the tables and the necessity of dealing with data expressed in time and in arc after G. A. T. is converted.

² In this particular case by coincidence a is approximately the same as d.

PLOTTING THE LINE OF POSITION

we find that the Sun's declination 12° 10' is comprised between 11° 44' and 12° 43' respectively corresponding to $b=12^{\circ}$ and $b=13^{\circ}$. Interpolating (here the interpolation is reduced to the multiplication of the factor $\frac{60'}{\Delta}=1.02$, by the difference between 12° 10' and 11° 44', that is 26'), we find that $b=12^{\circ}$ 26'.5 and t_{A} , corresponding to this value of b is 12° 17' (exactly 12° 17'.3). The ready reckoner on pp. 50 to 53 will save the trouble of doing these multiplications.

In order to do away with any corrections, this t_A , which differs from $t_{D.R.}$ seven minutes, is taken as the hour angle. Combining it with the \odot 's $t_a=25^{\circ}$ 54' W., we find a longitude which may be called assumed: $G_A=38^{\circ}$ 11' W.

In order to do away with any further interpolations, C is made a whole number of degrees by assuming a latitude, nearly the same as the Lat. by D. R., that will make it so. In our particular case it will be seen that $L_A = 16^{\circ}$ 33'.5 combined with $b = 12^{\circ}$ 26'.5, according to the precepts given, d and L contrary names: C = L + b; $L > 90^{\circ}$, will make C just 29°.

Therefore in the same column $a=12^{\circ}$ o' with $C=29^{\circ}$, we will find $h_{A}=58^{\circ}$ 49' and $Z_{A}=23^{\circ}$ 41'.

CHECK.

The necessary calculations to find h_A and Z_A are so simple and few, and, therefore, the liability to error so small, that we do not think a check is necessary.

However, the correctness of the calculations might be tested without new data by proceeding backwards, as explained further on for "identifying celestial bodies" (vide page xxxv).

To $h_A=58^\circ$ 49' and $Z_A=23^\circ$ 41' corresponds $B=61^\circ$ in column $a=12^\circ$ o'. If $L_A=16^\circ$ 33'.5, c will be found by the precepts on page xxxvi. As $Z>90^\circ$, $c=L_A+B=77^\circ$ 33'.5<90°, and we will find by interpolation (here it is reduced to the division of 33'.5 by the factor $\frac{60'}{\Delta}=1.02$ giving 33') $d=12^\circ$ 10' and $t_A=12^\circ$ 17', "d and L contrary names" and " $t<90^\circ$ ".

Of course, if d and t_A were not the same as used before, the calculations would be in error.

PLOTTING THE LINE OF POSITION.

Fig. 4, representing a section of a chart of the coast of Brazil, shows A the position by D. R. and A' the assumed position from which the line of position is determined. The altitude difference is A'B' = +21'. It is + when the true altitude h is greater than the

Group (3) constitutes the *check* group, because it contains d and t given, and h and Z required.

This development shows the time and trouble our tables save, besides doing away with the turning of pages, lessening the chances of error, and simultaneously checking, per se, part of the results. In these calculations advantage has been taken of our precepts, and therefore no algebraic signs or arcs greater than 90° appear.

EXPLANATION.

After the correction is applied to the chronometer time and the equation of time to the G. M. T. we find G. A. T. also called the "Sun's geographical longitude" (\odot 's t_G), because it is the Sun's hour angle from Greenwich. This G. A. T. is *immediately converted into arc*¹ and combined apart with the Long. by D. R., giving the Sun's hour angle from D. R. or $t_{D,R}$ in arc:

$$\odot$$
's $t_{G.} = 25^{\circ} 54'$ W
 $G_{D.R.} = 38 18$ W
 \odot 's $t_{D.R.} = 12^{\circ} 24'$ E

The declination of the Sun, found in the Nautical Almanac at the same time as the Eq. of T., is taken to the nearest minute of arc. (It is noticed that no seconds of arc are used in our method nor are they necessary, and the quantities expressed in arc need only be taken within one-tenth of one minute when greater accuracy is desired).

Entering the tables with $d=12^{\circ}$ o' and $t_{D.R.}=12^{\circ}$ 24' as arguments, we find in column $a:12^{\circ}$, which is an approximate value of a, and in column $b:12^{\circ}$, which is an approximate value of b.

Entering the tables again with $a = 12^{\circ}$ o'2 and $b = 12^{\circ}$ as arguments,

¹ This procedure, not usually followed in the text books, has the *triple* advantage of simplifying the determination of t, abolishing the argument in time in the tables and the necessity of dealing with data expressed in time and in arc after G. A. T. is converted.

² In this particular case by coincidence a is approximately the same as d.

PLOTTING THE LINE OF POSITION

we find that the Sun's declination 12° 10' is comprised between 11° 44' and 12° 43' respectively corresponding to $b=12^{\circ}$ and $b=13^{\circ}$. Interpolating (here the interpolation is reduced to the multiplication of the factor $\frac{60'}{\Delta}=1.02$, by the difference between 12° 10' and 11° 44', that is 26'), we find that $b=12^{\circ}$ 26'.5 and t_{A} corresponding to this value of b is 12° 17' (exactly 12° 17'.3). The ready reckoner on pp. 50 to 53 will save the trouble of doing these multiplications.

In order to do away with any corrections, this t_{A_n} , which differs from $t_{D.R.}$ seven minutes, is taken as the hour angle. Combining it with the \odot 's $t_{G.}=25^{\circ}$ 54' W., we find a longitude which may be called assumed: $G_{A.}=38^{\circ}$ 11' W.

In order to do away with any further interpolations, C is made a whole number of degrees by assuming a latitude, nearly the same as the Lat. by D. R., that will make it so. In our particular case it will be seen that $L_A = 16^{\circ}$ 33'.5 combined with $b = 12^{\circ}$ 26'.5, according to the precepts given, d and L contrary names: C = L + b; $L > 90^{\circ}$, will make C just 29°.

Therefore in the same column $a=12^{\circ}$ o' with $C=29^{\circ}$, we will find $h_{A.}=58^{\circ}$ 49' and $Z_{A.}=23^{\circ}$ 41'.

CHECK.

The necessary calculations to find h_A and Z_A are so simple and few, and, therefore, the liability to error so small, that we do not think a check is necessary.

However, the correctness of the calculations might be tested without new data by proceeding backwards, as explained further on for "identifying celestial bodies" (vide page xxxv).

To $h_A=58^\circ$ 49' and $Z_A=23^\circ$ 41' corresponds $B=61^\circ$ in column $a=12^\circ$ o'. If $L_A=16^\circ$ 33'.5, c will be found by the precepts on page xxxvi. As $Z>90^\circ$, $c=L_A+B=77^\circ$ 33'.5<90°, and we will find by interpolation (here it is reduced to the division of 33'.5 by the factor $\frac{60'}{\Delta}=1.02$ giving 33') $d=12^\circ$ 10' and $t_A=12^\circ$ 17', "d and L contrary names" and " $t<90^\circ$ ".

Of course, if d and t_A were not the same as used before, the calculations would be in error.

PLOTTING THE LINE OF POSITION.

Fig. 4, representing a section of a chart of the coast of Brazil, shows A the position by D. R. and A' the assumed position from which the line of position is determined. The altitude difference is A'B' = +21'. It is + when the true altitude h is greater than the

assumed altitude $h_{A_{\bullet}}$ and — when the true altitude is *smaller* than the assumed altitude. It is always taken in the direction of the observed body: *towards*, when + and in the opposite direction: *away from*, when —.

B'B'' is the line of position perpendicular to A'B'. B the foot of

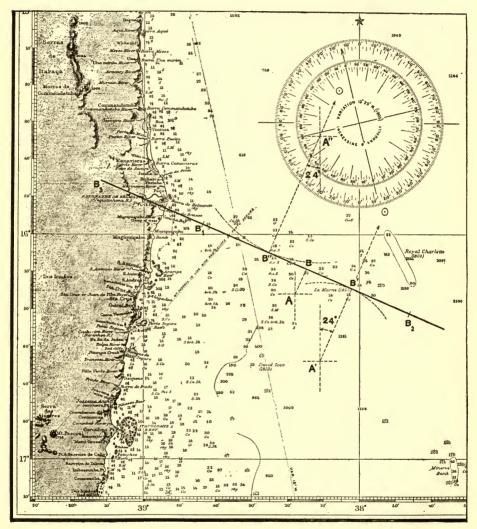


FIG. 4.—Section of a chart of the coast of Brazil showing how line of position is plotted and ship's most probable position found.

the perpendicular dropped from the position by D. R. on the line of position is the ship's most probable position and *must* be taken as the ship's position when only one observation is available.

This line of position is just as valuable as the isolated knowledge of

ALTITUDE AND AZIMUTH FROM D.R.

latitude or longitude, and represents the exact and only true interpretation of the sight.1

ALTITUDE AND AZIMUTH FROM D. R. POSITION.

When the observer wishes to find $h_{D.R.}$ and $Z_{D.R.}$ corresponding to the position by D. R., instead of taking an assumed position A' (or A'') (and this might be desirable when $t_{D.R.} - t_{A.}$ is large, when the altitude difference is greater than the established limits on page xxxii, or when 2, 3, and 4 lines of position have to be plotted simultaneously), it is necessary for him to find:

1st. The value of C with $L_{D.R.}$ and b according to the same precepts given on page xvi and by simple interpolation the corresponding values of h' and Z' (approximate values of $h_{D.R.}$ and $Z_{D.R.}$);

and Z' given by the tables due to the difference $t_{D.R.} - t_{A.} = \Delta t$.

These corrections are given by the following formulæ2:

$$\Delta h = \mp \cos L \sin Z' \Delta t$$
 or $\frac{\Delta h}{\Delta t} = \mp \cos L \sin Z'$
$$\Delta Z = \Delta_1 Z + \Delta_2 Z$$

where

and

and

$$\Delta_1 Z = \mp \sin L \, \Delta t$$
 or $\frac{\Delta_1 Z}{\Delta t} = \mp \sin L$
 $\Delta_2 Z = -\tan h' \cot Z' \, \Delta h$ or $\frac{\Delta_2 Z}{\Delta h} = -\tan h' \cot Z'$

Our tables on pages 170 and 172 give the absolute values of each one of these co-efficients $\frac{\Delta h}{\Delta t}$, $\frac{\Delta_1 Z}{\Delta t}$ and $\frac{\Delta_2 Z}{\Delta h}$ and at the top of page 170 the signs of the first two for each one of the four cases. $\frac{\Delta_2 Z}{\Delta h}$ is always negative provided Z' is smaller than 90° in absolute value, as our tables give it.

The correction ΔZ is generally negligible or unimportant unless Δz is large, but even in this case ΔZ can be small, depending as it does upon $\Delta_1 Z$ and $\Delta_2 Z$ with their signs + and -.

¹ Combinations of lines of position with terrestial bearings, with lines of soundings or with one or more lines of position are not discussed here, and will be found in any up-to-date text-book on Navigation or Nautical Astronomy.

² Vide DOTT. G. PESCI, Rivista Maritima for January 1909, page 62. In this article he shows how Δh can be simplified by dividing it by $\cos L$ and then $\frac{\Delta h}{\cos L} = \mp \sin Z' \Delta t$ represents Δh expressed in minutes of longitude. In order to find it then it is only necessary to multiply Δt by $\sin Z'$.

Taking our typical example it would be worked out as follows:

 $t_{D.R.} = 12^{\circ} 24' \text{ E}$

 $a = 12^{\circ}$ o'

$$\frac{d = 12 \quad 0}{b = 12^{\circ} 26' \cdot 5} \qquad d = 12^{\circ} 10' \text{ N} \qquad \frac{t_{D.R.} = 12^{\circ} 24' \text{ E}}{\Delta t = + 7'}$$

$$\frac{h_o = 59^{\circ} \quad 0'}{\Delta t = + 10}$$

$$\frac{h_o = 59^{\circ} \quad 0'}{h = 59^{\circ} 10'}$$

$$C = 28^{\circ} 42' \cdot 5 \qquad h' = 59^{\circ} 5' \cdot 1 \qquad Z' = 23^{\circ} 53' \qquad \frac{\Delta h}{\Delta t} = -0.39$$

$$\frac{h_D.R.}{h - h_{D.R.}} = \frac{12^{\circ} 26' \cdot 1}{10'}$$

$$\frac{\Delta h}{\Delta t} = -0.39$$

$$\frac{\Delta h$$

With 5 decimal place logarithms we would find $h_{D.R.} = 59^{\circ}$ 2'.4 and $Z_{D.R.} = 24^{\circ}$ 5'.

The altitude difference +7'.6 is exactly equal to the distance between A and B on the chart, and shows that "no greater accuracy is gained by determining the line of position from A than from A'."

The disposition of the arguments of the tables permits us to take, on the assumed meridian (38° 11' W.), any latitude comprised between 15° 33'.5 and 16° 33'.5 and the computed point will fall between B" and B' on the line of position.

If we took $L_A = 16^{\circ}$ o' the altitude difference would be small (=10' only), and the computed point would practically coincide with B.

If we took $L_{A}=16^{\circ}$ 10'.6 the altitude difference would be nil (0') and the line of position could be immediately drawn. This L_{A} is found by deducing the value of C that corresponds to $h_A = h$. This C combined with b by means of our fundamental precepts gives L_A :

$$d \text{ and } L_{A} \text{ same name} \begin{cases} t < 90^{\circ} & \{L_{A} < b : L_{A} = b - C; \ Z < 90^{\circ} \\ L_{A} > b : L_{A} = b + C; \ Z > 90^{\circ} \end{cases}$$

$$d \text{ and } L_{A} \text{ contrary names} \cdot \cdot \cdot : L_{A} = b + C; \ Z < 90^{\circ}$$

$$d \text{ and } L_{A} \text{ contrary names} \cdot \cdot \cdot : L_{A} = C - b; \ Z > 90^{\circ}$$

This shows the elasticity of our method whereby a better line of position (if necessary) can be plotted from a different assumed position without much additional calculation.

MERIDIAN SIGHTS.1

When a celestial body is on the meridian, its hour angle t is either o° or 180°, according to its position above or below the elevated pole. Its azimuth Z is then also oo or 180°. It is oo when the sight is taken with the observer's "face towards the elevated pole," and 180° when he has to turn his "back towards the elevated pole," to take the sight.

Introducing these values in groups of equations (3) and (1) we find that

$$a = 0^{\circ}$$
 o', $d = b$ and $h = B$.

Sights can generally be considered as meridian when $a < 0^{\circ}$ 15'. xxviii

PRECEPTS FOR MERIDIAN SIGHTS

This means that meridian sights could be worked out in column $a=0^{\circ}$ o' of our tables. It is better, however, to deduce directly from our general precepts, or from those giving L on page xxviii, special precepts giving *immediately* L with h and d.

These precepts will present the advantage, over the usual way of treating meridian sights, of doing away with the necessity of finding the meridian zenith distance, and giving it a confusing name or sign, such as now is in practice (N or + when facing South, and S or - when facing North). They show that even this simple time-honoured problem is capable of further simplification.

PRECEPTS FOR MERIDIAN SIGHTS.

$$Z=$$
 0° $\left\{\begin{array}{l} \text{Face towards} \\ \text{elevated pole} \end{array}\right. \left. \left\{\begin{array}{l} t=\text{ o}^{\circ} : L=(h+d)-90^{\circ}; d \text{ and } L \text{ same name.} \\ t=180^{\circ} : L=(90^{\circ}+h)-d; d \text{ and } L \end{array}\right. \right. ,$

$$Z=180^{\circ} \left\{\begin{array}{l} \text{Back towards} \\ \text{elevated pole} \end{array}\right. \left. \left\{\begin{array}{l} t=\text{ o}^{\circ} : L=(90^{\circ}+d)-h; d \text{ and } L \end{array}\right. , , ,$$

$$t=\text{ o}^{\circ} : L=90^{\circ}-(h+d); d \text{ and } L \text{ contr. names.} \right.$$

In Fig. 2 the 1st case corresponds to a body between P and Z.

1. Example. On August 27, 1908, in Lat. by D. R. 2° 40′ N., and Long. by D. R. 47° 22′ W., the observed meridian altitude of the sun's lower limb was 82° 21′. $Z = 0^{\circ}$ (face towards elevated pole and $t = 0^{\circ}$). Find the latitude.

OUR WAY.
 USUAL WAY.

$$h \odot = 82^{\circ} 21'$$
 $h \odot = 82^{\circ} 21'$

 Corr. = + 10.5
 Corr. = + 10.5

 $h \odot = 82^{\circ} 31'.5$
 $h \odot = 82^{\circ} 31'.5$
 $d \odot = 10 7.0 N$
 $z \odot = 7^{\circ} 28'.5 S$
 $L = 9)2^{\circ} 38'.5 N$
 $d \odot = 10 7.0 N$
 $L = 2^{\circ} 38'.5 N$

2. Example. On September 5, 1908, in Lat. by D. R. 35° N., and Long. by D. R. 70° 30′ W., the observed meridian altitude of the sun's lower limb was 61° 28′.1. $Z=180^{\circ}$ (back towards elevated pole). Find the latitude.

OUR WAY.

$$h \odot = 61^{\circ} 28'.\mathbf{1}$$
 $Corr. = + 10.2$
 $h \odot = 61^{\circ} 38'.3$
 $corr. = + 10.2$
 $corr. = + 10.2$

SIGHTS OF THE MOON, STARS, AND PLANETS.

Observations of the Moon, Stars, and Planets are worked out the same way as those of the Sun, excepting the way in which the $t_{D.R.}$ is determined. After correcting the chronometer and finding G. M. T. this interval of mean time is converted into an interval of sidereal time to which is added the Sidereal Time at Greenwich Mean Noon (or the R.A.M.S. at the same instant) in order to find G. S. T. This G. S. T. combined with the observed body's R. A. will give us the body's geographical longitude $(t_G.)$, or its hour angle from Greenwich. This t_G is converted *immediately* into arc and combined with the Long. by D. R., finally giving the body's $t_{D.R.}$

EXAMPLE.

C. =
$$9^h \ 39^m \ 43^s$$

C. C. = $-13 \ 16$
G. M. T. = $9^h \ 26^m \ 27^s$
Accel. = $+1 \ 33$
R. A. M. S. = $10 \ 17 \ 20$
G. S. T. = $19^h \ 45^m \ 20^s$
R. A. = $14 \ 11 \ 28$
 $t_G = 5^h \ 33^m \ 52^s$ or t_G . (in arc) = $83^\circ \ 28' \ W$
 $G_{D.R.} = 43 \ 42 \ W$
 $t_{D.R.} = 39^\circ \ 46' \ W$

SIGHTS OF a URSÆ MINORIS (Polaris).

Sights of *Polaris* are more easily and rapidly worked out, on account of its high declination: 88° 50' in 1910, and the consequent small value of a, always less than 1° 10'.

For this declination, the tables on pages 168 and 169 show that a and b vary very slowly for large variations of t, and it is then possible to determine immediately their exact values by inspection.

Turning to pages 54 and 55 of the tables, we notice that large variations of a do not sensibly affect the values of h for a given value of a. Whether a is 0° 0′, 0° 30′, or 1° 0′, we have practically always a0 up to a1 = 70°. Therefore it is not necessary to determine a2 exactly.

¹ The use of a sidereal chronometer on board ship would simplify matters and render more attractive observations of the Moon, Stars, and Planets. However, a mean time chronometer may be considered a sidereal chronometer as long as its daily rate is taken as $+3^{\text{m}}$ $56^{\text{s}}.56 \pm \text{daily}$ rate. If the *Nautical Almanac* gave the Sun's, the Moon's, and the Planets' declinations and right ascensions for oh G. S. T., only one process for finding t_G would need to be followed in all cases, and no mean time chronometers would be necessary.

LINES OF POSITION WITHOUT AZIMUTHS

As *Polaris* increases in declination (its Annual Variation is only 19"), the exact value of b can be obtained by simple interpolation between $d=88^{\circ}$ 50' and $d=89^{\circ}$ o'.

Example.¹ On March 6, 1910, in Longitude 37° W., at 10^h 11^m 35^s Greenwich Mean Time, suppose the true altitude of *Polaris* to be 46° 17'.5. Required the latitude (or the line of position).

G. M. T. = 10^h 11^m 35^s

Accel. = + 1 41

R. A. M. S. = 22 53 21

G. S. T. = 9^h 6^m 37^s

R. A. = 1 27 0

$$t_G = 7^h 39^m 37^s$$
 or t_G (in arc) = 114° 54′ W

 $G_{D,R} = 37 0 \text{ W}$
 $t_{D,R} = 77^\circ 54′ \text{ W}$

Entering the tables with $d=88^{\circ}$ 50', and $t_{D.R.}=77^{\circ}$ 54', we find immediately $a=1^{\circ}$ 9' and $b=89^{\circ}$ 45'. (As b corresponds to the exact value of d, it is not necessary to re-enter the tables with a and b as arguments, as explained on page xx). Entering the tables again with $a=1^{\circ}$ 0', we find corresponding to $h=46^{\circ}$ 17'.5: $B=46^{\circ}$ 18'.5 and $Z=1^{\circ}$ 27'. Combining this B with b by means of the precepts 2 for finding L at the bottom of page 168 ($t<90^{\circ}$), we have

$$L = 46^{\circ} \text{ 3'.5 N.}$$

With the latitude thus determined and the longitude by D. R., we find a position through which the line of position is drawn, as usual, perpendicular to the Star's true bearing.

As *Polaris'* azimuth is generally very small, the parallel of latitude will in the great majority of cases practically coincide with the line of position.

LINES OF POSITION DETERMINED WITHOUT AZIMUTHS.

If we assumed the latitude as 15° 33'.5, instead of 16° 33'.5, C would be 28°, $h_A = 59^\circ$ 44', and $Z_A = 24^\circ$ 22'. As the assumed longitude is the same, 38° 11' W., the assumed position would be A'' (vide Fig. 4), and the altitude difference -34'.

With the two assumed positions A' and A'' (60' apart on the same meridian) and the two altitude differences +21' and -34' the line of position can be found by drawing a line tangent to the two dotted circles drawn from A' and A'' respectively with 21' and 34' as radii.

This process appearing now for the first time gives a line of position independent of the observed body's azimuth, and its use

¹ Taken from the Nautical Almanac for 1910 for the sake of comparison.

² In the case of *Polaris* the four precepts for finding L with b and B are reduced to two, because L, in practice, is not *greater* than b, and d and L cannot be of contrary names.

facilitates the plotting of the line of position. It will prove very useful for plotting with great accuracy lines of position on Mercator's chart when the latitude is higher than 45°, especially when the body is near the prime vertical and the altitude difference large.

No error is committed in the plotting of the line when the altitude difference is $\leq 60'$ up to 75° latitude. With the ordinary process of plotting lines, as described on page xxv, a maximum error of 1° is introduced in the direction of the line of position when the azimuth is 90° with an

altitude difference = 60° when the latitude = 45° ,, ,, 48^{\prime} ,, ,, 50° ,, ,, 42^{\prime} ,, ,, 55° ,, ,, 36^{\prime} ,, ,, 60° ,, ,, 65°

A comparison of the two azimuths will control the coincidence of the straight line of position B'B'' and the curve of position (not represented on the chart), as it is evident the greater the difference between the two azimuths less will the two lines coincide.

However, this comparison need only be made when $t < 45^{\circ}$ and the observed body's declination is smaller than its altitude (d < h).\(^1\) When $t > 45^{\circ}$, and d < h, d > h, or d = h, the curve of position and the straight line of position on Mercator's chart coincide within 1' for a distance equal to or greater than 83' $(83'\sqrt{\cos L})$ in miles) on each side of the ship's most probable position. (Vide "Table for controlling the coincidence of lines of position," on page 173).

In our typical example the line of position B'B'' coincides with the corresponding curve of position within $\mathbf{1}$ mile for a distance of 59.5 miles on each side of the ship's most probable position B. B_1 and B_2 , 30 miles from B, are only 0.2 of a mile distant from the curve of position. B_3 and B_4 (not shown on the chart), 59.5 miles from B, are just $\mathbf{1}$ mile distant, and limit the *useful* part of the straight line of position.

RECTIFICATION OF LINES OF POSITION.

As the altitude of a celestial body increases, its zenith distance or the radius of the circle of position decreases, so it might happen that at a certain distance from the "computed point" the circle of position (or curve of position on Mercator's chart) and the straight line of position do not practically coincide.

The practical coincidence of the two lines takes place when the extreme points of the two lines are not further apart than I mile, as

¹ For details vide the author's: "Limites de coincidencia da recta Marcq Saint Hilaire com a curva de posição correspondente." (Reprinted from the Revista Maritima Brazileira, July 1906, page 41.)

RECTIFICATION OF LINES OF POSITION

in the case considered in Fig. 4. This limit can be increased or decreased according to the accuracy sought by the navigator, since it must not be forgotten that the circle of position is the line that contains the observer's position and that the straight line of position is only a practical substitute.

When only one line of position is determined it is generally not necessary to rectify it, that is to change its direction and position so that it will represent better the circle of position in the vicinity desired.

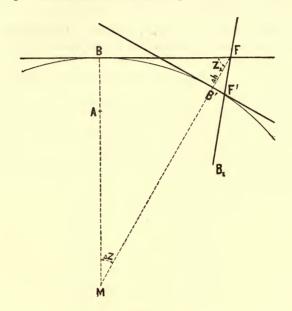


Fig. 5.

Let BF and B_1F in Fig. 5 be two lines of position, and F their intersection generally taken as the ship's position. Let us suppose that the body giving the line B_1F was low enough for us to be sure it is a practical substitute for the circle, meaning that F is less than $\mathbf{1}'$ from the circle of position. On the other hand, the body giving BF was very high (above 60°), and F is more than $\mathbf{1}'$ from the circle of position BB'. This means that F (the intersection of the two straight lines) is not a practical substitute for the intersection of the two circles of position (only one BB' being represented in the figure for demonstration).

It is then necessary to rectify BF. The tables 1 for rectifying lines

Abridged, by special permission of the author, from those accompanying a very remarkable article, entitled "Sulla Teoria e la Pratica della Nuova Navigazione Astronomica," by Dott. A. Alessio, Tenente di Vascello, Royal Italian Navy, published as a "supplement" to the *Rivista Marittima* for July-August 1908. *Vide* also Professor G. Pes' very interesting letter in the *Rivista Marittima* for March 1909, Appendice, page 14.

of position give the values of $FB' = \Delta h$ and Z_1 with the altitude h and the distance D = BF, and these are sufficient for determining the new line of position B'F' perpendicular to FB'. This new line intersects the line B_1F in F', which is taken as the ship's position.

Sometimes it may be necessary to rectify both lines, or to rectify one of them a second time, but this is very rare in practice.

This method recently devised by Lieut. Alessio saves the trouble of calculating a new altitude difference and azimuth for determining the line of position B'F' from F.

We have considered the angle Z_1 instead of the azimuth difference ΔZ given by Lieut. Alessio, because it saves drawing a perpendicular to BF.

When the altitude is lower than 60° generally it will not be necessary to rectify lines of position.

When the altitude is higher than 60° use a distance D in miles corresponding to which $\Delta h = 0'.5$, 1', 2' or more miles for the given altitude, according to the scale of the chart.

The tables show that the departure (Δh) between the circle and the straight line of position is $\leq 1'$ for

ALTITUDE AND AZIMUTH FOR SIGHTING

By determining the approximate altitudes and azimuths of several planets and bright stars, such as Venus and Jupiter, Sirius, Canopus, Vega, Capella, Rigel, Arcturus, Procyon, Achernar, &c., it is possible to take sights of them in broad daylight, provided their positions are far enough away from the Sun to be visible with the high power inverting telescope.

The previous knowledge of the approximate altitudes and azimuths of these and of many other celestial bodies will also enable the navigator during the twilight to take good sights of them in rapid succession with a daylight horizon, long before it would be possible to locate them with the naked eye alone.

Naturally the problem is the same as explained before on page xv,

¹ A brief account of the possibilities of daytime observations of stars and planets is given by Mr. C. E. MUMFORD (Union Castle Line), in his very interesting little pamphlet, "How to Identify Unknown Stars, &c." London, 1909, 6d.

IDENTIFICATION OF CELESTIAL BODIES

but as not so great accuracy is necessary the required altitudes and azimuths are found by inspection without interpolating.

The following precepts will show when the body is below the horizon, and therefore it cannot be seen at the time:

$$d$$
 and L same name $t>90^{\circ}$ $L+b<90^{\circ}$ d and L contrary names . . .
$$\begin{cases} t<90^{\circ} \dots L+b>90^{\circ} \\ t>90^{\circ} \end{cases}$$

If, for some reason, the bodies were not observed at the time for which the altitudes were calculated, the table giving the rate of "change of altitude per minute of time" on page 174 will enable the observer to find the altitude before or after a certain interval of time.

IDENTIFICATION OF CELESTIAL BODIES

The identification of celestial bodies, or star identification, is of prime importance nowadays, and is strictly indispensable when only one or a few stars are showing at a time. In this case it is impossible to identify the observed stars by alignments.

By rendering "the star observer independent of any previous knowledge of the name of the star he observes," and "by enabling him to identify it from the data used in his observation together with its approximate true bearing," our tables will permit, on account of the great number of arguments, the identification of any one of the 316 stars above magnitude 4.1 catalogued in the Nautical Almanac, without doubt or confusion, and practically without interpolation.²

Therefore, the greatest difficulty in the use of stars—the uncertainty or ignorance of the names of the stars observed—will be overcome.

A star is identified in the *Nautical Almanac* by means of its Right Ascension and Declination. The Right Ascension is found by combining the Greenwich Sidereal Time with the star's geographical longitude. This t_{G} is found by combining the star's hour angle with the longitude by D. R.

We have then to find the star's hour angle t and its declination d. They can be easily and readily obtained from our tables, if we know the star's true altitude and azimuth, or true bearing,³ the

¹ H. W. HARVEY, "What Star is it?" Tables for identifying unknown stars. London, 1909, page 3.

² a Ursæ Minoris (*Polaris*) is not included in this number, but is easily identified without computation. Below 70° latitude its greatest azimuth is 3°.4, and its altitude is always within 1° 10′ of the exact latitude of the observer.

³ When this azimuth or true bearing cannot be obtained by compass observation, determine by means of 3 or more altitudes taken in 3 or more minutes the rate of "change of altitude per minute of time," and our "change of altitude table" on page 174 will give approximately the azimuth with the rate of change, and the observer's latitude. Ex. Lat. 32° and rate of change 9'.o: Azimuth, 45°.

This method of finding the azimuth does not give good results when the body is near the prime vertical, as the table shows.

observer's latitude and longitude by D. R., and the Greenwich time of the observation.

Thus, the problem of identifying celestial bodies is the reverse of the problem of determining altitude and azimuth.

Given h, Z and L, find d and t.

DETERMINATION OF d AND t.

The lower equations of groups of equations (3) and (4) on page xiii are perfectly similar to the upper ones, and show, if we enter the tables with h and Z as arguments in place of d and t respectively, we will find in column a an approximate value of a, and in column b an approximate value of B.

Entering the tables again with a and B as arguments, we will find approximately the values of h and Z given. When greater accuracy is required a more exact value of B can be determined for the exact value of h.

The values of d and t will then be found in the same column a corresponding to b or its complement c.

Determination of $90^{\circ}-b$ or c.

The following precepts deduced from those for determining C facilitate the determination of c given L and B, and present the same advantages as the others. The name of the declination is readily shown.

$$Z < 90^{\circ}$$
 $\begin{cases} L < B \\ L > B \end{cases}$ \vdots $c = B - L \\ \vdots$ \vdots d and L same name $t < 90^{\circ}$ $t > 90^{\circ}$

$$Z>90^{\circ}$$
 $\begin{cases} L+B>90^{\circ}: c=180^{\circ}-(L+B); d, L, m, c < t<90^{\circ} \\ L+B<90^{\circ}: c=L+B, c, c; d, m < L < t<90^{\circ} \end{cases}$

When $Z < 90^{\circ}$, the *smaller* of the two quantities L and B is always subtracted from the *larger* of the two.

When $Z > 90^{\circ}$, L and B are always added together. If their sum is greater than 90°, it is subtracted from 180°.

The following example is one of many presenting themselves daily to navigators.

Example. On August 26, 1908, about 6h 30m P.M., in Lat. by D. R. xxxvi

TIME-AZIMUTHS FOR DEVIATION

o° 20′ N., and Long. by D. R. 44° 23′ W., the weather being cloudy, a bright star appeared and was observed through a break in the clouds in a S.W. direction, bearing true 17°.5 at 9^h 41^m 14^s of the Chronometer, 13^m 16^s fast of G. M. T. The true altitude at the same instant was 23° 48'. The Sidereal Time at Greenwich Mean Noon (R. A. M. S.), was 10^h 17^m 20^s . It was doubtful whether the star was a^2 or β Centauri, both being close to one another, and approximately of the same magnitude. What star was it?

Once known that the observed star was a^2 Centauri, we would work out the sight for position, and would find

$$L_A = 0^{\circ} \text{ 1o' N. and } G_A = 44^{\circ} 23' \text{ W.}$$

 $h_A = 23^{\circ} 58'$, $Z_A = 17^{\circ} 34' \text{ S.W.}$

with very little extra calculation.

TIME-AZIMUTHS FOR DEVIATION

These tables constitute *ideal time-azimuth tables*, as a little examination and comparison with other tables will show.

For the Sun and other celestial bodies with declinations less than 24° , time-azimuths can be easily and rapidly found without interpolation for every 30' (2 minutes of time) hour angles and every 1° of latitude. The hour angle interval increases slowly with the increasing declinations and decreases slowly for increasing values of a, while the latitude interval remains constant throughout.

¹ The determination of the R. A. by means of the G. S. T. and the t_{G_n} instead of determining it (as usually is done) by means of the R. A. M. (A. T. S. $+ \odot$'s R. A.) and the t_i might seem longer, but it must be remembered that stars are identified for position (not for pleasure), and G. S. T. and the t_{G_n} enter in this calculation, whereas the R. A. M. and the \odot 's R. A. are of no use at all afterwards, and give less accurate results.

Time-azimuths are found by the same method used for determining h and Z for lines of position, and as h is not necessary it is not taken into consideration. Unless great accuracy is required (which is not the case in practice) b can be immediately found by inspection without interpolating.

Example. August 26, 1908, A.M. Lat. by D. R. 0° 30' S., and Long. by D. R. 41° 40' W. The Sun's compass bearing was taken at 23^h 3^m 0^s Greenwich mean time. What was the Sun's true bearing or azimuth at the same instant?

G. M. T. =
$$23^h$$
 3^m 0^s Eq. of T. = -1 56 G. A. T. = 23^h 1^m 4^s $0's$ $t_G = 0.58$ 56 E $0's$ $t_G = 0.58$ 56 E $0's$ $t_G = 14^\circ$ $44'$ E $0's$ $t_G = 14^\circ$ $44'$ E $0's$ $t_G = 14^\circ$ 40 W $10's$ $t_{D.R.} = 10's$ $10's$ $10's$

TIME-ALTITUDE-AZIMUTHS

When d, t and h are given to find Z the tables give immediately its value.

Example. Same as above for time-azimuth. Given $d=10^{\circ}$ 29', $t=56^{\circ}$ 24', and $h=32^{\circ}$ 51', find Z.

Entering the tables with d and t as arguments, we will find in column $a: 55^{\circ}$ o', which is an approximate value of a, and in column $b: 18^{\circ}$, an approximate value of b. Entering the tables again with $a=55^{\circ}$ o' and $b=18^{\circ}$ as arguments, we will find approximately the values of d and t. In the same column $a=55^{\circ}$ o' corresponding to $h=32^{\circ}$ 51' we will find $Z=77^{\circ}$ 9'.

DISTANCE AND COURSE IN GREAT CIRCLE SAILING

The problem of finding distance and course in Great Circle Sailing may also be easily solved by our tables, because it is the same as determining altitude and azimuth. The distance corresponds to the zenith distance or complement of the altitude and the course to the azimuth. The only difference is that the distance between the two given points can be greater than 90°, whereas the zenith distance cannot be greater than 90°.

In Fig. 1 let A be the port of departure, M be the port of arrival and P the pole nearest to A. PQP'Q' the meridian of Greenwich and QA'M'Q' the Equator.

If L is the latitude of the port of departure A, L' the latitude of xxxviii

LUNAR DISTANCES

the port of arrival M and MPA or t the difference in longitude between the two ports, the following precepts enable us to determine the value of C given L and b and indicate also in the last two columns if the distance D and the course C_1 are smaller or greater than 90°. When <90° the values of D and C_1 given by the tables are the right ones. When >90° subtract the values found from 180°.

$$L' \text{ and } L \\ \text{same name} \begin{cases} t < 90^{\circ} \begin{cases} L < b \\ L > b \end{cases} \dots : C = b - L; D < 90^{\circ} \text{ and } C_{1} < 90^{\circ*} \\ L > b \end{cases} \dots : C = L - b; D < 90^{\circ} \text{ , } C_{1} > 90^{\circ*} \end{cases} \\ t > 90^{\circ} \begin{cases} L + b > 90^{\circ} : C = L + b; D < 90^{\circ} \text{ , } C_{1} < 90^{\circ*} \\ L + b < 90^{\circ} : C = L + b; D > 90^{\circ} \text{ , } C_{1} < 90^{\circ*} \end{cases} \\ L' \text{ and } L \\ \text{contrary names} \end{cases} \begin{cases} t < 90^{\circ} \begin{cases} L + b < 90^{\circ} : C = L + b; D < 90^{\circ} \text{ , } C_{1} < 90^{\circ*} \\ L + b > 90^{\circ} : C = L + b; D > 90^{\circ} \text{ , } C_{1} > 90^{\circ*} \end{cases} \\ t > 90^{\circ} \begin{cases} L > b \\ L < b \end{cases} \dots : C = L - b; D > 90^{\circ} \text{ , } C_{1} < 90^{\circ} \end{cases}$$

* These are the four cases corresponding to those for finding h and Z ($D < 90^{\circ}$). When L + b is greater than 90° it is subtracted from 180° .

In our tables L' takes the place of d, $90^{\circ}-D$ the place of h, and C_1 the place of Z.

We are of the opinion, however, that the Great Circle charts offer a more simple and practical solution of the problem, and the tables only ought to be used when they are not at hand.

LUNAR DISTANCES

We have already stated in the INTRODUCTION that the problem of calculating Lunar Distances is similar to the problem of determining Distance in Great Circle Sailing.

In Fig. 1 on page ix, let M be the Moon, A the other body observed, and P the pole nearest to A. MA will be the Lunar Distance. If QA'M'Q' is the celestial Equator and Q the first point of Aries or the true vernal equinox, QPA' or QA' will be the Right Ascension of A, QPM' or QM' the Right Ascension of the Moon and A'PM'=t equal to the difference between the two Right Ascensions. If we represent MM', the declination of the Moon by d_M and AA' the declination of the other body observed by d_A , the following formulæ and precepts will enable us to calculate the Lunar Distance MA=D without dealing with algebraic signs or arcs greater than 90°.

$$\tan b = \tan d_M \sec t$$

$$\cos D = \sin d_M \cos C \csc b$$

¹ Vide "The Development of Great Circle Sailing," by G. W. Littlehales, U.S. Hydrographic Office, Second Edition, Washington, 1899.

$$d_{M} \text{ and } d_{A} \text{ same name } \dots \begin{cases} t < 90^{\circ} \begin{cases} d_{A} < b & :: C = b - d_{A}; \ D < 90^{\circ} \\ d_{A} > b & :: C = d_{A} - b; \ D < 90^{\circ} \end{cases} \\ t > 90^{\circ} \begin{cases} d_{A} + b > 90^{\circ} : C = d_{A} + b; \ D < 90^{\circ} \\ d_{A} + b < 90^{\circ} : C = d_{A} + b; \ D > 90^{\circ} \end{cases} \\ d_{M} \text{ and } d_{A} \text{ contrary names} \end{cases} \begin{cases} t < 90^{\circ} \begin{cases} d_{A} + b < 90^{\circ} : C = d_{A} + b; \ D < 90^{\circ} \\ d_{A} + b > 90^{\circ} : C = d_{A} + b; \ D > 90^{\circ} \end{cases} \\ t > 90^{\circ} \begin{cases} d_{A} > b & ... : C = d_{A} - b; \ D > 90^{\circ} \\ d_{A} < b & ... : C = b - d_{A}; \ D > 90^{\circ} \end{cases} \end{cases}$$

For the sake of comparison we will work out the example explained on page 232 of the Nautical Almanac for 1910, Part I.

EXAMPLE I .- MOON AND SUN.

To find the true distance between the Moon and the Sun at noon, Greenwich Mean Time, on March 8, 1910.

From the Nautical Almanac, Part I.

RIGHT ASCENSION. DECLINATION.

Sun 23^h 12^m 20^s.0

Moon 20 41 3.4
diff.
$$2^h$$
 31^m 16^s.6 or 37° 49' 9" = t

log tan $d_M = 9.628846$
log sec $t = 0.102400$
log tan $b = 9.731246$
 $b = 28^\circ$ 18' 21"
$$d_A = 5 7 9$$
 $C = 23^\circ$ 11' 12"

DECLINATION.

$$5^\circ$$
 7' 9" S (d_A)

$$\frac{23 2 50 S}{37^\circ 49' 9" = t}$$

log sin $d_M = 9.592720$
log cos $C = 9.963423$
log cosec $b = 0.324059$
log cos $D = 9.880202$

$$D = 40^\circ$$
 37' 48"

Therefore, 40° 37′ 48″ is the *true distance* between the Moon and the Sun at noon on March 8, 1910.

ALL OTHER PROBLEMS SOLVED

All the other problems in Nautical Astronomy depending upon the solution of right-angled spherical triangles can be easily solved by these tables.

Some of these problems are: Amplitudes and horizon-azimuths, hour angle of a celestial body in the horizon (approximate time of sunset and sunrise, &c.), altitude and hour angle of a celestial body on the prime vertical, altitude and hour angle of a celestial body when position angle is 90°, &c.

ALL OTHER PROBLEMS SOLVED

	Problem	Formula	FORMULA
Fund	amental Formulæ	$\sin a = \cos d \sin t$	cot b=cot d cos t
	desgiven d and L $\left\{ \dots ,, d, t \right\}$	$\sin d = \cos L \sin (90^{\circ} - Z)$ $\sin Z = \cos d \sin t$	cot $(90^{\circ} - d) = -\cot L \cos t$ When d and L are of the same name, take $180^{\circ} - b$ for value of t .
n' in altitude is the I variation in azimuth and L same name).	Body on prime vertical: d <l< td=""><td>$\sin d = \cos (90^{\circ} - L) \sin h$</td><td>$\cot L = \cot d \cos t$</td></l<>	$\sin d = \cos (90^{\circ} - L) \sin h$	$\cot L = \cot d \cos t$
nen variation' in greatest and var the least (d and	1 14	•	11 1 1
When gree the	Body's position angle is 90° : $d > L$	$\sin L = \cos (90^\circ - d) \sin h$	$\cot d = \cot L \cos t$

A comparison of the formulæ for solving these problems with the fundamental formulæ will immediately show the navigator how to proceed. It is well to notice that, except the case in which horizon-azimuths are found by the formulæ

$$\sin Z = \cos d \sin t$$

the required quantity is always found in the tables from underneath in column t.

AMPLITUDES.

To find the amplitude of a celestial body in the true horizon enter the tables with L in the place of d. Run up column a with d opposite which will be found $90^{\circ}-Z$ in column t.

Amplitudes of the Sun for compass correction are generally the only ones observed and for a height of the eye= 10^{m} (33 ft.) the Sun's centre is on the true horizon when its lower limb is about 24' ($\frac{3}{4}$ of its diameter) above the horizon.

Example. $L=37^{\circ}$ N., and $d=22^{\circ}$ N. (rising), we will find $90^{\circ}-Z=28^{\circ}$ E.: N.

The amplitude always takes the name of the declination.

Sometimes it may be more convenient to observe the Sun just when its lower limb touches the horizon. A small correction given in the table below will then have to be applied to the amplitude found by the formula

$$\sin d = \cos L \sin (90^{\circ} - Z)$$
.

Dec.				Lati	tude.			
	o°	100	20°	30°	40°	50°	60°	65°
o°	0°.0	0°.1	0°.2	0°.2	o°.4	o°.5	o°.8	°.9
10	.0	. I	.2	•3	•4	.6	.8	1,0
20	.0	, I	.2	•3	•4	.6	1.0	1.6
24	.0	.1	.2	• 3	•4	•7	1.3	3.4

d and L same name add correction to $90^{\circ}-Z$ d and L contrary names . . subtract , from ,

This table will be practically good for heights of the eye varying from 6^m to 15^m (20 ft. to 49 ft.).

To find the hour angle of a body in the true horizon enter the tables with L in the place of d. Run up column b with $90^{\circ}-d$ opposite which will be found t in column t.

Example. $L=37^{\circ}$ N., and $d=22^{\circ}$ N. (rising), we will find $t=108^{\circ}$ E.

HORIZON-AZIMUTHS.

To find horizon-azimuths enter the tables with d and t (or $180^{\circ}-t$) as arguments. In column a we will find Z.

Example. $d=22^{\circ}$ N., and $t=108^{\circ}$ E. We will have $Z=62^{\circ}$ N.E. They always take the name of the declination.

BODY ON PRIME VERTICAL.

To find the altitude of a celestial body on the prime vertical entertables with $90^{\circ}-L$ in the place of d, and run up column a with d. In column t will be found h.

To find the hour angle of a celestial body on the prime vertical enter tables with d as argument, and run up column b with L. In column t will be found t. In column a will be found a volumn a volum

Example. $d=8^{\circ}$ N., and $L=39^{\circ}$ N. We will find $h=12^{\circ}$ 47', and $t=80^{\circ}$.

BODY'S POSITION ANGLE: 90°.

To find the altitude of a celestial body when its position angle is 90° enter tables with $90^{\circ}-d$ in the place of d, and run up column α with L. In column t will be found h.

To find the hour angle of a celestial body when its position angle is 90° enter tables with L in the place of d, and run up column b with d. In column t will be found t. In column a will be found 90° -h.

Example. $d=23^{\circ}$ S., and $L=12^{\circ}$ S. We will find $h=32^{\circ}$ 9', and $t=60^{\circ}$.

CONCLUSION AND APPENDIX

CONCLUSION

The author since 1908, during a trip from Rio de Janeiro to New York on the s.s. *Voltaire*—Lamport and Holt—has worked out many sights for lines of position taken under various circumstances by his modified tables and the improved methods as explained here, with the most satisfactory results.

Only two openings of the tables are necessary. The first is immediately indicated by the value of d, and the second by the value of a. No time is lost in turning pages. If indexed the desired pages will be found quicker.

The fact that the perpendicular a is common to the two right-angled triangles reduces the bulk of the tables to a minimum.

The use of an assumed position instead of the position by D. Regreatly simplifies the calculations involved in the determination of h and Z, as we have seen.

In the typical example presented no actual figures used have been suppressed. The tables give h with an approximation of one minute, and in the majority of cases with greater approximation. Z is always found with sufficient approximation for practical use.

The simplicity and readiness with which all the other problems are also solved show that: They are "the simplest and readiest in solution."

APPENDIX I

Navigators "ought to be spared the waste of time in making calculations, which can be 'better done once for all by a single computer on dry land."

LORD KELVIN. Letter to Lord Ellenborough, R.N., December 4, 1902. ["Stars and Sextants," Published by J. D. Potter, London, 1903.]

It is easier to turn pages than to interpolate.

In order to spare navigators "the waste of time in making calculations," and especially to reduce the chances of error to a *minimum*, the author proposes, as a simple and easy solution of the problem, an extension of his tables where d and t would be tabulated for every *minute of arc* (1') of a and every *thirty minutes of arc* (30') of b.

With such tables, occupying a little over 1000 pages in large 8vo, no interpolation would be necessary, and the only calculation

involved would be the determination of C with L and b by means of our simple precepts.

Thus the problem of determining lines of position at sea would be nearly as simple as the problem of determining latitude by a meridian sight.

Our typical example on page xxiii would be solved by such tables as follows:

$$\frac{a = 12^{\circ} 13' \quad \text{G. A. T.} = 1^{\text{h}} 43^{\text{m}} 36^{\text{s}}}{\bar{b} = 12^{\circ} 27'} \quad d = 12^{\circ} 10' \text{ N}$$

$$\frac{L_{A.} = 16 \quad 3 \text{ S}}{L_{A.} = 16 \quad 3 \text{ S}} \quad \frac{t_{A.} = 12 \quad 30 \quad \text{E}}{G_{A.} = 38^{\circ} 24' \text{ W}}$$

$$\frac{h_{o} = 59^{\circ} \text{ o'}}{\text{Corr.} = + \quad 10}$$

$$\frac{h = 59^{\circ} 10'}{h = 59^{\circ} 10'}$$

$$L_{A.} = 24^{\circ} 24' \text{ NE}$$

$$\frac{h - h_{A.} = - \quad 2'}{h - h_{A.} = - \quad 2'}$$

EXPLANATION.

Entering the tables with $d=12^{\circ}$ 10', and $t_A=12^{\circ}$ 30', as arguments, we would find *immediately* $a=12^{\circ}$ 13', and $b=12^{\circ}$ 27'.

(As b corresponds to the *exact* value of d, it is not necessary to reenter the tables with a and b as arguments, as explained on page xx.)

Entering the tables again with $a=12^{\circ}$ 13' and $C=28^{\circ}$ 30', as arguments, we would find *immediately* $h_{A}=59^{\circ}$ 12', and $Z_{A}=24^{\circ}$ 24'.

Although it is well known that "it is easier to turn pages than to interpolate," the question appears whether it would be worth while to extend the tables as mentioned above in order to do away with the two simple interpolations occurring in our method.

However, it would be convenient to extend the tabulation for every 10' of a, and for every 1° of b. The tables would then have 360 pages similar to those published now.

If these tables meet with success, the author will publish the above 360 page tables, which he is already preparing for his own use.²

¹ This method may be advantageously used with the present tables when the hour angle t is near 90°, especially when the declination is large. Hardly any calculation is then necessary to find h and Z.

Example. $d=30^{\circ}$ 15' S., $t=89^{\circ}$ 0', and $L=10^{\circ}$ 17' S. We would find $a=59^{\circ}$ 44', $b=88^{\circ}$ 17', $C=78^{\circ}$ 0', $h=6^{\circ}$ 1', and $Z=60^{\circ}$ 17'.

² The author has decided to reduce these 360 pages to 166 in view or the fact that the factors $\frac{60'}{\Delta}$ and $\frac{\Delta}{60'}$ are not necessary for every 10' of α . (January, 1912.)

APPENDIX II

The true spirit of the "Newest Navigation" requires the plotting of each line of position upon Mercator's chart or upon squared paper representing a Plane chart, and for this reason we have given Figs. 3 and 4 showing how these lines are plotted.¹

However, the classical Noon position deduced by combining the morning (or afternoon) sight with the meridian sight of the Sun continues and will continue to render good services to many navigators, and at the request of several friends, we have decided to add this Appendix showing how the Noon position can be easily and rapidly determined with our Tables by calculation alone.

This case also applies itself to the combination of a time sight with the meridian sight of any celestial body.

Example.—The same as on page xix. The distance run from 8 A.M. to Noon is represented by GT (Fig. 3): 5'.5 N. in latitude and 40'.1 W. in longitude.

The observed meridian altitude of the Sun was 42° 35'.6. BACK towards the elevated pole.

What was the ship's position at NOON?

¹ See also "The New Navigation: Presented in a Familiar Way for Captains and Officers of the Merchant Service." By F. C. Cross, Lieut. R.N.R. Glasgow: James Brown & Son. Price 2s. net.

EXPLANATION.

The first part of the calculation is developed as explained on

page xx.

The application of the first correction (Corr.=8'.9 W) to G_A gives us the longitude of the point G where the line of position GBL intersects the assumed parallel of latitude 36° 51'.6 N. This correction is found by multiplying the coefficient $\frac{\Delta t}{\Delta k}$ =1.48 by $k-k_A$ =6'.

This coefficient $\frac{\Delta t}{\Delta k}$ is taken from the Table 1 on page 171 giving the "Change of Hour Angle per Minute of Arc of Altitude" by extrapolation.

When $h-h_A$ is plus (+) the name of the correction is East or West according to the name of the azimuth.

When $h - h_A$ is minus (-) the name is contrary to the name of the azimuth, as in our case.

The longitude factor or PAGEL's coefficient is obtained from the Tables, as explained on page xvii.

Thus, entering the Tables on page 122 with $L=37^{\circ}$ in column b/B and with $Z=58^{\circ}$ in column Z we would find 0.79, which is the "change of hour angle or of longitude per minute of arc of latitude." The name of the longitude correction or PAGEL's correction, or simply the PAGEL, 4'.7 (the result of the multiplication of 0.79 by the difference 6'.0 between the two latitudes: the assumed brought up to NOON and the meridian latitude), is easily given by JOHNSON's well-known rule: "Under the sun's bearing at the time of the observation write the opposite bearing, and suppose the letters to be connected diagonally, then that connected with the name of the correction for latitude will be the name of the correction for the longitude." ²

Thus S E

and as the meridian latitude was 6'.0 to the SOUTH of the assumed latitude, the PAGEL 4'.7 is to W.

The third and last correction is g=40'. I W for the run in longitude from the time of observation to Noon.³

² "On Finding the Latitude and Longitude in Cloudy Weather, &c.," page 7;

32nd edition, London, 1909. Published by Mr. J. D. Potter. Price 5s.

¹ This Table is limited to azimuths comprised between 60° and 90°. For observations where the azimuth is smaller than 60° a simplification results, and it is better to follow the other method, slightly different, explained further on.

³ In practice it is not necessary to apply *separately* each one of the three corrections to the assumed longitude G_A . They can be combined and the result then applied to G_A . The total correction to be applied to G_A . W. would be 53'.7 W. (8'.9 W.+4'.7 W.+40'.1 W) giving us immediately G at NOON=9° o'.0 W.

APPENDIX II

Therefore N, in Fig. 3, represents the ship's position at NOON.

ANOTHER SIMPLIFIED METHOD.

When the azimuth of the observed body is smaller than 60° we can use with more advantage the process explained on page xxviii, it not being necessary to apply to G_A the correction due to $h-h_A$, reduced to o in this case.

Our example would be developed as follows:-

$$\frac{a^{8} - 52^{\circ} \quad o'}{b = 17^{\circ} \quad 8'.4} \frac{d = 10^{\circ} \quad 27' \quad S}{d = 10^{\circ} \quad 27' \quad S} \underbrace{\begin{array}{c} t_{A.} = 45^{\circ} \quad 9'.0 \quad E \\ h_{o} = 20^{\circ} \quad 59'.2 \\ Corr. = + \quad 7.8 \\ A_{o} = 10^{\circ} \quad 7'.0 \\ A_{o} = 10^{\circ} \quad 7'.0 \\ A_{o} = 10^{\circ} \quad 11'.3 \\ A_{o} = 10^{\circ} \quad 11' \quad 10^{\circ} \\ A_{o} = 10^{\circ} \quad 10^{\circ} \quad 10^{\circ} \quad 10^{\circ} \quad 10^{\circ} \\ A_{o} = 10^{\circ} \quad 10^{\circ} \quad 10^{\circ} \quad 10^{\circ} \\ A_{o} = 10^{\circ} \quad 10^{\circ} \quad 10^{\circ} \quad 10^{\circ} \\ A_{o} = 10^{\circ} \quad 10^$$

After finding the values of a, b and t_A as explained before, the assumed longitude $G_A=8^\circ$ 6'.3 W. is determined. In order to determine the assumed latitude $L_A=37^\circ$ 2'.9, the latitude of L in Fig. 3, where $h=h_A$ and therefore $h-h_A=0$, we deduce the value of C corresponding to the true altitude $h=21^\circ$ 7'.0 and we find $C=54^\circ$ 11'.3. This value of C combined with $b=17^\circ$ 8'.4 gives us $L_A=37^\circ$ 2'.9.

The corrections for finding the true longitude at NOON are then found, as explained before on page xlvi. This process, evidently very simple, will always render good services when the azimuth is *smaller* than 60°, especially to those navigating the North Atlantic Ocean from Europe to the United States of America and *vice versa* in winter time.

When the azimuth is *larger* than 60° it is better to use the first process explained in this Appendix, because then to small changes of h correspond large changes of C, and the assumed latitude would sometimes differ very much from the true latitude, therefore making the longitude correction or the PAGEL too large and not very exact.

Although the author obtained in 1910 very good results going from England to the United States on board the Brazilian battleship *Minas Geraes* with azimuths as large as 77° and 78°.5, he would advise the method to be used with care beyond 60°.

For exercise, work out the same examples by both methods with $a=51^{\circ}$ 30' instead of $a=52^{\circ}$ 0'.

APPENDIX III

An interesting article recently published by Mr. H. B. GOODWIN in the *Nautical Magazine* for February 1912, page 176, describing "A New Form of Table for Calculating Altitude" from an *assumed position*, interpolation being reduced to the odd minutes of declination, has suggested to us this Appendix, where we will show how easily and rapidly the altitude *alone* from an *assumed position* can be found by inspection in our Tables, by simply "interchanging the latitude L and the declination d."

Only one simple interpolation is required for the odd minutes of declination, as in Mr. GOODWIN'S method.

This interchanging of L and d in our Tables geometrically corresponds to dropping the perpendicular a from Z upon the circle of declination MP (Fig. 2), instead of dropping it from the body M upon the meridian PZQ.

This perpendicular has the disadvantage of dividing the azimuth Z into two parts.

Special Tables for solving the triangle thus divided were published in Paris, in 1893, by Lieut. R. Delafon, French Navy, and are entitled "Méthode rapide pour déterminer les Droites et Courbes de Hauteur et faire le Point." 1

For the sake of comparison we will take and work out Mr. GOODWIN'S example on page 186 by means of our Tables.

April 22, 1911, at 4^h 12^m Greenwich Apparent Time, in latitude by account, 36° 41′ N., longitude 32° 47′ W., the Sun's altitude was observed, the declination being 11° 58′.2 N.

Find the position to be assumed, and calculate the zenith distance at that point for the time of observation.

If h_A is reduced to $L=37^{\circ}$ N. and $t=30^{\circ}$ (Mr. GOODWIN'S assumed position) we would find

$$h = 53^{\circ} \text{ 16'.1 or } z = 36^{\circ} 43'.9.$$

He found
$$h=53^{\circ} \text{ 15'.6 or } z=36^{\circ} 44'.4.$$

APPENDIX III

EXPLANATION.

Entering the Tables with $L=37^{\circ}$ in the place of $d=37^{\circ}$ and $t=30^{\circ}$ on page 102, we find in column a approximately $a=23^{\circ}$ 30'. Entering on page 84 in column $a=23^{\circ}$ 30', we find in column d/h, $L_A=36^{\circ}$ 59', and in column t/Z, $t_A=29^{\circ}$ 57'.

They correspond to $b=41^{\circ}$. Combining this b with the declina-

tion $d = 11^{\circ} 58'.2$ we find $C = 29^{\circ} 1'.8$.

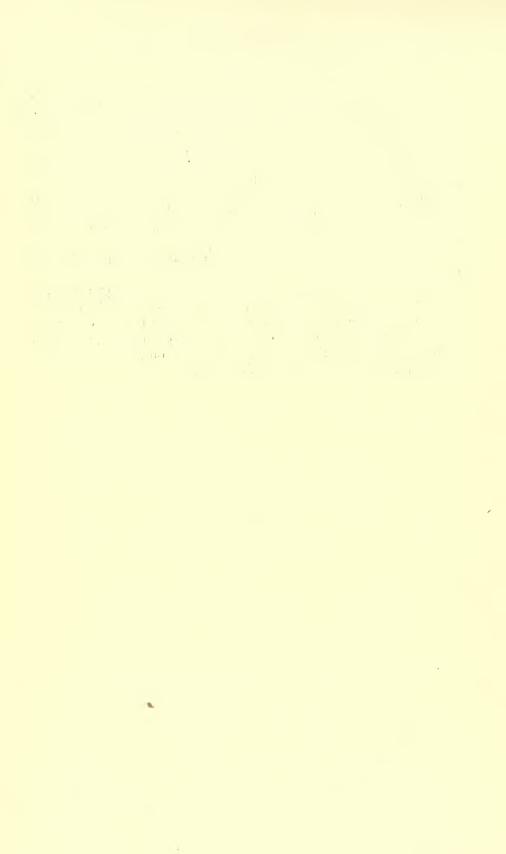
Therefore entering the Tables on the next page 85 in column $a=23^{\circ}$ 30' we find corresponding to $C=29^{\circ}$ 1'.8: $h_{A}=53^{\circ}$ 18'.7. If necessary, the position angle would be found alongside this h_{A} in column t/Z, approximately equal to 41° 53'.

This is the "simplest and readiest" way of finding altitude alone

from an assumed position.

However, as the azimuth is always necessary (except when the method explained on page xxxi is used) to show the direction of the line of position or to facilitate the calculation of the corrections it is always preferable to use our method for determining simultaneously the altitude and the azimuth, as explained on pages xix et seq.

It is the "simplest and readiest in solution."



THE "NEWEST" NAVIGATION ALTITUDE AND AZIMUTH TABLES

a de la composition della comp

PLANE TRAVERSE TABLES

								P	lan	e 7	Гга	.ver	se	Та	ble	:							
Course.	D:	=1'	D=	=2'	D=	=3′	D=	=4'	D=	=5′	D=	=6′	D=	=7′	D=	-8′	D=	=9′	D =	10′	D =	11'	Course.
Cor	LAT	DEP	Lat	DEP	Lat	DEP	LAT	DEP	Lat	DEP	LAT	DEP	Lat	DEP	Lat	DEP	LAT	DEP	LAT	DEP	Lat	Dep	Co
0 1 2 3 4	, i.o i.o i.o i.o	0.0		, 0.0 0.0 0.1 0.1 0.1	3.0 3.0 3.0 3.0	0.0 0.1 0.1 0.2 0.2	4.0 4.0 4.0	0.1	5.0 5.0 5.0 5.0	0.0 0.1 0.2 0.3 0.3	6.0 6.0 6.0 6.0 6.0	0.2	7.0 7.0	0.4 0.5		0.1 0.3 0.4 0.6	9.0 9.0 9.0		10.0 10.0 10.0 10.0		11.0 11.0 11.0 11.0	0.4 0.6 0.8	90 89 88 87 86 85
56 78 9	I.0 I.0 I.0 I.0	0. I 0. I 0. I 0. I 0. 2	2.0 2.0 2.0 2.0	0.2	3.0 3.0 3.0 3.0	0.3 0.3 0.4 0.4 0.5	4.0 4.0 4.0 4.0	0.4 0.5 0.6 0.6	5.0 5.0 5.0 4.9	0.4 0.5 0.6 0.7 0.8	6.0 6.0 5.9 5.9	0.5 0.6 0.7 0.8 0.9	1	0.7 0.9 1.0 1.1	8.0 7.9 7.9 7.9	1.3	9.0 8.9 8.9 8.9	0.9 1.1 1.3 1.4	9.9 9.9 9.9	1.0 1.2 1.4 1.6	11.0 10.9 10.9 10.9	1.1 1.3 1.5 1.7	84 83 82 81
10 11 12 13 14	I.0 I.0 I.0 I.0	0.2 0.2 0.2 0.2 0.2	2.0 2.0 1.9 1.9	0.3 0.4 0.4 0.4 0.5	3.0 2.9 2.9 2.9 2.9	0.5 0.6 0.6 0.7 0.7	3.9 3.9 3.9 3.9	0.8	4.9 4.9 4.9 4.9	I.O I.I I.2	5.9 5.9 5.8 5.8	1.0 1.1 1.2 1.3	6.8 6.8	1.7	7.8 7.8 7.8	1.8	8.8 8.8 8.8	1.6 1.7 1.9 2.0 2.2	9.8 9.8 9.8 9.7 9.7	2.4	10.8 10.8 10.8 10.7	2.5	80 79 78 77 76
15 16 17 18 19	1.0 1.0 1.0 0.9	0.3 0.3 0.3 0.3 0.3	1.9	o.5 o.6 o.6 o.6	2.9 2.9 2.9	0.8 0.9 0.9	3.8 3.8 3.8		4.8 4.8 4.8 4.8 4.7	1.3 1.4 1.5 1.5	5.8 5.7 5.7 5.7	1.6 1.7 1.8 1.9 2.0	6.6	1.8 1.9 2.0 2.2 2.3	7·7 7·7 7·7 7·6 7·6	2.6	8.7 8.6 8.6 8.5	2.3 2.5 2.6 2.8 2.9	9.7 9.6 9.6 9.5 9.5	3.1	10.6 10.5 10.5 10.5	3.2 3.4 3.6	75 74 73 72 71
20 21 22 23 24	0.9 0.9 0.9 0.9	0.3 0.4 0.4 0.4 0.4	1.9 1.9 1.9 1.8 1.8	0.7	2.8	I.O I.I I.I I.2 I.2	3·7 3·7 3·7	1.6	4.7 4.6 4.6 4.6 4.6	2.0	5.6 5.6	2.1 2.2 2.2 2.3 2.4	6.5 6.5 6.4 6.4		7·5 7·5 7·4 7·4 7·3	2.9 3.0	8.3 8.3	3. I 3. 2 3. 4 3. 5 3. 7	9.4 9.3 9.3 9.2 9.1	3.4 3.6 3.7 3.9 4.1	10.3	3.9 4.1 4.3	70 69 68 67 66
25 26 27 28 29	0.9 0.9 0.9 0.9	0.4 0.4 0.5 0.5 0.5	1.8 1.8 1.8 1.7	o.8 o.9 o.9 o.9	2.7 2.7 2.6	1.3 1.3 1.4 1.4 1.5	3.6 3.5	1.8	4·5 4·5 4·5 4·4 4·4	2.3	5.3	2.7	6.3 6.2 6.2 6.1	3.3	7.1	3.8		3.8 3.9 4.1 4.2 4.4	9.1 9.0 8.9 8.8 8.7	4.5	9.9 9.8 9.7 9.6	4.8 5.0 5.2	65 64 63 62 61
30 31 32 33 34	o.9 o.9 o.8 o.8 o.8	0.5 0.5 0.5 0.5 0.6	1.7 1.7 1.7 1.7		2.6 2.5 2.5	1.5 1.6 1.6 1.6	3·4 3·4	2.1	4·3 4·2 4·2	2.6	5.1 5.0	3.1 3.2 3.3	5·9 5·9	3.7	6.8 6.7	4. I 4.2	7.6 7.5	4.5 4.6 4.8 4.9 5.0		5·3 5·4	9·5 9·4 9·3 9·2 9·1	5.7 5.8 6.0	60 59 58 57 56
35 36 37 38 39	o.8 o.8 o.8 o.8	o.6 o.6 o.6 o.6 o.6	1.6 1.6 1.6 1.6	1.1 1.2 1.2 1.2 1.3	2.5 2.4 2.4 2.4 2.3	1.7 1.8 1.8 1.8	3.2 3.2 3.1	2.5 2.5	4.0 4.0 3.9 3.9	2.9 3.0 3.1 3.1		3.5 3.6 3.7 3.8	5.4	4.1 4.2 4.3 4.4	6.3 6.2	4.7 4.8 4.9 5.0	7·3 7·2 7·1 7·0	5.2 5.3 5.4 5.5 5.7	8.2 8.1 8.0 7.9 7.8	5.9 6.0 6.2 6.3	8.9 8.8 8.7 8.5	6.6 6.8 6.9	55 54 53 52 51
40 41 42 43 44	0.8 0.7 0.7	0.6 0.7 0.7 0.7 0.7	I.5 I.5 I.5	1.3 1.3 1.4	2.3 2.2 2.2	2.0 2.0 2.0 2.1	3.0 3.0 2.9 2.9	2.6 2.7 2.7 2.8	3.8 3.8 3.7 3.7 3.6	3·3 3·3 3·4 3·5	4.5 4.5 4.4 4.3	3.9 4.0 4.1 4.2	5·3 5·2 5·1 5·0	4.6 4.7 4.8	6.0 5.9	5.2 5.4 5.5	6.8 6.7 6.6 6.5	5.9 6.0 6.1 6.3	7·5 7·4 7·3 7·2	6.6 6.7 6.8 6.9	8.3 8.2 8.0 7.9	7.1 7.2 7.4 7.5 7.6	49 48 47 46
45	0.7	_	_	1.4	2. I	-	=	=	3.5	_	-	=	_		5·7	-		_	7.1	=	<u> </u>	7.8	45
Course.	_	$D = \mathbf{1'} D = \mathbf{2'} D = \mathbf{3'}$						=4'	-	=5'	-	=6'	-	LAT =7'		=8'	\vdash	LAT = 9'	DEP D=	LAT	DEP	<u></u>	Course.

						Pla	ne î	Γrav	erse	е Та	able						
Course.	D=	12'	D =	13′	D =	:14'	D=	15'	D =	16′	D=	=17′	D=	=18′	D =	19'	Course.
ပိ	LAT. I	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
°0 1 2 3 4	12.0 0 12.0 0	0.0 0.2 0.4 0.6 0.8	13.0 13.0 13.0 13.0	0.0 0.2 0.5 0.7 0.9	, 14.0 14.0 14.0 14.0	0.0 0.2 0.5 0.7 1.0	15.0 15.0 15.0 15.0	0.3 0.5 0.8	16.0 16.0 16.0 16.0 16.0	0.0 0.3 0.6 0.8	17.0 17.0	0.0 0.3 0.6 0.9	18.0 18.0	0.0 0.3 0.6 0.9	19.0	0.0 0.3 0.7 1.0	90 89 88 87 86
5 6 7 8 9	11.9	1.0 1.3 1.5 1.7	13.0 12.9 12.9 12.9	1.1 1.4 1.6 1.8 2.0	13.9 13.9 13.9 13.9	I.2 I.5 I.7 I.9 2.2	14.9 14.9 14.9 14.8	1.6 1.8 2.1 2.3	15.9 15.9 15.8 15.8	1.9 2.2 2.5	16.9 16.9 16.8 16.8	1.5 1.8 2.1 2.4 2.7	17.9 17.8 17.8	1.6 1.9 2.2 2.5 2.8	18.9 18.8 18.8	1.7 2.0 2.3 2.6 3.0	85 84 83 82 81
10 11 12 13 14	11.8 2 11.7 2 11.7 2 11.6 2	2.1 2.3 2.5 2.7 2.9	12.8 12.8 12.7 12.7 12.6	2.3 2.5 2.7 2.9 3.1	13.8 13.7 13.7 13.6 13.6	2.4 2.7 2.9 3.1 3.4	14.8 14.7 14.7 14.6 14.6	3.1 3.4 3.6	15.8 15.7 15.7 15.6 15.5	3.9	16.7	3.0 3.2 3.5 3.8 4.1	17.7 17.6 17.5 17.5	3.1 3.4 3.7 4.0 4.4	18.7	3.3 3.6 4.0 4.3 4.6	80 79 78 77 76
15 16 17 18 19	11.5 11.5 11.4 11.3	3.1 3.3 3.5 3.7 3.9	12.6 12.5 12.4 12.4 12.3	3.4 3.6 3.8 4.0 4.2	13.5 13.5 13.4 13.3 13.2	3.6 3.9 4.1 4.3 4.6	14.5 14.4 14.3 14.3 14.2	4.1 4.4 4.6 4.9	15.4 15.3 15.2 15.1	4·7 4·9 5·2	16.3 16.3 16.2 16.1	4.4 4.7 5.0 5.3 5.5 5.8		4.7 5.0 5.3 5.6 5.9 6.2	18.3 18.2 18.1 18.0	4.9 5.2 5.6 5.9 6.2	75 74 73 72 71
21 22 23 24	II.2 4 II.1 4 II.0 4	4.1 4.3 4.5 4.7 4.9	12.1 12.1 12.0 11.9	4.4 4.7 4.9 5.1 5.3	13.2 13.1 13.0 12.9 12.8	5.0 5.2 5.5 5.7	14.0 13.9 13.8 13.7	5.4 5.6 5.9 6.1		5.7 6.0 6.3 6.5	15.9 15.8 15.6 15.5	6.1 6.4 6.6 6.9	16.8 16.7 16.6 16.4	6.5 6.7 7.0 7.3	17.7 17.6 17.5 17.4	6.5 6.8 7.1 7.4 7.7	70 69 68 67 66
25 26 27 28 29	10.8 10.7 10.6 10.5	5.1 5.3 5.4 5.6 5.8	11.8 11.7 11.6 11.5 11.4	5.5 5.7 5.9 6.1 6.3	12.7 12.6 12.5 12.4 12.2	5.9 6.1 6.4 6.6 6.8	13.5 13.4 13.2 13.1	6.8 7.0 7.3	14.4 14.3 14.1 14.0	7·5 7·8	15.3 15.1 15.0 14.9	7.2 7.5 7.7 8.0 8.2	16.2 16.0 15.9 15.7	7.9 8.2 8.5 8.7		8.3 8.6 8.9 9.2	65 64 63 62 61
30 31 32 33 34	10.3 10.2 10.1 9.9	6.0 6.2 6.4 6.5 6.7	11.3 11.1 11.0 10.9 10.8	6.5 6.7 6.9 7.1 7.3	12.1 12.0 11.9 11.7 11.6	7.0 7.2 7.4 7.6 7.8	13.0 12.9 12.7 12.6 12.4	7·7 7·9 8.2 8.4	13.9 13.7 13.6 13.4 13.3	8.2 8.5 8.7 8.9		9.0 9.3 9.5	14.9	9.5 9.8 10.1	16.3 16.1 15.9 15.8	9.5 9.8 10.1 10.3 10.6	59 58 57 56
35 36 37 38 39	9.7 9.6 9.5 9.3	6.9 7.1 7.2 7.4 7.6	10.6 10.5 10.4 10.2 10.1	7.5 7.6 7.8 8.0 8.2	11.5 11.3 11.2 11.0 10.9	8.0 8.2 8.4 8.6 8.8	12.3 12.1 12.0 11.8 11.7	8.8 9.0 9.2 9.4	12.6 12.4	9.4 9.6 9.9 10.1	13.6 13.4 13.2	10.5	14.6 14.4 14.2 14.0	10.6		10.9 11.2 11.4 11.7 12.0	55 54 53 52 51
40 41 42 43 44	9.1 8.9 8.8 8.6	8.2	9.8 9.7 9.5 9.4	8.5 8.7 8.9	10.6 10.4 10.2 10.1	9.2 9.4 9.5 9.7	11.1	9.8 10.0 10.2 10.4	12.1 11.9 11.7 11.5	10.5 10.7 10.9 11.1	12.8 12.6 12.4 12.2	11.4 11.6 11.8	13.6 13.4 13.2 12.9	11.8 12.0 12.3 12.5	14.6 14.3 14.1 13.9 13.7	12.7 13.0 13.2	47 46
45	DEP. I	_	<u> </u>	_		9.9 									13.4 === DEP.		45
Course.	D = 1	_	Der.	_	_	14'		15'		16'	DEP.		DEP.		DEP.		Course.

						Pla	ne 7	Γrav	erse	Та	able						
Course.	D =	20′	D=	21'	D =	22'	D =	23'	D =	24′	D =	25′	D =	26′	D =	27′	Course.
Col	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	Cor
°0 1 2 3 4	20.0 20.0 20.0 20.0 20.0	0.3 0.7 1.0 1.4	21.0 21.0 21.0 21.0 20.9	0.4 0.7 1.1	, 22.0 22.0 22.0 22.0 21.9	0.4	23.0 23.0 23.0 23.0 23.0	0.4 0.8 1.2	24.0 24.0 24.0 24.0 23.9	0.4 0.8 1.3	25.0 25.0 25.0 25.0 25.0 24.9	0.4 0.9 1.3	26.0 26.0 26.0 26.0 25.9	0.5 0.9 1.4	27.0 27.0 27.0 27.0 27.0 26.9	, 0.0 0.5 0.9 1.4 1.9	90 89 88 87 86
5 6 7 8 9	19.9 19.9 19.8 19.8	2.1 2.4 2.8 3.1	20.9 20.9 20.8 20.8 20.7	2.2 2.6 2.9 3·3	21.9 21.9 21.8 21.8 21.7	2.3 2.7 3.1 3.4	22.9 22.8 22.8 22.7	2.4 2.8 3.2 3.6	23.9 23.9 23.8 23.8 23.7 23.6	2.5 2.9 3.3 3.8	24.9 24.8 24.8 24.7 24.6	2.6 3.0 3.5 3.9	25.9 25.9 25.8 25.7 25.7 25.6	2.7 3.2 3.6 4.1	26.9 26.8 26.7 26.7 26.7	2.4 2.8 3.3 3.8 4.2	85 84 83 82 81
11 12 13 14	19.6 19.6 19.5 19.4	3.8 4.2 4.5 4.8	20.6 20.5 20.5 20.4 20.3	4.0 4.4 4.7 5.1	21.6 21.5 21.4 21.3	4.2 4.6 4.9 5.3	22.6 22.5 22.4 22.3	1.4 4.8 5.2 5.6 6.0	23.6 23.5 23.4 23.3 23.2	4.6 5.0 5.4 5.8 6.2	24.5 24.5 24.4 24.3 24.1	4.8 5.2 5.6 6.0	25.5 25.4 25.3 25.2 25.1	5.0 5.4 5.8 6.3 6.7	26.5 26.4 26.3 26.2 26.1	5.2 5.6 6.1 6.5	79 78 77 76 75
16 17 18 19	19.2 19.1 19.0 18.9	5.5 5.8 6.2 6.5 6.8	20.2 20.1 20.0 19.9	5.8 6.1 6.5 6.8	21.1 21.0 20.9 20.8	6.1 6.4 6.8 7.2 7.5	22.1 22.0 21.9 21.7 21.6	6.7 7.1 7.5 7.9	23.1 23.0 22.8 22.7 22.6	7.0 7.4 7.8 8.2	24.0 23.9 23.8 23.6 23.5	7·3 7·7 8.1 8.6	25.0 24.9 24.7 24.6	7.6 8.0 8.5 8.9	26.0 25.8 25.7 25.5 25.4	7·4 7·9 8.3 8.8 9.2	74 73 72 71 70
21 22 23 24 25	18.7 18.5 18.4 18.3	7·5 7·8 8.1	19.6 19.5 19.3 19.2	8.2 8.5	20.5 20.4 20.3 20.1	8.2 8.6 8.9	21.5 21.3 21.2 21.0	8.6 9.0 9.4	22.4 22.3 22.1 21.9	9.0 9.4 9.8	1	9.4 9.8 10.2	23.8	9.7 10.2 10.6	25.2 25.0 24.9 24.7 24.5	10.1	
26 27 28 29	18.0 17.8 17.7 17.5	8.8 9.1 9.4 9.7	18.9 18.7 18.5 18.4	9.2 9.5 9.9 10.2	19.8 19.6 19.4 19.2	9.6 10.0 10.3 10.7	20.7 20.5 20.3 20.1	10.1 10.4 10.8 11.2	21.6 21.4 21.2 21.0	10.5 10.9 11.3 11.6	22.5 22.3 22.1 21.9	11.0	23.4 23.2 23.0 22.7	11.4 11.8 12.2 12.6	24.3 24.1 23.8 23.6	11.8 12.3 12.7 13.1	64 63 62 61
30 31 32 33 34	17.3 17.1 17.0 16.8 16.6	10.3 10.6 10.9 11.2	17.8 17.6 17.4	10.8	18.9 18.7 18.5 18.2	11.3 11.7 12.0 12.3	19.7 19.5 19.3 19.1	11.8 12.2 12.5 12.9	20.6 20.4 20.1 19.9	12.4 12.7 13.1 13.4	21.4 21.2 21.0 20.7	12.9 13.2 13.6 14.0	22.3 22.0 21.8 21.6	13.4 13.8 14.2 14.5	23.1 22.9 22.6 22.4	14.7	59 58 57 56
35 36 37 38 39	15.8 15.5	11.8 12.0 12.3 12.6		12.3 12.6 12.9 13.2	17.8 17.6 17.3 17.1	12.9 13.2 13.5 13.8	18.6 18.4 18.1 17.9	13.5 13.8 14.2 14.5	19.4 19.2 18.9 18.7	14.1 14.4 14.8 15.1	20.2 20.0 19.7 19.4	14.7 15.0 15.4 15.7	21.0 20.8 20.5 20.2	15.3 15.6 16.0 16.4	21.8 21.6 21.3 21.0	16.2 16.6 17.0	54 53 52 51
42 43 44	14.6 14.4	13.4 13.6 13.9	15.6 15.4 15.1	13.5 13.8 14.1 14.3 14.6	16.3 16.1 15.8	14.7	17.1 16.8 16.5	15.4	17.8 17.6 17.3	16.4	18.3	17.0	19.3	17.4	19.7	18.4	40
45	-				-		DEP.	_		-	-		<u> </u>	-	_		
Course.	D_{EP} , LAT. D_{EP} , LAT. D_{EP}					= 22'	_	=23'		=24'		=25′	\vdash	= 26′		=27′	Course.

						Pla	ne '	Tra	vers	e T	able					*	
Course.	D =	=28 ′	D=	29′	D =	30′	D=	=31 ′	D=	=32 ′	D=	=33′	D=	=34′	D=	=35′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ										
°0 1 2 3 4	28.0 28.0 28.0 28.0 28.0	0.5 1.0 1.5	29.0 29.0 29.0 29.0 29.0	0.5 1.0 1.5	30.0 30.0 30.0 30.0 29.9	0.5	31.0 31.0 31.0 31.0 30.9	0.5 1.1 1.6	32.0 32.0 32.0 32.0 31.9	0.6 1.1 1.7	33.0 33.0 33.0 33.0 32.9	0.6		0.6 1.2 1.8	0.0	0.0 0.6 1.2 1.8	90 89 88 87 86
5 6 7 8 9	27.9 27.8 27.8 27.7 27.7	2.9 3.4 3.9	28.9 28.8 28.8 28.7 28.6	3.0 3.5 4.0	29.9 29.8 29.8 29.7 29.6	3. I 3. 7	30.7	3.2 3.8 4.3	31.9 31.8 31.8 31.7 31.6	3·3 3·9 4·5	32.9 32.8 32.8 32.7 32.6	2.9 3.4 4.0 4.6 5.2	33.9 33.8 33.7 33.7 33.6	3.6	34·7 34·7	3.1 3.7 4.3 4.9 5.5	85 84 83 82 81
10 11 12 13 14	27.6 27.5 27.4 27.3 27.2	4.9 5.3 5.8 6.3	28.6 28.5 28.4 28.3 28.1	5.0 5.5 6.0 6.5	29.5 29.4 29.3 29.2 29.1	5·7 6.2	30.3 30.2	5.9 6.4	31.5 31.4 31.3 31.2 31.0	6.1 6.7	32.5 32.4 32.3 32.2 32.0	5.7 6.3 6.9 7.4 8.0		6.5 7.1 7.6	34·5 34·4 34·2 34·1 34·0	6.1 6.7 7.3 7.9 8.5	80 79 78 77 76
15 16 17 18 19	27.0 26.9 26.8 26.6 26.5	7·7 8.2 8.7	28.0 27.9 27.7 27.6 27.4	8.0 8.5 9.0	29.0 28.8 28.7 28.5 28.4	8.3 8.8 9.3	29.9 29.8 29.6 29.5 29.3	8.5 9.1	30.9 30.8 30.6 30.4 30.3	9.4 9.9	31.9 31.7 31.6 31.4 31.2	9.6	32.3		33.8 33.6 33.5 33.3 33.1	9.6	75 74 73 72 71
20 21 22 23 24	26.0 25.8	10.0	27.1 26.9 26.7	10.4	28.0 27.8 27.6	10.8	28.9 28.7 28.5	11.1 11.6 12.1	29.9 29.7 29.5	11.5 12.0 12.5		11.8 12.4 12.9	31.7 31.5 31.3	12.2 12.7 13.3	32.9 32.7 32.5 32.2 32.0	12.5 13.1 13.7	69 68
25 26 27 28 29	25.2	12.3 12.7 13.1	26.1 25.8 25.6	12.7 13.2 13.6	27.0 26.7 26.5	13.2 13.6 14.1	27.9 27.6 27.4	13.6 14.1 14.6	28.8 28.5 28.3	14.0 14.5 15.0	29.7 29.4	14.5 15.0 15.5	30.6 30.3 30.0	14.9	31.2 30.9	15.3	65 64 63 62 61
30 31 32 33 34	23.7 23.5	14.4 14.8 15.2	24.9 24.6 24.3	14.9 15.4 15.8	25.7 25.4 25.2	15.5 15.9 16.3	26.6 26.3 26.0	16.4	27.4 27.1 26.8	16.5 17.0 17.4	28.6 28.3 28.0 27.7 27.4	17.0 17.5 18.0	29.1 28.8 28.5	18.0	30.3 30.0 29.7 29.4 29.0	18.5	60 59 58 57 56
35 36 37 38 39	22.7 22.4 22.1 21.8	16.5 16.9 17.2 17.6	23.5 23.2 22.9 22.5	17.0 17.5 17.9 18.3	24.3 24.0 23.6 23.3	17.6 18.1 18.5 18.9	25.1 24.8 24.4 24.1	18.2 18.7 19.1 19.5	25.9 25.6 25.2 24.9	18.8 19.3 19.7 20.1	26.7 26.4 26.0 25.6	19.4 19.9 20.3 20.8	27.5 27.2 26.8 26.4	20.0 20.5 20.9 21.4	1	20.6 21.1 21.5 22.0	55 54 53 52 51
40 41 42 43 44	20.5 20.1	18.4 18.7 19.1 19.5	21.6 21.2 20.9	19.0 19.4 19.8 20.1	22.6 22.3 21.9 21.6	19.7 20.1 20.5 20.8	23.4 23.0 22.7 22.3	20.3 20.7 21.1 21.5	24.2 23.8 23.4 23.0	21.4 21.8 22.2	24.9 24.5 24.1 23.7	21.6 22.1 22.5 22.9	25.7 25.3 24.9 24.5	22.3 22.8 23.2 23.6	26.4 26.0 25.6 25.2	23.0	50 49 48 47 46
45	_							_					24.0			24.7	45
Course.	DEP.	LAT. 28'	DEP.		DEP.		DEP.	31'	DEP.	-	DEP.	33'	DEP.		DEP.	35'	Course.

						Pla	ne 7	Γrav	erse	e Ta	able						
Course.	D=	-36′	D=	-37'	D =	38′	D =	=39′	D=	40′	D=	-41′	D =	42'	D=	43'	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	S
°0 1 2 3 4	36.0 36.0 36.0 36.0 35.9	0.6	36.9	0.0 0.6 1.3 1.9 2.6	38.0 38.0 38.0 37.9 37.9	0.7 1.3 2.0 2.7	39.0 39.0 39.0 38.9 38.9	0.7 1.4	40.0 40.0 40.0 39.9 39.9	0.7 1.4 2.1	41.0 41.0 41.0 40.9 40.9	0.7 1.4 2.1 2.9	42.0 42.0 42.0 41.9 41.9	0.7 1.5 2.2	43.0 43.0 43.0 42.9 42.9	0.0 0.8 1.5 2.3 3.0	90 89 88 87 86
56 78 9	35.9 35.8 35.7 35.6 35.6		36.9 36.8 36.7 36.6 36.5	4·5 5.1 5.8	37.9 37.8 37.7 37.6 37.5	4.6 5.3	38.9 38.8 38.7 38.6 38.5	4.8 5.4	39.8 39.7 39.6 39.5	4.2 4.9 5.6	40.8 40.8 40.7 40.6 40.5	5.0 5.7	41.8 41.7 41.6 41.5	4.4 5.1 5.8	42.8 42.8 42.7 42.6 42.5	3.7 4.5 5.2 6.0 6.7	85 84 83 82 81
10 11 12 13 14	35.5 35.3 35.2 35.1 34.9	7.5	36.3	6.4 7.1 7.7 8.3 9.0	37.2 37.0 36.9	7·3 7·9 8·5 9·2	38.4 38.3 38.1 38.0 37.8	6.8 7.4 8.1 8.8 9.4	39.0 38.8	7.6 8.3 9.0 9.7		7.8 8.5 9.2 9.9		8.0 8.7 9.4 10.2		7.5 8.2 8.9 9.7 10.4	80 79 78 77 76
15 16 17 18 19	34.8 34.6 34.4 34.2 34.0	9.3 9.9 10.5 11.1	35.6 35.4		36.7 36.5 36.3 36.1 35.9	10.5	37·3 37·1		38.5 38.3 38.0	11.7		12.0	40.4 40.2 39.9	11.6	41.3 41.1 40.9		75 74 73 72 71
20 21 22 23 24	33.8 33.6 33.4 33.1 32.9	13.5	34.5	13.9	35.7 35.5 35.2 35.0 34.7	13.6 14.2 14.8 15.5	35.6	14.6 15.2 15.9	37·3 37·1 36.8 36.5	14.3 15.0 15.6 16.3	38.0 37.7 37.5	15.4 16.0 16.7	39.2 38.9 38.7 38.4	15.7 16.4 17.1	40.1 39.9 39.6 39.3	16.1 16.8 17.5	
25 26 27 28 29	32.6 32.4 32.1 31.8 31.5	15.2 15.8 16.3 16.9	33.5 33.3 33.0 32.7 32.4	15.6 16.2 16.8 17.4 17.9	33.9	16.1 16.7 17.3 17.8 18.4		17.1	36.0 35.6 35.3	17.5 18.2 18.8	36.9 36.5	18.6 19.2	37·7 37·4 37·1	18.4 19.1 19.7	39.0 38.6 38.3 38.0 37.6	18.8 19.5 20.2	65 64 63 62 61
30 31 32 33 34	31.2 30.9 30.5 30.2 29.8	18.5	31.7 31.4 31.0	19.1	32.2	19.6 20.1 20.7	33.8 33.4 33.1 32.7 32.3	20.7	34.6 34.3 33.9 33.5 33.2	20.6	35.5 35.1 34.8 34.4 34.0	21.1 21.7 22.3	36.4 36.0 35.6 35.2 34.8	21.6 22.3 22.9	37.2 36.9 36.5 36.1 35.6	22.8	60 59 58 57 56
35 36 37 38 39	29.5 29.1 28.8 28.4 28.0	21.2 21.7 22.2 22.7	29.9 29.5 29.2 28.8	21.7 22.3 22.8 23.3	30.7 30.3 29.9 29.5	22.3 22.9 23.4 23.9	31.6 31.1 30.7 30.3	22.9 23.5 24.0 24.5	31.9 31.5 31.1	23.5 24.1 24.6 25.2	33.2 32.7 32.3 31.9	24.1 24.7 25.2 25.8	34.0 33.5 33.1 32.6	24.7 25.3 25.9 26.4	35·2 34·8 34·3 33·9 33·4	25.3 25.9 26.5 27.1	55 54 53 52 51
41 42 43 44	27.6 27.2 26.8 26.3 25.9	23.6 24.1 24.6 25.0	27.9 27.5 27.1 26.6	24.3 24.8 25.2 25.7	28.7 28.2 27.8 27.3	24.9 25.4 25.9 26.4	29.4 29.0 28.5 28.1	25.6 26.1 26.6 27.1	30.2 29.7 29.3 28.8	26.2 26.8 27.3 27.8	30.9 30.5 30.0 29.5	26.9 27.4 28.0 28.5	31.7 31.2 30.7 30.2	27.6 28.1 28.6 29.2	32.5 32.0 31.4 30.9	28.2 28.8 29.3 29.9	48 47 46
45	25.5	25.5	_	26.2			27.6					29.0			30.4 DER	30.4 LAT.	45
Course.	-	= 36'	_	=37'	-	= 38'		= 39'	DEP.	=40'	-	LAT. =41'		=42'		=43'	Course.

					Pla	ne '	Trav	rers	e Ta	able						
Course.	D=44'	D = 0	45′	D =	₌46′	D=	=47 ′	D=	=48 ′	D=	=49′	D =	50′	D=	=51 ′	Course.
රී	LAT. DEP	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3 4	44.0 0.8 44.0 1.9 43.9 2.3 43.9 3.1	45.0 45.0 45.0 45.0 44.9 44.9	0,8 1.6 2.4	46.0 46.0 46.0 45.9 45.9	0.8 1.6 2.4 3.2	47.0 47.0 47.0 46.9 46.9	0.8 1.6 2.5	48.0 48.0 48.0 47.9 47.9	0.8 1.7 2.5 3.3	49.0 49.0 49.0 48.9 48.9	0.9	50.0 50.0 50.0 49.9 49.9	0.9	51.0 51.0 51.0 50.9 50.9	0.0 0.9 1.8 2.7 3.6	90 89 88 87 86
56 78 9	43.7 43.6 6.1 43.5 6.9	44.8 44.7 44.6 44.4	5·5 6·3 7·°	45.8 45.7 45.7 45.6 45.4	4.8 5.6 6.4 7.2	46.8 46.7 46.6 46.5 46.4	4·9 5·7 6.5 7·4	47.8 47.7 47.6 47.5 47.4	5.0 5.8 6.7 7.5	48.8 48.7 48.6 48.5 48.4	6.0 6.8 7·7	49.8 49.7 49.6 49.5 49.4	5.2 6.1 7.0 7.8	50.8 50.7 50.6 50.5 50.4	4.4 5.3 6.2 7.1 8.0	85 84 83 82 81
10 11 12 13 14	43.2 8.4 43.0 9.1 42.9 9.9 42.7 10.6	43.8	9·4 10.1 10.9	45.3 45.2 45.0 44.8 44.6	8.8 9.6 10.3 11.1	46.3 46.1 46.0 45.8 45.6	9.0 9.8 10.6 11.4	46.8 46.6	9.2 10.0 10.8 11.6	47·7 47·5	9.3 10.2 11.0	48.7 48.5	9.5 10.4 11.2 12.1		11.5	80 79 78 77 76
15 16 17 18 19	42.3 12.1 42.1 12.0 41.8 13.6 41.6 14.3	43.3 43.0 42.8 42.5	12.4 13.2 13.9 14.7	44.0 43.7 43.5	14.2	45.2 44.9 44.7 44.4	13.0 13.7 14.5 15.3	45·7 45·4	13.2 14.0 14.8 15.6	47.1 46.9 46.6 46.3	14.3 15.1 16.0	48.1 47.8 47.6 47.3	13.8 14.6 15.5 16.3	49.0 48.8 48.5 48.2	14.9 15.8 16.6	74 73 72 71
20 21 22 23 24	41.1 15.8 40.8 16.9 40.5 17.2 40.2 17.9	42.0 41.7 41.4 41.1	16.1 16.9 17.6 18.3	42.9 42.7 42.3 42.0	15.7 16.5 17.2 18.0	43.9 43.6 43.3 42.9	16.8 17.6 18.4 19.1	44.8 44.5 44.2 43.9	17.2 18.0 18.8 19.5	45.7 45.4 45.1 44.8	17.6 18.4 19.1 19.9	46.7 46.4 46.0 45.7	17.9 18.7 19.5 20.3	47.9 47.6 47.3 46.9 46.6	18.3 19.1 19.9 20.7	70 69 68 67 66
25 26 27 28 29	39.5 19.5 39.2 20.6 38.8 20.7 38.5 21.5	40.4 40.1 39.7 39.4	19.7 20.4 21.1 21.8	41.7 41.3 41.0 40.6 40.2	20.2 20.9 21.6 22.3	41.9 41.5 41.1	20.6 21.3 22.1 22.8	43.1 42.8 42.4 42.0	21.0 21.8 22.5 23.3	44.0 43.7 43.3 42.9	21.5	44.9 44.6 44.1	21.9 22.7 23.5	46.2 45.8 45.4 45.0 44.6	22.4	65 64 63 62 61
30 31 32 33 34	37.7 22.7 37.3 23.3 36.9 24.6 36.5 24.6	38.6 38.2 37.7 37.3	23.8 24.5 25.2	39.8 39.4 39.0 38.6 38.1	24.4 25.1 25.7	40.3 39.9 39.4 39.0	24.2 24.9 25.6 26.3	40.7 40.3 39.8	24.7 25.4 26.1 26.8	42.0 41.6 41.1 40.6	25.2 26.0 26.7 27.4	42.4 41.9 41.5	25.8 26.5 27.2 28.0	43·3 42.8 42·3	25.5 26.3 27.0 27.8 28.5	59 58 57 56
35 36 37 38 39	35.6 25.9 35.1 26.9 34.7 27.1 34.2 27.7	36.4 35.9 35.5 35.0	28.3	35.7	26.4 27.0 27.7 28.3 28.9	38.0 37.5 37.0 36.5	27.6 28.3 28.9 29.6	38.8 38.3 37.8 37.3	28.2 28.9 29.6 30.2	39.6 39.1 38.6 38.1	28.8 29.5 30.2 30.8	40.5 39.9 39.4 38.9	29.4 30.1 30.8 31.5		30.0 30.7 31.4 32.1	53 52 51
42 43 44	32.2 30.0 31.7 30.0	34.0 33.4 32.9 32.4	29.5 30.1 30.7	34.7 34.2 33.6 33.1	30.2 30.8 31.4 32.0	35·5 34·9 34·4 33.8	30.8 31.4 32.1 32.6	36.2 35.7 35.1 34.5	31.5 32.1 32.7 33.3	37.0 36.4 35.8 35.2	32.1 32.8 33.4 34.0	37.7 37.2 36.6 36.0	32.8 33.5 34.1 34.7	38.5 37.9 37.3 36.7	33.5 34.1 34.8 35.4	49 48 47 46
45	31.1 31.1 DEP. LAT		_	32.5 DEP.	132.5 LAT.	33.2	33.2 LAT.		33.9	34.6	34.6 ————————————————————————————————————			36.1 ————————————————————————————————————	36.1	45
Course.	D = 44'			_	46′		=47'	D =			49'	D =	-	D = D		Course

						Pla	ne î	Γrav	erse	e Ta	able						
Course.	D=	=52′	D =	⁼53′	D =	54′	D =	=55 ′	D =	56′	D =	· 57′	D =	=58′	D =	59′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	52.0 52.0 52.0 51.9 51.9		50	0.0 0.9 1.8 2.8 3.7	54.0 54.0 54.0 53.9 53.9		55.0 55.0 55.0 54.9 54.9	1.0 1.9 2.9	56.0 56.0 56.0 55.9 55.9	, 0.0 1.0 2.0 2.9 3.9	57.0 57.0 56.9 56.9	1.0 2.0 3.0	58.0 58.0 58.0 57.9 57.9	1.0 2.0 3.0 4.0	59.0 59.0 59.0 58.9 58.9	, 0.0 1.0 2.1 3.1 4.1	90 89 88 87 86
56 78 9	51.8 51.7 51.6 51.5 51.4	8.1	52.7 52.6 52.5 52.3	4.6 5.5 6.5 7.4 8.3	53.8 53.7 53.6 53.5 53.3	8.4	54.8 54.7 54.6 54.5 54.3	5·7 6.7 7·7 8.6	55.8 55.7 55.6 55.5 55.3	8.8	56.7 56.6 56.4 56.3	6.0 6.9 7.9 8.9	57.8 57.7 57.6 57.4 57.3	6.1 7.1 8.1 9.1		5.1 6.2 7.2 8.2 9.2	85 84 83 82 81
10 11 12 13 14	51.2 51.0 50.9 50.7 50.5	9.9 10.8 11.7	52.2 52.0 51.8 51.6 51.4	9.2 10.1 11.0 11.9 12.8	53.2 53.0 52.8 52.6 52.4	9.4 10.3 11.2 12.1 13.1	54.2 54.0 53.8 53.6 53.4	10.5		11.6	56.0 55.8 55.5 55.3	10.9 11.9 12.8 13.8	57.1 56.9 56.7 56.5 56.3	11.1 12.1 13.0 14.0		12.3 13.3 14.3	80 79 78 77 76
16 17 18 19	50.0 49.7 49.5 49.2	14.3 15.2 16.1 16.9	50.9 50.7 50.4 50.1	14.6	51.9 51.6 51.4 51.1	14.9	52.9 52.6 52.3 52.0	15.2 16.1 17.0 17.9	53.8 53.6 53.3 52.9 52.6	15.4 16.4 17.3 18.2	54.8 54.5	15.7 16.7 17.6 18.6	55.8 55.5 55.2 54.8	16.0 17.0 17.9 18.9	56.7 56.4 56.1 55.8	16.3 17.2 18.2 19.2	73 74 73 72 71
21 22 23 24 25	48.5 48.2 47.9 47.5	18.6 19.5 20.3 21.2	49.5 49.1 48.8 48.4 48.0	19.0 19.9 20.7 21.6	50.4	19.4 20.2 21.1 22.0	51.3 51.0 50.6 50.2	19.7 20.6 21.5 22.4	52.3 51.9 51.5 51.2 50.8	20.1 21.0 21.9 22.8	53.2 52.8 52.5 52.1	20.4 21.4 22.3 23.2	54.1 53.8 53.4 53.0	20.8 21.7 22.7 23.6	55. I 54.7 54.3 53.9	21.1 22.1 23.1 24.0	69 68
26 27 28 29	46.7 46.3 45.9 45.5	22.8	47.6 47.2 46.8 46.4	23.2 24.1 24.9 25.7	48.5 48.1 47.7 47.2	23.7 24.5 25.4 26.2	49.4 49.0 48.6 48.1	24.1 25.0 25.8 26.7	50.3 49.9 49.4 49.0	24.5 25.4 26.3 27.1	51.2 50.8 50.3 49.9	25.0 25.9 26.8 27.6	52.1 51.7 51.2 50.7	25.4 26.3 27.2 28.1	53.0 52.6 52.1 51.6	25.9 26.8	64 63 62 61
30 31 32 33 34	45.0 44.6 44.1 43.6 43.1	26.8 27.6 28.3 29.1	45.4 44.9 44.4 43.9	28.1 28.9 29.6	46.3 45.8 45.3 44.8	27.8 28.6 29.4 30.2	46.6 46.1 45.6	28.3 29.1 30.0 30.8	47.5 47.0 46.4	28.8 29.7 30.5 31.3	48.9 48.3 47.8 47.3	29.4 30.2 31.0 31.9	49.7 49.2 48.6 48.1	29.9 30.7 31.6 32.4	51.1 50.6 50.0 49.5 48.9	30.4 31.3 32.1 33.0	59 58 57 56
35 36 37 38 39	42.6 42.1 41.5 41.0 40.4	32.0 32.7	43.4 42.9 42.3 41.8 41.2	31.2 31.9 32.6 33.4	43.1 42.6 42.0	31.7 32.5 33.2 34.0	44.5 43.9 43.3 42.7	33.1 33.9 34.6	45·3 44·7 44·1 43·5	32.9 33.7 34.5 35.2	46.7 46.1 45.5 44.9 44.3	33.5 34.3 35.1 35.9	47.5 46.9 46.3 45.7 45.1	34.1 34.9 35.7 36.5		35.5 36.3 37.1	55 54 53 52 51
40 41 42 43 44	39.2 38.6 38.0	34.1 34.8 35.5 36.1	40.0 39.4 38.8 38.1	34.8 35.5 36.1 36.8	40.8 40.1 39.5 38.8	35.4 36.1 36.8 37.5	41.5 40.9 40.2 39.6	36.1 36.8 37.5 38.2	42.3 41.6 41.0 40.3	36.7 37.5 38.2 38.9	43.7 43.0 42.4 41.7 41.0	37.4 38.1 38.9 39.6	43.8 43.1 42.4 41.7	38.1 38.8 39.6 40.3	44.5 43.8 43.1 42.4	38.7 39.5 40.2	48 47 46
45			37.5	_							40.3		41.0		41.7 Dep		45
Course.	-	EAT.	_	E 53'	DEP.	E 54'	_	55'		EAT.	DEP.	_	_	=58'	DEP.		Course.

						Pla	ne	Tra	vers	e T	able						
Course.	D=	=60′	D=	=61 <i>′</i>	D=	=62′	D=	=63′	D=	=64′	D=	=65′	D =	=66′	D=	=67 ′	Course.
රි	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	Lat.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3 4	60.0 60.0 60.0 59.9 59.9	0.0 1.0 2.1 3.1 4.2	61.0 61.0 61.0 60.9 60.9		62.0 62.0 62.0 61.9 61.8			1. I 2. 2	64.0 63.9	1.1 2.2 3.3	65.0 65.0 65.0 64.9 64.8	0.0 1.1 2.3 3.4 4.5	66.0 66.0 65.9	1.2 2.3 3.5	67.0 67.0 67.0 66.9 66.8	0.0 1.2 2.3 3.5 4.7	90 89 88 87 86
56 78 9	59.8 59.7 59.6 59.4 59.3	5.2 6.3 7.3 8.4 9.4	60.7 60.5 60.4 60.2	5·3 6.4 7·4 8.5 9·5	61.4	6.5 7.6 8.6 9.7	62.2	7.7 8.8 9.9	63.6 63.5 63.4 63.2	6.7 7.8 8.9 10.0	64.8 64.6 64.5 64.4 64.2	9.0	65.6 65.5 65.4 65.2	9.2	66.6 66.5 66.3 66.2	_	82 81
10 11 12 13 14	59.1 58.9 58.7 58.5 58.2	12.5 13.5 14.5	59.7 59.4 59.2	12.7 13.7 14.8	60.9 60.6 60.4 60.2	12.9 13.9 15.0	61.8 61.6 61.4 61.1	12.0 13.1 14.2 15.2	63.0 62.8 62.6 62.4 62.1	12.2 13.3 14.4 15.5	63.8 63.6 63.3 63.1	12.4 13.5 14.6 15.7	64.8 64.6 64.3 64.0	12.6 13.7 14.8 16.0	65.3 65.0	11.6 12.8 13.9 15.1 16.2	80 79 78 77 76
15 16 17 18 19	57·7 57·4 57·1 56·7	7.7 16.5 58.6 16. 7.4 17.5 58.3 17. 7.1 18.5 58.0 18. 6.7 19.5 57.7 19. 6.4 20.5 57.3 20. 6.0 21.5 56.9 21. 6.6 22.5 56.6 22.		16.8 17.8 18.9 19.9	59.6 59.3 59.0 58.6	17.1 18.1 19.2 20.2	60.6 60.2 59.9 59.6	17.4 18.4 19.5 20.5		17.6 18.7 19.8 20.8	62.5 62.2 61.8 61.5	17.9 19.0 20.1 21.2	63.4 63.1 62.8 62.4	18.2 19.3 20.4 21.5	64.4 64.1 63.7 63.3	17.3 18.5 19.6 20.7 21.8	75 74 73 72 71
20 21 22 23 24	56.4 56.0 55.6 55.2 54.8	21.5 22.5 23.4 24.4	56.9 56.6 56.2 55.7	22.9 23.8 24.8	57·9 57·5 57·1 56.6	24.2 25.2	58.8 58.4 58.0 57.6	22.6 23.6 24.6 25.6	59.7 59.3 58.9 58.5	22.9 24.0 25.0 26.0	59.8 59.4	23.3 24.3 25.4 26.4	61.6 61.2 60.8 60.3	23.7 24.7 25.8 26.8	62.5 62.1 61.7 61.2	22.9 24.0 25.1 26.2 27.3	70 69 68 67 66
25 26 27 28 29	54.4 53.9 53.5 53.0 52.5	26.3 27.2 28.2 29.1	54·4 53·9 53·4	29.6	55.7 55.2 54.7 54.2	26.2 27.2 28.1 29.1 30.1	56.6 56.1 55.6 55.1	29.6 30.5	57.5 57.0 56.5 56.0	28.1 29.1 30.0 31.0	57·4 56.9	28.5 29.5 30.5 31.5	59·3 58.8 58·3 57·7	28.9 30.0 31.0 32.0	59.7 59.2 58.6	28.3 29.4 30.4 31.5 32.5	65 64 63 62 61
30 31 32 33 34	52.0 51.4 50.9 50.3 49.7	33.6	52.3 51.7 51.2 50.6	34.1	53. I 52. 6 52. 0 51. 4	31.9 32.9 33.8 34.7	54.0 53.4 52.8 52.2	32.4 33.4 34.3 35.2	54·9 54·3 53·7 53·1	33.9 34.9 35.8	56.3 55.7 55.1 54.5 53.9	33·5 34·4 35·4 36·3	56.6 56.0 55.4 54.7	34.0 35.0 35.9 36.9	56.2 55.5	33.5 34.5 35.5 36.5 37.5	59 58 57 56
35 36 37 38 39	49.1 48.5 47.9 47.3 46.6	35·3 36.1 36.9 37.8	49.4 48.7 48.1 47.4	36.7 37.6 38.4	50.2 49.5 48.9 48.2	37·3 38.2 39.0	51.0 50.3 49.6 49.0	37.9 38.8 39.6	51.8 51.1 50.4 49.7	38.5 39.4 40.3		39. I 40.0 40.9	53.4 52.7 52.0 51.3	38.8 39.7 40.6 41.5	53.5 52.8 52.1	38.4 39.4 40.3 41.2 42.2	55 54 53 52 51
40 41 42 43 44 45	45·3 44·6 43·9 43·2	39·4 40.1 40.9	45.3 44.6 43.9	40.0 40.8 41.6	46.8 46.1 45.3 44.6	40.7 41.5 42.3 43.1	47.5 46.8 46.1 45.3	41.3 42.2 43.0 43.8	49.0 48.3 47.6 46.8 46.0	42.0 42.8 43.6 44.5	49. I 48. 3 47. 5 46. 8	42.6 43.5 44.3 45.2	49.8 49.0 48.3 47.5	43·3 44·2 45·0 45.8	50.6 49.8 49.0 48.2	44.0 44.8 45.7 46.5	50 49 48 47 46
-		_					DEP.		DEP.		DEP.					LAT.	45
Course.		Dep. LAT. Dep. LAT D=60' D=61'				62′	D =		D =	_	D =	-	D =		D =	_	Course.

						Pla	ne ′	Trav	vers	e Ta	able						
Course.	D=	=68 <i>′</i>	D=	=6ġ′	D =	=70′	D=	71′	D=	72′	D =	73′	D =	74′	D =	75′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	68.0 68.0 68.0 67.9 67.8	0.0 1.2 2.4 3.6 4.7	69.0 69.0 69.0 68.9 68.8	1.2 2.4 3.6 4.8	70.0 70.0 70.0 69.9 69.8	1.2 2.4 3.7 4.9	70.9 70.8	1.2 2.5 3.7 5.0	71.8	1.3 2.5 3.8	73.0 73.0 73.0 73.0 72.9 72.8	1.3 2.5 3.8 5.1	74.0 74.0 74.0 74.0 73.9 73.8	1.3 2.6 3.9	75.0 75.0 75.0 74.9 74.8	0.0 1.3 2.6 3.9 5.2	90 89 88 87 86
5 6 7 8 9	67.7 67.6 67.5 67.3 67.2	8.3 9.5 10.6	68.6 68.5 68.3 68.2	7.2 8.4 9.6 10.8		8.5 9.7 11.0	70.6 70.5 70.3 70.1	8.7 9.9 11.1	71.6 71.5 71.3 71.1	7.5 8.8 10.0 11.3	72.7 72.6 72.5 72.3 72.1	7.6 8.9 10.2 11.4	73.1	7·7 9.0 10.3 11.6	74.7 74.6 74.4 74.3 74.1	6.5 7.8 9.1 10.4 11.7	85 84 83 82 81
11 12 13 14	66.8 66.5 66.3 66.0	6.5 14.1 67.5 14.6 15.3 67.2 15.6 16.5 67.0 16.5 67.0 16.5 66.6 17.6 66.3 19.5 19.9 66.0 20.		13.2 14.3 15.5 16.7	68.7 68.5 68.2 67.9	13.4 14.6 15.7 16.9	69.7 69.4 69.2 68.9	13.5 14.8 16.0 17.2	70.7 70.4 70.2 69.9	13.7 15.0 16.2 17.4	71.7 71.4 71.1 70.8	13.9 15.2 16.4 17.7	72.6 72.4 72.1 71.8	14.1 15.4 16.6 17.9	73.6 73.4 73.1 72.8	14.3 15.6 16.9 18.1	79 78 77 76
15 16 17 18	64.7	18.7 19.9 21.0 22.1	66.3 66.0 65.6 65.2	19.0 20.2 21.3 22.5	67.3 66.9 66.6 66.2	19.3 20.5 21.6 22.8	68.2 67.9 67.5 67.1	19.6 20.8 21.9 23.1	69.2 68.9 68.5 68.1	19.8 21.1 22.2 23.4	70.2 69.8 69.4 69.0	20.1 21.3 22.6 23.8	71.1 70.8 70.4 70.0	20.4 21.6 22.9 24.1	72. I 71.7 71.3 70.9	23.2	75 74 73 72 71
20 21 22 23 24	63.9 63.5 63.0 62.6 62.1	24.4 25.5 26.6 27.7	64.4 64.0 63.5 63.0	25.8 27.0 28.1	65.4 64.9 64.4 63.9	25.1 26.2 27.4 28.5	66.3 65.8 65.4 64.9	26.6 27.7 28.9	67.2 66.8 66.3 65.8	25.8 27.0 28.1 29.3	68.2 67.7 67.2 66.7	26.2 27.3 28.5 29.7	69. 1 68. 6 68. 1 67. 6	26.5 27.7 28.9 30.1		28. I 29. 3 30. 5	70 69 68 67 66
25 26 27 28 29	61.6 61.1 60.6 60.0 59.5	29.8 30.9	62.0 61.5 60.9	30.2 31.3 32.4 33.5	62.9 62.4 61.8 61.2	30.7 31.8 32.9 33.9	63.8 63.3 62.7 62.1	31.1 32.2 33.3 34.4	64.7 64.2 63.6 63.0	31.6 32.7 33.8 34.9	65.6 65.0 64.5 63.8	32.0 33.1 34.3 35.4	66. 5 65. 9 65. 3 64. 7	32.4 33.6 34.7 35.9	66.2 65.6	32.9 34.0 35.2 36.4	65 64 63 62 61
30 31 32 33 34	57.7	36.0 37.0	59. I 58. 5	35.5 36.6 37.6 38.6	59.4 58.7 58.0	36.1 37.1 38.1 39.1	60.9 60.2 59.5 58.9	36.6 37.6 38.7 39.7	61.7 61.1 60.4 59.7	37.1 38.2 39.2 40.3	62.6 61.9 61.2 60.5	37.6 38.7 39.8 40.8	63.4 62.8 62.1 61.3	38.1 39.2 40.3 41.4		38.6 39.7 40.8 41.9	60 59 58 57 56
35 36 37 38 39	54·3 53.6 52.8	40.0 40.9 41.9 42.8	55.8 55.1 54.4 53.6	40.6 41.5 42.5 43.4	56.6 55.9 55.2 54.4	41. I 42. I 43. I 44. I	57.4 56.7 55.9 55.2	41.7 42.7 43.7 44.7	58.2 57.5 56.7 56.0	42.3 43.3 44.3 45.3	59. I 58. 3 57. 5 56. 7	42.9 43.9 44.9 45.9	59.9 59.1 58.3 57.5	43.5 44.5 45.6 46.6	61.4 60.7 59.9 59.1 58.3	44.1 45.1 46.2 47.2	52 51
41 42 43 44	51.3 50.5 49.7 48.9	44.6 45.5 46.4 47.2	52.1 51.3 50.5 49.6	45.3 46.2 47.1 47.9	52.8 52.0 51.2 50.4	45.9 46.8 47.7 48.6	53.6 52.8 51.9 51.1	46.6 47.5 48.4 49.3	54·3 53·5 52·7 51.8	47.2 48.2 49.1 50.0	55.1 54.2 53.4 52.5	47.9 48.8 49.8 50.7	55.8 55.0 54.1 53.2	48.5 49.5 50.5 51.4	57.5 56.6 55.7 54.9 54.0	50.2 51.1	50 49 48 47 46 45
45		48.1									DEP.			LAT.	DEP.	_	
Course	-	EAT.	_	EAT.		TAT.	_	71'	-	72'		73′		=74'	D =		Course.

						Pla	ne '	Trav	vers	e Ta	able						
Course.	D=	=76′	D =	77′	D=	=78′	D=	=79′	D=	=8o′	D=	-81 ′	D =	=82′	D=	=83 ′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	76.0 76.0 76.0 75.9 75.8	1.3 2.7	77.0 76.9	1.3 2.7 4.0 5.4	78.0 78.0 78.0 78.0 77.9 77.8	2.7	79.0 79.0 79.0 78.9 78.8	0.0 1.4 2.8 4.1 5.5		1.4 2.8 4.2 5.6	81.0 81.0 81.0 80.9 80.8	1.4 2.8 4.2 5.7	82.0 82.0 82.0 81.9 81.8	1.4 2.9 4.3 5.7	82.9 82.9 82.8	0.0 1.4 2.9 4.3 5.8	°0 89 88 87 86
5 6 7 8 9	75.7 75.6 75.4 75.3 75.1	7·9 9·3 10.6 11.9	76.7 76.6 76.4 76.3 76.1	9·4 10.7 12.0	77.6 77.4 77.2 77.0	9.5 10.9 12.2	78.6 78.4 78.2 78.0	8.3 9.6 11.0 12.4		8.4 9.7 11.1 12.5	80.0	8.5 9.9 11.3 12.7	81.0	8.6 10.0 11.4 12.8	82.7 82.5 82.4 82.2 82.0	7.2 8.7 10.1 11.6 13.0	85 84 83 82 81
10 11 12 13 14	74.8 74.6 74.3 74.1 73.7	14.5 15.8 17.1 18.4	75.3 75.0 74.7	14.7 16.0 17.3 18.6	76.6 76.3 76.0 75.7	16.2 17.5 18.9	77.5 77.3 77.0 76.7	15.1 16.4 17.8 19.1	78.5 78.3 77.9 77.6	15.3 16.6 18.0 19.4	79·5 79·2 78·9 78·6	16.8 18.2 19.6	80.5 80.2 79.9 79.6	15.6 17.0 18.4 19.8	81.7 81.5 81.2 80.9 80.5	20.1	80 79 78 77 76
15 16 17 18 19	72.3 71.9	20.9 22.2 23.5 24.7	73.2 72.8	21.2 22.5 23.8 25.1	75.0 74.6 74.2 73.8	21.5 22.8 24.1 25.4	75.9 75.5 75.1 74.7	25.7	76.9 76.5 76.1 75.6	23.4 24.7 26.0	77.9 77.5 77.0 76.6	23.7 25.0 26.4	78.8 78.4 78.0 77.5	22.6 24.0 25.3 26.7	79.4 78.9 78.5	21.5 22.9 24.3 25.6 27.0	75 74 73 72 71
20 21 22 23 24	71.0 70.5 70.0 69.4	26.0 27.2 28.5 29.7 30.9	71.9 71.4 70.9 70.3	27.6 28.8 30.1 31.3	72.8 72.3 71.8 71.3	28.0 29.2 30.5 31.7	73.2 72.7 72.2	28.3 29.6 30.9 32.1		28.7 30.0 31.3 32.5	75.6 75.1 74.6 74.0	30.3 31.6 32.9	76.6 76.0 75.5 74.9	29.4 30.7 32.0 33.4		28.4 29.7 31.1 32.4 33.8	70 69 68 67 66
25 26 27 28 29	68.9 68.3 67.7 67.1 66.5	33·3 34·5 35·7 36.8	69.2 68.6 68.0 67.3	35.0 36.1 37.3	70.1 69.5 68.9 68.2	34.2 35.4 36.6 37.8	71.0 70.4 69.8 69.1	34.6 35.9 37.1 38.3	72.5 71.9 71.3 70.6 70.0	35.1 36.3 37.6 38.8	72.8 72.2 71.5 70.8	36.8 38.0 39.3	73.1 73.1 72.4 71.7	35.9 37.2 38.5 39.8	74.0 73.3	35.1 36.4 37.7 39.0 40.2	65 64 63 62 61
30 31 32 33 34	65.1 64.5 63.7 63.0	40.3 41.4 42.5	66.0 65.3 64.6 63.8	40.8 41.9 43.1	66.1 65.4 64.7	40.2 41.3 42.5 43.6	67.0 66.3 65.5	40.7 41.9 43.0 44.2	69.3 68.6 67.8 67.1 66.3	41.2 42.4 43.6 44.7	69.4 68.7 67.9 67.2	42.9 44.1 45.3	70.3 69.5 68.8 68.0	42.2 43.5 44.7 45.9	68.8	41.5 42.7 44.0 45.2 46.4	60 59 58 57 56
35 36 37 38 39	61.5 60.7 59.9 59.1	44.7 45.7 46.8 47.8	62.3 61.5 60.7 59.8	45·3 46.3 47·4 48.5	63.1 62.3 61.5 60.6	45.8 46.9 48.0 49.1	63.9 63.1 62.3 61.4	46.4 47.5 48.6 49.7	64.7 63.9 63.0 62.2	47.0 48.1 49.3 50.3	65.5 64.7 63.8 62.9	47.6 48.7 49.9 51.0	66.3 65.5 64.6 63.7	48.2 49.3 50.5 51.6	68.0 67.1 66.3 65.4 64.5	48.8 50.0 51.1 52.2	55 54 53 52 51
41 42 43 44	57·4 56·5 55·6 54·7	49.9 50.9 51.8 52.8	58.1 57.2 56.3 55.4	50.5 51.5 52.5 53.5	58.9 58.0 57.0 56.1	51.2 52.2 53.2 54.2	59.6 58.7 57.8 56.8	51.8 52.9 53.9 54.9	59.5 58.5 57.5	52.5 53.5 54.6 55.6	61.1 60.2 59.2 58.3	53.1 54.2 55.2 56.3	61.9 60.9 60.0 59.0	53.8 54.9 55.9 57.0	63.6 62.6 61.7 60.7 59.7	54·5 55·5 56.6 57·7	49 48 47 46
45	53.7			54.4	_				56.6	56.6	57.3		58.0			58.7	45
Course.	DEP.	EAT.	DEP.	TAT.		TAT.	_	TAT.		EAT.	_	81'	DEP.	_	$D_{\text{EP.}}$		Course.

						Pla	ne î	Trav	rers	e Ta	able		-				
Course.	D =	=84 ′	D =	85'	D =	86′	D =	87′	D=	-88 ′	D =	89′	D =	90'	D =	91'	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP,	La~.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	84.0 84.0 83.9 83.9 83.8	1.5 2.9	85.0 85.0 84.9 84.9 84.8	3.0 4.4	86.0 86.0 85.9 85.9 85.8	1.5	87.0 87.0 86.9 86.9 86.8	1.5 3.0 4.6	88.0 88.0 87.9 87.9 87.8	0.0 1.5 3.1 4.6 6.1	89.0 88.9 88.9	4.7		0.0 1.6 3.1 4.7 6.3	91.0 90.9 90.9	0.0 1.6 3.2 4.8 6.3	90 89 88 87 86
5 6 7 8 9	83.7 83.5 83.4 83.2 83.0	11.7	84.7 84.5 84.4 84.2 84.0	11.8	85.5 85.4 85.2 84.9	12.0	86.2 85.9	9.1 10.6 12.1 13.6	87.7 87.5 87.3 87.1 86.9	12.2	88.5 88.3 88.1 87.9	9.3 10.8 12.4 13.9	89.7 89.5 89.3 89.1 88.9	7.8 9.4 11.0 12.5 14.1	90.5 90.3 90.1 89.9	12.7	85 84 83 82 81
10 11 12 13 14	82.2 17.5 83.1 17 81.8 18.9 82.8 19 81.5 20.3 82.5 20 81.1 21.7 82.1 22 80.7 23.2 81.7 23 80.3 24.6 81.3 24 79.9 26.0 80.8 26				84.1 83.8 83.4	17.9 19.3 20.8	85.4 85.1 84.8 84.4	16.6 18.1 19.6 21.0	85.4	18.3 19.8 21.3	87.4 87.1 86.7 86.4	17.0 18.5 20.0 21.5	88.6 88.3 88.0 87.7 87.3	17.2 18.7 20.2 21.8	88.3	15.8 17.4 18.9 20.5 22.0	80 79 78 77 76
15 16 17 18 19	80.7 80.3 79.9 79.4	23.2 24.6 26.0 27.3	81.7 81.3 80.8 80.4	23.4 24.9 26.3 27.7	82.2 81.8 81.3	23.7 25.1 26.6 28.0	83.6 83.2 82.7 82.3	24.0 25.4 26.9 28.3		24.3 25.7 27.2 28.7	85.6 85.1 84.6 84.2	24.5 26.0 27.5 29.0	86.9 86.5 86.1 85.6 85.1	26.3 27.8 29.3	87.5 87.0 86.5 86.0	23.6 25.1 26.6 28.1 29.6	75 74 73 72 71
20 21 22 23 24	78.9 78.4 77.9 77.3 76.7	28.7 30.1 31.5 32.8 34.2	78.8 78.2	29.1 30.5 31.8 33.2 34.6	79.7	32.2 33.6 35.0	80.1 79·5	32.6 34.0 35.4	82.2 81.6 81.0 80.4	31.5 33.0 34.4 35.8	83.6 83.1 82.5 81.9 81.3	33·3 34.8 36.2	84.0 83.4 82.8 82.2	33.7 35.2 36.6	85.0 84.4 83.8 83.1	31.1 32.6 34.1 35.6 37.0	70 69 68 67 66
25 26 27 28 29	76.1 75.5 74.8 74.2 73.5	36.8 38.1 39.4 40.7	76.4 75.7 75.1 74.3	35.9 37.3 38.6 39.9 41.2	77.9 77.3 76.6 75.9 75.2	36.3 37.7 39.0 40.4 41.7	78.2 77.5 76.8	38.1 39.5 40.8 42.2	79.8 79.1 78.4 77.7 77.0	38.6 40.0 41.3 42.7	80.7 80.0 79.3 78.6 77.8	39.0 40.4 41.8 43.1	79·5 7 8·7	39.5 40.9 42.3 43.6	80.3 79.6	38.5 39.9 41.3 42.7 44.1	65 64 63 62 61
30 31 32 33 34	72.7 72.0 71.2 70.4 69.6	44·5 45·7 47·0	7.2.9 72.1 71.3 70.5	45.0 46.3 47.5	72.1	43.0 44.3 45.6 46.8 48.1	74.6 73.8	44.8 46.1 47.4	75.4	46.6	76.3 75.5 74.6	44.5 45.8 47.2 48.5 49.8	77.1 76.3 75.5	46.4 47.7 49.0 50.3	77·2 76·3 75·4	45.5 46.9 48.2 49.6 50.9	59 58 57 56
35 36 37 38 39	68.8 68.0 67.1 66.2 65.3	50.6 51.7 52.9	68.8 67.9 67.0 66.1	51.2 52.3 53.5	68.7 67.8 66.8	50.5 51.8 52.9 54.1	69.5 68.6 67.6	51.1 52.4 53.6 54.8	70.3 69.3 68.4	51.7 53.0 54.2 55.4	71.1 70.1 69.2	53.6 54.8 56.0	72.8 71.9 70.9 69.9	52.9 54.2 55.4 56.6	′ ′	52.2 53.5 54.8 56.0 57.3	55 54 53 52 51
40 41 42 43 44	63.4 62.4 61.4 60.4	55.1 56.2 57.3 58.4	64.2 63.2 62.2 61.1	55.8 56.9 58.0 59.0	64.9 63.9 62.9 61.9	56.4 57.5 58.7 59.7	65.7 64.7 63.6 62.6	57.1 58.2 59.3 60.4	65.4 64.4 63.3	57.7 58.9 60.0 61.1	67.2 66.1 65.1 64.0	58.4 59.6 60.7 61.8	66.9 65.8 64.7	59.0 60.2 61.4 62.5	66.6 65.5	59.7 60.9 62.1 63.2	50 49 48 47 46
45					_									-	-		45
Course.		59.4 59.4 60.1 60.1 DEP. LAT. DEP. LAT. D=84' D=85'			DEP.			EAT.		E88'	DEP. $ $	EAT.	DEP.	PO'	DEP.	_	Course.

						Pla	ne	Tra	vers	е Т	able						
Course.	D=g)2'	D=	93′	D=	94′	D =	95′	D =	96′	D=	97′	D =	=98 ′	D =	99′	Course.
<u>క</u>	LAT. I	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3 4	92.0 91.9 91.9	1.6 3.2	93.0 93.0 92.9 92.9 92.8	3.2	94.0 94.0 93.9 93.9 93.8	1.6 3.3 4.9	95.0 95.0 94.9 94.9 94.8	3·3 5.0	96.0 96.0 95.9 95.9 95.8	5.0 6.7	96.9 96.8	1.7		1.7 3.4	98.9 98.9 98.8	0.0 1.7 3.5 5.2 6.9	90 89 88 87 86
5 6 7 8 9	91.5 91.3 91.1	1.2 2.8 4·4	92.6 92.5 92.3 92.1 91.9	9.7 11.3 12.9 14.5	93·3 93·1 92.8	11.5 13.1 14.7	94·5 94·3 94·1 93.8	9.9 11.6 13.2	95·3 95·1 94.8	10.0 11.7 13.4 15.0	96.3 96 I	11.8 13.5 15.2	97·5 97·3 97·0 96.8	10.2 11.9 13.6 15.3	98.5 98.3 98.0	12.1 13.8 15.5	85 84 83 82 81
11 12 13 14	90.3 I 90.0 I 89.6 2	7.6 9.1 0.7 2.3	91.3 91.0 90.6 90.2	17.7 19.3 20.9 22.5	92.3 91.9 91.6 91.2	17.9	93·3 92·9 92·6 92·2	18.1 19.8 21.4 23.0	94.2 93.9 93.5 93.1	18.3 20.0 21.6 23.2	95.2 94.9	18.5 20.2 21.8 23.5	96.2 95.9 95.5	18.7 20.4 22.0 23.7	97.2 96.8 96.5 96.1	18.9 20.6 22.3	79 78 77 76 75
16 17 18 19	88.4 2 88.0 2 87.5 2 87.0 3	5.4 6.9 8.4 0.0	89.4 88.9 88.4 87.9	25.6	90.4 89.9 89.4 88.9	25.9 27.5 29.0 30.6	91.3 90.8 90.4 89.8	26.2 27.8 29.4 30.9	92.3 91.8 91.3 90.8	26.5 28.1 29.7 31.3	93.2 92.8 92.3 91.7	26.7 28.4 30.0 31.6	94.2 93.7 93.2	27.0 28.7 30.3 31.9	95.2 94.7 94.2 93.6	27.3 28.9 30.6 32.2	73 74 73 72 71
21 22 23 24	85.9 3 85.3 3 84.7 3 84.0 3	3.0 4.5 5.9 7.4	86.8 86.2 85.6 85.0	33·3 34.8 36.3 37.8	87.8 87.2 86.5 85.9	33.7 35.2 36.7 38.2	88.7 88.1 87.4 86.8	34.0 35.6 37.1 38.6	89.6 89.0 88.4 87.7	34·4 36.0 37·5 39·0	90.6 89.9 89.3 88.6	34.8 36.3 37.9 39.5	91.5 90.9 90.2 89.5	35.1 36.7 38.3 39.9	92.4 91.8 91.1 90.4 89.7	35·5 37·1 38·7	69 68 67 66 65
25 26 27 28 29	82.7 4 82.0 4 81.2 4 80.5 4	.0.3 .1.8 .3.2 .4.6	83.6 82.9 82.1 81.3	40.8 42.2 43.7 45.1	84.5 83.8 83.0 82.2	41.2 42.7 44.1 45.6	85.4 84.6 83.9 83.1	41.6 43.1 44.6 46.1	86.3 85.5 84.8 84.0	42.1 43.6 45.1 46.5	87.2 86.4 85.6 84.8	42.5 44.0 45.5 47.0	88.1 87.3 86.5 85.7	43.0 44.5 46.0 47.5	89.0 88.2 87.4 86.6	43.4 44.9 46.5 48.0	64 63 62 61
30 31 32 33 34	78.9 4 78.0 4 77.2 5 76.3 5	7·4 8.8 0.1	79.7 78.9 78.0 77.1	47.9 49.3 50.7 52.0	80.6 79.7 78.8 77.9	48.4 49.8 51.2 52.6	81.4 80.6 79.7 78.8	48.9 50.3 51.7 53.1	82.3 81.4 80.5 79.6	49·4 50·9 52·3 53·7	82.3 81.4 80.4	50.0 51.4 52.8 54.2	84.0 83.1 82.2 81.2	50.5 51.9 53.4 54.8	82.1	52.5 53.9 55.4	60 59 58 57 56
35 36 37 38 39	74.4 5 73.5 5 72.5 5 71.5 5	5·4 6.6 7·9	75.2 74.3 73.3 72.3	56.0 57.3 58.5	76.0 75.1 74.1 73.1	55.3 56.6 57.9 59.2	76.9 75.9 74.9 73.8	55.8 57.2 58.5 59.8	77·7 76·7 75·6 74·6	56.4 57.8 59.1 60.4	78.5 77.5 76.4 75.4	57.0 58.4 59.7 61.0	79·3 78·3 77·2 76·2	57.6 59.0 60.3 61.7	81.1 80.1 79.1 78.0 76.9	58.2 59.6 61.0 62.3	55 54 53 52 51
42 43 44	70.5 69.4 68.4 67.3 66.2 66.2	0.4 1.6 2.7 3.9	70.2 69.1 68.0 66.9	61.0 62.2 63.4 64.6	70.9 69.9 68.7 67.6	61.7 62.9 64.1 65.3	71.7 70.6 69.5 68.3	62.3 63.6 64.8 66.0	72.5 71.3 70.2 69.1	63.0 64.2 65.5 66.7	73.2 72.1 70.9	63.6 64.9 66.2 67.4	74.° 72.8 71.7 7°.5	64.3 65.6 66.8 68.1	74.7 73.6 72.4 71.2	64.9 66.2 67.5 68.8	49 48 47 46
45	-					-									70.0		45
Course.		65.1 65.1 65.8 65.8 DEP. LAT. DEP. LAT. D=92' D=93'				94′		LAT. ■95′	D=		DEP.		D =		DEP.	-	Course.

						Pla	ane '	Trav	erse	Tat	ole					
Jonnes	urse.	D =	100′	D =	101'	D =	102'	D =	103'	D =	104'	D=	105'	D=	106′	Course.
2	5	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
	00	100.0	0.0	101.0	0.0	102.0		103.0	0.0	104.0	0.0	105.0	0.0	106.0	0.0	90
	I 2	99.9	1.7 3.5	101.0	1.8 3.5	102.0	1.8 3.6	103.0	1.8 3.6	104.0	1.8 3.6	105.0	1.8 3.7	105.9	1.8 3.7	89 88
	3 4	99.9 99.8		100.9	5·3 7·0	101.9	5·3 7·1			103.9	5·4 7·3	104.9	5·5 7·3	105.9	5·5 7·4	87 86
	5	99.6		100.6		101.6	8.9			103.6	9.1	104.6	9.2	105.6	9.2	85
	7 8	99.5	12.2	100.4	12.3	101.4		102.2	12.6	103.4	10.9	104.4	12.8	105.4	11.1	84 83
	9	99.0	13.9 15.6	99.8		101.0		102.0		103.0	14.5	104.0		105.0	14.8 16.6	82 81
	10	98.5	17.4	99.5	17.5	100.5	17.7	101.4	17.9	102.4	18.1	103.4	18.2	104.4	18.4	80
I	2	97.8	20.8	98.8	21.0	99.8	21.2	100.7	21.4	101.7	21.6	102.7	21.8	103.7	22.0	79 78
	[3 [4	97.4 97.0	22.5	98.4 98.0	22.7	99.4 99.0	22.9 24.7	99.9	23.2	100.9	23.4	102.3	23.6	103.3	23.8 25.6	77 76
1	15	96.6 96.1	25.9 27.6	97.6 97.1	26.1 27.8	98.5 98.0	26.4 28.1	99.5	26.7 28.4	100.5	26.9 28.7	101.4		102.4	27.4 29.2	75 74
I	7 8	95.6	29.2	96.6	29.5	-	29.8 31.5	98.5 98.0	30.1	99.5 98.9	30.4 32.1	100.4		101.4	31.0	73 72
	19	95.1 94.6	32.6	95.5	32.9	96.4	33.2	97.4	33.5	98.3	33.9	99.9		100.0	34.5	71
	20	94.0 93.4	34·2 35.8	94·9 94·3	34·5 36.2	95.8 95.2	34·9 36.6	96.8 96.2	35.2 36.9	97·7 97·1	35.6 37·3	98.7 98.0	35·9 37.6		36.3 38.0	70 69
2	22	92.7	37·5 39·1	93.6 93.0	37.8 39.5	94.6 93.9	38.2	95·5 94.8	38.6	96.4 95.7	39.0	97·4 96.7	39.3	98.3	39·7 41·4	68 67
	24	91.4	40.7	92.3	41.1	93.2	41.5	94.1	41.9	95.0	42.3	95.9	42.7	96.8	43.1	66
2 2	25 26	90.6 89.9	42.3 43.8	91.5 90.8	42.7 44.3	92.4	43.1 44.7	93·3 92.6	43.5	94·3 93·5	44.0	95.2 94.4	44.4		44.8 46.5	65 64
	27 28	89.1 88.3	45·4 46.9	90.0	45·9 47·4	90.9	46.3	91.8	46.8	92.7 91.8	47.2 48.8	93.6	47·7 49·3	94·4 93.6	48.1 49.8	63
	29	87.5	48.5	88.3	49.0	89.2	49.5	90.1	49.9	91.0	50.4	91.8	50.9	92.7	51.4	61
	30 31	86.6 85.7	50.0	87.5 86.6	50.5	88.3 87.4	51.0 52.5	89.2 88.3	51.5	90.1	52.0 53.6	90.9	52.5 54.1	90.9	53.0 54.6	60 59
	32	84.8	53.0 54.5	85.7 84.7	53.5 55.0	86.5 85.5	54.1 55.6	87.3 86.4	54.6 56.1	88.2 87.2	55. I 56.6	89.0	55.6 57.2	89.9 88.9	56.2 57.7	57
3	34	82.9	55.9	83.7	56.5	84.6	57.0	85.4	57.6	86.2	58.2	87.0	58.7	87.9	59.3	56
1 3	35 36	81.9 80.9	57·4 58.8	82.7 81.7	57·9 59·4	83.6	58.5 60.0	84.4	59.1 60.5	85.2 84.1	59·7 61.1	86.0	60.2	85.8	60.8	55 54
3	37 38	79.9 78.8	60.2	80.7 79.6	60.8	81.5	61.4	82.3 81.2	62.0	83.1 82.0	62.6	83.9 82.7	63.2 64.6		63.8 65.3	53 52
3	39	77-7	62.9	78.5	63.6	79-3	64.2	80.0	64.8	80.8	65.4	81.6	66.1		66.7	51
	10 11	76.6 75.5	64.3 65.6	77.4 76.2		77.0	65.6 66.9			78.5	66.8 68.2	79.2	,	80.0	69.5	49
1 4	13	74·3 73·1	66.9 68.2		67.6 68.9		68.3 69.6	76.5	68.9 70.2	77·3 76.1	69.6 70.9		70.3 71.6		70.9	47
4	14	71.9	69.5	72.7	70.2	73.4	70.9	74.1	71.5	74.8	72.2	75.5	72.9		73.6	46
=	15	70-7	70.7	71.4	71.4	72.1	72.1	72.8	72.8	73.5	73.5	74.2	74.2		75.0	45
	Course.	DEP.	EP. LAT. DEP. LAT.		LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	Course.
(5	D =	D = 100' $D = 101'$			D =	102'	D =	103'	D =	104'	D =	105'	D=	106′	ပိ

						Pla	ane	Trav	erse	Tal	ole					
	Course.	D =	107′	D =	108′	D =	109′	D =	110'	D =	111'	D =	112'	D =	113'	Course.
	S	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	Col								
	0	107.0	0.0	108.0		109.0		110.0	0.0			112.0		113.0	0.0	90 89
l	2	106.9	3·7 5.6	107.9		109.0		10.0		111.0	3.9	111.9 111.8	3.9	112.9 112.8	3.9 5.9	88 87
	4	106.7		107.7	7·5	108.7	7.6	109.7	7·7 9.6	110.7	7.7	111.7 111.6	1	112.7	7·9 9.8	86 85
	5 6 7 8	106.4	11.2	107.4	11.3	108.4	11.4	109.4	11.5	110.4		111.4		112.4 112.2	11.8	84 83
-	9	106.0		106.9		107.9		108.9		109.9	15.4	110.6		111.9	15.7 17.7	82 81
-	10	105.4	20.4	106.4	20.6	107.3	20.8	108.3	21.0	109.3	19.3	110.3	21.4	111.3	19.6	80 79
	12 13 14	104.7 104.3 103.8	24.1	105.6 105.2 104.8	22.5 24.3 26.1	106.6 106.2 105.8	24.5	107.6		108.6 108.2 107.7	23.1 25.0 26.9	109.6	25.2	110.5 110.1 109.6	23.5 25.4 27.3	78 77 76
	15 16	103.4	27.7	104.3	28.0	105.3	28.2	106.3	28.5	107.2	28.7	108.2	29.2	109.1	29.2	75 74
	17 18	102.3	31.3 33.1	103.3	31.6 33.4	104.2	31.9	105.2 104.6	32.2 34.0	106.1	32.5 34.3	107.1	32.7 34.6	108.1	33.0 34.9	73 72
	19 20	101.2		102.1	35.2 36.9	103.1		104.0		105.0		105.9		106.8	36.8 38.6	7 ^I 70
	21 22 23	99.9	40.1	100.8	38.7 40.5		40.8	102.7 102.0 101.3	39·4 41.2	102.9	41.6	104.6	40.1 42.0	104.8	40.5	69 68 67
	24	98.5 97.7	41.8	99·4 98·7	43.9	99.6	44-3	100.5	43.0	101.4	45.1	102.3		103.2	44.2	66
	25 26 27	97.0 96.2 95.3	45.2 46.9 48.6	97.9 97.1 96.2	45.6 47.3 49.0	98.8 98.0 97.1	46.1 47.8 49.5	99.7 98.9 98.0	46.5 48.2 49.9	99.8 98.9	48.7 50.4	101.5 100.7 99.8	47·3 49·1 50·8	102.4	47.8 49.5 51.3	65 64 63
	28 29	94·5 93.6	50.2 51.9	95·4 94·5	50.7 52.4	96.2 95·3	51.2	97.1 96.2	51.6 53.3	98.0 97.1	52.1 53.8	98.9 98.0	52.6 54·3	99.8 98.8	53.1 54.8	62 61
	30 31	92.7 91.7	53·5 55·1	93·5 92.6	54.0 55.6	94·4 93·4	54·5 56.1	95·3 94·3	55.0 56.7	96.1 95.1	55·5 57·2	9 7. 0 96.0	56.0 57.7	97·9 96.9	56.5 58.2	60 59
	32 33 34	90.7 89.7 88.7	56.7 58.3 59.8	91.6 90.6 89.5	57.2 58.8 60.4	92.4 91.4 90.4	57.8 59.4 61.0	93·3 92·3 91·2	58.3 59.9 61.5	94.1 93.1 92.0	58.8 60.5 62.1	95.0 93.9 92.9	59.4 61.0 62.6	95.8 94.8 93.7	59.9 61.5 63.2	58 57 56
	35 36	87.6 86.6	61.4	88.5	61.9		62.5 64.1	1	63.1 64.7	90.9	63.7 65.2	91.7	64.2 65.8	92.6	64.8 66.4	55 54
	37 38	85.5 84.3	64.4 65.9	86.3 85.1	65.0	87.1 85.9	65.6 67.1	87.8 86.7	66.2 67.7	88.6 87.5	66.8	89.4 88.3	67.4 69.0	90.2 89.0	68.0 69.6	53 52
100	39 40	83.2		83.9	68.0	84.7 83.5	68.6	84.3	69.2 70.7	86.3 85.0	69.9	87.0 85.8	7°-5	87.8 86.6	71.1 72.6	51 50
The same of the same	41 42 43	80.8 79.5 78.3		81.5	70.9 72.3	82.3 81.0	71.5 72.9	83.0 81.7	72.2 73.6	83.8	72.8	84.5 83.2	73-5	85.3	74.1 75.6	49 48
-	44	77.0	74.3	77.7	75.0	78.4	75.7	79.1	75.0 76.4	79.8	77-1	80.6	77.8	81.3	78.5	46
	45	75.7	75.7						77.8	78.5		79-2	79.2	79.9 Dep.		45
	Course.		Dep. LAT. Dep. LAT.			DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.		LAT.	Course.
	ŭ	D = 107' $D = 108'$		<i>D</i> =	109′	D=	110′	D=	111'	D=	112'	D=	113′	ŭ		

					Pl	ane	Trav	erse	Tal	ole					
Course.	D =	114'	D =	115'	D =	116′	D =	117′	D =	118′	D =	119'	D =	120′	Course.
ပိ	LAT.	DEP.	Co												
0 1 2 3 4	114.0 114.0 113.9 113.8	2.0 4.0 6.0	115.0 115.0 114.9 114.8	2.0 4.0 6.0	116.0 116.0 115.9 115.8 115.7	2.0 4.0 6.1	117.0 117.0 116.9 116.8	2.0 4.1 6.1	118.0 118.0 117.9 117.8	2.1 4.1 6.2	119.0 119.0 118.9 118.8 118.7	2.1 4.2 6.2	120.0 120.0 119.9 119.8 119.7	0.0 2.1 4.2 6.3 8.4	° 90 89 88 87 86
5 6 7 8 9	113.6 113.4 113.2 112.9 112.6	11.9 13.9 15.9 17.8	114.6 114.4 114.1 113.9 113.6	12.0 14.0 16.0 18.0	115.1 114.9 114.6	12.1 14.1 16.1 18.1	116.6 116.4 116.1 115.9 115.6	12.2 14.3 16.3 18.3	117.1 116.9 116.5	12.3 14.4 16.4 18.5	118.5 118.3 118.1 117.8 117.5	16.6 18.6	119.3 119.1 118.8 118.5	10.5 12.5 14.6 16.7 18.8	82 81
10 11 12 13 14	112.3 111.9 111.5 111.1 110.6	21.8 23.7 25.6 27.6	113.3 112.9 112.5 112.1 111.6	23.9 25.9 27.8	114.2 113.9 113.5 113.0 112.6	22.I 24.I 26.I 28.I	115.2 114.9 114.4 114.0 113.5	24.3 26.3 28.3	115.8 115.4 115.0 114.5	22.5 24.5 26.5 28.5	117.2 116.8 116.4 116.0	26.8 28.8	117.4 116.9 116.4	20.8 22.9 24.9 27.0 29.0	80 79 78 77 76
15 16 17 18 19	110.1 109.6 109.0 108.4 107.8	31.4 33.3 35.2 37.1	111.1 110.5 110.0 109.4 108.7	29.8 31.7 33.6 35.5 37.4	112.0 111.5 110.9 110.3 109.7	32.0 33.9 35.8	113.0 112.5 111.9 111.3 110.6	32.2 34.2 36.2 38.1	114.0 113.4 112.8 112.2 111.6	32.5 34.5 36.5 38.4	114.9 114.4 113.8 113.2 112.5	34.8 36.8 38.7	115.4 114.8 114.1 113.5	31.1 33.1 35.1 37.1 39.1	75 74 73 72 71
20 21 22 23 24	107.1 106.4 105.7 104.9	40.9 42.7 44.5	108.1 107.4 106.6 105.9 105.1	39·3 41·2 43·1 44·9 46.8	109.0 108.3 107.6 106.8 106.0	41.6 43.5 45.3	109.9 109.2 108.5 107.7 106.9	41.9 43.8	110.9 110.2 109.4 108.6 107.8	44.2 46.1	111.8 111.1 110.3 109.5 108.7	44.6 46.5 48.4	112.8 112.0 111.3 110.5 109.6	41.0 43.0 45.0 46.9 48.8	69 68 67 66
25 26 27 28 29	103.3 102.5 101.6 100.7 99.7	50.0 51.8	104.2 103.4 102.5 101.5	48.6 50.4 52.2 54.0 55.8	105.1 104.3 103.4 102.4 101.5	50.9 52.7 54.5 56.2	106.0 105.2 104.2 103.3 102.3	51.3 53.1 54.9	106.9 106.1 105.1 104.2 103.2	51.7 53.6 55.4	106.0 105.1 104.1	52.2 54.0 55.9 57:7		50.7 52.6 54.5 56.3 58.2	65 64 63 62 61
30 31 32 33 34	98.7 97.7 96.7 95.6 94.5	57.0 58.7 60.4 62.1 63.7	99.6 98.6 97.5 96.4 95.3	57·5 59·2 60·9 62·6 64·3	99.4 98.4 97.3 96.2	58.0 59.7 61.5 63.2 64.9	99.2 98.1	60.3	102.2 101.1 100.1 99.0 97.8	59.0 60.8 62.5 64.3 66.0	102.0 100.9 99.8	61.3 63.1 64.8 66.5	103.9 102.9 101.8 100.6 99.5	60.0 61.8 63.6 65.4 67.1	59 58 57 56
35 36 37 38 39	93.4 92.2 91.0 89.8 88.6	65.4 67.0 68.6 70.2 71.7	94.2 93.0 91.8 90.6 89.4	66.0 67.6 69.2 70.8 72.4	95.0 93.8 92.6 91.4 90.1	66.5 68.2 69.8 71.4 73.0	94·7 93·4 92·2 90·9	67.1 68.8 70.4 72.0 73.6		67.7 69.4 71.0 72.6 74.2		68.3 69.9 71.6 73.3 74.9	95.8 94.6 93·3	68.8 7°.5 72.2 73.9 75.5	51
40 41 42 43 44	87.3 86.0 84.7 83.4 82.0	73·3 74.8 76·3 77·7 79·2	86.8 85.5 84.1 82.7	77.0 78.4 79.9	87.5 86.2 84.8 83.4	77.6 79.1 80.6	88.3 86.9 85.6 84.2	78.3 79.8 81.3	89.1 87.7 86.3 84.9	79.0 80.5 82.0	89.8 88.4 87.0 85.6	78.1 79.6 81.2 82.7	90.6 89.2 87.8 86.3	80.3 81.8 83.4	49 48 47 46
45	80.6	80.6	81.3	81.3	82.0	82.0	82.7	82.7	83.4	83.4	84.1	84.1	84.9	84.9	45
Course.	DEP.	LAT.	Course.												
Col	D =	D=114' D=115'		115'	D=	116'	D =	117'	D =	118'	D =	119'	D =	120′	ပိ

Plane	Traverse	Table
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Course.	D =	121′	D =	122'	D =	123′	D =	124′	D =	125′	D =	126′	D =	127'	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
°	121.0	0.0	122.0		123.0	0.0	124.0	0.0	125.0	0.0	126.0	0.0	127.0	0.0	90 89
I 2	121.0	2.I 4.2	122.0		123.0	2.I 4.3	124.0	2.2 4.3		2.2 4.4	126.0	2.2 4.4	127.0	2.2 4.4	89 88
3 4	120.8	6.3 8.4	121.8	6.4	122.8	6.4 8.6	123.8	6.5 8.6	124.8	6.5 8.7	125.8	6.6 8.8	126.8	6.6 8.9	87 86
	120.5	10.5	121.5		122.5	10.7			124.5	· 1	125.5	11.0	, '	11.1	85
5 6	120.3	12.6	121.3	12.8	122.3	12.9	123.3	13.0	124.3	13.1	125.3	13.2	126.3	13.3	84
7 8	119.8	16.8	121.1	17.0	122.1 121.8		123.1 122.8	17.3	124.1		125.1	15.4		15.5	83 82
9	119.5		120.5		121.5		122.5		123.5	19.6	124.4	19.7		19.9	87
10	119.2		120.1		121.1	21.4	122.1	21.5	123.I 122.7	21.7	124.1	21.9		22.I 24.2	70
12	118.4	25.2	119.3	25.4	120.3	25.6	121.3	25.8	122.3	26.0	123.2	26.2	124.2	26.4	79 78
13	117.9		118.9 118.4		119.8		120.8		121.8	28.1 30.2		30.5	123.7 123.2	28.6 30.7	77 76
15	116.9		117.8		118.8	31.8	119.8		120.7		121.7		122.7	32.9	75
16 17	116.3	33·4 35·4	117.3		118.2	33.9	119.2 118.6		120.2 119.5	34·5 36.5	121.1	34·7 36.8	122.1	35.0 37.1	74
18	115.1	37.4	116.0	37.7	117.0	38.0	117.9	38.3	118.9	38.6	119.8	38.9	120.8	39.2	73 72
19	114.4		115.4		116.3		117.2		118.2		119.1		120.1	41.3	71
20 2I	113.7	41.4 43.4	114.6	43.7	115.6	42.I 44.I	115.8		117.5 116.7	42.8 44.8	117.6		118.6	43·4 45·5	70 69
22 23	112.2		113.1 112.3	45.7	114.0 113.2		115.0		115.9	46.8 48.8	116.8		117.8	47.6 49.6	68
24	110.5		111.5		112.4		113.3		114.2		115.1		116.0	51.7	67 66
25 26	109.7	51.1	110.6		111.5		112.4		113.3	52.8	114.2		115.1	53.7	65
27	107.8	54.9	109.7	55.4	10.6	55.8	111.5	56.3	112.3		I13.2 I12.3		114.I 113.2	55·7 57·7	64 63
28 29	106.8		107.7	57·3	108.6	57.7	109.5		10.4	58.7 60.6	111.3	59 .2 61.1	I 12.1	59.6 61.6	62 61
30	104.8		105.7		106.5		107.4		108.3	62.5	109.1		111.0	63.5	60
31	103.7	62.3	104.6	62.8	105.4	63.3	106.3	63.9	107.1	64.4	108.0	64.9	108.9	65.4	
32 33	102.6		103.5		104.3		105.2		106.0 104.8	68.1	106.9		107.7	67.3 69.2	59 58 57 56
34	100.3	67.7	101.1	68.2	102.0		102.8		103.6	69.9	104.5	70.5	105.3	71.0	56
35	99.1 97.9	69.4	99.9 98.7	70.0 71.7	100.8	7°.5 72.3		71.I 72.9	102.4	71.7	103.2	72·3 74·1	104.0	72.8	55
36 37 38	96.6	72.8	97.4	73.4	99·5 98·2	74.0	99.0	74.6	99.8	73·5 75·2	100.6	75.8	101.4	74.6 76.4	54
38	95·3 94.0	74·5 76.1	96.1 94.8	75.1 76.8	96.9 95.6	75·7 77·4	97 ·7 96 · 4	76.3	98.5 97.1	77.0 78.7	99·3 97·9	77.6 79.3		78.2 79.9	54 53 52 51
40	92.7	77.8	93.5	78.4	94.2	79.1	95.0	79.7	95.8	80.3	96.5	81.0	97.3	81.6	50
41	91.3	79·4 81.0	92.1	80.0 81.6	92.8	80.7	93.6	81.4	94.3	82.0	95.1	82.7	95.8	83.3	49 48
42	89.9 88.5	82.5	90.7 89.2	83.2	90.0	82.3 83.9	92.1	83.0 84.6	92.9	83.6 85.2	93.6	84.3 85.9	94.4	85.0 86.6	47
44	87.0	84.1	87.8	84.7	88.5	85.4	89.2	86.1	89.9	86.8	90.6	87.5	91.4	88.2	46
45	85.6	85.6	86.3	86.3	87.0	87.0	87.7	87.7	88.4	88.4	89.1	89.1	89.8	89.8	45
se.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	se.
Course.	D =	121'	D =	122'	D =	123′	D =	124′	D =	125′	D =	126′	D =	127′	Course.
		D=121 D=122													

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					Pla	ane	Trav	erse	Tal	ole					
Course.	D =	128′	D=	129′	D =	130′	D =	131'	D =	132′	D =	133'	D = 1	134'	Course.
Col	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	S
0 1 2 3 4	128.0 128.0 127.9 127.8 127.7	2.2 4.5 6.7	129.0 129.0 128.9 128.8 128.7	2.3 4.5 6.8	130.0 130.0 129.9 129.8 129.7	2.3 4.5 6.8	131.0 131.0 130.9 130.8 130.7	2.3 4.6 6.9	132.0 132.0 131.9 131.8 131.7	2.3 4.6 6.9	133.0 133.0 132.9 132.8 132.7	2.3 4.6 7.0	134.0 134.0 133.9 133.8 133.7	0.0 2.3 4.7 7.0 9.3	90 89 88 87 86
5 6 7 8 9	127.5 127.3 127.0 126.8 126.4	13.4 15.6 17.8 20.0	128.5 128.3 128.0 127.7 127.4	13.5 15.7 18.0 20.2	129.5 129.3 129.0 128.7 128.4	13.6 15.8 18.1 20.3	130.5 130.3 130.0 129.7 129.4	13.7 16.0 18.2 20.5	131.5 131.3 131.0 130.7 130.4	16.1 18.4 20.6	132.3 132.0 131.7 131.4	13.9 16.2 18.5 20.8	133.5 133.3 133.0 132.7 132.4	11.7 14.0 16.3 18.6 21.0	85 84 83 82 81
10 11 12 13 14	125.6 24.4 126.6 2. 125.2 26.6 126.2 2. 124.7 28.8 125.7 2. 124.2 31.0 125.2 3. 123.6 33.1 124.6 3. 123.0 35.3 124.0 3. 122.4 37.4 123.4 3.			24.6 26.8 29.0 31.2	128.0 127.6 127.2 126.7 126.1	24.8 27.0 29.2 31.4	129.0 128.6 128.1 127.6 127.1	25.0 27.2 29.5 31.7		25.2 27.4 29.7 31.9	131.0 130.6 130.1 129.6 129.0	25.4 27.7 29.9 32.2	132.0 131.5 131.1 130.6 130.0	23.3 25.6 27.9 30.1 32.4	80 79 78 77 76
15 16 17 18 19	123.0 122.4 121.7 121.0	35·3 37·4 39.6 41·7	124.0 123.4 122.7 122.0	37·7 39·9 42.0	125.6 125.0 124.3 123.6 122.9	35.8 38.0 40.2 42.3	126.5 125.9 125.3 124.6 123.9	36.1 38.3 40.5 42.6	127.5 126.9 126.2 125.5 124.8	36.4 38.6 40.8 43.0	128.5 127.8 127.2 126.5 125.8	36.7 38.9 41.1 43.3	129.4 128.8 128.1 127.4 126.7	34·7 36·9 39·2 41·4 43·6 45.8	75 74 73 72 71
20 21 22 23 24	120.3 119.5 118.7 117.8 116.9	45.9 47.9 50.0 52.1	121.2 120.4 119.6 118.7 117.8	46.2 48.3 50.4 52.5	122.2 121.4 120.5 119.7 118.8	46.6 48.7 50.8 52.9	123.1 122.3 121.5 120.6 119.7	46.9 49.1 51.2 53.3	124.0 123.2 122.4 121.5 120.6	47·3 49·4 51.6 53·7	121.5	47·7 49.8 52.0 54·1	125.1 124.2 123.3 122.4	48.0 50.2 52.4 54.5	67 66
25 26 27 28 29	116.0 115.0 114.0 113.0	56.1 58.1 60.1 62.1	116.9 115.9 114.9 113.9 112.8	56.5 58.6 60.6 62.5	117.8 116.8 115.8 114.8 113.7	57.0 59.0 61.0 63.0	118.7 117.7 116.7 115.7 114.6	57·4 59·5 61.5 63·5	119.6 118.6 117.6 116.5	57.9 59.9 62.0 64.0	118.5 117.4 116.3	58.3 60.4 62.4 64.5	121.4 120.4 119.4 118.3	56.6 58.7 60.8 62.9 65.0	63 62 61
30 31 32 33 34	110.9 109.7 108.6 107.3 106.1	65.9 67.8 69.7	111.7 110.6 109.4 108.2 106.9	66.4 68.4 70.3 72.1	112.6 111.4 110.2 109.0 107.8	67.0 68.9 70.8 72.7		67.5 69.4 71.3 73.3	114.3 113.1 111.9 110.7 109.4	68.0 69.9 . 71.9 73.8	115.2 114.0 112.8 111.5	68.5 7°.5 72.4 74.4	116.0 114.9 113.6 112.4 111.1	69.0 71.0 73.0 74.9	59 58 57 56
35 36 37 38 39	104.9 103.6 102.2 100.9 99.5	75.2 77.0 78.8 80.6	105.7 104.4 103.0 101.7 100.3	75.8 77.6 79.4 81.2	106.5 105.2 103.8 102.4 101.0	76.4 78.2 80.0 81.8	104.6 103.2 101.8	77.0 78.8 80.7 82.4		77.6 79.4 81.3 83.1	108.9 107.6 106.2 104.8	78.2 80.0 81.9 83.7	109.8 108.4 107.0 105.6 104.1	78.8 80.6 82.5 84.3	52 51
40 41 42 43 44	95.1 93.6 92.1	84.0 85.6 87.3 88.9	97·4 95·9 94·3 92.8	84.6 86.3 88.0 89.6	95.1 93.5	85.3 87.0 88.7 90.3	97·4 95.8 94·2	85.9 87.7 89.3 91.0	98.1 96.5 95.0	86.6 88.3 90.0 91.7	98.8 97·3 95·7	87.3 89.0 90.7 92.4	99.0 98.0 96.4	87.9 89.7 91.4 93.1	49 48 47
45	90.5			-		-		-	93·3 DEP.	-	DEP.		DEP.		_
Course.	DEP.	LAT. = 128'		LAT.	DEP.	130'	-	131'	_	132′		=133′	-	=134′	Course.

					Pl	ane	Trav	erse	Tal	ole					
Course.	D =	135'	D =	136′	D =	137'	D =	138′	D =	139'	D=	140′	D=	141′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	Dep.	ပိ
0 1 2 3 4	135.0 135.0 134.9 134.8 134.7	0.0 2.4 4.7 7.1 9.4	136.0 135.9 135.8	2.4 4.7 7.1	137.0 137.0 136.9 136.8 136.7	2.4 4.8 7.2	138.0 138.0 137.9 137.8 137.7	2.4 4.8 7.2	139.0 139.0 138.9 138.8 138.7	2.4 4.9 7.3	140.0 140.0 139.9 139.8 139.7	2.4 4.9 7.3	141.0 141.0 140.9 140.8 140.7	7.4 9.8	90 89 88 87 86
5 6 7 8 9	134.5 134.3 134.0 133.7 133.3	11.8 14.1 16.5 18.8 21.1	135.3	14.2 16.6 18.9	136.5 136.2 136.0 135.7 135.3	14.3 16.7 19.1	137.5 137.2 137.0 136.7 136.3	14.4 16.8 19.2	138.5 138.2 138.0 137.7 137.3	14.5 16.9 19.3	139.5 139.2 139.0 138.6 138.3	14.6 17.1 19.5	140.5 140.2 139.9 139.6 139.3	12.3 14.7 17.2 19.6 22.1	85 84 83 82 81
10 11 12 13 14	132.9 132.5 132.0 131.5 131.0	30.4		26.0 28.3 30.6	134.9 134.5 134.0 133.5 132.9	28.5 30.8	135.9 135.5 135.0 134.5 133.9	26.3 28.7 31.0	136.9 136.4 136.0 135.4 134.9	26.5 28.9 31.3	137.9 137.4 136.9 136.4 135.8	26.7 29.1 31.5	138.9 138.4 137.9 137.4 136.8	24.5 26.9 29.3 31.7 34.1	80 79 78 77 76
15 16 17 18	130.4 129.8 129.1 128.4 127.6	37.2 39.5 41.7	131.4 130.7 130.1 129.3 128.6	37·5 39.8 42.0	132.3 131.7 131.0 130.3 129.5	35.5 37.8 40.1 42.3 44.6	133.3 132.7 132.0 131.2 130.5	38.0 40.3 42.6	134.3 133.6 132.9 132.2 131.4	38.3 40.6 43.0	135.2 134.6 133.9 133.1 132.4	38.6 40.9 43.3	136.2 135.5 134.8 134.1 133.3	36.5 38.9 41.2 43.6 45.9	75 74 73 72 71
20 21 22 23 24	126.9 126.0 125.2 124.3 123.3	48.4 50.6	127.8 127.0 126.1 125.2 124.2	48.7 50.9 53.1	128.7 127.9 127.0 126.1 125.2	46.9 49.1 51.3 53.5 55.7	129.7 128.8 128.0 127.0 126.1	49·5 51·7 53·9	130.6 129.8 128.9 128.0		131.6 130.7 129.8 128.9 127.9	50.2 52.4 54.7	132.5 131.6 130.7 129.8 128.8	48.2 50.5 52.8 55.1 57.3	70 69 68 67 66
25 26 27 28 29	122.4 121.3 120.3 119.2 118.1	61.3 63.4	123.3 122.2 121.2 120.1 118.9	59.6 61.7 63.8	124.2 123.1 122.1 121.0 119.8	62.2	125.1 124.0 123.0 121.8 120.7	62.7 64.8	126.0 124.9 123.8 122.7 121.6	63.1 65.3	126.9 125.8 124.7 123.6 122.4	61.4 63.6 65.7	127.8 126.7 125.6 124.5 123.3	59.6 61.8 64.0 66.2 68.4	65 64 63 62 61
30 31 32 33 34	116.9 115.7 114.5 113.2 111.9	67.5 69.5 71.5 73.5 75.5	116.6 115.3 114.1	70.0 72.1 74.1	118.6 117.4 116.2 114.9 113.6	70.6 72.6 74.6	119.5 118.3 117.0 115.7 114.4	71.1 73.1 75.2		71.6 73.7	121.2 120.0 118.7 117.4 116.1	72.1 74.2 76.2	122.1 120.9 119.6 118.3 116.9	7°.5 72.6 74.7 76.8 78.8	60 59 58 57 56
35 36 37 38 39	110.6 109.2 107.8 106.4 104.9	83.I 85.0	110.0 108.6 107.2 105.7	79.9 81.8 83.7	112.2 110.8 109.4 108.0 106.5	80.5 82.4 84.3 86.2	113.0 111.6 110.2 108.7 107.2	81.1 83.1 85.0 86.8	113.9 112.5 111.0 109.5 108.0	81.7 83.7 85.6	114.7 113.3 111.8 110.3 108.8	82.3 84.3 86.2	115.5 114.1 112.6 211.1 109.6	80.9 82.9 84.9 86.8 88.7	55 54 53 52 51
40 41 42 43 44	103.4 101.9 100.3 98.7 97.1	88.6 90.3 92.1 93.8	99·5 97·8	89.2 91.0 92.8 94.5	104.9 103.4 101.8 100.2 98.5	89.9 91.7 93.4 95.2	105.7 104.1 102.6 100.9 99.3	90.5 92.3 94.1 95.9	100.0	91.2 93.0 94.8 96.6	107.2 105.7 104.0 102.4 100.7	91.8 93.7 95.5 97.3	108.0 106.4 104.8 103.1 101.4		50 49 48 47 46
45	95.5	95.5	96.2	96.2	96.9	96.9	97.6		98.3	98.3	-	99.0	99.7	99.7	45
Course.	D_{EP} .	135'	Dep.	136'	Dep.	LAT.	Dep.	138'	D_{EP} .	139'	DEP.	140'	D_{EP}	LAT.	Course.

					Pl	ane	Trav	erse	Tal	ole					
Course.	D=	142'	D =	143'	D =	144'	D =	145'	D=	146′	D =	147'	D=	148'	rse.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	Course
0 1 2 3 4	142.0 142.0 141.9 141.8	0.0 2.5 5.0 7.4 9.9	143.0 142.9 142.8	5.0 7.5	144.0 144.0 143.9 143.8 143.6	5.0 7.5	145.0 144.9	7.6 10.1	146.0 145.9 145.8	7.6 10.2	147.0 147.0 146.9 146.8 146.6	7.7	148.0 147.9	7.7 10.3	90 89 88 87 86
56 78 9	141.5 141.2 140.9 140.6 140.3	19.8		14.9 17.4 19.9	143.5 143.2 142.9 142.6 142.2	15.1	143.9 143.6	17.7	145.2	12.7 15.3 17.8 20.3 22.8	146.4 146.2 145.9 145.6 145.2	17.9	147.4 147.2 146.9 146.6 146.2	12.9 15.5 18.0 20.6 23.2	85 84 83 82 81
10 11 12 13 14	139.8 139.4 138.9 138.4 137.8	27.1 29.5 31.9 34.4	140.8 140.4 139.9 139.3 138.8	27.3 29.7 32.2	141.8 141.4 140.9 140.3 139.7	27·5 29·9	142.8 142.3 141.8 141.3 140.7	27.7 30.1		3°.4 32.8 35·3	144.8 144.3 143.8 143.2 142.6	28.0 30.6 33.1 35.6	145.8 145.3 144.8 144.2 143.6	25.7 28.2 30.8 33.3 35.8	80 79 78 77 76
15 16 17 18 19	137.2 136.5 135.8 135.1 134.3	39.1 41.5 43.9 46.2	138.1 137.5 136.8 136.0 135.2	39.4 41.8 44.2 46.6	139.1 138.4 137.7 137.0 136.2	37·3 39·7 42·1 44·5 46·9	137.9 137.1	42.4 44.8 47.2	138.9 138.0	40.2 42.7 45.1 47.5	142.0 141.3 140.6 139.8 139.0	40.5 43.0 45.4	143.0 142.3 141.5 140.8 139.9	38.3 40.8 43.3 45.7 48.2	75 74 73 72 71
20 21 22 23 24	133.4 132.6 131.7 130.7 129.7	50.9 53.2 55.5	134.4 133.5 132.6 131.6 130.6	51.2 53.6 55.9	135.3 134.4 133.5 132.6 131.6	53·9 56.3	136.3 135.4 134.4 133.5 132.5	52.0 54.3 56.7	137.2 136.3 135.4 134.4 133.4	52·3 54·7 57·0	138.1 137.2 136.3 135.3 134.3	52.7 55.1 57.4	139.1 138.2 137.2 136.2 135.2	50.6 53.0 55.4 57.8 60.2	70 69 68 67 66
25 26 27 28 29	128.7 127.6 126.5 125.4 124.2	62.2 64.5 66.7	129.6 128.5 127.4 126.3 125.1	62.7 64.9 67.1	130.5 129.4 128.3 127.1 125.9	65.4 67.6	130.3	68. 1		64.0 66.3 68.5	133.2 132.1 131.0 129.8 128.6	66.7 69.0	134.1 133.0 131.9 130.7 129.4	62.5 64.9 67.2 69.5 71.8	65 64 63 62 61
30 31 32 33 34	123.0 121.7 120.4 119.1 117.7	73.1 75.2 77.3	123.8 122.6 121.3 119.9 118.6	73·7 75·8 77·9	124.7 123.4 122.1 120.8 119.4	72.0 74.2 76.3 78.4 80.5	124.3 123.0 121.6 120.2	74.7 76.8 79.0 81.1	125.1 123.8 122.4 121.0	75.2 77.4 79.5	127.3 126.0 124.7 123.3 121.9	73·5 75·7 77·9 80.1 82.2	126.9 125.5	74.0 76.2 78.4 80.6 82.8	60 59 58 57 56
35 36 37 38 39	116.3 114.9 113.4 111.9 110.4	85.5 87.4 89.4	115.7 114.2 112.7 111.1	84.1 86.1 88.0 90.0	118.0 116.5 115.0 113.5 111.9	84.6 86.7 88.7 90.6	115.8 114.3 112.7	85.2 87.3 89.3 91.3	113.5	87.9 89.9 91.9	120.4 118.9 117.4 115.8 114.2	86.4 88.5 90.5 92.5	121.2 119.7 118.2 116.6 115.0	84.9 87.0 89.1 91.1 93.1	55 54 53 52 51
40 41 42 43 44	108.8 107.2 105.5 103.9 102.1	93.2 95.0 96.8	109.5 107.9 106.3 104.6 102.9	93.8 95.7 97.5 99.3		94.5 96.4 98.2 100.0	107.8 106.0 104.3	95.1 97.0 98.9 100.7		95.8 97.7 99.6 101.4	107.5	96.4 98.4 100.3 102.1	110.0 108.2 106.5	99.0 100.9 102.8	50 49 48 47 46
45	100.4	-		101.1			_								45
Course.	D_{EP}	LAT.	D _{EP} .	I43'		I44'	D_{EP} .	145'	D_{EP} .	146'	D=	IAT.	DEP.	148'	Course.

					Pl	ane	Trav	rerse	Tal	ble					
Course.	D=	149′	D=	150′	D=	151'	D=	152′	D=	153′	D=	154′	D=	155′	Course.
Con	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3 4	149.0 149.0 148.9 148.8 148.6	2.6 5.2 7.8	150.0 150.0 149.9 149.8 149.6	2.6 5.2	151.0 151.0 150.9 150.8 150.6	2.6 5·3 7·9	152.0 152.0 151.9 151.8 151.6	0.0 2.7 5.3 8.0 10.6	153.0 153.0 152.9 152.8 152.6	2.7 5.3	154.0 154.0 153.9 153.8 153.6	2.7 5.4 8.1	155.0 155.0 154.9 154.8 154.6	0.0 2.7 5.4 8.1 10.8	90 89 88 87 86
56 78 9	148.4 148.2 147.9 147.5 147.2	15.6 18.2 20.7 23.3	149.4 149.2 148.9 148.5 148.2	13.1 15.7 18.3 20.9 23.5	150.4 150.2 149.9 149.5 149.1	15.8 18.4 21.0 23.6	151.4 151.2 150.9 150.5 150.1	13.2 15.9 18.5 21.2 23.8	152.4 152.2 151.9 151.5 151.1	13.3 16.0 18.6 21.3 23.9	153.4 153.2 152.9 152.5 152.1	16.1 18.8 21.4 24.1	154.4 154.2 153.8 153.5 153.1	13.5 16.2 18.9 21.6 24.2	85 84 83 82 81
10 11 12 13 14	146.7 146.3 145.7 145.2 144.6	28.4 31.0 33.5 36.0	147.7 147.2 146.7 146.2 145.5	26.0 28.6 31.2 33.7 36.3	148.2 147.7 147.1 146.5	28.8 31.4 34.0 36.5	149.7 149.2 148.7 148.1 147.5	26.4 29.0 31.6 34.2 36.8	150.7 150.2 149.7 149.1 148.5	29.2 31.8 34.4 37.0	151.7 151.2 150.6 150.1 149.4 148.8	29.4 32.0	152.6 152.2 151.6 151.0 150.4	29.6 32.2 34.9 37.5	79 78 77 76
15 16 17 18 19	143.9 143.2 142.5 141.7 140.9	41.1 43.6 46.0 48.5	144.2 143.4 142.7 141.8	41.3 43.9 46.4 48.8	145.2 144.4 143.6 142.8	41.6 44.1 46.7 49.2	146.1 145.4 144.6 143.7	39·3 41·9 44·4 47·0 49·5	147.1 146.3 145.5 144.7	42.2 44.7 47.3 49.8	148.0 147.3 146.5 145.6	42.4 45.0 47.6 50.1	149.0 148.2 147.4 146.6	42.7 45.3 47.9 50.5	75 74 73 72 71
20 21 22 23 24	140.0 139.1 138.2 137.2 136.1	53.4 55.8 58.2 60.6	141.0 140.0 139.1 138.1 137.0	56.2 58.6 61.0	141.9 141.0 140.0 139.0 137.9	54.1 56.6 59.0 61.4	141.9 140.9 139.9 138.9	52.0 54.5 56.9 59.4 61.8	141.9 140.8 139.8	52.3 54.8 57.3 59.8 62.2	144.7 143.8 142.8 141.8 140.7	57.7 60.2 62.6	144.7 143.7 142.7 141.6	53.0 55.5 58.1 60.6 63.0	70 69 68 67 66
25 26 27 28 29	135.0 133.9 132.8 131.6 130.3	65.3 67.6 70.0 72.2	135.9 134.8 133.7 132.4 131.2	65.8 68.1 70.4 72.7	136.9 135.7 134.5 133.3 132.1	66.2 68.6 70.9 73.2	137.8 136.6 135.4 134.2 132.9	64.2 66.6 69.0 71.4 73.7	138.7 137.5 136.3 135.1 133.8	64.7 67.1 69.5 71.8 74.2	139.6 138.4 137.2 136.0 134.7	67.5 69.9 72.3 74.7	140.5 139.3 138.1 136.9 135.6	65.5 67.9 70.4 72.8 75.1	65 64 63 62 61
30 31 32 33 34	129.0 127.7 126.4 125.0 123.5	79.0 81.2 83.3	128.6 127.2 125.8 124.4	77·3 79·5 81·7 83·9	130.8 129.4 128.1 126.6 125.2	77.8 80.0 82.2 84.4	126.0	76.0 78.3 80.5 82.8 85.0	129.8 128.3 126.8	76.5 78.8 81.1 83.3 85.6	133.4 132.0 130.6 129.2 127.7	81.6 83.9 86.1	132.9 131.4 130.0 128.5	77.5 79.8 82.1 84.4 86.7	59 58 57 56
35 36 37 38 39	122.1 120.5 119.0 117.4 115.8	87.6 89.7 91.7 93.8	122.9 121.4 119.8 118.2 116.6	88.2 90.3 92.3 94.4	123.7 122.2 120.6 119.0 117.3	90.9 93.0 95.0	123.0 121.4 119.8 118.1	89.3 91.5 93.6 95.7	122.2 120.6 118.9	96.3	126.1 124.6 123.0 121.4 119.7	90.5 92.7 94.8 96.9	127.0 125.4 123.8 \$22.1 120.5	88.9 91.1 93.3 95.4 97.5	55 54 53 52 51
42 43 44	107.2	97.8 99. 7 101.6 103.5	114.9 113.2 111.5 109.7 107.9	98.4 100.4 102.3 104.2	112.2 110.4 108.6	99.1 101.0 103.0 104.9	111.2	99.7 101.7 103.7 105.6	113.7 111.9 110.1	100.4 102.4 104.3 106.3	114.4 112.6 110.8	101.0 103.0 105.0 107.0	115.2 113.4 111.5	101.7 103.7 105.7 107.7	48 47 46
45	105.4		106.1	-			107.5			108.2		_	109.6		45
Course.	DEP.	149'	DEP.	150'		151'	DEP.	152'	DEP.	153'	DEP.	154'	DEP.	155'	Course.

					Pla	ane '	Trav	erse	Tat	ole					
Course.	D=	156′	D=	157′	D=	158′	D =	159′	D=	160′	D=	161′	D=	162'	Course.
Con	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	Cot
° 0 1 2 3 4	156.0 156.0 155.9 155.8 155.6	2.7 5.4 8.2	157.0 157.0 156.9 156.8 156.6	2.7 5.5 8.2	158.0 158.0 157.9 157.8 157.6	2.8 5.5 8.3	159.0 159.0 158.9 158.8 158.6	, 0.0 2.8 5.5 8.3 11.1	160.0 160.0 159.9 159.8 159.6	0.0 2.8 5.6 8.4 11.2	161.0 161.0 160.9 160.8 160.6	2.8		0.0 2.8 5.7 8.5 11.3	90 89 88 87 86
5 6 7 8 9	155.4 155.1 154.8 154.5 154.1	16.3 19.0 21.7 24.4	156.4 156.1 155.8 155.5 155.1	19.1 21.9 24.6	157.4 157.1 156.8 156.5 156.1	16.5 19.3 22.0 24.7	158.4 158.1 157.8 157.5 157.0	13.9 16.6 19.4 22.1 24.9	159.4 159.1 158.8 158.4 158.0	13.9 16.7 19.5 22.3 25.0	160.4 160.1 159.8 159.4 159.0	16.8 19.6 22.4 25.2	160.0	14.1 16.9 19.7 22.5 25.3	85 84 83 82 81
10 11 12 13 14	153.6 153.1 152.6 152.0 151.4	29.8 32.4 35.1	154.6 154.1 153.6 153.0 152.3	30.0 32.6 35.3 38.0	155.6 155.1 154.5 154.0 153.3	27.4 30.1 32.9 35.5 38.2	156.1 155.5 154.9 154.3	27.6 30.3 33.1 35.8 38.5	157.6 157.1 156.5 155.9 155.2	27.8 30.5 33.3 36.0 38.7	158.6 158.0 157.5 156.9 156.2	3°.7 33.5 36.2 38.9	159.5 159.0 158.5 157.8 157.2	28.1 30.9 33.7 36.4 39.2	80 79 78 77 76 75
15 16 17 18 19	150.7 150.0 149.2 148.4 147.5	43.0 45.6 48.2 50.8	150.9 150.1 149.3 148.4	43·3 45·9 48·5 51·1	151.9 151.1 150.3 149.4	43.6 46.2 48.8 51.4	152.8 152.1 151.2	43.8 46.5 49.1 51.8	153.8 153.0 152.2 151.3	44.1 46.8 49.4 52.1	154.8 154.0 153.1 152.2	44.4 47.1 49.8 52.4	150.5 155.7 154.9 154.1 153.2	41.9 44.7 47.4 50.1 52.7	73 74 73 72 71
21 22 23 24	145.6 144.6 143.6 142.5	55.9 58.4 61.0 63.5	146.6 145.6 144.5 143.4	56.3 58.8 61.3 63.9	147.5 146.5 145.4 144.3	56.6	148.4 147.4 146.4 145.3	57.0 59.6 62.1 64.7	149.4 148.3	57·3 59·9 62.5 65.1	150.3 149.3 148.2 147.1	57.7 60.3 62.9 65.5	151.2 150.2 149.1 148.0	58.1 60.7 63.3 65.9	69 68 67 66 65
25 26 27 28 29	141.4 140.2 139.0 137.7 136.4	68.4 70.8 73.2 75.6	142.3 141.1 139.9 138.6 137.3	68.8 71.3 73.7 76.1	142.0 140.8 139.5 138.2	69.3 71.7 74.2 76.6	142.9 141.7 140.4 139.1	69.7 72.2 74.6 77.1	143.8 142.6 141.3 139.9	70.1 72.6 75.1 77.6	144.7 143.5 142.2 140.8	70.6 73.1 75.6 78.1	145.6 144.3 143.0 141.7	71.0 73.5 76.1 78.5	64 63 62 61
30 31 32 33 34	135.1 133.7 132.3 130.8 129.3	80.3 82.7 85.0 87.2	136.0 134.6 133.1 131.7 130.2	80.9 83.2 85.5 87.8	131.0	86.1 88.4	136.3 134.8 133.3 131.8	84.3 86.6 88.9	132.6	82.4 84.8 87.1 89.5	139.4 138.0 136.5 135.0 133.5	82.9 85.3 87.7 90.0	140.3 138.9 137.4 135.9 134.3	85.8 88.2 90.6	60 59 58 57 56
35 36 37 38 39	127.8 126.2 124.6 122.9 121.2	91.7 93.9 96.0 98.2	128.6 127.0 125.4 123.7 122.0	92.3 94.5 96.7 98.8	129.4 127.8 126.2 124.5 122.8	90.6 92.9 95.1 97.3 99.4	128.6 127.0 125.3 123.6	93.5 95.7 97.9 100.1	129.4 127.8 126.1 124.3	94.0 96.3 98.5		94.6 96.9 99.1		95.2 97.5 99.7 101.9	54 53 52 51
40 41 42 43 44	117.7 115.9 114.1 112.2	102.3 104.4 106.4 108.4	118.5 116.7 114.8 112.9	103.0 105.1 107.1 109.1	121.0 119.2 117.4 115.6 113.7	103. 7 105.7 107.8 109.8	120.0 118.2 116.3 114.4	104.3 106.4 108.4 110.5	120.8 118.9 117.0 115.1	105.0 107.1 109.1 111.1	121.5 119.6 117.7 115.8	105.6	122.3 120.4 118.5 116.5	108.4 110.5 112.5	49 48 47 46
45	-		-	-	111.7			112.4	-	113.1	-			114.6	
Course.	DET.	LAT.	_	LAT.	DEP.	LAT.	D_{EP}	159'	DEP.	LAT. = 160'	D_{EP}	LAT.	-	LAT.	Course.

					Pl	ane	Trav	erse	Tal	ole					
rse.	D=	163′	D=	164′	D=	165′	D=	166′	D=	167′	D=	168′	D=	169′	Course.
Course.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	163.0 163.0 162.9 162.8 162.6	2.8 5·7 8.5	164.0 164.0 163.9 163.8 163.6	2.9 5.7 8.6	165.0 165.0 164.9 164.8 164.6	5.8 8.6	166.0 165.9 165.8	0.0 2.9 5.8 8.7 11.6	167.0 167.0 166.9 166.8 166.6	2.9 5.8 8.7	168.0 168.0 167.9 167.8 167.6	2.9 5.9 8.8	169.0 169.0 168.9 168.8 168.6	0.0 2.9 5.9 8.8 11.8	90 89 88 87 86
5 6 7 8 9	162.4 162.1 161.8 161.4 161.0	17.0 19.9 22.7 25.5	163.4 163.1 162.8 162.4 162.0	17.1 20.0 22.8 25.7	164.4 164.1 163.8 163.4 163.0	23.0 25.8	164.8 164.4 164.0	14.5 17.4 20.2 23.1 26.0	166.4 166.1 165.8 165.4 164.9	17.5 20.4 23.2 26.1	167.4 167.1 166.7 166.4 165.9	17.6 20.5 23.4 26.3	168.4 168.1 167.7 167.4 166.9	14.7 17.7 20.6 23.5 26.4	85 84 83 82 81
10 11 12 13 14	160.5 160.0 159.4 158.8 158.2	31.1 33.9 36.7 39.4		31.3 34.1 36.9 39.7	162.5 162.0 161.4 160.8 160.1	28.7 31.5 34.3 37.1 39.9	163.0 162.4 161.7 161.1	28.8 31.7 34.5 37.3 40.2	164.5 163.9 163.4 162.7 162.0	31.9 34.7 37.6 40.4	165.4 164.9 164.3 163.7 163.0	34.9 37.8 40.6	166.4 165.9 165.3 164.7 164.0	29.3 32.2 35.1 38.0 40.9	80 79 78 77 76
15 16 17 18 19	156.7 155.9 155.0 154.1	47·7 50·4 53·1	157.6 156.8 156.0 155.1	45·2 47·9 50·7 53·4	158.6 157.8 156.9 156.0	45.5 48.2 51.0 53.7	159.6 158.7 157.9 157.0	43.0 45.8 48.5 51.3 54.0	160.5 159.7 158.8 157.9	46.0 48.8 51.6 54.4	161.5 160.7 159.8 158.8	46.3 49.1 51.9 54.7	162.5 161.6 160.7 159.8	43.7 46.6 49.4 52.2 55.0	75 74 73 72 71
20 21 22 23 24	153.2 152.2 151.1 150.0 148.9	58.4 61.1 63.7 66.3	154.1 153.1 152.1 151.0 149.8	58.8 61.4 64.1 66.7	155.0 154.0 153.0 151.9 150.7	56.4 59.1 61.8 64.5 67.1	155.0 153.9 152.8 151.6	56.8 59.5 62.2 64.9 67.5	152.6	59.8 62.6 65.3 67.9	157.9 156.8 155.8 154.6 153.5	60.2 62.9 65.6 68.3	158.8 157.8 156.7 155.6 154.4	57.8 60.6 63.3 66.0 68.7	70 69 68 67 66
25 26 27 28 29	147.7 146.5 145.2 143.9 142.6	71.5 74.0 76.5 79.0	148.6 147.4 146.1 144.8 143.4	71.9 74.5 77.0 79.5	149.5 148.3 147.0 145.7 144.3	69.7 72.3 74.9 77.5 80.0	149.2 147.9 146.6 145.2	77·9 80.5	148.8 147.5 146.1	73.2 75.8 78.4 81.0	149.7 148.3 146.9	73.6 76.3 78.9 81.4	153.2 151.9 150.6 149.2 147.8	71.4 74.1 76.7 79.3 81.9	65 64 63 62 61
30 31 32 33 34	141.2 139.7 138.2 136.7 135.1	84.0 86.4 88.8	142.0 140.6 139.1 137.5 136.0	84.5 86.9 89.3 91.7	142.9 141.4 139.9 138.4 136.8	92.3	142.3 140.8 139.2 137.6	85.5 88.0 90.4 92.8	144.6 143.1 141.6 140.1 138.4	86.0 88.5 91.0 93.4	145.5 144.0 142.5 140.9 139.3	86.5 89.0 91.5 93.9	146.4 144.9 143.3 141.7 140.1	84.5 87.0 89.6 92.0 94.5	59 58 57 56
35 36 37 38 39	126.7	95.8 98.1 100.4 102.6	134.3 132.7 131.0 129.2 127.5	96.4 98.7 101.0 103.2	128.2	97.0 99.3 101.6 103.8	134.3 132.6 130.8 129.0	97.6 99.9 102.2 104.5	129.8	98.2 100.5 102.8 105.1	137.6 135.9 134.2 132.4 130.6	98.7 101.1 103.4 105.7	133.2	104.0	51
42 43 44	123.0 121.1 119.2 117.3	106.9	123.8 121.9 119.9 118.0	107.6 109.7 111.8 113.9	124.5 122.6 120.7 118.7	108.2 110.4 112.5 114.6	125.3 123.4 121.4 119.4	108.9 111.1 113.2 115.3	126.0 124.1 122.1 120.1	109.6 111.7 113.9 116.0	126.8 124.8 122.9 120.8	110.2 112.4 114.6 116.7	127.5 125.6 123.6 121.6		49 48 47 46
45	115.3	=	116.0					117.4		-	-			119.5	45
Course.	DEP.	163'	DEP.	LAT.	-	LAT.	DEP.	166'	DEP.	167'	$D_{\rm EP}$.	168'	DEP.	169'	Course.

					Pl	ane	Trav	erse	Tab	ole					
Course.	D=	170′	D=	171′	D=	172′	D=	173′	D=	174′	D=	175′	D=	176′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0	170.0	0.0	171.0	0.0	172.0	0.0	173.0	0.0	174.0	0.0	175.0	0,0	176.0	0.0	° 90
I 2	170.0	3.0	171.0	3.0	172.0	3.0 6.0	173.0	3.0 6.0	174.0	3.0	175.0	3.1	176.0	3.I 6.1	89 88
3	169.8	8.9	170.8	8.9	171.8	9.0	172.8	9.1	173.8	9.1	174.8	9.2	175.8	9.2	87
4	169.4	14.8	170.6		171.6	12.0	172.6	12.1	173.6	12.1	174.6	15.3	175.6	12.3	86 85
5	169.1	17.8	170.1	17.9	171.1	18.0	172.1	18.1	173.0	18.2	174.0	18.3	175.0	18.4	84
7 8	168.7	23.7	169.7	23.8	170.7	23.9	171.7	21.1	172.7		173.7		174.7 174.3	21.4	83 82
9	167.9		168.9	26.8	169.9	26.9	170.9	27.1	171.9	27.2	172.8		173.8	27.5	81
10	167.4	29.5 32.4	167.9	32.6	169.4	29.9 32.8	170.4	30.0	171.4	33.2	172.3 171.8	33.4		30.6 33.6	80 79 78
12	166.3 165.6	35·3 38·2	167.3 166.6	35.6 38.5	168.2 167.6	35.8 38.7	169.2 168.6	36.0 38.9	170.2		171.2		172.2	36.6 39.6	78 77
14	165.0		165.9	41.4	166.9	41.6	167.9	41.9	168.8	42.1	169.8	42.3	170.8	42.6	77 76
15	164.2		165.2	44·3 47·1		44·5 47·4	166.3	44.8 47.7	168.1		169.0	45.3 48.2	170.0	45.6	75 74
17	162.6 161.7		163.5 162.6	50.0	164.5	50.3 53.2	165.4 164.5	50.6 53.5	166.4	50.9	167.4 166.4	51.2	168.3 167.4	51.5	73 72
19	160.7		161.7		162.6	56.0	163.6	56.3	164.5		165.5	57.0		57.3	71
20 2I	159.7		160.7 159.6		161.6 160.6	58.8 61.6	162.6 161.5	59.2 62.0	163.5 162.4		164.4		165.4 164.3	60.2 63.1	70 69
22	157.6	63.7	158.5	64.1	159.5	64.4	160.4	64.8	161.3	65.2	162.3	65.6	163.2	65.9 68.8	68
23 24	156.5		157.4 156.2		158.3 157.1	70.0	159.2 158.0	67.6	160.2 159.0		161.1 159.9	68.4 71.2	162.0 160.8	71.6	67 66
25 26	154.1		155.0		155.9	72.7	156.8	73.1	157.7		158.6		159.5	74-4	65
27	152.8	77.2	153.7 152.4	77.6	154.6	75.4 78.1		75.8 78.5	156.4	79.0	157.3 155.9		156.8	77.2	64 63
28 29	150.1		151.0 149.6		151.9	80.7 83.4	152.7 151.3	81.2	153.6		154.5	82.2	155.4	82.6 85.3	62 61
30	147.2	85.0	148.1		149.0	86.0	149.8	86.5	150.7	87.0		87.5		88.0	60
3 ¹ 3 ²	145.7 144.2		146.6		147.4	88.6		89.1	149.1		150.0		150.9	90.6	59 58
33 34	142.6	-	143.4 141.8		144.3	93.7 96.2	145.1 143.4	94.2	145.9 144.3		146.8 145.1	95·3 97·9		95.9 98.4	57 56
	139.3		140.1		140.9		141.7	99.2			143.4			100.9	55
35 36 37	137.5		138.3 136.6		139.2		140.0	101.7	140.8		141.6		142.4 140.6		54 53
38	134.0	104.7	I34.7	105.3	135.5	105.9	136.3	106.5	137.1	107.1	137.9	107.7	138.7	108.4	52
39			132.9			108.2			135.2		136.0		136.8		51 50
	128.3	111.5	129.1	112.2	129.8	112.8	130.6	113.5	131.3	114.2	132.1	114.8	132.8	115.5	49
42	124.3	115.9	127.1 125.1	116.6	125.8	117.3	126.5	118.0		118.7	128.0	119.3	128.7	120.0	48 47 46
44	122.3	118.1	123.0	118.8	123.7	119.5	124.4	120.2	125.2	120.9			126.6		
45	120.2	120.2	120.9	120.9	121.0	121.6	122.3	122.3	123.0	123.0	123.7	123.7	124.5	124-5	45
Course.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	Course.
Cou	D=	DEP. LAT. DEP. LAT. DEP. LAT. DEP. LAT.			D =	172'	D =	173′	D=	174′	D=	175′	D=	176′	Cor

	`				Pl	ane	Trav	rerse	Tal	ble					
Course.	D=	177′	D=	178′	D=	179′	D=	180′	D=	181'	D=	182′	D=	183′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	177.0 177.0 176.9 176.8 176.6	0.0 3.1 6.2 9.3 12.3	178.0 178.0 177.9 177.8 177.6	0.0 3.1 6.2 9.3 12.4	179.0 179.0 178.9 178.8 178.6	0.0 3.1 6.2 9.4 12.5	180.0 180.0 179.9 179.8 179.6	0.0 3.1 6.3 9.4 12.6	181.0 181.0 180.9 180.8 180.6	3.2 6.3 9.5	182.0 182.0 181.9 181.8 181.6	3.2 6.4 9.5	183.0 183.0 182.9 182.7 182.6	, 0.0 3.2 6.4 9.6 12.8	90 89 88 87 86
56 78 9	176.3 176.0 175.7 175.3 174.8	15.4 18.5 21.6 24.6 27.7	177.3 177.0 176.7 176.3 175.8		178.3 178.0 177.7 177.3 176.8	15.6 18.7 21.8 24.9 28.0	179.3 179.0 178.7 178.2 177.8	15.7 18.8 21.9 25.1 28.2		18.9 22.1	181.3 181.0 180.6 180.2 179.8	19.0 22.2 25.3	182.3 182.0 181.6 181.2 180.7	15.9 19.1 22.3 25.5 28.6	85 84 83 82 81
10 11 12 13 14	174.3 173.7 173.1 172.5 171.7	39.8 42.8	175.3 174.7 174.1 173.4 172.7	34.0 37.0 40.0 43.1	176.3 175.7 175.1 174.4 173.7	31.1 34.2 37.2 40.3 43.3	176.1 175.4 174.7	31.3 34.3 37.4 40.5 43.5	177.7 177.0 176.4 175.6	4°.7 43.8	176.6	34.7 37.8 40.9 44.0	180.2 179.6 179.0 178.3 177.6	31.8 34.9 38.0 41.2 44.3	80 79 78 77 76
15 16 17 18 19	171.0 170.1 169.3 168.3 167.4	48.8 51.7 54.7 57.6	171.9 171.1 170.2 169.3 168.3	49.1 52.0 55.0 58.0	172.9 172.1 171.2 170.2 169.2	46.3 49.3 52.3 55.3 58.3	173.0 172.1 171.2 170.2	52.6 55.6 58.6	174.0 173.1 172.1 171.1	49.9 52.9 55.9 58.9	172.1	50.2 53.2 56.2 59.3	176.8 175.9 175.0 174.0 173.0	47.4 50.4 53.5 56.6 59.6	75 74 73 72 71
20 21 22 23 24	166.3 165.2 164.1 162.9 161.7	63.4 66.3 69.2 72.0	167.3 166.2 165.0 163.8 162.6	63.8 66.7 69.6 72.4	168.2 167.1 166.0 164.8 163.5	61.2 64.1 67.1 69.9 72.8	165.7 164.4	70.3 73.2	167.8 166.6 165.4	64.9 67.8 70.7 73.6	169.9 168.7 167.5 166.3	65.2 68.2 71.1 74.0	172.0 170.8 169.7 168.5 167.2	65.6 68.6 71.5 74.4	70 69 68 67 66
25 26 27 28 29	160.4 159.1 157.7 156.3 154.8	80.4 83.1 85.8	160.0 158.6 157.2 155.7	78.0 80.8 83.6 86.3	162.2 160.9 159.5 158.0 156.6	75.6 78.5 81.3 84.0 86.8	160.4 158.9 157.4	81.7 84.5 87.3	162.7 161.3 159.8 158.3	79.3 82.2 85.0 87.8	160.7 159.2	79.8 82.6 85.4 88.2	165.9 164.5 163.1 161.6 160.1	77·3 80.2 83·1 85·9 88·7	65 64 63 62 61
30 31 32 33 34	153.3 151.7 150.1 148.4 146.7	91.2 93.8 96.4 99.0	154.2 152.6 151.0 149.3 147.6	91.7 94.3 96.9 99.5	155.0 153.4 151.8 150.1 148.4	100.1	152.6 151.0 149.2	92.7 95.4 98.0	153.5 151.8 150.1	93.2 95.9 98.6 101.2	157.6 156.0 154.3 152.6 150.9	93.7 96.4 99.1 101.8	158.5 156.9 155.2 153.5 151.7	91.5 94.3 97.0 99.7 102.3	59 58 57 56
35 36 37 38 39	139.5	104.0 106.5 109.0	145.8 144.0 142.2 140.3 138.3	104.6 107.1 109.6 112.0	144.8 143.0 141.1 139.1	105.2 107.7 110.2 112.6	145.6 143.8 141.8 139.9	105.8 108.3 110.8 113.3	146.4 144.6 142.6 140.7	106.4 108.9 111.4 113.9	143.4 141.4	107.0 109.5 112.1 114.5	148.1 146.2 144.2 142.2	112.7	55 54 53 52 51
40 41 42 43 44	133.6 131.5 129.4 127.3	116.1 118.4 120.7 123.0	134.3 132.3 130.2 128.0	116.8 119.1 121.4 123.6	135.1 133.0 130.9 128.8	117.4 119.8 122.1 124.3	135.8 133.8 131.6 129.5	118.1 120.4 122.8 125.0	138.7 136.6 134.5 132.4 130.2	118.7 121.1 123.4 125.7	137.4 135.3 133.1 130.9	119.4 121.8 124.1 126.4	138.1 136.0 133.8 131.6	120.1 122.5 124.8 127.1	48 47 46
45	DEP.	LAT.		LAT.	DEP.		DEP.	LAT.		LAT.	DEP.	LAT.	DEP.	LAT.	45 ——
Course.		177′	-	178′		179′	-	180′	_	181'	_	182′		183′	Course.

Plane Traverse Table D = 187'Course. Course D = 184'D = 185'D = 186'D = 188'D = 180'D = 190'LAT. DEP. LAT. DEP. LAT. DEP. LAT. DEB LAT. DEP. DEP. LAT. DEP. T.AT 0 185.0 186.0 187.0 188.0 184.0 0.0 0.0 0.0 0.0 0.0 189.0 0.0 190.0 0.0 90 89 88 3.2 185.0 184.0 186.0 187.0 188.0 3.3 190.0 6.6 189.9 3.2 3·3 6.6 1 3.2 3.3 3.3 189.0 183.9 185.9 6.5 187.9 188.9 6.4 184.9 6.5 6.5 186.9 6.6 2 183.7 9.6 184.7 185.7 186.7 188.7 9.9 189.7 3 9.7 9.7 187.7 9.8 9.9 87 183.6 185.5 12.8 184.5 186.5 13.2 189.5 12.9 13.0 13.0 187.5 13.1 188.5 13.3 86 4 183.3 185.3 85 16.0 184.3 16.2 186.3 16.3 16.5 189.3 16.6 16.1 187.3 16.4 188.3 5 183.0 187.0 19.3 185.0 19.7 188.0 19.2 184.0 19.4 186.0 19.5 19.8 189.0 19.9 84 83 22.9 187.6 26.2 187.2 78 182.6 22.4 183.6 25.6 183.2 184.6 184.2 185.6 186.6 23.0 188.6 22.5 22.7 23.2 185.2 182.2 26.0 186.2 26.3 188.2 25.7 25.9 26.4 82 28.9 183.7 184.7 181.7 28.8 182.7 29.6 187.7 185.7 29.4 186.7 29.7 9 29.I 29.3 81 185.1 181.2 32.0 182.2 32.1 183.2 184.2 32.6 186.1 32.8 187.1 10 32.3 32.5 33.0 80 180.6 35.1 181.6 35.3 182.6 184.5 36.3 35·5 38·7 183.6 36.1 186.5 ΙI 35.7 35.9 185.5 79 38.3 181.0 182.9 183.9 39.3 185.8 180.0 38.5 181.9 38.9 39.1 184.9 39.5 78 12 41.6 181.2 41.8 42.1 183.2 179.3 41.4 180.3 182.2 42.3 184.2 42.5 185.1 42.7 77 76 13 44.8 180.5 45.7 184.4 181.4 182.4 45.5 183.4 46.0 14 178.5 44.5 179.5 45.0 45.2 48.7 182.6 51.8 181.7 47.6 178.7 179.7 178.8 48.1 180.6 48.4 181.6 48.9 183.5 49.2 15 47.9 75 177.8 51.5 180.7 16 176.9 50.7 51.0 51.3 179.8 52.I 182.6 52.4 74 55.3 181.7 58.4 180.7 178.8 53.8 176.9 54.1 177.9 54·7 57.8 179.8 55.0 180.7 55.6 73 72 17 18 176.0 54.4 57.2 176.9 178.8 58.1 179.7 58.7 56.9 175.9 177.8 175.0 57-5 60.2 175.9 60.6 176.8 19 59.9 174.9 60.9 177.8 61.2 178.7 61.5 179.6 61.9 174.0 71 20 172.9 62.9 173.8 63.3 174.8 63.6 175.7 64.0 176.7 64.3 177.6 64.6 178.5 65.0 70 69 68.ı 171.8 65.9 172.7 66.3 173.6 66.7 174.6 67.0 175.5 67.4 176.4 67.7 177.4 21 69.7 70.8 170.6 68.9 171.5 69.3 172.5 70.1 70.4 175.2 176.2 71.2 173.4 174.3 22 169.4 71.9 170.3 72.7 73.8 74.2 67 23 72.3 171.2 172.1 73.1 173.1 73.5 174.0 174.9 75.2 169.9 168.1 74.8 169.0 170.8 66 24 75.7 76.1 171.7 76.5 172.7 76.9 173.6 77.3 77.8 167.7 80.7 166.3 78.6 81.5 79.9 172.2 82.9 170.8 85.8 169.3 80.3 166.8 78.2 168.6 65 25 169.5 79.0 170.4 79.5 171.3 82.4 169.9 83.3 81.1 167.2 82.0 169.0 168.1 26 165.4 64 163.9 167.5 86.3 63 83.5 164.8 84.0 165.7 84.4 84.9 166.6 85.4 168.4 27 88.7 167.8 28 162.5 86.4 163.3 86.9 164.2 87.3 165.1 87.8 166.0 88.3 166.9 89.2 62 164.4 160.9 89.2 161.8 89.7 162.7 163.6 91.1 165.3 91.6 166.2 92.1 20 90.2 90.7 61 92.0 160.2 92.5 161.1 162.8 161.9 94.0 163.7 94.5 164.5 60 95.0 30 159.3 93.0 93.5 157.7 94.8 158.6 95.3 159.4 156.0 97.5 156.9 98.0 157.7 154.3 100.2 155.2 100.8 156.0 96.8 **162.0** 99.6 **160.3** 95.8 160.3 97.3 162.9 96.3 161.1 97.9 31 59 58 98.6 161.1 32 158.6 100.2 100.7 99.1 159.4 156.8 102.4 158.5 101.8 102.9 159.3 103.5 101.3 157.7 57 33 105.1 156.7 56 152.5 102.9 153.4 103.5 154.2 104.0 155.0 104.6 155.9 105.7 157.5 106.2 34 108.4 155.6 106.7 154.0 107.8 154.8 105.5 151.5 106.1 152.4 55 150.7 153.2 107.3 35 36 108.7 150.5 111.7 109.3 110.5 152.9 111.1 153.7 148.9 108.2 149.7 151.3 109.9 152.1 54 53 113.1 150.9 113.7 151.7 115.7 148.9 116.4 149.7 114.3 146.9 110.7 147.7 111.3 148.5 37 111.9 149.3 112.5 150.1 148.1 145.0 113.3 145.8 113.9 146.6 114.5 147.4 115.1 117.0 52 38 119.6 143.0 115.8 143.8 146.1 118.3 146.9 118.9 147.7 39 116.4 144.5 117.1 145.3 117.7 51 120.8 122.1 118.9 142.5 119.6 120.2 144.0 144.8 121.5 145.5 50 141.0 118.3 141.7 143.3 40 121.4 140.4 123.8 138.2 142.6 124.0 143.4 124.7 49 48 41 122.7 138.9 120.7 139.6 122.0 141.1 141.9 123.3 139.7 125.8 140.5 126.5 141.2 127.1 136.7 123.1 137.5 124.5 139.0 125.1 42 137.5 128.2 138.2 128.9 139.0 129.6 136.8 127.5 134.6 125.5 132.4 127.8 126.2 136.0 126.9 47 135.3 43 128.5 133.8 132.0 129.9 135.2 130.6 136.0 131.3 136.7 133.1 129.2 134.5 46 44 130.8 130.8 133.6 133.6 134.4 134.4 45 130.1 130.1 131.5 131.5 132.2 132.2 132.9 132.9 45 DEP. Course. DEP. DEP. LAT. DEP. LAT. DEP. LAT. DEP. LAT. DEP. LAT. LAT. Course. LAT. D = 184'D = 185'D = 186'D = 187'D = 188'D = 180'D = 190'

					Pl	ane	Trav	erse	Tal	ole					
Course.	D=	191′	D=	192'	D=	193′	D=	194′	D=	195′	D=	196′	D=	197′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	191.0 191.0 190.9 190.7 190.5	3·3 6·7	192.0 192.0 191.9 191.7	3.4 6.7 10.0	193.0 193.0 192.9 192.7 192.5	6.7 10.1 13.5	194.0 194.0 193.9 193.7 193.5	0.0 3.4 6.8 10.2 13.5	195.0 195.0 194.9 194.7 194.5	0.0 3.4 6.8 10.2 13.6	196.0 196.0 195.9 195.7 195.5	3.4 6.8 10.3	197.0 197.0 196.9 196.7 196.5	6.9 10.3 13.7	90 89 88 87 86
5 6 7 8 9	190.3 190.0 189.6 189.1 188.6	23.3 26.6 29.9	190.9 190.6 190.1 189.6	23.4 26.7 30.0	192.3 191.9 191.6 191.1 190.6	23.5 26.9 30.2	192.1 191.6	16.9 20.3 23.6 27.0 30.3	194.3 193.9 193.5 193.1 192.6	27.1 3°·5	195.3 194.9 194.5 194.1 193.6	17.1 20.5 23.9 27.3 30.7	196.3 195.9 195.5 195.1 194.6	17.2 20.6 24.0 27.4 30.8	85 84 83 82 81
10 11 12 13 14	188.1 187.5 186.8 186.1 185.3	36.4 39.7 43.0 46.2	189.1 188.5 187.8 187.1 186.3	39.9 43.2 46.4	190.1 189.5 188.8 188.1 187.3	33.5 36.8 40.1 43.4 46.7	189.0 188.2	33.7 37.0 40.3 43.6 46.9	190.7	37.2 40.5 43.9 47.2	193.0 192.4 191.7 191.0 190.2	34.0 37.4 40.8 44.1 47.4	194.0 193.4 192.7 192.0 191.1	34.2 37.6 41.0 44.3 47.7	80 79 78 77 76
15 16 17 18 19	183.6 182.7 181.7 180.6	52.6 55.8 59.0 62.2	184.6 183.6 182.6 181.5	52.9 56.1 59.3 62.5	185.5 184.6 183.6 182.5	53.2 56.4	186.5 185.5 184.5 183.4	53.5 56.7 59.9 63.2	187.4 186.5 185.5 184.4	53.7 57.0 60.3 63.5		50.7 54.0 57.3 60.6 63.8	189.4 188.4 187.4 186.3	54.3 57.6 60.9 64.1	75 74 73 72 71 70
21 22 23 24	178.3 177.1 175.8 174.5	68.4 71.5 74.6 77.7	179.2 178.0 176.7 175.4	68.8 71.9 75.0 78.1	180.2 178.9 177.7 176.3	69.2 72.3 75.4 78.5	181.1 179.9 178.6 177.2	69.5 72.7 75.8 78.9 82.0	182.0 180.8 179.5 178.1	69.9 73.0 76.2 79.3	183.0 181.7 180.4 179.1	70.2 73.4 76.6 79.7 82.8	183.9 182.7 181.3 180.0	70.6 73.8 77.0 80.1	69 68 67 66
25 26 27 28 29	173.1 171.7 170.2 168.6 167.1	83.7 86.7 89.7 92.6	172.6 171.1 169.5 167.9	84.2 87.2 90.1 93.1	173.5 172.0 170.4 168.8	84.6 87.6 90.6 93.6	174.4 172.9 171.3 169.7	85.0 88.1 91.1 94.1	175.3 173.7 172.2 170.6	85.5 88.5 91.5 94.5	176.2 174.6 173.1 171.4	85.9 89.0 92.0 95.0	177.1 175.5 173.9 172.3	86.4 89.4 92.5 95.5	64 63 62 61
30 31 32 33 34	160.2 158.3	98.4. 101.2 104.0 106.8	166.3 164.6 162.8 161.0 159.2	98.9 101.7 104.6 107.4	161.9 160.0	102.3	164.5 162.7 160.8	102.8 105.7 108.5	165.4 163.5 161.7	100.4 103.3 106.2 109.0	164.4 162.5	103.9	165.2 163.3	104.4	58 57 56
35 36 37 38 39	154.4 152.5 150.5 148.4	112.3 114.9 117.6 120.2	157.3 155.3 153.3 151.3 149.2	112.9 115.5 118.2 120.8	156.1 154.1 152.1 150.0	113.4 116.2 118.8 121.5	156.9 154.9 152.9 150.8	114.0 116.8 119.4 122.1	153.7	114.6 117.4 120.1 122.7	158.6 156.5 154.5 152.3	112.4 115.2 118.0 120.7 123.3	159.4 157.3 155.2 153.1	115.8 118.6 121.3 124.0	54 53 52 51
40 41 42 43 44 45	144.1 141.9 139.7 137.4	125.3 127.8 130.3 132.7	147.1 144.9 142.7 140.4 138.1	126.0 128.5 130.9 133.4	145.7 143.4 141.2 138.8	126.6 129. 1 131.6	146.4 144.2 141.9 139.6	127.3	147.2 144.9 142.6 140.3	127.9 130.5 133.0 135.5	147.9 145.7 143.3 141.0	128.6	148.7 146.4 144.1 141.7	129.2 131.8 134.4 136.8	49 48 47
	DEP.		DEP.		DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	
Course.		191′	D=	192'		193′	-	194'	D=	195′	D=	196′		197′	Course.

					Pla	ane '	Trav	erse	Tab	ole					
Course.	D=	198′	D =	199′	D=	200′	D=	201'	D=	202'	D=	203′	D=	204′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3	198.0 198.0 197.9	3·5 6.9	199.0 199.0 198.9 198.7	3·5 6.9	200.0 200.0 199.9	0.0 3.5 7.0 10.5	200.9	0.0 3.5 7.0 10.5	202.0 202.0 201.9 201.7	3·5 7·0	203.0 203.0 202.9 202.7	3·5 7·1	204.0 204.0 203.9 203.7	0.0 3.6 7.1 10.7	90 89 88 87
5 6	197.5	17.3	198.5	17.3	199.5	17.4		17.5	201.5	17.6	202.5	17.7	203.5	14.2	86
6 7 8 9	196.9 196.5 196.1 195.6	20.7 24.1 27.6 31.0	197.9 197.5 197.1 196.5	20.8 24.3 27.7 31.1	198.9 198.5 198.1 197.5	20.9 24.4 27.8 31.3	199.9 199.5 199.0 198.5	21.0 24.5 28.0 31.4	200.9 200.5 200.0 199.5	28.1	201.9 201.5 201.0 200.5	28.3	202.9 202.5 202.0 201.5	21.3 24.9 28.4 31.9	84 83 82 81
10 11 12 13 14	195.0 194.4 193.7 192.9 192.1	34·4 37·8 41·2 44·5 47·9	196.0 195.3 194.7 193.9		197.0 196.3 195.6 194.9 194.1	34.7 38.2 41.6 45.0 48.4	196.6 195.8	34.9 38.4 41.8 45.2 48.6	198.9 198.3 197.6 196.8 196.0	42.0 45.4	199.9 199.3 198.6 197.8 197.0	38.7 42.2 45.7	200.9 200.3 199.5 198.8	35·4 38·9 42·4 45·9 49·4	80 79 78 77 76
15 16 17 18	191.3 190.3 189.3 188.3 187.2	54.6 57.9	192.2 191.3 190.3 189.3 188.2	58.2 61.5	193.2 192.3 191.3 190.2 189.1	51.8 55.1 58.5 61.8 65.1	193.2 192.2 191.2	52.0 55.4 58.8 62.1 65.4	194.2 193.2	55.7 59.1 62.4		56.0 59.4 62.7	197.0 196.1 195.1 194.0 192.9	52.8 56.2 59.6 63.0 66.4	75 74 73 72 71
20 21 22 23 24	186.1 184.8 183.6 182.3 180.9	67.7 71.0 74.2 77.4 80.5	187.0 185.8 184.5 183.2 181.8	74.5	186.7 185.4 184.1	68.4 71.7 74.9 78.1 81.3	187.6 186.4	68.7 72.0 75.3 78.5 81.8	189.8 188.6 187.3 185.9 184.5	72.4 75.7 78.9	190.8 189.5 188.2 186.9 185.4	72.7 76.0 79.3	191.7 190.5 189.1 187.8 186.4	69.8 73.1 76.4 79.7 83.0	70 69 68 67 66
25 26 27 28 29	179.4 178.0 176.4 174.8 173.2	93.0	180.4 178.9 177.3 175.7 174.0	84.1 87.2 90.3 93.4 96.5	179.8 178.2 176.6	84.5 87.7 90.8 93.9 97.0	177.5	84.9 88.1 91.3 94.4 97.4	183.1 181.6 180.0 178.4 176.7	88.6 91.7 94.8	184.0 182.5 180.9 179.2 177.5	89.0 92.2 95.3		86.2 89.4 92.6 95.8 98.9	62
30 31 32 33 34	171.5 169.7 167.9 166.1 164.1	99.0 102.0 104.9 107.8	168.8 166.9	102.5	169.6 167.7	103.0	172 3 170.5 168.6	103.5	173.1 171.3 169.4	104.0	172.2	104.6 107.6 110.6	176.7 174.9 173.0 171.1 169.1	108.1	59 58 57
35 36 37 38 39	162.2 160.2 158.1 156.0 153.9	116.4	161.0	117.0	159.7	117.6 120.4 123.1	162.6 160.5 158.4	121.0	163.4 161.3 159.2	118.7 121.6 124.4	164.2 162.1 160.0	119.3 122.2 125.0	167.1 165.0 162.9 160.8 158.5	119.9 122.8 125.6	54 53
40 41 42 43 44	149.4 147.1 144.8	129.9 132.5 135.0	150.2 147.9 145.5	130.6 133.2 135.7	150.9 148.6 146.3	131.2 133.8 136.4	151.7 149.4 147.0	131.9 134.5 137.1	154.7 152.5 150.1 147.7 145.3	132.5 135.2 137.8	153.2 150.9 148.5	133.2 135.8 138.4	154.0 151.6 149.2	133.8 136.5 139.1	49 48 47
45	140.0	140.0	140.7	140.7	141.4	141.4	142.1	142.1	142.8	142.8	143.5	143.5	144.2	144.2	45
Course.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	Course.
Cou	D=	198′	D=	199′	D =	200′	D=	201′	D=	202′	D=	203′	D=	204′	ပိ

					Pl	ane	Tra	verse	та Та	ble					
Course.	D=	205′	D=	206′	D=	207′	D=	208′	D=	209′	D=	210′	D=	211′	Course.
Co	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3	205.0 205.0 204.9 204.7 204.5	3.6 7.2 10.7	206.0 206.0 205.9 205.7 205.5	3.6 7.2 10.8	207.0 207.0 206.9 206.7 206.5	3.6 7.2 10.8	207.9 207.7	3.6 7·3 10.9	209.0 209.0 208.9 208.7 208.5	3.6 7·3 10.9	210.0 210.0 209.9 209.7 209.5	3.7 7.3 11.0	210.7	0.0 3.7 7.4 11.0	90 89 88 87
4 56 7 8 9	204.2 203.9 203.5 203.0 202.5	17.9 21.4 25.0 28.5	205.2 204.9 204.5 204.0 203.5	18.0 21.5 25.1 28.7	206.2 205.9 205.5 205.0 204.5	18.0 21.6 25.2 28.8	207.5 207.2 206.9 206.4 206.0 205.4	18.1 21.7 25.3 28.9	208.2 207.9 207.4 207.0 206.4	18.2 21.8 25.5 29.1	209.2 208.8 208.4 208.0 207.4	18.3 22.0 25.6	210.2 209.8 209.4 208.9	14.7 18.4 22.1 25.7 29.4 33.0	86 85 84 83 82 81
10 11 12 13 14	201.9 201.2 200.5 199.7 198.9	39.1 42.6 46.1	202.9 202.2 201.5 200.7 199.9	39·3 42.8 46.3	203.9 203.2 202.5 201.7 200.9	39·5 43·0 46.6	204.8 204.2 203.5 202.7 201.8	43.2 46.8	205.8 205.2 204.4 203.6 202.8	43.5 47.0	206.8 206.1 205.4 204.6 203.8		207.8 207.1 206.4 205.6 204.7	36.6 40.3 43.9 47.5 51.0	80 79 78 77 76
15 16 17 18 19	198.0 197.1 196.0 195.0 193.8	56.5 59.9 63.3 66.7	199.0 198.0 197.0 195.9 194.8	60.2 63.7 67.1	199.9 199.0 198.0 196.9 195.7	57.1 60.5 64.0 67.4	200.9 199.9 198.9 197.8 196.7	57·3 60.8 64.3 67·7	199.9 198.8 197.6	57.6 61.1 64.6 68.0	199.7 198.6	68.4	201.8 200.7 199.5	54.6 58.2 61.7 65.2 68.7	75 74 73 72 71
20 21 22 23 24	192.6 191.4 190.1 188.7 187.3	73.5 76.8 80.1 83.4	193.6 192.3 191.0 189.6 188.2	80.5 83.8	194.5 193.3 191.9 190.5 189.1	74.2 77.5 80.9 84.2	195.5 194.2 192.9 191.5	74·5 77·9 81.3 84.6	1 1	74.9 78.3 81.7 85.0	197.3 196.1 194.7 193.3 191.8	85.4	198.3 197.0 195.6 194.2 192.8	72.2 75.6 79.0 82.4 85.8	70 69 68 67 66
25 26 27 28 29	185.8 184.3 182.7 181.0	89.9 93.1 96.2 99.4	186.7 185.2 183.5 181.9 180.2	93·5 96·7 99·9		90.7 94.0 97.2 100.4	1	91.2 94.4 97.7 100.8		91.6 94.9 98.1 101.3	183.7	98.6	191.2 189.6 188.0 186.3 184.5	89.2 92.5 95.8 99.1 102.3	65 64 63 62 61
30 31 32 33 34	175.7 173.8 171.9 170.0	105.6 108.6 111.7 114.6	170.8	106.1 109.2 112.2 115.2	177.4 175.5 173.6 171.6	106.6 109.7 112.7 115.8	178.3 176.4 174.4 172.4	104.0 107.1 110.2 113.3 116.3	179.1 177.2 175.3 173.3	107.6 110.8 113.8 116.9	180.0 178.1 176.1 174.1	111.3 114.4 117.4	180.9 178.9 177.0 174.9	108.7 111.8 114.9	60 59 58 57 56
35 36 37 38 39	165.8 163.7 161.5 159.3	120.5 123.4 126.2 129.0	166.7 164.5 162.3 160.1	121.1 124.0 126.8 129.6	167.5 165.3 163.1 160.9	121.7 124.6 127.4 130.3	168.3 166.1 163.9 161.6	119.3 122.3 125.2 128.1 130.9	169.1 166.9 164.7 162.4	122.8 125.8 128.7 131.5	169.9 167.7 165.5 163.2	123.4 126.4 129.3 132.2	170.7 168.5 166.3 164.0	129.9	52 51
40 41 42 43 44 45	149.9	134.5 137.2 139.8 142.4	155.5 153.1 150.7 148.2	135.1 137.8 140.5 143.1	156.2 153.8 151.4 148.9	135.8 138.5 141.2 143.8	157.0 154.6 152.1 149.6	133.7 136.5 139.2 141.9 144.5	157.7 155.3 152.9 150.3	137.1 139.8 142.5 145.2	158.5 156.1 153.6 151.1	137.8 140.5 143.2 145.9	159.2 156.8 154.3 151.8	138.4 141.2 143.9 146.6	49 48 47 46
	DEP.	LAT.	DEP.	LAT.	DEP.		DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	 Lат.	45
Course.	D=			206′	D=			208′	D=		D=		D=	-	Course.

					Pl	ane	Trav	verse	Tai	ble					
Course.	D=	212′	D=	213′	D=	214′	D=	215′	D=	216′	D=	217′	D=	218′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0	212.0		213.0		214.0		215.0		216.0		217.0		218.0	0.0	9°
1 2 3	211.9 211.7		213.0 212.9 212.7	7.4	214.0 213.9 213.7	7.5	215.0	1 , -	215.9	7.5	217.0		217.9	7.6	
4	211.5	14.8	212.5	14.9	213.5	14.9	214.7 214.5		215.7 215.5		216.7 216.5		217.7 217.5	11.4	87 86
5 6	211.2	22.2	212.2 211.8	22.3	213.2 212.8	22.4	214.2 213.8	22.5	215.2 214.8	22.6	216.2 215.8	22.7	217.2 216.8	22.8	85 84
7 8	209.9	29.5	211.4	29.6	212.4	29.8	213.4	29.9	214.4 213.9	30.1	215.4 214.9	30.2	216.4 215.9		83 82
10	209.4		209.8		211.4		212.4	1	213.3	1	214.3		215.3	34.1	80 81
11	208.1	44.1	209.1 208.3	40.6	210.1	40.8	211.0 210.3	41.0	212.0	41.2	213.0	41.4 45.1	214.0 213.2	41.6	79 78
13 14	206.6		207.5 206.7		208.5 207.6		209.5 208.6		210.5 209.6		211.4 210.6		212.4 211.5	49.0 52.7	77 76
15 16	204.8 203.8		205.7 204.7	58.7	206.7		207.7 206.7		208.6 207.6	55·9 59·5	209.6 208.6	56.2 59.8	210.6 209.6	56.4 60.1	75 74
17 18	202.7 201.6	65.5	203.7 202.6	65.8	204.6 203.5	66.1	205.6 204.5	66.4	206.6 205.4	63.2	207.5 206.4	63.4 67.1	208.5	63.7 67.4	73 72
19	199.2		201.4	1	202.3	69.7	203.3	'	204.2	, ,	203.9		206.1	71.0	71
2I 22	197.9	76.0 79.4	198.9	76.3	199.8	76.7	200.7	77.0	201.7	77.4	202.6	77.8	203.5	78.1 81.7	70 69 68
23 24	195.1	82.8	196.1 194.6	83.2	197.0		197.9 196.4	84.0	198.8 197.3	84.4	199.7 198.2		200.7 199.2	85.2 88.7	67 66
25 26	192.1		193.0	90.0 93.4	193.9		194.9		195.8		196.7		197.6 195.9	92.1 95.6	65 64
27 28	188.9	96.2	189.8	96.7	190.7	97.2	191.6	97.6	192.5	98.1	193.3	98.5	194.2	99.0	63
29	185.4 183.6		186.3 184.5	103.3		103.7			188.9		189.8	105.2	190.7	105.7	61
30 31 32	181.7	109.2	182.6 180.6	109.7	185.3 183.4	110.2	184.3	110.7	187.1 185.1	111.2	187.9 186.0 184.0	111.8	186.9	112.3	59 58
33 34	177.8	115.5	178.6 176.6	116.0	179.5	116.6	180.3	117.1	181.2	117.6	182.0	118.2	182.8	118.7	57 56
35 36	173.7	121.6	174.5	122.2	175.3	122.7	176.1	123.3	176.9						55
37 38	169.3	127.6	172.3 170.1 167.8	128.2	170.9	128.8	171.7	129.4	172.5	130.0	173.3	130.6	174.1	131.2	54 53 52
39	164.8	133.4	165.5	134.0	166.3	134.7	167.1	135.3	167.9	135.9	168.6	136.6	169.4	137.2	51
	162.4 160.0	139.1	160.8	139.7	161.5	140.4	162.3	141.1	163.0	141.7	163.8	142.4	164.5	143.0	49
42 43 44	155.0	144.6	158.3 155.8 153.2	145.3	156.5	145.9	157.2	146.6	158.0	147.3	158.7	148.0	159.4	148.7	48 47 46
45			150.6												45
se.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	ee.
Course.	D=2	212'	D=2	213′	D=	214′	D=	215′	D=	216′	D=	217′	D=	218′	Course.

					Pl	ane	Trav	verse	Та	ble					
Course.	D=	219′	D=	220′	D=	221′	D=	222′	D=	223′	D=	224′	D=	225′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	Co
0	219.0	o.o 3.8	220.0 220.0	o.o 3.8	221.0	1	222.0		223.0 223.0		224.0 224.0		225.0 225.0	0.0	90 90
2	218.9		219.9	7.7	221.0 220.9 220.7	3.9 7.7 11.6		3.9 7.7 11.6	222.9	3.9 7.8 11.7	223.9 223.7	3.9 7.8 11.7	224.9	3.9 7.9 11.8	89 88 87
4	218.5	15.3	219.5		220.5		221.5		222.5		223.5 223.1	_	224.5 224.1	15.7	86 85
100	217.8	22.9	218.8 218.4	23.0	219.8 219.4	23.I 26.9	220.8 220.3	23.2	221.8	23.3	222.8	23.4 27.3	223.8 223.3	23.5 27.4	84 83
9	216.3	34.3	217.9	34.4	218.8	34.6	219.8	34.7		34.9	221.8	35.0	222.8	31.3	82 81
11	215.0	41.8	216.7 216.0 215.2	42.0	217.6 216.9 216.2	42.2	218.6 217.9 217.1	42.4	219.6 218.9 218.1		220.6 219.9 219.1	42.7	221.6 220.9 220.1	39.1 42.9 46.8	80 79 78
13	213.4	49.3	214.4	49.5	215.3 214.4	49.7	216.3 215.4	49.9	217.3 216.4	50.2	218.3	50.4	219.2 218.3	50.6 54.4	77 76
15	210.5	60.4	212.5	60.6	213.5 212.4	60.9	214.4	61.2	215.4 214.4		215.3	61.7	217.3 216.3	58.2 62.0	75 74
17	208.3	67.7	210.4 209.2 208.0	68.0	211.3 210.2 209.0	68.3	212.3 211.1 209.9	68.6	213.3 212.1 210.9	68.9	214.2 213.0 211.8	69.2	215.2 214.0 212.7	65.8 69.5 73.3	73 72 71
20	205.8		206.7		207.7		208.6	75.9	209.6 208.2	76.3 79.9	210.5	76.6	211.4	77.0 80.6	70 69
22 23	203.1	82.0 85.6	204.0	82.4 86.0	204.9	82.8 86.4	205.8 204.4	83.2 86.7	206.8	83.5 87.1	207.7 206.2	83.9 87.5	208.6	84.3 87.9	68 67
25	198.5	92.6	199.4	93.0	200.3	93.4	201.2	93.8		94.2	203.0	94.7	203.9	95.1	66
27 27 28	195.1	99.4	197.7 196.0 194.2	99.9	198.6 196.9	100.3	199.5 197.8 196.0	100.8	200.4 198.7 196.9	101.2	199.6 197.8	101.7		98.6 102.1 105.6	64 63 62
29 30		- 3	192.4		193.3	107.1	194.2		195.0		195.9	108.6		109.1	61 60
31 32	187.7	116.1	186.6	116.6	187.4	113.8	188.3	117.6	191.1 189.1 187.0	118.2	190.0	118.7	190.8	115.9 119.2 122.5	59 58
33 34	181.6	122.5	182.4	123.0	183.2		184.0	124.1	184.9	124.7	185.7	125.3	186.5	125.8	57 56
35 36 37	177.2	128.7		129.3	178.8	129.9	179.6	130.5	180.4	131.1	181.2	131.7	182.0	129.1 132.3 135.4	55 54 53
38	172.6	137.8	173.4	138.5	171.7		172.5	139.7	173.3	140.3	174.1	137.9	174.9	138.5	52 51
40	165.3	143.7	166.0	144.3	166.8	142.1 145.0 147.9	167.5	145.6	168.3	146.3	169.1	147.0	169.8	144.6	50 49
42 43 44	160.2	149.4	160.9	150.0	161.6	150.7	162.4	151.4	163.1	152.1	163.8	152.8	164.6	153.4	48 47 46
45	154.9	154.9	155.6	155.6	156.3	156.3	157.0	157.0	157.7	157.7	158.4	158.4	159.1	159.1	45
Course.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	Course.
ပိ	D=	219′				221′	D=	222′	D=	223′	D=	224′	D=	225′	Cou

					Pl	ane	Trav	rerse	Tal	ole					
Course.	D=	226′	D=	227′	D=	228′	D=	229′	D=	230′	D=	231′	D=	232'	Course.
Col	LAT.	DEP.	Col												
° 0 1 2 3 4	226.0 226.0 225.9 225.7 225.4	3·9 7·9 11.8	227.0 227.0 226.9 226.7 226.4	7.9 11.9	228.0 228.0 227.9 227.7 227.4	4.0 8.0 11.9	229.0 229.0 228.9 228.7 228.4	4.0 8.0 12.0	230.0 230.0 229.9 229.7 229.4	4.0 8.0 12.0	231.0 231.0 230.9 230.7 230.4	4.0 8.1 12.1	232.0 232.0 231.9 231.7 231.4	,0.0 4.0 8.1 12.1 16.2	90 89 88 87 86
5 6 7 8 9	225.1 224.8 224.3 223.8 223.2	23.6 27.5 31.5	226.1 225.8 225.3 224.8 224.2	23.7 27.7 31.6	227.1 226.8 226.3 225.8 225.2	23.8 27.8 31.7	228.1 227.7 227.3 226.8 226.2	23.9 27.9 31.9 35.8	229.1 228.7 228.3 227.8 227.2	24.0 28.0 32.0	230.I 229.7 229.3 228.8 228.2	24.I 28.I 32.I	231.1 230.7 230.3 229.7 229.1	20.2 24.3 28.3 32.3 36.3	85 84 83 82 81
10 11 12 13 14	222.6 221.8 221.1 220.2 219.3	43.1 47.0 50.8	223.6 222.8 222.0 221.2 220.3	43·3 47·2 51.1	224.5 223.8 223.0 222.2 221.2	43·5 47·4 51·3	225.5 224.8 224.0 223.1 222.2	43·7 47.6	226.5 225.8 225.0 224.1 223.2	43.9 47.8 51.7	227.5 226.8 226.0 225.1 224.1	44.1 48.0 52.0	228.5 227.7 226.9 226.1 225.1	40.3 44.3 48.2 52.2 56.1	80 79 78 77 76
15 16 17 18 19	218.3 217.2 216.1 214.9 213.7	62.3 66.1 69.8	219.3 218.2 217.1 215.9 214.6	62.6 66.4 70.1	220.2 219.2 218.0 216.8 215.6	62.8 66.7 70.5	221.2 220.1 219.0 217.8 216.5	63.1 67.0 70.8	222.2 221.1 220.0 218.7 217.5	63.4 67.2 71.1	223.1 222.1 220.9 219.7 218.4	63.7 67.5	224.1 223.0 221.9 220.6 219.4	60.0 63.9 67.8 71.7 75.5	75 74 73 72 71
20 21 22 23 24	212.4 211.0 209.5 208.0 206.5	81.0 84.7 88.3	213.3 211.9 210.5 209.0 207.4	81.3 85.0 88.7	214.2 212.9 211.4 209.9 208.3	81.7 85.4 89.1	215.2 213.8 212.3 210.8 209.2	82.1 85.8	213.3	82.4 86.2 89.9	217.1 215.7 214.2 212.6 211.0	82.8 86.5 90.3	218.0 216.6 215.1 213.6 211.9	79·3 83.1 86.9 90.6 94·4	70 69 68 67 66
25 26 27 28 29	204.8 203.1 201.4 199.5 197.7	99.1 102.6 106.1	205.7 204.0 202.3 200.4 198.5	99.5 103.1 106.6 110.1	201.3 199.4	103.5	205.8 204.0 202.2 200.3	100.4 104.0 107.5 111.0	203.1	100.8 104.4 108.0 111.5	205.8 204.0 202.0	101.3 104.9 108.4 112.0	206.7 204.8 202.9	105.3 108.9 112.5	65 64 63 62 61
30 31 32 33 34	195.7 193.7 191.7 189.5 187.4	116.4 119.8 123.1 126.4		116.9 120.3 123.6 126.9	195.4 193.4 191.2 189.0	117.4 120.8 124.2 127.5	196.3 194.2 192.1 189.8	117.9 121.4 124.7 128.1	197.1 195.1 192.9 190.7	118.5 121.9 125.3 128.6	198.0 195.9 193.7 191.5	119.0 122.4 125.8 129.2	198.9 196.7 194.6 192.3	129.7	58 57 56
35 36 37 38 39	180.5 178.1 175.6	132.8 136.0 139.1 142.2	185.9 183.6 181.3 178.9 176.4	133.4 136.6 139.8 142.9	184.5 182.1 179.7 177.2	134.0 137.2 140.4 143.5	185.3 182.9 180.5 178.0	134.6 137.8 141.0 144.1	186.1 183.7 181.2 178.7	135.2 138.4 141.6 144.7	186.9 184.5 182.0	135.8 139.0 142.2 145.4	187.7 185.3 182.8 180.3	136.4 139.6 142.8 146.0	54 53 52 51
41 42 43 44	168.0 165.3 162.6	148.3 151.2 154.1 157.0	171.3 168.7 166.0 163.3	148.9 151.9 154.8 157.7	172.1 169.4 166.7	149.6 152.6 155.5 158.4	172.8 170.2 167.5 164.7	150.2 153.2 156.2 159.1	173.6 170.9 168.2 165.4	150.9 153.9 156.9 159.8	174.3 171.7 168.9 166.2	151.5 154.6 157.5 160.5	175.1 172.4 169.7 166.9	152.2 155.2 158.2 161.2	50 49 48 47 46 45
45	==	159.8	_		DEP,	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	
Course.	DEP.					228′	_	229′	_	230′	-	231'		232'	Course.

					P	lane	Tra	verse	e Ta	ble					
Course.	D=	233′	D=	234′	D=	235′	D=	236′	D=	237′	D=	238′	D=	239′	Course.
Cor	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0	233.0	0.0	234.0	0.0	235.0	0.0	236.0	0.0	237.0	0.0	238.0	0.0	239.0	0.0	9°
I 2	233.0 232.9	4.I 8.I	234.0 233.9	4.1	235.0 234.9	4.I 8.2	236.0 235.9	8.2	237.0 236.9	8.3	238.0 237.9	8.3	239.0 238.9	4.2 8.3	89 88
3 4	232.7 232.4		233.7 233.4		234.7 234.4		235·7 235·4		236.7 236.4		237·7 237·4		238.7 238.4	12.5	87 86
5 6	232.I 231.7		233.I 232.7		234.I 233.7	20.5	235.I 234.7	20.6			237.1 236.7		238.1 237.7	20.8	85 84
7 8	231.3	28.4	232.3	28.5	233.2 232.7	28.6	234.2 233.7		235.2	28.9	236.2 235.7	29.0	237.2 236.7	29.1	
9	230.1	36.4	231.1	36.6	232.1	36.8	233.1	36.9	234.1	37.1	235.1	37.2	236.1	37-4	81
10	229.5 228.7	44.5	230.4	44.6	231.4	44.8	232.4	45.0	233.4	45.2	234.4 233.6	45.4	235.4	41.5 45.6	80 79
12	227.9	52.4	228.9	52.6	229.9	52.9	230.8	53.1	231.8	53.3	232.8	53.5	233.8	49·7 53.8	78 77
14	225.1		227.0		228.0		229.0		230.0		230.9		231.9	57.8 61.9	76 75
16 17	224.0	64.2	224.9 223.8		225.9 224.7		226.9 225.7		227.8 226.6		228.8 227.6	65.6	229.7 228.6	65.9 69.9	74 73
18	221.6 220.3		222.5		223.5 222.2		224.4 223.1		225.4 224.1		226.4 225.0		227.3 226.0	73.9 77.8	72 71
20 2I	218.9		219.9		220.8		221.8		222.7		223.6		224.6 223.1	81.7 85.6	70
22	216.0	87.3	217.0	87.7	217.9	88.0	218.8	88.4	219.7	88.8	220.7	89.2	221.6	89.5 93.4	69 68
23 24	212.9		213.8		214.7		217.2	96.0	216.5	96.4	217.4	96.8	218.3	97.2	67 66
25 26	211.2 209.4	102.1	212.I 210.3	102.6		103.0		103.5	213.0	103.9	213.9	104.3	214.8	101.0	65 64
27 28	205.7	109.4	206.6	109.9	207.5	106.7	208.4	110.8	209.3	111.3	210.1	111.7	211.0	112.2	63 62
29			204.7			113.9						115.4			61 60
30 31	199.7	120.0	200.6	120.5	201.4	121.0	202.3	121.5	203.1	122.1	204.0	122.6	204.9	123.1	59 58
32 33 34	195.4	126.9	196.2	127.4	197.1	128.0	197.9	128.5	198.8	129.1	199.6	129.6	200.4	130.2	5° 57 56
35 36	190.9	133.6	191.7	134.2	192.5	134.8	193.3	135.4	194.1	135.9	195.0	136.5	195.8	137.1	55
36 37 38	186.1	140.2	186.9	140.8	187.7	138.1	188.5	142.0	189.3	142.6	190.1	143.2	190.9	143.8	54 53
38	181.1	143.4	181.9	144.1	185.2	144.7 147.9	183.4	145.3	184.2	145.9	185.0	149.8	185.7	147.1	52 51
40 41	175.8	152.9	176.6	153.5	177.4	151.1 154.2	178.1	154.8	178.9	155.5	179.6	156.1	180.4	156.8	50 49
42 43	173.2	155.9	173.9	156.6	174.6	157.2	175.4	157.9 161.0	176.1	158.6 161.6	176.9	159.3	177.6	159.9	48
44	167.6	161.9	168.3	162.6	169.0	163.2	169.8	163.9	170.5	164.6	171.2	165.3	171.9	166.0	46
45															45
Course.		LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	_	DEP.	LAT.	DEP.	LAT.	Course.
ပိ	D=	233′	D=	234′	D=	235′	D=2	236′	D=2	237′	D=	238′	D=	239′	ŭ

33

					Pl	ane	Trav	verse	Та	ble					
Course.	D=	240′	D=	241′	D=	242'	D=	243′	D=	244′	D=	245′	D=	246′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	So
0 I	240.0	4.2	241.0 241.0 240.0	4.2	242.0 242.0 241.9	4.2	243.0 243.0 242.9	4.2	244.0 244.0	4.3	245.0 245.0	4.3	246.0 246.0 245.9	, 0.0 4.3 8.6	90 89 88
3 4	239.9 239.7 239.4	12.6 16.7	240.7 240.4	12.6	241.7 241.4	12.7	242.7 242.4	12.7	243.9 243.7 243.4	12.8	244.4	12.8	245.7 245.4	12.9	87 86
56 78 9	239.1 238.7 238.2 237.7 237.0	25.1 29.2 33.4	240.1 239.7 239.2 238.7 238.0	25.2 29.4 33.5	241.1 240.7 240.2 239.6 239.0	29.5 33.7	242.1 241.7 241.2 240.6 240.0	25.4 29.6 33.8	243.1 242.7 242.2 241.6 241.0	29.7 34.0	244.I 243.7 243.2 242.6 242.0	25.6 29.9 34.1	245.1 244.7 244.2 243.6 243.0	21.4 25.7 30.0 34.2 38.5	85 84 83 82 81
10 11 12 13	236.4 235.6 234.8 233.8	41.7 45.8 49.9 54.0	237·3 236.6 235·7 234.8	41.8 46.0 50.1 54.2	238.3 237.6 236.7 235.8	42.0 46.2 50.3 54.4	239.3 238.5 237.7 236.8	42.2 46.4 50.5 54.7	240.3 239.5 238.7 237.7	42.4 46.6 50.7 54.9	241.3 240.5 239.6 238.7	42.5 46.7 50.9 55.1	242.3 241.5 240.6 239.7	42.7 46.9 51.1 55.3	80 79 78 77 76
14 15 16 17 18 19	232.9 231.8 230.7 229.5 228.3 226.9	62.1 66.2 70.2 74.2	233.8 232.8 231.7 230.5 229.2 227.9	62.4 66.4 70.5	234.8 233.8 232.6 231.4 230.2 228.8	62.6 66.7 70.8 74.8	235.8 234.7 233.6 232.4 231.1 229.8	62.9 67.0 71.0 75.1	236.8 235.7 234.5 233.3 232.1 230.7	63.2 67.3 71.3 75.4	237.7 236.7 235.5 234.3 233.0 231.7	63.4 67.5 71.6 75.7	238.7 237.6 236.5 235.3 234.0 232.6	59.5 63.7 67.8 71.9 76.0 80.1	75 74 73 72 71
20 21 22 23 24	225.5 224.1 222.5 220.9 219.3	82.1 86.0 89.9 93.8	226.5 225.0 223.5 221.8 220.2	82.4 86.4 90.3 94.2	227.4 225.9 224.4 222.8 221.1	82.8 86.7 90.7 94.6	228.3 226.9 225.3 223.7 222.0	83.1 87.1 91.0 94.9	229.3 227.8 226.2 224.6 222.9	83.5 87.4 91.4 95.3	230.2 228.7 227.2 225.5 223.8	83.8 87.8 91.8 95.7	231.2 229.7 228.1 226.4 224.7	84.1 88.2 92.2 96.1	70 69 68 67 66
25 26 27 28 29	215.7 213.8	105.2 109.0 112.7	216.6 214.7	105.6 109.4 113.1	217.5 215.6 213.7	106.1	218.4 216.5 214.6	106.5 110.3 114.1	219.3	107.0 110.8 114.6	222.0 220.2 218.3 216.3 214.3	107.4 111.2 115.0		107.8	65 64 63 62 61
30 31 32 33 34	205.7 203.5 201.3	130.7	206.6 204.4 202.1	124.1 127.7 131.3	207.4 205.2 203.0	124.6 128.2 131.8	208.3 206.1 203.8	125.2 128.8 132.3	209.1 206.9 204.6	125.7 129.3 132.9	212.2 210.0 207.8 205.5 203.1	126.2 129.8 133.4	210.9 208.6 206.3	126.7 130.4 134.0	59 58
35 36 37 38 39	194.2 191.7 189.1	141.1 144.4 147.8	195.0 192.5 189.9	141.7 145.0 148.4	195.8 193.3 190.7	142.2 145.6 149.0	196.6 194.1 191.5	142.8 146.2 149.6	197.4 194.9 192.3	143.4 146.8 150.2	200.7 198.2 195.7 193.1 190.4	144.0 147.4 150.8	199.0 196.5 193.9	144.6 148.c 151.5	55 54 53 52 51
40 41 42 43 44	181.1 178.4 175.5	157.5 160.6	181.9 179.1 176.3	158.1	182.6 179.8 177.0	158.8 161.9 165.0 168.1	183.4 180.6 177.7 174.8	159.4 162.6 165.7 168.8	184.1 181.3 178.5 175.5	160.1 163.3 166.4 169.5	182.1 179.2 176.2	160.7 163.9 167.1 170.2	185.7 182.8 179.9 177.0	161.4 164.6 167.8 170.9	49 48 47 46
45	169.7	169.7	170.4		171.1		171.8			172.5			173.9	173.9	45
Course.	DEP.	LAT. 240'	DEP.	LAT. 241'	DEP.	242'	DEP.		DEP.	LAT. 244'	DEP.	LAT. 245'	DEP.	246'	Course.

					P	lane	Tra	verse	е Та	ble					
Course.	D=	247′	D=	248′	D=	249′	D=	250′	D=	251′	D=	252′	D=	253′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3 4	247.0 247.0 246.8 246.7 246.4	4.3 8.6 12.9		4·3 8·7 13·0 17·3	249.0 249.0 248.8 248.7 248.4	0.0 4.3 8.7 13.0 17.4	250.0 249.8 249.7	4·4 8.7	251.0 251.0 250.8 250.7 250.4	4.4 8.8 13.1	252.0 252.0 251.8 251.7 251.4	4.4 8.8 13.2	253.0 253.0 252.8 252.7 252.4	4.4 8.8	90 89 88 87 86
56 78 9	246.1 245.6 245.2 244.6 244.0	25.8 30.1 34.4 38.6	247.1 246.6 246.2 245.6 244.9	25.9 30.2 34.5 38.8	248.1 247.6 247.1 246.6 245.9	21.7 26.0 30.3 34.7 39.0	248.6 248.1 247.6 246.9	30.5 34.8 39.1	249.6 249.1 248.6 247.9	26.2 30.6 34.9 39.3	251.0 250.6 250.1 249.5 248.9	26.3 30.7 35.1 39.4	252.0 251.6 251.1 250.5 249.9	22.1 26.4 30.8 35.2 39.6	85 84 83 82 81
10 11 12 13 14	243.2 242.5 241.6 240.7 239.7	47.1 51.4 55.6 59.8	244.2 243.4 242.6 241.6 240.6	51.6 55.8 60.0	244.4 243.6 242.6 241.6	60.2	243.6 242.6	56.2 60.5	246.4 245.5 244.6 243.5	52.2 56.5 60.7	248.2 247.4 246.5 245.5 244.5	48.1 52.4 56.7 61.0	248.4 247.5 246.5 245.5	43.9 48.3 52.6 56.9 61.2	80 79 78 77 76
15 16 17 18 19	238.6 237.4 236.2 234.9 233.5	68.1 72.2 76.3 80.4	239.5 238.4 237.2 235.9 234.5	68.4 72.5 76.6 80.7	240.5 239.4 238.1 236.8 235.4	76.9 81.1	239.1 237.8 236.4	77·3 81.4	240.0 238.7 237.3	69.2 73.4 77.6 81.7	243.4 242.2 241.0 239.7 238.3	69.5 73.7 77.9 82.0	244.4 243.2 241.9 240.6 239.2	65.5 69.7 74.0 78.2 82.4	75 74 73 72 71
20 21 22 23 24		88.5 92.5 96.5 100.5		88.9 92.9 96.9 100.9		101.3		89.6 93.7 97.7 101.7		94.0 98.1 102.1	230.2	90.3 94.4 98.5 102.5		86.5 90.7 94.8 98.9 102.9	70 69 68 67 66
25 26 27 28 29	222.0 220.1 218.1 216.0	112.1 116.0 119.7	222.9 221.0 219.0 216.9	108.7 112.6 116.4 120.2	223.8 221.9 219.9 217.8	109.2 113.0 116.9 120.7	224.7 222.8	109.6	225.6 223.6	106.1 110.0 114.0 117.8 121.7	226.5 224.5	110.5 114.4 118.3	227.4 225.4 223.4	106.9 110.9 114.9 118.8 122.7	-0 1
30 31 32 33 34	211.7 209.5 207.2 204.8	134.5	212.6 210.3 208.0 205.6	127.7 131.4 135.1 138.7	213.4 211.2 208.8 206.4	128.2 131.9 135.6 139.2	214.3 212.0 209.7 207.3	128.8 132.5 136.2 139.8	215.1 212.9 210.5 208.1		216.0 213.7 211.3 208.9	129.8 133.5 137.2 140.9	216.9 214.6 212.2 209.7	130.3 134.1 137.8 141.5	6 58 57 56
35 36 37 38 39	197.3 194.6 192.0	145.2 148.6 152.1 155.4	200.6 198.1 195.4 192.7	149.3 152.7 156.1	201.4 198.9 196.2 193.5	146.4 149.9 153.3 156.7	202.3 199.7 197.0 194.3	146.9 150.5 153.9 157.3	203.1 200.5 197.8 195.1	151.1 154.5 158.0	203.9 201.3 198.6 195.8	148.1 151.7 155.1 158.6	204.7 202.1 199.4 196.6	148.7 152.3 155.8 159.2	55 54 53 52 51
40 41 42 43 44 45	186.4 183.6 180.6 177.7	162.0 165.3 168.5	187.2 184.3 181.4 178.4	162.7 165.9 169.1 172.3	187.9 185.0 182.1 179.1	160.1 163.4 166.6 169.8 173.0	188.7 185.8 182.8 179.8	164.0 167.3 170.5 173.7	189.4 186.5 183.6 180.6	164.7 168.0 171.2	190.2 187.3 184.3 181.3	165.3 168.6 171.9 175.1	190.9 188.0 185.0 182.0	166.0 169.3 172.5 175.7	48 47 46
	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	45
Course.	D=		D=		_	249′	D=		D=		D=		D=		Course.

						Pla	ane '	Trav	erse	Tal	ole					
Course.	1	D=2	54′	D=	255′	D=2	256′	D=	257′	D=2	258′	D=	259′	D=	260′	Course.
S	1	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
2 3	2 2 2 2	54.0 54.0 53.8 53.7 53.4	4.4 8.9 13.3	255.0 255.0 254.8 254.7 254.4	4.5 8.9 13.3	256.0 256.0 255.8 255.6 255.4	4.5 8.9 13.4	257.0 257.0 256.8 256.6 256.4	4.5 9.0 13.5	258.0 258.0 257.8 257.6 257.4	4·5 9.0 13.5	259.0 259.0 258.8 258.6 258.4	4.5 9.0 13.6	260.0 260.0 259.8 259.6 259.4	0.0 4.5 9.1 13.6 18.1	90 89 88 87 86
200	2 2 2 2 2 2 2	53.0 52.6 52.1 51.5 50.9	22.1 26.6 31.0 35.3	254.0 253.6 253.1 252.5 251.9	22.2 26.7 31.1 35.5	255.0 254.6 254.1 253.5 252.8	22.3 26.8 31.2 35.6	256.0 255.6 255.1 254.5 253.8	22.4 26.9 31.3 35.8	257.0 256.6 256.1 255.5 254.8	27.0 31.4 35.9	258.0 257.6 257.1 256.5 255.8	27.1 31.6 36.0	259.0 258.6 258.1 257.5 256.8	22.7 27.2 31.7 36.2 40.7	85 84 83 82 81
10 12 13 14	2 2 2 2 3 2	49·3 48·4 47·5 46·5	48.5 52.8 57.1	251.1 250.3 249.4 248.5 247.4	48.7 53.0	252.1 251.3 250.4 249.4 248.4	53.2	252.3 251.4 250.4	49.0 53.4	254.1 253.3 252.4 251.4 250.3	49.2 53.6 58.0	255.1 254.2 253.3 252.4 251.3	49·4 53.8 58·3	256.1 255.2 254.3 253.3 252.3	45.1 49.6 54.1 58.5 62.9	80 79 78 77 76
10	6 2 7 2 8 2	45·3 44·2 42·9 41·6	70.0 74.3 78.5	246.3 245.1 243.9 242.5 241.1	78.8	247.3 246.1 244.8 243.5 242.1	66.3 70.6 74.8 79.1 83.3		75.1 79.4	249.2 248.0 246.7 245.4 243.9	75·4 79·7 84.0	244.9	71.4 75.7 80.0 84.3	251.1 249.9 248.6 247.3 245.8	67.3 71.7 76.0 80.3 84.6	75 74 73 72 71
2: 2: 2: 2:	1 2 2 2 3 2	238.7 237.1 235.5 233.8 232.0	91.0 95.2 99.2	239.6 238.1 236.4 234.7 233.0	91.4 95.5 99.6	240.6 239.0 237.4 235.6 233.9	91.7 95.9 100.0	241.5 239.9 238.3 236.6 234.8	92.1 96.3 100.4	242.4 240.9 239.2 237.5 235.7	92.5 96.6 100.8	243.4 241.8 240.1 238.4 236.6	92.8 97.0 101.2 105.3	244.3 242.7 241.1 239.3 237.5	105.8	70 69 68 67 66
2 2 2 2 2	6 2 7 2 8 2	230.2 228.3 226.3 224.3 222.2	111.3 115.3 119.2	227.2 225.2	111.8 115.8 119.7	232.0 230.1 228.1 226.0 223.9	112.2 116.2 120.2	231.0 229.0 226.9	112.7 116.7 120.7	229.9	113.1 117.1 121.1	234.7 232.8 230.8 228.7 226.5	113.5 117.6 121.6	233.7 231.7 229.6	109.9 114.0 118.0 122.1 126.1	65 64 63 62 61
3 3 3 3 3	1 2 2 2 3 2	217.7	130.8 134.6 138.3	218.6 216.3 213.9	131.3 135.1 138.9	221.7 219.4 217.1 214.7 212.2	131.8 135.7 139.4	220.3 217.9 215.5	132.4 136.2 140.0	221.I 218.8	132.9 136.7 140.5 144.3	219.6 217.2 214.7	133.4 137.2 141.1 144.8	222.9 220.5 218.1 215.5	130.0 133.9 137.8 141.6 145.4	56
3 3 3 3 3	6 2 7 2 8 2 9 1	205.5 202.9 200.2 197.4	149.3 152.9 156.4 159.8	206.3 203.7 200.9 198.2	149.9 153.5 157.0 160.5		150.5 154.1 157.6 161.1	207.9 205.2 202.5 199.7	151.1 154.7 158.2 161.7	200.5	151.6 155.3 158.8 162.4	209.5 206.8 204.1 201.3	152.2 155.9 159.5 163.0	210.3 207.6 204.9 202.1	149.1 152.8 156.5 160.1 163.6	53 52 51
4 4 4	1 2 1 3 3 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	191.7 188.8 185.8 182.7	166.6 170.0 173.2 176.4	192.5 189.5 186.5 183.4	167.3 170.6 173.9 177.1	193.2 190.2 187.2 184.2	168.0 171.3 174.6 177.8	194.0 191.0 188.0 184.9	172.0 175.3 178.5	194.7 191.7 188.7 185.6	172.6 176.0 179.2	195.5 192.5 189.4 186.3	173.3 176.6 179.9	190.2 193.2 190.2 187.0		49 48 47 46
	=			180.3				181.7				-	183.1			45
	Course.		LAT.	DEP.		DEP.	LAT.	DEP.	257'	DEP.	LAT.	DEP.	259'	DEP.	260'	Course.
1	ا د	D=	254′	D	255′		250		4 5/		250		239			0

	6				Pla	ine '	Trav	erse	Tab	ole					
Course.	D=	261′	D=	262'	D=	263′	D=	264′	D=	265′	D=	266′	D=	267′	Course.
ပီ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	
0 1 2	261.0 261.0 260.8	4.6 9.1	262.0 262.0 261.8		263.0 263.0 262.8	4.6 9.2	264.0 264.0 263.8	4.6 9.2	265.0 265.0 264.8	4.6 9.2	266.0 266.0 265.8	4.6 9.3	267.0 267.0 266.8	0.0 4.7 9.3	90 89 88
3 4	260.6 260.4 260.0	18.2	261.6 261.4	13.7	262.6 262.4 262.0	18.3	263.6 263.4	18.4	264.6 264.4	18.5	265.6 265.4	18.6	266.6 266.3	18.6	87 86
5 6 7 8 9	259.6 259.1 258.5 257.8	27.3 31.8 36.3	261.0 260.6 260.0 259.5 258.8	22.8 27.4 31.9 36.5 41.0	261.6 261.0	27.5 32.1 36.6	263.0 262.6 262.0 261.4 260.7	27.6 32.2 36.7	264.0 263.5 263.0 262.4 261.7	27.7 32.3 36.9	265.0 264.5 264.0 263.4 262.7	27.8 32.4 37.0	266.0 265.5 265.0 264.4 263.7	23.3 27.9 32.5 37.2 41.8	85 84 83 82 81
10 11 12 13 14	257.0 256.2 255.3 254.3 253.2	49.8 54.3 58.7	258.0 257.2 256.3 255.3 254.2	50.0 54.5 58.9	259.0 258.2 257.3 256.3 255.2	50.2 54.7 59.2	260.0 259.1 258.2 257.2 256.2	50.4 54.9 59.4	261.0 260.1 259.2 258.2 257.1	50.6 55.1 59.6	262.0 261.1 260.2 259.2 258.1	50.8 55.3 59.8	262.9 262.1 261.2 260.2 259.1	46.4 50.9 55.5 60.1 64.6	80 79 78 77 76
15 16 17 18	252.1 250.9 249.6 248.2 246.8	71.9 76.3 80.7	253.1 251.9 250.6 249.2 247.7	76.6 81.0	254.0 252.8 251.5 250.1 248.7	72.5 76.9 81.3	255.0 253.8 252.5 251.1 249.6	72.8 77.2 81.6	256.0 254.7 253.4 252.0 250.6	73.0 77.5 81.9	256.9 255.7 254.4 253.0 251.5	73·3 77·8 82.2	257.9 256.7 255.3 253.9 252.5	73.6	75 74 73 72 71
20 21 22 23 24	245.3 243.7 242.0 240.3 238.4	93.5 97.8 102.0	246.2 244.6 242.9 241.2 239.3	93.9 98.1 102.4	247.I 245.5 243.8 242.I 240.3	94·3 98·5 102.8	248.1 246.5 244.8 243.0 241.2	94.6 98.9 103.2	249.0 247.4 245.7 243.9 242.1	90.6 95.0 99.3 103.5	250.0 248.3 246.6 244.9 243.0	91.0 95.3 99.6 103.9	250.9 249.3 247.6	95.7 100.0	70 69 68 67 66
25 26 27 28 29	232.6 230.4	114.4 118.5 122.5	233.4 231.3	110.7 114.9 118.9 123.0 127.0	236.4 234.3 232.2	119.4	237.3 235.2 233.1	115.7 119.9 123.9	240.2 238.2 236.1 234.0 231.8	116.2 120.3 124.4	237.0	116.6 120.8 124.9	237.9 235.7	112.8 117.0 121.2 125.3 129.4	65 64 63 62 61
30 31 32 33 34	223.7 221.3 218.9	134.4	224.6 222.2 219.7	134.9 138.8 142.7	225.4 223.0 220.6	135.5 139.4 143.2	226.3 223.9 221.4	132.0 136.0 139.9 143.8	229.5 227.1 224.7 222.2 219.7	132.5 136.5 140.4 144.3	230.4 228.0 225.6 223.1	133.0 137.0 141.0	231.2 228.9 226.4 223.9	137.5 141.5 145.4	60 59 58 57 56
35 36 37 38 39	211.2 208.4 205.7	153.4 157.1	212.0 209.2 206.5	154.0 157.7 161.3	212.8 210.0 207.2	154.6	213.6 210.8 208.0	155.2 158.9 162.5	217.1 214.4 211.6 208.8 205.9	155.8 159.5 163.2	215.2 212.4 209.6	156.4 160.1 163.8	216.0 213.2 210.4	156.9 160.7	55 54 53 52 51
40 41 42 43 44	197.0 194.0 190.9 187.7	171.2 174.6 178.0 181.3	197.7 194.7 191.6 188.5	175.3 178.7 182.0	198.5 195.4 192.3 189.2	172.5 176.0 179.4 182.7	199.2 196.2 193.1 189.9	173.2 176.7 180.0 183.4	196.9 193.8 190.6	173.9 177.3 180.7 184.1	200.8 197.7 194.5 191.3	174.5 178.0 181.4 184.8	201.5 198.4 195.3	175.2 178.7 182.1	50 49 48 47 46
45	184.6	184.6	185.3	185.3	186.0	186.0	186.7	186.7	187.4	187.4	188.1	188.1	188.8	188.8	45
Course.	DEP.	LAT. 261'	DEP.	Lат. 262'	DEP.	Lat. 263'	DEP.	LAT. 264'	DEP.	Lat. 265'	DEP.	LAT. 266'	DEP.	LAT. 267'	Course.

					Pl	ane	Trav	erse	Tal	ole				-	
Course.	D=	268′	D=	269'	D=	270′	D=	271′	D=	272′	D=	273′	D=	274′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	
0	268.0 268.0		269.0		270.0		271.0		272.0	0.0	273.0	0.0	274.0	0.0	90
1 2 3	267.8 267.6	9.4	269.0 268.8 268.6	9.4	270.0 269.8 269.6		271.0 270.8 270.6	9.5	272.0 271.8 271.6	9.5	273.0 272.8 272.6	4.8 9.5 14.3	274.0 273.8 273.6	4.8 9.6 14.3	89 88 87
4	267.3 267.0	18.7	268.3 268.0		269.3 269.0	18.8	270.3 270.0	18.9	271.3 271.0	19.0	272.3 272.0	19.0	273.3 273.0	19.1	86
5 6 7 8	266.5 266.0	28.0	267.5 267.0	28.1	268.5 268.0	28.2	269.5 269.0	28.3	270.5 270.0	28.4	271.5 271.0	28.5		23.9 28.6 33.4	85 84 83
8 9	265.4 264.7	37·3 41·9	266.4 265.7	37·4 42.1	267.4 266.7		268.4 267.7	37· 7 42·4	269.4 268.7		270.3 269.6	38.0 42.7		38.1 42.9	82 81
10	263.9 263.1	51.1	264.9 264.1	51.3	265.9 265.0	51.5	266.9 266.0	51.7	267.9 267.0	51.9	268.9 268.0	52.1	269.0	47.6 52.3	80 79 78
12 13 14	262.1 261.1 260.0	60.3	263.1 262.1 261.0	60.5	264.1 263.1 262.0	60.7	265.1 264.1 263.0	61.0	266.1 265.0 263.9	61.2	267.0 266.0 264.9	56.8 61.4 66.0			78 77 76
15 16	258.9 257.6	69.4	259.8 258.6	69.6	260.8 259.5	69.9	261.8 260.5	70.1	262.7 261.5	70.4	263.7 262.4	70.7 75.2	3 /	70.9	75
17 18	256.3 254.9	78.4	257.2 255.8	78.6	258.2 256.8	78.9	259.2 257.7	79.2	260.1 258.7	79.5	261.1 259.6	79.8 84.4	262.0	75.5 80.1 84.7	74 73 72
19 20	253.4 251.8		254.3 252.8		255·3 253·7	87.9 92.3	256.2 254.7		257.2 255.6		258.1 256.5	88.9 93.4		93.7	71 70
2I 22	250.2 248.5	96.0 100.4	251 .1 249.4	96.4 100.8	252. I 250.3	96.8 101.1	253.0 251.3	97.1	253.9 252.2	97·5 101.9	254.9 253.1	97.8	255.8 254.0	98.2 102.6	69 68
23 24	246.7 244.8		247.6 245.7		248.5 246.7	109.8	247.6	110.2	25°.4 248.5	110.6	2 49 4	111.0	250.3	107.1	67 66
25 26 27	240.9	117.5	243.8 241.8	117.9		118.4	243.6	118.8	246.5 244.5	119.2	245.4	119.7	246.3	115.8	65 64
28 29		125.8	239.7 237.5 235.3	126.3	238.4 236.1	126.8	239.3	127.2	242.4 240.2 237.9	127.7	241.0	128.2		124.4 128.6 132.8	63 62 61
30 31	232.1	134.0	233.0	134.5	233.8									137.0	60 50
32 33	227.3 224.8	142.0 146.0	228.1 225.6	142.5 146.5	229.0 226.4	143.1 147.1	229.8 227.3	143.6 147.6	230.7 228.1	144. 1 148. 1	231.5 229.0	144.7	232.4 229.8	145.2	59 58 57 56
34 35	219.5	153.7	220.4	154.3	223.8	154.9	222.0	155.4	222.8	156.0	223.6	156.6	224.4	153.2	55
35 36 37 38	216.8 214.0	157.5	217.6	158.1	218.4 215.6 212.8	162.5	216.4	163.1	217.2	163.7	218.0	164.3	218.8	161.1 164.9 168.7	54 53 52
39	208.3	168.7	209.1	169.3	209.8	169.9	210.6	170.5	211.4	171.2	212.2	171.8	212.9	172.4	51
40 41 42	205.3 202.3 199.2	175.8	203.0	176.5	206.8 203.8 200.6	177.1	204.5	177.8	205.3	178.4	206.0	179.1	206.8	179.8	50 49 48
43 44	196.0	182.8	196.7	183.5		184.1	198.2	184.8	198.9 195.7	185.5	199.7	186.2	200.4		47 46
45	189.5	189.5	190.2	190.2	190.9	190.9	191.6	191.6	192.3	192.3	193.0	193.0	193.7	193.7	45
Course.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	Course.
Cor	D=	268′	D=	269′	D=	270′	D=	271′	D=	272′	D=	273′	D=	274'	Cor

					Pl	ane	Trav	rerse	Tal	ble					
Course.	D=	275′	D=2	276′	D=	277′	D=	278′	D=	279′	D=	280′	D=	281′	Course.
	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	
0 1 2 3 4	275.0 275.0 274.8 274.6 274.3	0.0 4.8 9.6 14.4 19.2	276.0 275.8	4.8 9.6 14.4	277.0 277.0 276.8 276.6 276.3	4.8 9.7 14.5	278.0 278.0 277.8 277.6 277.3	4.9 9.7 14.5	279.0 279.0 278.8 278.6 278.3	4.9 9.7 14.6	280.0 280.0 279.8 279.6 279.3	0.0 4.9 9.8 14.7 19.5	281.0 281.0 280.8 280.6 280.3	9.8 14.7 19.6	90 89 88 87 86
56 78 9	274.0 273.5 273.0 272.3 271.6	24.0 28.7 33.5 38.3 43.0	274.5 273.9 273.3 272.6	28.8 33.6 38.4 43.2	275.9 275.5 274.9 274.3 273.6	29.0 33.8 38.6 43.3	276.9 276.5 275.9 275.3 274.6	29.1 33.9 38.7 43.5	277.9 277.5 276.9 276.3 275.6	29.2 34.0 38.8 43.6	278.9 278.5 277.9 277.3 276.6	24.4 29.3 34.1 39.0 43.8	277.5	24.5 29.4 34.2 39.1 44.0	85 84 83 82 81
10 11 12 13 14	270.8 269.9 269.0 268.0 266.8	57.2 61.9 66.5	271.8 270.9 270.0 268.9 267.8	52.7 57.4 62.1 66.8	272.8 271.9 270.9 269.9 268.8	52.9 57.6 62.3 67.0	273.8 272.9 271.9 270.9 269.7	57.8 62.5 6 7. 3	273.9 272.9 271.8 270.7	53.2 58.0 62.8 67.5	275.7 274.9 273.9 272.8 271.7	63.0	274.9 273.8 272.7	48.8 53.6 58.4 63.2 68.0	80 79 78 77 76
15 16 17 18 19	265.6 264.3 263.0 261.5 260.0	80.4 85.0 89.5	266.6 265.3 263.9 262.5 261.0	76.1 80.7 85.3 89.9	267.6 266.3 264.9 263.4 261.9	76.4 81.0 85.6 90.2	268.5 267.2 265.9 264.4 262.9	76.6 81.3 85.9 90.5	269.5 268.2 266.8 265.3 263.8	76.9 81.6 86.2 90.8	270.5 269.2 267.8 266.3 264.7	86.5 91.2	267.2 265.7	72.7 77.5 82.2 86.8 91.5	75 74 73 72 71
20 21 22 23 24	258.4 256.7 255.0 253.1 251.2	103.0	259.4 257.7 255.9 254.1 252.1	98.9 103.4 107.8	255.0	99.3 103.8 108.2		99.6 104.1 108.6	258.7 256.8	100.0	263.1 261.4 259.6 257.7 255.8	100.3 104.9 109.4	260.5	109.8	70 69 68 67 66
25 26 27 28 29	245.0 242.8	120.6	250.1 248.1 245.9 243.7 241.4	121.0	249.0 246.8 244.6	121.4 125.8 130.0	249.9 24 7. 7 245.5	121.9 126.2 130.5	250.8 248.6 246.3	122.3 126.7 131.0	251.7	122.7 127.1 131.5	250.4 248.1	123.2	.~
30 31 32 33 34	235.7 233.2 230.6 228.0	141.6 145.7 149.8	234.1	142.2 146.3 150.3	237.4 234.9 232.3	142.7 146.8 150.9	238.3 235.8 233.2 230.5	143.2 147.3 151.4 155.5	239.1 236.6 234.0 231.3	143.7 147.8 152.0 156.0	237.5 234.8 232.1	144.2 148.4 152.5 156.6	240.9 238.3 235.7	140.5 144.7 148.9 153.0 157.1	59 58
35 36 37 38 39	216.7 213.7	165.5 169.3 173.1		162.2 166.1 169.9 173.7	221.2 218.3 215.3	162.8 166.7 170.5 174.3	224.9 222.0 219.1 216.0	163.4 167.3 171.2 175.0	225.7 222.8 219.9 216.8	164.0 167.9 171.8 175.6	223.6 220.6 217.6	164.6 168.5 172.4 176.2	224.4 221.4 218.4	165.2 169.1 173.0 176.8	54 53 52 51
42 43 44	207.5 204.4 201.1 197.8	180.4 184.0 187.5 191.0	205.1 201.9 198.5	181.1 184.7 188.2 191.7	209. 1 205.9 202.6 199.3	181.7 185.3 188.9 192.4	209.8 206.6 203.3	182.4 186.0 189.6 193.1	210.6 207.3 204.0 200.7	183.0 186.7 190.3 193.8	211.3 208.1 204.8 201.4	183.7 187.4 191.0 194.5	212.1 208.8 205.5 202.1	184.4 188.0 191.6 195.2	48 47 46
45	194.5 Dep.	194.5 LAT.	DEP.	195.2 LAT.	195.9 Dep.	195.9 LAT.	DEP.	LAT.	DEP.	197.3	198.0 Dep.	LAT.	DEP.	198.7 LAT.	45 ===
Course.		275′		276′		277′		278′		279′		280′		281'	Course.

					P	ane	Tra	verse	e Ta	ble					
Course.	D=	282′	D=	283′	D=	284′	D=	285′	D=	286′	D=	287′	D=	288′	Course.
රී	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
° 0 1 2 3 4	282.0 282.0 281.8 281.6 281.3	0.0 4.9 9.8 14.8 19.7	283.0 283.0 282.8 282.6 282.3	4.9 9.9 14.8 19.7	284.0 284.0 283.8 283.6 283.3	5.0 9.9 14.9	285.0 285.0 284.8 284.6 284.3	5.0 9.9 14.9	286.0 286.0 285.8 285.6 285.3	5.0 10.0 15.0	287.0 287.0 286.8 286.6 286.3	5.0 10.0 15.0	288.0 288.0 287.8 287.6 287.3	0.0 5.0 10.1 15.1 20.1	° 90 89 88 87 86
56 78 9	280.9 280.5 279.9 279.3 278.5	24.6 29.5 34.4 39.2 44.1	281.9 281.4 280.9 280.2 279.5	29.6 34.5 39.4 44.3	282.9 282.4 281.9 281.2 280.5	29.7 34.6 39.5 44.4	283.9 283.4 282.9 282.2 281.5	29.8 34.7 39.7 44.6	284.9 284.4 283.9 283.2 282.5	29.9 34.9 39.8 44.7	285.9 285.4 284.9 284.2 283.5	30.0 35.0 39.9 44.9	286.9 286.4 285.9 285.2 284.5	25.1 30.1 35.1 40.1 45.1	85 84 83 82 81
10 11 12 13 14	277.7 276.8 275.8 274.8 273.6	63.4 68.2	278.7 277.8 276.8 275.7 274.6	54.0 58.8 63.7 68.5	279.7 278.8 277.8 276.7 275.6	59.0 63.9 68.7	280.7 279.8 278.8 277.7 276.5	59·3 64.1 68.9	281.7 280.7 279.8 278.7 277.5	54.6 59.5 64.3 69.2	282.6 281.7 280.7 279.6 278.5	59.7 64.6 69.4	282.7 281.7 280.6	50.0 55.0 59.9 64.8 69.7	80 79 78 77 76
16 17 18 19	272.4 271.1 269.7 268.2 266.6	77.7 82.4 87.1 91.8	273.4 272.0 270.6 269.1 267.6	78.0 82.7 87.5 92.1	274.3 273.0 271.6 270.1 268.5	78.3 83.0 87.8 92.5	274.0 272.5 271.1 269.5	78.6 83.3 88.1 92.8	270.3 274.9 273.5 272.0 270.4 268.8	78.8 83.6 88.4 93.1	277.2 275.9 274.5 273.0 271.4 269.7	79.1 83.9 88.7 93.4	276.8 275.4 273.9 272.3	74·5 79·4 84·2 89.0 93·8	75 74 73 72 71
2I 22 23 24	261.5 259.6 257.6	101.1 105.6 110.2 114.7	264.2 262.4 260.5 258.5	101.4 106.0 110.6 115.1	265.1 263.3 261.4 259.4	101.8 106.4 111.0 115.5	266.1 264.2 262.3 260.4	102.1 106 8 111.4 115.9	267.0 265.2 263.3 261.3	102.5 107.1 111.7 116.3	267.9 266.1 264.2 262.2	102.9 107.5 112.1 116.7	268.9 267.0 265.1 263.1	103.2 107.9 112.5 117.1	70 69 68 67 66
25 26 27 28 29	253.5 251.3 249.0	123.6	256.5 254.4 252.2 249.9 247.5	124.1 128.5 132.9 137.2	255.3 253.0 250.8 248.4	124.5 128.9 133.3 137.7	256.2 253.9 251.6 249.3	124.9 129.4 133.8 138.2	257.1 254.8 252.5 250.1	125.4 129.8 134.3 138.7	258.0 255.7 253.4 251.0	125.8 130.3 134.7 139.1	258.9 256.6 254.3 251.9	126.3	65 64 63 62 61
30 31 32 33 34	236.5 233.8	145.2 149.4 153.6 157.7	242.6 240.0 237.3 234.6	145.8 150.0 154.1 158.3	243.4 240.8 238.2 235.4	150.5 154.7 158.8	244.3 241.7 239.0 236.3	146.8 151.0 155.2 159.4	245.1 242.5 239.9 237.1	147.3 151.6 155.8 159.9	246.0 243.4 240.7 237.9	147.8 152.1 156.3 160.5	246.9 244.2 241.5 238.8	152.6 156.9 161.0	60 59 58 57 56
35 36 37 38 39	228.1 225.2 222.2 219.2	169. 7 173.6 177.5	229.0 226.0 223.0 219.9	166.3 170.3 174.2 178.1	229.8 226.8 223.8 220.7	166.9 170.9 174.8 178.7	230.6 227.6 224.6 221.5	167.5 171.5 175.5 179.4	231.4 228.4 225.4 222.3	168.1 172.1 176.1 180.0	232.2 229.2 226.2 223.0	168.7 172.7 176.7 180.6	235.9 233.0 230.0 226.9 223.8	169.3 173.3 177.3 181.2	55 54 53 52 51
40 41 42 43 44 45	212.8 209.6 206.2	185.0 188.7 192.3 195.9	210.3	185.7 189.4 193.0 196.6	214.3	186.3 190.0 193.7 197.3	215.1 211.8 208.4	187.0 190. 7 194. 4 198.0	215.8 212.5 209.2 205.7	187.6 191.4 195.1 198.7	216.6	188.3 192.0 195.7	217.4 214.0 210.6 207.2	188.9 192.7 196.4 200.1	50 49 48 47 46 45
-		LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	
Course.	D=		D=			284′	D=	285′	D=	286′	D=	287′	D=	288′	Course.

		7 4000.00			Pl	ane	Tra	verse	Ta	ble					
Course.	D=	289′	D=	290′	D=	291′	D=	292′	D=	293′	D=	294'	D=	295′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	ပိ
0 1 2 3 4	289.0 289.0 288.8 288.6 288.3	0.0 5.0 10.1 15.1 20.2	290.0 290.0 289.8 289.6 289.3	5.1 10.1 15.2	291.0 291.0 290.8 290.6 290.3	5.1 10.2 15.2	292.0 292.0 291.8 291.6 291.3	5.1 10.2	293.0 293.0 292.8 292.6 292.3	5.1 10.2 15.3	294.0 294.0 293.8 293.6 293.3	0.0 5.1 10.3 15.4 20.5	295.0 295.0 294.8 294.6 294.3	0.0 5.1 10.3 15.4 20.6	°90 89 88 87 86
56 78 9	287.9 287.4 286.8 286.2 285.4	25.2 30.2 35.2 40.2 45.2	287.8 287.2 286.4	30-3 35-3 40-4 45-4	289.9 289.4 288.8 288.2 287.4	30.4 35.5 40.5 45.5	290.9 290.4 289.8 289.2 288.4	30.5 35.6 40.6 45.7	291.9 291.4 290.8 290.1 289.4	30.6 35.7 40.8 45.8	292.9 292.4 291.8 291.1 290.4	25.6 30.7 35.8 40.9 46.0	291.4	25.7 30.8 36.0 41.1 46.1	85 84 83 82 81
10 11 12 13 14	284.6 283.7 282.7 281.6 280.4	50.2 55.1 60.1 65.0 69.9	284.7	55·3 60.3 65.2 70.2	286.6 285.7 284.6 283.5 282.4 281.1	55.5 60.5 65.5 70.4	287.6 286.6 285.6 284.5 283.3 282.1	55.7 60.7 65.7 70.6	288.5 287.6 286.6 285.5 284.3	55.9 60.9 65.9 70.9	289.5 288.6 287.6 286.5 285.3	66.1 71.1	289.6 288.6 287.4 286.2	51.2 56.3 61.3 66.4 71.4	80 79 78 77 76
15 16 17 18 19	279.2 277.8 276.4 274.9 273.3 271.6	79.7 84.5 89.3 94.1	278.8 277.3 275.8 274.2	94.4	279. 7 278.3 276.8 275.1	80.2 85.1 89.9 94.7	280.7 279.2 277.7 276.1	80.5 85.4 90.2 95.1	283.0 281.6 280.2 278.7 277.0	80.8 85.7 90.5 95.4	278.0	86.0 90.9 95.7	283.6 282.1 280.6 278.9	1	75 74 73 72 71
2I 22 23 24	269.8 268.0 26 6.0 264.0	103.6 108.3 112.9	270.7 268.9 266.9 264.9	103.9 108.6 113.3 118.0	271.7 269.8 267.9 265.8	104.3 109.0 113.7 118.4	270.7 268.8 266.8	104.6 109.4 114.1 118.8	273.5 271. 7 269.7 267.7	109.8	274.5 272.6 270.6 268.6	105.4 110. 1 114.9 119.6	275.4 273.5 271.5 269.5	115.3 115.0	70 69 68 67 66
25 26 27 28 29	259.8 257.5 255.2 252.8	126. 7 131. 2 135. 7 140. 1	262.8 260.7 258.4 256.1 253.6	127.1 131. 7 136.1 140.6	251.5 259.3 256.9 254.5	127.6 132.1 136.6 141.1	262.4 260.2 257.8 255.4	128.0 132.6 137.1 141.6	263.3 261.1 258.7 256.3	128.4 133.0 137.6 142.0	264.2 262.0 259.6 257.1	133.5 138.0 142.5	265.1 262.8 260.5 258.0	129.3 133.9 138.5 143.0	65 64 63 62 61
30 31 32 33 34	247.7 245.1 242.4 239.6	157.4 161.6	248.6 245.9 243.2 240.4	149.4 153.7 157.9 162.2	249.4 246.8 244.1 241.2	149.9 154.2 158.5 162.7	250.3 247.6 244.9 242.1	150.4 154. 7 159.0 163. 3	251.2 248.5 245.7 242.9	150.9 155.3 159.6 163.8	252.0 249.3 246.6 243.7	160. 1 164.4	252.9 250.2 247.4 244.6	151.0	60 59 58 57 56
35 36 37 38 39	233.8 230.8 227.7 224.6	169.9 173.9 177.9 181.9	237.6 234.6 231.6 228.5 225.4	170.5 174.5 178.5 182.5	235.4 232.4 229.3 226.1	171.0 175.1 179.2 183.1	236.2 233.2 230.1 226.9	171.6 175.7 179.8 183.8	237.0 234.0 230.9 227.7	172.2 176.3 180.4 184.4	237.9 234.8 231.7 228.5	172.8 176.9 181.0 185.0	238.7 235.6 232.5 229.3	169.2 173.4 177.5 181.6 185.6	55 54 53 52 51
40 41 42 43 44	218.1 214.8 211.4 207.9	189.6 193.4 197.1 200.8	222.2 218.9 215.5 212.1 208.6 205.1	190.3 194.0 197.8 201.5	219.6 216.3 212.8 209.3	190.9 194.7 198.5 202.1	220.4 217.0 213.6 210.0	191.6 195.4 199.1 202.8	221.1 217.7 214.3 210.8	192.2 196.1 199.8 203.5	221.9 218.5 215.0 211.5	192.9 196.7 200.5 204.2	222.6 219.2 215.7 212.2	193.5 197.4 201.2 204.9	
45 		LAT.			DEP.			LAT.	DEP.	207.2 LAT.		207.9 LAT.	DEP.	208.0 LAT.	45
Course.		289'	D=			291'	D=			293′		294'		295'	Course.

					P	lane	Tra	verse	Та	ble					
Course.	D=	296′	D=	297′	D=	298′	D=	299′	D=	300′	D=	400′	D=	500′	Course.
ပိ	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	LAT.	DEP.	Col
0 1 2 3 4	296.0 296.0 295.8 295.6 295.3	5.2 10.3 15.5	297.0 297.0 296.8 296.6 296.3	5.2 10.4 15.5	298.0 298.0 297.8 297.6 297.3	5.2 10.4 15.6	299.0 299.0 298.8 298.6 298.3	5.2 10.4 15.6	300.0 300.0 299.8 299.6 299.3	5.2 10.5 15.7	400.0 399.9 399.8 399.4 399.0	7.0 13.9 20.9	500.0 499.9 499.7 499.3 498.8		90 89 88 87 86
56 78 9	294.9 294.4 293.8 293.1 292.4	25.8 30.9 36.1 41.2	295.9 295.4 294.8 294.1 293.3	25.9 31.0 36.2 41.3	296.9 296.4 295.8 295.1 294.3	26.0 31.1 36.3 41.5	297.9	26.1 31.3 36.4 41.6	298.9 298.4 297.8 297.1 296.3	26.1 31.4 36.6 41.8	398.5 397.8 397.0 396.1 395.1	34.9 41.8 48.7 55.7	498.1 497.3 496.3 495.1 493.8	43.6 52.3 61.0 69.6 78.2	85 84 83 82 81
10 11 12 13 14	291.5 290.6 289.5 288.4 287.2	56.5 61.5 66.6	292.5 291.5 290.5 289.4 288.2	56.7 61.7 66.8 71.9	293.5 292.5 291.5 290.4 289.1	56.9 62.0 67.0	294.5 293.5 292.5 291.3 290.1	57.1 62.2 67.3 72.3	295.4 294.5 293.4 292.3 291.1	57.2 62.4 67.5	393.9 392.6 391.3 389.8 388.1	76.3 83.1 90.0	492.4 490.8 489.1 487.2 485.1	112.4	80 79 78 77 76
15 16 17 18 19	285.9 284.5 283.1 281.5 279.9	81.6 86.5 91.5 96.4	286.9 285.5 284.0 282.5 280.8	81.9 86.8 91.8 96.7	287.8 286.5 285.0 283.4 281.8	82.1 87.1 92.1 97.0	288.8 287.4 285.9 284.4 282.7	82.4 87.4 92.4 97.3	289.8 288.4 286.9 285.3 283.7	82.7 87.7 92.7 97.7	384.5 382.5 380.4 378.2	103.5 110.2 117.0 123.6 130.2	480.6 478.1 475.5 472.8	1 37.8 1 4 6.2 1 5 4.5 1 6 2.8	75 74 73 72 71
20 21 22 23 24	278.1 276.3 274.4 272.5 270.4	106.1 110.9 115.7 120.4	277·3 275·4 273·4 271·3	106.4 111.3 116.0 120.8	278.2 276.3 274.3 272.2	106.8 111.6 116.4 121.2	279.1 277.2 275.2 273.2	107.2 112.0 116.8 121.6	280.1 278.2 276.2 274.1	102.6 107.5 112.4 117.2 122.0	373·4 370·9 368·2 365·4	143.4 149.8 156.3 162.7	466.8 463.8 460.2 456.8	179.2 187.3 195.4 203.4	70 69 68 67 66
25 26 27 28 29		129.8 134.4 139.0 143.5	266.9 264.6 262.2 259.8	130.2 134.8 139.4 144.0	267.8 265.5 263.1 260.6	130.6 135.3 139.9 144.5	268.7 266.4 264.0 261.5	131.1 135.7 140.4 145.0	269.6 267.3 264.9 262.4	126.8 131.5 136.2 140.8 145.4	359.5 356.4 353.1 349.8	175.4 181.6 187.8 193.9	449·4 445·5 441·5 437·3	219.2 227.0 234.7 242.4	63 62 61
30 31 32 33 34	253.7 251.0	152.5 156.9 161.2	254.6 251.9 249.1	153.0 157.4 161.8 166.1	255.4 252.7 249.9 247.1	153.5 157.9 162.3 166.6	256.3 253.6 250.8 247.9	154.0 158.4 162.8 167.2	257. 1 254.4 251.6 248.7	150.0 154. 5 159.0 163.4 167.8	342.9 339.2 335.5 331.6	206.0 211.9 217.8 223.7	428.6 424.0 419.3 414.5	257.5 265.0 272.3 279.6	60 59 58 57 56
35 36 37 38 39	239.5 236.4 233.3 230.0	178.1 182.2 186.3	240.3 237.2 234.0 230.8	174.6 178.7 182.9 186.9	24 1.1 238.0 234.8 231.6	175.2 179.3 183.5 187.5	241.9 238.8 235.6 232.4	175.7 179.9 184.1 188.2	242.7 239.6 236.4 233.1	172.1 176.3 180.5 184.7 188.8	323.6 319.4 315.2 310.9	235.1 240.7 246.3 251.7	404.5 399.3 394.0 388.6	293.9 300.9 307.8 314.7	55 54 53 52 51
42 43 44	223.4 220.0 216.5 212.9	194.2 198.1 201.9 205.6	224.1 220.7 217.2 213.6	194.8 198.7 202.6 206.3	224.9 221.5 217.9 214.4	195.5 199.4 203.2 207.0	225.7 222.2 218.7 215.1	196.2 200.1 203.9 207. 7	226.4 222.9 219.4 215.8	200.7 204.6 208.4	301.9 297.3 292.6 287.7	262.4 267.7 272.8 277.9	377·3 371·6 365·7 359·7	328.0 334.6 341.0 347.3	49 48 47 46
45										212.1					45
Course.	DEP.		DEP.	LAT. 297'	DEP.	298′	DEP.	299'	DEP.	300′	DEP.		DEP.	_	Course.

•	•	
7		

Total correction of the observed altitude of a Star or Planet.

· Star's	[C	H Correct		of th									:.]	Star's
Altitude	3 ^m	4 ^m	5 ^m	6 ^m	7 ^m	8 ^m	9 ^m	10^{m}	IIm	12 ^m	13 ^m	I4 ^m	15 ^m	Altitude
	10′	13'	16′	20'	23'	26′	30′	33′	36′	39'	43'	46′	49'	
8° 0' 10 20 30 40 50	9.8 9.6 9.5 9.4 9.3 9.2	10.3 10.1 10.0 9.9 9.8 9.7	10.7 10.5 10.4 10.3 10.2	11.1 10.9 10.8 10.7 10.6	/ 11.5 11.3 11.2 11.1 11.0	11.8 11.6 11.5 11.4 11.3	12.1 11.9 11.8 11.7 11.6	12.4 12.2 12.1 12.0 11.9 11.8	12.7 12.5 12.4 12.3 12.2 12.1	13.0 12.8 12.7 12.6 12.5 12.4	13.3 13.1 13.0 12.9 12.8 12.7	13.6 13.4 13.3 13.2. 13.1 13.0	13.8 13.6 13.5 13.4 13.3 13.2	8° 0 10 20 30 40 50
9 0 20 40 10 0 20	9.1 8.9 8.7 8.5 8.4	9.6 9.4 9.2 9.0 8.9	9.8 9.6 9.4 9.3	10.4 10.2 10.0 9.8 9.7	10.8 10.6 10.4 10.2 10.1	11.1 10.9 10.7 10.5 10.4	11.4 11.2 11.0 10.8 10.7	11.7 11.5 11.3 11.1	12.0 11.8 11.6 11.4 11.3	12.3 12.1 11.9 11.7 11.6	12.6 12.4 12.2 12.0 11.9	12.9 12.7 12.5 12.3 12.2	13.1 12.9 12.7 12.5 12.4	9 0 20 40 10 0 20
40 11 0 30 12 0 30	8.2 8.0 7.8 7.7 7.5	8.7 8.5 8.3 8.2 8.0	9.1 8.9 8.7 8.6 8.4	9.5 9.3 9.1 9.0 8.8	9.9 9.7 9.5 9.4 9.2	10.2 10.0 9.8 9.7 9.5	10.5 10.3 10.1 10.0 9.8	10.8 10.6 10.4 10.3 10.1	11.1 10.9 10.7 10.6 10.4	11.4 11.2 11.0 10.9 10.7	11.7 11.5 11.3 11.2	11.8 11.6 11.5 11.3	12.2. 12.0 11.8 11.7 11.5	40 11 0 30 12 0 30
13 0 30 14 0 30 15 0	7·3 7·2 7·0 6.9 6.8	7.8 7.7 7.5 7.4 7.3	8.2 8.1 7.9 7.8 7.7	8.6 8.5 8.3 8.2 8.1	9.0 8.9 8.7 8.6 8.5	9.3 9.2 9.0 8.9 8.8	9.6 9.5 9.3 9.2 9.1	9.9 9.8 9.6 9.5 9.4	10.2 10.1 9.9 9.8 9.7	10.5 10.4 10.2 10.1 10.0	10.8 10.7 10.5 10.4 10.3	11.1 11.0 10.8 10.7 10.6	11.3 11.2. 11.0 10.9 10.8	13 0 30 14 0 30 15 0
30 16 0 17 0 18 0 19 0	6.7 6.5 6.3 6.1 6.0	7.2 7.0 6.8 6.6 6.5	7.6 7.4 7.2 7.0 6.9	8.0 7.8 7.6 7.4 7.3	8.4 8.2 8.0 7.8 7.7	8.7 8.5 8.3 8.1 8.0	9.0 8.8 8.6 8.4 8.3	9·3 9·1 8·9 8·7 8.6	9.6 9.4 9.2 9.0 8.9	9·9 9·7 9·5 9·3 9·2	10.2 10.0 9.8 9.6 9.5	10.5 10.3 10.1 9-9 9.8	10.7 10.5 10.3 10.1	30 16 0 17 0 18 0 19 0
20 0 22 0 24 0 26 0 28 0	5.8 5.6 5.4 5.2 5.0	6.3 6.1 5.9 5.7 5.5	6.7 6.5 6.3 6.1 5.9	7.1 6.9 6.7 6.5 6.3	7·5 7·3 7·1 6.9 6.7	7.8 7.6 7.4 7.2 7.0	8.1 7.9 7.7 7.5 7.3	8.4 8.2 8.0 7.8 7.6	8.7 8.5 8.3 8.1 7.9	9.0 8.8 8.6 8.4 8.2	9·3 9·1 8·9 8·7 8·5	9.6 9.4 9.2 9.0 8.8	9.8 9.6 9.4 9.2 9.0	20 0 22 0 24 0 26 0 28 0
30 0 32 0 34 0 36 0 38 0	4.9 4.7 4.6 4.5 4.4	5.4 5.2 5.1 5.0 4.9	5.8 5.6 5.5 5.4 5.3	6.2 6.0 5.9 5.8 -5.7	6.6 6.4 6.3 6.2 6.1	6.9 6.7 6.6 6.5 6.4	7.2 7.0 6.9 6.8 6.7	7·5 7·3 7·2 7·1 7·0	7.8 7.6 7.5 7.4 7.3	8.1 7.9 7.8 7.7 7.6	8.4 8.2 8.1 8.0 7.9	8.7 8.5 8.4 8.3 8.2	8.9 8.7 8.6 8.5 8.4	30 0 32 0 34 0 36 0 38 0
40 0 45 0 50 0 55 0 60 0	4.3 4.2 4.0 3.9 3.7	4.8 4.7 4.5 4.4 4.2	5.2 5.1 4.9 4.8 4.6	5.6 5.5 5.3 5.2 5.0	6.0 5.9 5.7 5.6 5.4	6.3 6.2 6.0 5.9 5.7	6.6 6.5 6.3 6.2 6.0	6.9 6.8 6.6 6.5 6.3	7.2 7.1 6.9 6.8 6.6	7.5 7.4 7.2 7.1 6.9	7.8 7.7 7.5 7.4 7.2	8.1 8.0 7.8 7.7 7.5	8.3 8.2 8.0 7.9 7.7	40 0 45 0 50 0 55 0 60 0
65 0 70 0 75 0 80 0 85 0	3.6 3.5 3.4 3.4 3.3	4.1 4.0 3.9 3.9 3.8	4.5 4.4 4.3 4.3 4.2	4.9 4.8 4.7 4.7 4.6	5.3 5.2 5.1 5.1 5.0	5.6 5.5 5.4 5.4 5.3	5.9 5.8 5.7 5.7 5.6	6.2 6.1 6.0 6.0 5.9	6.5 6.4 6.3 6.3 6.2	6.8 6.7 6.6 6.6 6.5	7.1 7.0 6.9 6.9 6.8	7.4 7.3 7.2 7.2 7.1	7.6 7.5 7.4 7.4 7.3	65 o 70 o 75 o 80 o 85 o
90 0 Dip of Sea	3.2	3.7	4.1	4.5	4.9	5.2	5-5	5.8	6.1	6.4	6.7	7.0		{ 90 0 Horizon.

Correction	unet's itude			Pla		itude	Additional Correction to be added to						
for parallax to be	Pla	6′′	9"	12"	15"	18"	21"	24''	27′′	30′′	33''	Pla	Correction given for 15 ^m
subtracted from Star's Correction	10° 30 50 70 90	o'.I o.I o.0 o.0	1.°0 1.0 1.0 1.0	o'.2 o.2 o.I o.I	o'.2 o.2 o.2 o.1 o.0	o'.3 o.3 o.2 o.1	o'.3 o.3 o.2 o.1 o.0	o'.4 o.3 o.2 o.1	o'.4 o.4 o.3 o.2 o.0	o'.5 o.4 o.3 o.2 o.0	o'.5 o.5 o.4 o.2	10° 30 50 70 90	16 ^m or 52 /.2 17 ,, 56 .4 18 ,, 59 .6 19 ,, 62 .8 20 ,, 66 1.0

Mean Time		Conversion of Intervals of Mean Solar Time into Equivalent Intervals of Sidereal Time. [Correction to be added to the Interval of Mean Time.]																Mean Time																																																			
2	OI	n	4	ni	8	3m	r	12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		12 ^m		6m	2	o m	2	4 ^m	2	8m	3	2m	3	6m	40	om	4	4 ^m	4	8m	5	2m	5	6 m	M
h 0 1 2 3	0 2	s 0 10 20	0	s 1 11 20 30	m 0 0 0	s 1 11 21 31	m 0 0 0	s 2 12 22 32	m 0 0 0	s 3 12 22 32	m 0 0 0	s 3 13 23 33	0	s 4 14 24 34	m. 0 0 0	5 14 24 34		s 5 15 25 35	m 0 0 0 0	s 6 16 26 36	0	s 7 16 26 36		s 7 17 27 37	m 0 0 0 0	s 8 18 28 37	m 0 0 0 0	s 9 18 28 38	0	s 9 19 29	h 0 1 2																																						
4 5 6 7	0 4 0 5 I	39 19 39 9	O I I		o I I	41 51 0	0 1	41 51 1	I I	42 52 2 12	O I I	43 53 2 12	O I I	43 53 3 13	O I I	44 54 4 14	0 1	45 55 4 14	O I I	45 55 5	I	46 56 6 16	O I I	47 57 6 16		47 57 7 17	0 1	48 58 8 18	0 1 1	49 58 8 18	4 5 6 7																																						
8 9 10 11	1 3 1 4	9	I I	29 39 49	I I	30 40 50	I I	31 41 50		21 31 41 51	I	32 42 52	I	23 33 43 52	I I I I	23 33 43 53	I I I I	24 34 44 54	I I	25 35 45 54	I	25 35 45 55	I I I I	26 36 46 56		27 37 46 56	I I I I	27 37 47 57	1	28 38 48 58	8 9 10 11																																						
13 14 15	2 2 I 2 2	8	2 2 2	9 19 29	2 2 2	9 19 29	2 2	10 20 30	2 2 2	11 21 30	2 2	11 21 31	2 2	12 22 32 42	2 2 2	13 23 32 42	2 2 2	13 23 33	2	14 24 34 44	2 2 2	15 25 34 44	2 2 2	15	2	16 26 36	2 2 2	17 27 36 46	2 2	17 27 37	13 14 15																																						
17 18 19	2 4 2 5	8 7 7	2 3			49 59 9		50 59 9	2 3 3	50 0 10	3	51 1 11		52 I II	3	52 2 12		53 3 13	3	53 3 13	3 3	54 4 14	3 3	55 5 15 24	3	55 5 15	3 3	56 6 16	3	57 7 16	17 18 19																																						
21 22 23	3 2 3 3 3 4	7 7 7	3 3 3 3 3	28 38 47	3 3 3	28 38 48	3 3	29 39 49	3 3 3	30 39 49	3 3 3	30 40 50	3 3	31 41 51	3 3	32 41 51	3 3 3	32 42 52	3 3 3	33 43 53	3 3	34 43 53	3 3	34 44 54	3 3 3	35 45 55	3 3 3	36 45 55	3 3 3	36 46 56	21 22 23																																						
	This	tal	ble	giv	es	the	A	ccele	era	tion	<i>z</i> 0	$f \left\{ $	he	R.A	l o	n M	Iea . (S	n S side:	ola rea	r T	im	e. e at	G	reer	ıwi	ch l	Me	an i	No	on)																																							

Conversion of Time into Arc and vice-versa																	
	o h	rh	2h	3 ^h	4 ^h	5 ^h	6h	7 ^h	8 ^h	9 ^h	10h	IIh		om	Im	2 ^m	3 ^m
m 0 4 8	0 0 I 2	° 15 16	30 31 32	45 46 47	60 61 62	75 76 77	90 91 92	105 106 107	0 120 121 122	135 136 137	150 151 152	165 166 167	s 0 4 8	, o I 2	15 16 17	30 31 32	45 46 47
12 16 20	3 4 5	18 19 20	33 34 35	48 49 50	63 64 65	78 79 80	93 94 95	109	123 124 125	138 139 140	153 154 155	168 169 170	12 16 20	3 4 5	18 19 20	33 34 35	48 49 50
24 28 32	6 7 8	2I 22 23	36 37 38	51 52 53	66 6 7 68	81 82 83	96 97 98	111 112 113	126 127 128	141 142 143	156 157 158	171 172 173	24 28 32	6 7 8	21 22 23	36 37 38	51 52 53
36 40 44	9 10	24 25 26	39 40 41	54 55 56	69 70 71	84 85 86	99 100	114 115 116	129 130 131	144 145 146	159 160 161	174 175 176	36 40 44	9 10	24 25 26	39 40 41	54 55 56
48 52 56	12 13 14	27 28 29	42 43 44	57 58 59	72 73 74	87 88 89	102 103 104	117	132 133 134	147 148 149	162 163 164	177 178 179	48 52 56	13	27 28 29	42 43 44	57 58 59

Sidereal Time	F		E	version of quivalent orrection to b	Inte	rvals of	Mean S	Solar Ti	ne.		Sidereal Time				
Sid	o m	4 ^m	8 ^m	12 ^m 16 ^m	20 ^m	24 ^m 28 ^m	32 ^m 36 ^m	40 ^m 44 ^m	48 ^m 52	^m 56 ^m	Sid				
h 0 1 2	0 0 0 0 1 0 1 0 1 0 2 0 3 0 3 0 4 0 5 0 5 0 6 0 7 0 7 0 8 0 9 0 9 0 1 0 10 0 10 0 11 0 12 0 12 0														
4 5 6 7	1 0 10 0 10 0 11 0 12 0 12 0 13 0 14 0 14 0 15 0 16 0 16 0 17 0 18 0 18 0 19 1 2 0 20 0 20 0 21 0 22 0 23 0 24 0 24 0 25 0 26 0 26 0 27 0 28 0 28 0 29 2 3 0 29 0 30 0 31 0 31 0 32 0 33 0 33 0 34 0 35 0 35 0 36 0 37 0 37 0 38 0 39 3 4 0 39 0 40 0 41 0 41 0 42 0 43 0 43 0 44 0 45 0 45 0 45 0 46 0 47 0 47 0 48 0 48 4 5 0 49 0 50 0 50 0 51 0 52 0 52 0 53 0 54 0 54 0 55 0 56 0 56 0 57 0 58 0 58 5 6 0 59 1 0 1 0 1 1 1 2 1 2 1 3 1 4 1 4 1 5 1 6 1 6 1 7 1 7 1 8 6														
9 10 11	1 19 1 28 1 38 1 48	1 19 1 29 1 39 1 49	1 20 1 30 1 40 1 49	1 40 1 41	I 32 I I 42 I	I 23 I 23 I 33 I 42 I 43 I 52 I 53	I 24 I 25 I 34 I 34 I 44 I 44 I 53 I 54	1 25 1 26 1 35 1 36 1 45 1 46 1 55 1 55	1 36 1 1 1 46 1 4	27 I 28 37 I 38 47 I 47 57 I 57	9 10 11				
12 13 14 15	1 58 2 8 2 18 2 27	1 59 2 8 2 18 2 28	1 59 2 9 2 19 2 29	2 10 2 10 2 20 2 20	2 II 2 2 2I 2	2 2 2 3 2 12 2 12 2 22 2 22 2 31 2 32	2 3 2 4 2 13 2 14 2 23 2 24 2 33 2 33	2 5 2 5 2 14 2 15 2 24 2 25 2 34 2 35	2 25 2	6 2 7 16 2 17 26 2 27 36 2 37	12 13 14 15				
16 17 18 19	2 37 2 47 2 57 3 7	2 38 2 48 2 58 3 7	2 39 2 48 2 58 3 8	2 39 2 40 2 49 2 50 2 59 3 0 3 9 3 9	2 50 2	2 41 2 42 2 51 2 52 3 1 3 2 3 11 3 11	2 43 2 43 2 52 2 53 3 2 3 3 3 12 3 13	2 44 2 44 2 54 2 54 3 3 3 4 3 13 3 14	2 55 2 3	46 2 46 56 2 56 5 3 6 15 3 16	16 17 18 19				
20 21 22 23	3 17 3 26 3 36 3 46	3 17 3 27 3 37 3 47	3 18 3 28 3 38 3 47	3 19 3 19 3 28 3 29 3 38 3 39 3 48 3 49	3 30 3 3 40 3	3 21 3 21 3 30 3 31 3 40 3 41 3 50 3 51	3 22 3 22 3 32 3 32 3 41 3 42 3 51 3 52	3 23 3 24 3 33 3 34 3 43 3 43 3 53 3 53	3 34 3 3 44 3	25 3 26 35 3 36 45 3 45 55 3 55	20 21 22 23				
			This	table gives	the Reta	ardation of	Mean Solar	on Sidereal	Γime.						

			Cor	vers	sion	of 7	$\Gamma im \epsilon$	e int	o A	rc a	nd v	vice-	ver	sa.			
	12h	13 ^h	14 ^h	15 ^h	16 ^h	17 ^h	18h	19 ^h	20 ^h	21 ^h	22 ^h	23 ^h		o ^m	1 ^m	2 ^m	3 ^m
m 0 4 8 12 16 20 24 28 32 36	m																
40 44	190	204 205 206	219 220 221	234 235 236	249 250 251	264 265 266	279 280 281	294 295 296	310	324 325 326	339 340 341	354 355 356	36 40 44	9 10 11	24 25 26	39 40 41	54 55 56
48 52 56	192 193 194	207 208 209	222 223 224	237 238 239	252 253 254	267 268 269	282 283 284	297 298 299	312 313 314	327 328 329	342 343 344	357 358 359	48 52 56	12 13 14	27 28 29	42 43 44	57 58 59

O Tota	al co	orrec	tion	of t	he o	bser	ved	altitı	ıde o	of the	Su	n's l	lowe	r limb.
Sun's										res an Sun's le				6. 1
Altitude	3 ^m	4 ^m	5 ^m	6m	7 ^m	8m	9 ^m	10 ^m	II ^m	-		14 ^m	15 ^m	Sun's
7 Intitude	10'	13'	16'	20'	23'	26'	30'	33'	36′		43'	46'	49'	Altitude
8° 0' 10 20 30 40 50	6.4 6.5 6.6 6.7 6.9 7.0	5.9 6.0 6.1 6.2 6.4 6.5	5.5 5.6 5.7 5.8 6.0 6.1	5.1 5.2 5.3 5.4 5.6 5.7	4.7 4.8 4.9 5.0 5.2 5.3		4.1 4.2 4.3 4.4 4.6 4.7	3.8 3.9 4.0 4.1 4.3 4.4	3.5 3.6 3.7 3.8 4.0 4.1	3.2 3.3 3.4 3.5 3.7 3.8	2.9 3.0 3.1 3.2 3.4 3.5	2.6 2.7 2.8 2.9 3.1 3.2	2.4 2.5 2.6 2.7 2.9 3.0	8° 0' 10 20 30 40 50
9 0 20 40 10 0 20	7·1 7·3 7·5 7·6 7·8	6.6 6.8 7.0 7.1 7.3	6.2 6.4 6.6 6.7 6.9	5.8 6.0 6.2 6.3 6.5	5.4 5.6 5.8 5.9 6.1	5.1 5.3 5.5 5.6 5.8	4.8 5.0 5.2 5.3 5.5	4.5 4.7 4.9 5.0 5.2	4.2 4.4 4.6 4.7 4.9	3.9 4.1 4.3 4.4 4.6	3.6 3.8 4.0 4.1 4.3	3·3 3·5 3·7 3.8 4·0	3.1 3.3 3.5 3.6 3.8	9 0 20 40 10 0 20
40 11 0 30 12 0 30	8.0 8.1 8.3 8.5 8.7	7.5 7.6 7.8 8.0 8.2	7.1 7.2 7.4 7.6 7.8	6.7 6.8 7.0 7.2 7.4	6.3 6.4 6.6 6.8 7.0	6.0 6.1 6.3 6.5 6.7	5.7 5.8 6.0 6.2 6.4	5.4 5.5 5.7 5.9 6.1	5.1 5.2 5.4 5.6 5.8	4.8 4.9 5.1 5.3 5.5	4.5 4.6 4.8 5.0 5.2	4.2 4.3 4.5 4.7 4.9	4.0 4.1 4.3 4.5 4.7	40 11 0 30 12 0 30
13 0 30 14 0 30 15 0	8.8 9.0 9.1 9.2 9.3	8.3 8.5 8.6 8.7 8.8	7.9 8.1 8.2 8.3 8.4	7.5 7.7 7.8 7.9 8.0	7·1 7·3 7·4 7·5 7·6	6.8 7.0 7.1 7.2 7.3	6.5 6.7 6.8 6.9 7.0	6.2 6.4 6.5 6.6 6.7	5.9 6.1 6.2 6.3 6.4	5.6 5.8 5.9 6.0 6.1	5·3 5·5 5.6 5·7 5.8	5.0 5.2 5.3 5.4 5.5	4.8 5.0 5.1 5.2 5.3	13 0 30 14 0 30 15 0
19 0	9.4 9.6 9.8 10.0	8.9 9.1 9.3 9.5 9.7	8.5 8.7 8.9 9.1 9.3	8.1 8.3 8.5 8.7 8.9	7·7 7·9 8.1 8.3 8.5	7.4 7.6 7.8 8.0 8.2	7.1 7.3 7.5 7.7 7.9	6.8 7.0 7.2 7.4 7.6	6.5 6.7 6.9 7.1 7.3	6.2 6.4 6.6 6.8 7.0	5.9 6.1 6.3 6.5 6.7	5.6 5.8 6.0 6.2 6.4	5.4 5.6 5.8 6.0 6.2	30 16 0 17 0 18 0 19 0
22 0 24 0 26 0	10.3 10.6 10.8 10.9	9.8 10.1 10.3 10.4 10.6	9.4 9.7 9.9 10.0	9.0 9.3 9.5 9.6 9.8	8.6 8.9 9.1 9.2 9.4	8.3 8.6 8.8 8.9 9.1	8.0 8.3 8.5 8.6 8.8	7.7 8.0 8.2 8.3 8.5	7·4 7·7 7·9 8.0 8.2	7.1 7.4 7.6 7.7 7.9	6.8 7.1 7.3 7.4 7.6	6.5 6.8 7.0 7.1 7.3	6.3 6.6 6.8 6.9 7.1	20 0 22 0 24 0 26 0 28 0
32 0 34 0 36 0	11.3 11.4 11.5 11.6	10.8 10.9 11.0 11.1 11.2	10.4 10.5 10.6 10.7 10.8	10.0 10.1 10.2 10.3 10.4	9.6 9.7 9.8 9.9	9·3 9·4 9·5 9.6 9·7	9.0 9.1 9.2 9.3 9.4	8.7 8.8 8.9 9.0 9.1	8.4 8.5 8.6 8.7 8.8	8. I 8. 2 8. 3 8. 4 8. 5	7.8 7.9 8.0 8.1 8.2	7.5 7.6 7.7 7.8 7.9	7·3 7·4 7·5 7·6 7·7	30 0 32 0 34 0 36 0 38 0
45 0 50 0 55 0	11.8 11.9 12.1 12.2 12.3	11.3 11.4 11.6 11.7 11.8	10.9 11.0 11.2 11.3 11.4	10.5 10.6 10.8 10.9	10.1 10.2 10.4 10.5 10.6	9.8 9.9 10.1 10.2 10.3	9.5 9.6 9.8 9.9	9.2 9.3 9.5 9.6 9.7	8.9 9.0 9.2 9.3 9.4	8.6 8.7 8.9 9.0 9.1	8.3 8.4 8.6 8.7 8.8	8.0 8.1 8.3 8.4 8.5	7.8 7.9 8.1 8.2 8.3	40 0 45 0 50 0 55 0 60 0
70 0 75 0 80 0	12.4 12.5 12.6 12.7 12.7	II.9 I2.0 I2.I I2.2 I2.2	11.5 11.6 11.7 11.8 11.8	11.1 11.2 11.3 11.4 11.4	10.7 10.8 10.9 11.0	10.6	10.1 10.2 10.3 10.4 10.4	9.8 9.9 10.0 10.1	9.5 9.6 9.7 9.8 9.8	9.2 9.3 9.4 9.5 9.5	8.9 9.0 9.1 9.2 9.2	8.6 8.7 8.8 8.9 8.9	8.4 8.5 8.6 8.7 8.7	65 o 70 o 75 o 80 o 85 o
90 0 Distance of	3.6	12.3	4.7	11.5	11.1 5.6	6.0	10.5	10.2	9.9 7.0	9.6 7·3	9.3	9.0 7.9	8.8	90 0 Sea Horizon
Addition Correcti for Varia of Sun Semidiam	nal ion ition	Jan + 0'	. 1 Feb	о. т М	Ī	April 1			July 1	Aug. 1	i	ı Oc	==	o'.1 Dec. 1
Addition		16	m 17	7 ^m I	8 ^m	19 ^m	20 ^m	21 ^m	22 ^m	23 ^m	24 ⁿ			6m 27m
Correction be subtracte Correct	d from	n 52	5	6′ !	59'	62'	66′	62'	72'	76′	79′	-		85′ 89′
given for I		-0'	.2 - 0	0'.4 -	0′.6	-0'.8	- 1'.0	- 1'.2	- 1'.4	- 1'.6	- I'.	8 - 1	./9 -	2'.0 - 2'.1

⊙ Tot	al co	orrec	tion	of th	ie o	bserv	red a	eltitu	de o	f the	Su	n's ı	ıppe	r limb.
Sun's	[Co		0			abov							nb.]	Sun's
Altitude	3 ^m	4 ^m	5 ^m	6 ^m	7 ^m	8 ^m	9 ^m	10 ^m	IIm	12 ^m	13 ^m	14 ^m	15 ^m	Altitude
	10′	13'	16'	20′	23′	26′	30′	33′	36′	39′	43′	46′	49'	
8° 0' 10 20 30 40 50	25.6 25.5 25.4 25.3 25.1 25.0	26.1 26.0 25.9 25.8 25.6 25.5	26.5 26.4 26.3 26.2 26.0 25.9	26.9 26.8 26.7 26.6 26.4 26.3	27.3 27.2 27.1 27.0 26.8 26.7	27.6 27.5 27.4 27.3 27.1 27.0	27.9 27.8 27.7 27.6 27.4 27.3	28.2 28.1 28.0 27.9 27.7 27.6	28.5 28.4 28.3 28.2 28.0 27.9	28.8 28.7 28.6 28.5 28.3 28.2	29.1 29.0 28.9 28.8 28.6 28.5	29.4 29.3 29.2 29.1 28.9 28.8	29.6 29.5 29.4 29.3 29.1 29.0	8° 0′ 10 20 30 40 50
9 0 20 40 10 0 20	24.9 24.7 24.5 24.4 24.2	25.4 25.2 25.0 24.9 24.7	25.8 25.6 25.4 25.3 25.1	26.2 26.0 25.8 25.7 25.5	26.6 26.4 26.2 26.1 25.9	26.9 26.7 26.5 26.4 26.2	27.2 27.0 26.8 26.7 26.5	27.5 27.3 27.1 27.0 26.8	27.8 27.6 27.4 27.3 27.1	28.I 27.9 27.7 27.6 27.4	28.4 28.2 28.0 27.9 27.7	28.7 28.5 28.3 28.2 28.0	28.9 28.7 28.5 28.4 28.2	9 0 20 40 10 0 20
40 11 0 30 12 0 30	24.0 23.9 23.7 23.5 23.3	24.5 24.4 24.2 24.0 23.8	24.9 24.8 24.6 24.4 24.2	25.3 25.2 25.0 24.8 24.6	25.7 25.6 25.4 25.2 25.0	26.0 25.9 25.7 25.5 25.3	26.3 26.2 26.0 25.8 25.6	26.6 26.5 26.3 26.1 25.9	26.9 26.8 26.6 26.4 26.2	27.2 27.1 26.9 26.7 26.5	27.5 27.4 27.2 27.0 26.8	27.8 27.7 27.5 27.3 27.1	28.0 27.9 27.7 27.5 27.3	40 11 0 30 12 0 30
13 0 30 14 0 30 15 0	23.2 23.0 22.9 22.8 22.7	23.7 23.5 23.4 23.3 23.2	24.1 23.9 23.8 23.7 23.6	24.5 24.3 24.2 24.1 24.0	24.9 24.7 24.6 24.5 24.4	25.2 25.0 24.9 24.8 24.7	25.5 25.3 25.2 25.1 25.0	25.8 25.6 25.5 25.4 25.3	26.1 25.9 25.8 25.7 25.6	26.4 26.2 26.1 26.0 25.9	26.7 26.5 26.4 26.3 26.2	27.0 26.8 26.7 26.6 26.5	27.2 27.0 26.9 26.8 26.7	13 0 30 14 0 30 15 0
30 16 0 17 0 18 0 19 0	22.6 22.4 22.2 22.0 21.8	23.1 22.9 22.7 22.5 22.3	23.5 23.3 23.1 22.9 22.7	23.9 23.7 23.5 23.3 23.1	24.3 24.1 23.9 23.7 23.5	24.6 24.4 24.2 24.0 23.8	24.9 24.7 24.5 24.3 24.1	25.2 25.0 24.8 24.6 24.4	25.5 25.3 25.1 24.9 24.7	25.8 25.6 25.4 25.2 25.0	26.1 25.9 25.7 25.5 25.3	26.4 26.2 26.0 25.8 25.6	26.6 26.4 26.2 26.0 25.8	30 16 0 17 0 18 0 19 0
20 0 22 0 24 0 26 0 28 0	21.7 21.5 21.3 21.1 20.9	22.2 22.0 21.8 21.6 21.4	22.6 22.4 22.2 22.0 21.8	23.0 22.8 22.6 22.4 22.2	23.4 23.2 23.0 22.8 22.6	23.7 23.5 23.3 23.1 22.9	24.0 23.8 23.6 23.4 23.2	24.3 24.1 23.9 23.7 23.5	24.6 24.4 24.2 24.0 23.8	24.9 24.7 24.5 24.3 24.1	25.2 25.0 24.8 24.6 24.4	25.5 25.3 25.1 24.9 24.7	25.7 25.5 25.3 25.1 24.9	20 0 22 0 24 0 26 0 28 0
30 0 32 0 34 0 36 0 38 0	20.7 20.6 20.5 20.4 20.3	21.2 21.1 21.0 20.9 20.8	21.6 21.5 21.4 21.3 21.2	22.0 21.9 21.8 21.7 21.6	22.4 22.3 22.2 22.1 22.0	22.7 22.6 22.5 22.4 22.3	23.0 22.9 22.8 22.7 22.6	23.3 23.2 23.1 23.0 22.9	23.6 23.5 23.4 23.3 23.2	23.9 23.8 23.7 23.6 23.5	24.2 24.1 24.0 23.9 23.8	24.5 24.4 24.3 24.2 24.1	24.7 24.6 24.5 24.4 24.3	30 0 32 0 34 0 36 0 38 0
40 0 45 0 50 0 55 0 60 0	20.2 20.1 19.9 19.8 19.7	20.7 20.6 20.4 20.3 20.2	21.1 21.0 20.8 20.7 20.6	21.5 21.4 21.2 21.1 21.0	21.9 21.8 21.6 21.5 21.4	22.2 22.1 21.9 21.8 21.7	22.5 22.4 22.2 22.1 22.0	22.8 22.7 22.5 22.4 22.3	23.I 23.0 22.8 22.7 22.6	23.4 23.3 23.1 23.0 22.9	23.7 23.6 23.4 23.3 23.2	24.0 23.9 23.7 23.6 23.5	24.2 24.1 23.9 23.8 23.7	40 0 45 0 50 0 55 0 60 0
65 0 70 0 75 0 80 0 85 0	19.6 19.5 19.4 19.3	20.1 20.0 19.9 19.8 19.8	20.5 20.4 20.3 20.2 20.2	20.9 20.8 20.7 20.6 20.6	21.3 21.2 21.1 21.0 21.0	3	21.9 21.8 21.7 21.6 21.6	22.2 22.1 22.0 21.9 21.9	22.5 22.4 22.3 22.2 22.2	22.8 22.7 22.6 22.5 22.5	23.I 23.0 22.9 22.8 22.8	23.4 23.3 23.2 23.1 23.1	23.6 23.5 23.4 23.3 23.3	65 0 70 0 75 0 80 0 85 0
90 0 Distance of	19.2 3.6	19.7 4.2	20.1 4·7	20.5 5.2	20.9 5.6	6.0	6.3	21.8 6.7	7.0	7:3	^{22.} 7 7.6	7.9	23.2 8.1	90 0 Sea Horizon
Additi Correct for Varion of Su Semidia	tion iation in's	Jan	_		o'.2	April 1		June 1 +0'.2	July 1	Aug. +0'.	Sept 2 +0	-	et. 1 N	ov. I Dec. I
Additi Correct		16			8 ^m	19 ^m	20 ^m	2I ^m	22 ^m	23 ^m				26 ^m 27 ^m
be add Correct given fo	ed to	+0			59' o'.6	62' + o'.8	66′ + 1′.0	69' + 1'.2	72' + 1'.4	76' + 1'.	=			85' 89' 2'.0 +2'.1

Total correction of the observed altitude of the Moon's lower limb.

itude.		[Cor					oove t								tude.	
Moon's Altitude.			Ho	rizont	al Se	midia	amete	r fron	ı Naı	ıtical	Alma	inac.			Moon's Altitude.	
Moor		4′				5′					1	6′			Moon	
	40′′	50"	0"	10"	20"	30"	40"	50"	0"	10"	20"	30"	40"	50"		
8° 9	57.0 57.6	57.8 58.3	58.6 59.1	59.3 59.8	60.1 60.6	60.9 61.4	61.7 62.2	62.4 62.9	63.2 63.7	64.0 64.5	64.7 65.3	65.5 66.1	66.3 66.8	67.1 67.6	8° 9	
10 11 12 13	58.c 58.3 58.5 58.6	58.8 59.0 59.3 59.4	59.5 59.8 60.0 60.1	60.3 60.6 60.8 60.9	61.0 61.3 61.5 61.6	61.8 62.1 62.3 62.4	62.6 62.9 63.1 63.2	63.3 63.6 63.8 63.9	64.1 64.3 64.6 64.7	64.9 65.2 65.4 65.5	65.6 65.9 66.1 66.2	66.4 66.7 66.9 67.0	67.2 67.5 67.7 67.8	68.0 68.2 68.4 68.5	10 11 12 13	
14 15 16 17	58.7 58.7 58.7 58.6	59·5 59·5 59·5 59·4	60.2 60.2 60.1	61.0 61.0 61.0 60.9	61.7 61.7 61.7 61.6	62.5 62.5 62.5 62.4	63.3 63.2 63.1	64.0 64.0 63.9	64.8 64.8 64.7 64.6	65.6 65.5 65.5 65.4	66.3 66.2 66.1	67.0 67.1 67.0 66.9	67.8 67.8 67.7 67.6	68.6 68.6 68.5 68.4	14 15 16 17	
18 19 20	58.5 59.3 60.0 60.8 61.5 62.3 63.0 63.8 64.5 65.3 66.0 66.8 67.5 68.2 58.4 59.1 59.9 60.6 61.3 62.1 62.9 63.6 64.4 65.1 65.8 66.6 67.3 68.1 58.2 59.0 59.7 60.5 61.2 61.9 62.7 63.4 64.2 64.9 65.6 66.4 67.1 67.9 58.0 58.8 59.5 60.3 61.0 61.7 62.5 63.2 63.9 64.7 65.4 66.1 66.9 67.6 57.8 58.6 59.3 60.0 60.7 61.5 62.2 63.0 63.7 64.4 65.1 65.9 66.6 67.4															
21 22 23 24	58.0 \$8.8 \$59.5 \$60.3 \$61.0 \$61.7 \$62.5 \$63.2 \$63.9 \$64.7 \$65.4 \$61.1 \$60.9 \$67.6 \$7.8 \$8.6 \$59.3 \$60.0 \$60.7 \$61.5 \$62.2 \$63.0 \$63.7 \$64.4 \$65.1 \$65.9 \$66.6 \$67.4 \$7.6 \$8.3 \$59.0 \$59.7 \$60.5 \$61.2 \$61.9 \$62.7 \$63.4 \$64.1 \$64.8 \$65.6 \$66.3 \$67.0 \$7.7 \$8.7 \$59.5 \$60.2 \$60.9 \$61.6 \$62.4 \$63.1 \$63.8 \$64.5 \$65.3 \$66.0 \$66.7 \$7.0 \$7.7 \$8.4 \$59.2 \$59.9 \$60.6 \$61.3 \$62.0 \$62.8 \$63.5 \$64.2 \$64.9 \$65.7 \$66.4 \$6.7 \$7.4 \$58.1 \$58.9 \$59.6 \$60.3 \$61.0 \$61.7 \$62.4 \$63.2 \$63.9 \$64.6 \$65.3 \$66.0															
25 26 27 28 29		$\begin{array}{cccccccccccccccccccccccccccccccccccc$														
30 31 32 33 34	55.2 54.8 54.4 54.0 53.5	55.5 55.1 54.6 54.2	56.6 56.2 55.8 55.3 54.8	57·3 56.9 56.5 56.0 55·5	58.0 57.6 57.1 56.7 56.2	58.7 58.3 57.8 57.4 56.9	59.4 59.0 58.5 58.0 57.5	60.1 59.6 59.2 58.7 58.2	60.8 6c.3 59.9 59.4 58.9	61.5 61.0 60.6 60.1 59.6	62.2 61.7 61.3 60.7 60.2	62.9 62.4 61.9 61.4 60.9	63.6 63.1 62.6 62.1 61.6	64.3 63.8 63.3 62.8 62.2	30 31 32 33 34	
35 36 37 38 39	53.0 52.5 52.0 51.5 51.0	53.7 53.2 52.6 52.1 51.6	54.4 53.9 53.3 52.8 52.2	55.0 54.5 54.0 53.4 52.9	55.7 55.1 54.6 54.1 53.5	56.4 55.8 55.3 54.7 54.2	57.0 56.5 55.9 55.4 54.8	57.7 57.2 56.6 56.0 55.4	58.4 57.8 57.3 56.7 56.1	59.0 58.5 57.9 57.3 56.7	59.7 59.1 58.6 58.0 57.4	60.4 59.8 59.2 58.6 58.0	61.0 60.5 59.9 59.3 58.7	61.7 61.1 60.5 59.9 59.3	35 36 37 38 39	
40 41 42 43 44	50.4 49.8 49.2 48.6 48.0	51.0 50.4 49.9 49.3 48.7	51.7 51.1 50.5 49.9 49.3	52.3 51.7 51.1 50.5 49.9	52.9 52.3 51.7 51.1 50.4	53.6 53.0 52.4 51.7 51.1	54.2 53.6 53.0 52.3 51.7	54.8 54.2 53.6 52.9 52.3	55.5 54.8 54.2 53.5 52.9	56.1 55.5 54.8 54.2 53.5	56.8 56.1 55.4 54.8 54.1	57.4 56.7 56.1 55.4 54.7	58.0 57.4 56.7 56.0 55.3	58.7 58.0 57.3 56.6 55.9	40 41 42 43 44	
45 46 47 48	47.4 46.8 46.1 45.5	48.0 47.4 46.7 46.1	48.6 48.0 47.3 46.6	49.2 48.6 47.9 47.2	49.8 49.1 48.5 47.8		51.0 50.3 49.6 48.9				53.4 52.7 52.0 51.2	54.0 53.3 52.6 51.8	54.6 53.9 53.1 52.4	55.2 54.5 53.7 53.0	45 46 47 48	
49	44.8		45-9	46.5	47.1	<u> </u>	48.2		49-3		50.5	51.1		52.2	1	
Height of eye		-	5 ^m	7 ^m	8m 26'			6' 39			15 ^m	16 th	56'		62' 66'	
Addition			+0.4	-0.4	-0.7		_	r.6 - 1		-	,	- 2.9			3.5 -3.7	
	Obs	ervat	ion.	For	subi	ract t	he Mo	on's I	Diame	ter fra	m val	ues g	iven f	or <u>(</u> .		

a	Total	correction	of	the	obs	erved	altitude	of	the	Moon's
				10	wer	limb.				

tude.			Heig ection													1	tude.
Moon's Altitude.			Hor	izont	al Se	midi	amet	er fr	om	Naut	lical .	Almai	nac.				Moon's Altitude.
Moon	14		-11			5′	1/		-"	o" l	10"	20"		1 40"	50′		Mooi
	40″	50"	o''	10"	20"	30"		= =	0"				30"	40"	50		
49°	44.8	45.4	45.9	46.5	47.1	47.6		١.	- 1	49.3	49.9	50.5	51.1	51.6	1		49°
50 51 52 53 54	44. I 43.4 42.7 42.0 41.3	44.7 44.0 43.3 42.5 41.8	45·3 44·5 43.8 43·1 42·3	45.8 45.1 44.3 43.6 42.8	46.4 45.6 44.9 44.1 43.4	46.9 46.2 45.5 44.7 43.9	46.	7 42	6. ₅	48.6 47.8 47.1 46.3 45.5	49.2 48.4 47.6 46.8 46.0	49.7 48.9 48.1 47.3 46.5	50.3 49.5 48.7 47.9 47.1	50.9 50.0 49.2 48.4 47.6	50.6 49.8 48.6	8	50 51 52 53 54
55 56 57 58 59	40.5 39.8 39.0 38.3 37.5	41.0 40.3 39.5 38.8 38.0	41.6 40.8 40.0 39.2 38.4	42.1 41.3 40.5 39.7 38.9	42.6 41.8 41.0 40.2 39.4	43.1 42.3 41.5 40.7 39.9	42.0	3 43 5 43 2 43	3·3 2·5	44.7 43.9 43.0 42.2 41.3	45.2 44.4 43.5 42.7 41.8	45.7 44.9 44.0 43.2 42.3	46.2 45.4 44.5 43.7 42.8	46.7 45.9 45.0 44.2 43.3	46.45.	5	55 56 57 58 59
60 61 62 63 64	36.7 37.2 37.6 38.1 38.6 39.1 39.5 40.0 40.5 41.0 41.4 41.9 42.4 42.8 35.9 36.4 36.8 37.3 37.8 38.2 38.7 39.1 39.6 40.1 40.5 41.0 41.5 41.9 35.1 35.6 36.0 36.5 36.9 37.4 37.8 38.3 38.7 39.2 39.6 40.1 40.6 41.0 34.3 34.7 35.2 35.6 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.2 39.6 40.1 40.6 41.0 33.5 33.9 34.3 34.8 35.2 35.7 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.2 39.6 40.1 33.5 33.9 34.3 34.8 35.2 35.7 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.2 39.6 40.1 33.5 33.9 34.3 34.8 35.2 35.7 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.1 32.7 33.1 33.5 33.9 34.4 34.8 35.2 35.7 36.1 36.5 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.1															3	60 61 62 63 64
65 66 67 68 69	32.7 31.8 31.0 30.2 29.3	35.1 35.6 36.0 36.5 36.9 37.4 37.8 38.3 38.7 39.2 39.6 40.1 40.6 41.0 34.3 34.7 35.2 35.6 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.2 39.6 40.1 33.5 33.9 34.3 34.8 35.2 35.7 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.1 32.7 33.1 33.5 33.9 34.4 34.8 35.2 35.6 36.1 36.5 37.0 37.4 37.8 38.3 38.7 39.1 32.7 33.1 33.5 33.9 34.4 34.8 35.2 35.6 36.1 36.5 36.9 37.3 37.8 38.2 31.8 32.2 32.6 33.1 33.5 33.9 34.3 34.7 35.1 35.6 36.0 36.4 36.8 37.2 31.0 31.4 31.8 32.2 32.6 33.0 33.4 33.8 34.2 34.6 35.0 35.5 35.9 36.3 30.2 30.2 30.5 30.9 31.3 31.7 32.1 32.5 32.9 33.3 33.7 34.1 34.5 34.9 35.3															65 66 67 68 69
70 71 72 73 74	28.4 27.5 26.7 25.8 24.9	28.8 27.9 27.0 26.1 25.3	29.2 28.3 27.4 26.5 25.6	29.6 28.6 27.7 26.8 25.9	29.9 29.0 28.1 27.2 26.3	30.3 29.4 28.5 27.5 26.6	29. 28. 27.	7 30	1.0 0.1 9.2 8.2 7.3	31.4 30.5 29.5 28.6 27.6	31.8 30.9 29.9 28.9 27.9	32.2 31.2 30.2 29.3 28.3	32.6 31.6 30.6 29.6 28.6	32.9 31.9 30.9 29.9 28.9	32. 31. 30.	3 3 3	70 71 72 73 74
75 76 77 78 79	24.0 23.1 22.3 21.4 20.4	24.4 23.5 22.6 21.7 20.7	24.7 23.8 22.9 21.9 21.0	25.0 24.1 23.2 22.2 21.3	25.3 24.4 23.5 22.5 21.6	25.7 24.7 23.8 22.8 21.9	25. 24. 23.	0 2 I 2 I 2	6.3 5.3 4.4 3.4 2.4	26.6 25.7 24.7 23.7 22.7	27.0 26.0 25.0 24.0 23.0	27.3 26.3 25.3 24.3 23.3	27.6 26.6 25.6 24.6 23.6	27.9 26.9 25.9 24.9 23.9	27. 26. 25.	2 2 2	75 76 77 78 79
80 81 82 83 84	19.5 18.6 17.7 16.8 15.9	19.8 18.9 18.0 17.0 16.1	20.1 19.2 18.2 17.3 16.4	20.4 19.4 18.5 17.5 16.6	20.6 19.7 18.7 17.8 16.8	20.0 20.0 19.0 18.0	20.	2 2 2 3 1 3 1 3 1 3 1 3 1 3 1 3 1 3 1 3	1.5 0.5 9.5 8.5	21.7 20.7 19.8 18.8 17.8	22.0 21.0 20.0 19.0 18.0	22.3 21.3 20.3 19.2 18.2	22.6 21.5 20.5 19.5 18.5	22.8 21.8 20.8 19.7 18.7	22.	0	80 81 82 83 84
85 86 87 88 89	15.0 14.1 13.1 12.2 11.3	15.2 14.3 13.3 12.4 11.5	15.4 14.5 13.5 12.6 11.7	15.6 14.7 13.7 12.8 11.8	15.9 14.9 13.9 13.0		15. 14. 13.	3 I 3 I 4 I	- 1	16.8 15.8 14.7 13.7 12.7		-	17.4 16.4 15.3 14.3 13.3	17.6 16.6 15.5 14.5	16. 15. 14. 13.	7 7 6	85 86 87 88 89
Height	10.4 3 ^m		10.7	10.9	8m	9 ^m	IOm	4 I		_	11.9		12.2	12.4	12.	6 19 ^m	90 20 ^m
of eye	10	13'	16'	23′	26′	30′	33′	36′	39	43	46'	49'	52	56′	59′	62'	66′
Addition	al + i.	3 +0.8	+44	-0.4	- ó· 7	- i.o	- i.3	- i.6	- i.	9 - 2.	2 - 2.5	- 2.7	- 2.9	- ź. r	- 3.3	- 3.5	-3.7
	Ot	serva	tion.	For	(su	btrac	the	Moo	n's l	Diam	eter fi	rom va	alues	given	for (<u>[</u>	

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60'					Nu	mbe	er of	M	inut	es o	f b					Δ
Δ	I'	2'	3'	4'	5′	6′	7′	8′	9′	10'	II'	12'	13'	14'	15'	60′
1.00 1.02 1.03 1.05 1.07	1.0 1.0 1.0 1.0	2.0 2.0 2.0 1.9	3.0 3.0 2.9 2.9 2.8	4.0 4.0 3.9 3.8 3.8	5.0 5.0 4.9 4.8 4.7	6.0 5.9 5.8 5.7 5.6	7.0 6.9 6.8 6.7 6.6	8.0 7.9 7.7 7.6 7.4	9.0 8.9 8.7 8.6 8.4	9.8 9.7 9.5 9.3	11.0 10.8 10.6 10.5	11.8 11.6 11.4	13.0 12.8 12.6 12.3 12.1	14.0 13.8 13.5 13.3 13.1	15.0 14.7 14.5 14.2	1.00 0.98 •97 •95 •93
1.09 1.11 1.13 1.15 1.18	0.9 .9 .9	1.9 1.8 1.8 1.7	2.8 2.7 2.7 2.6 2.6	3.7 3.6 3.6 3.5 3.4	4.6 4.5 4.5 4.4 4.3	5·5 5·4 5·3 5·2 5·1	6.5 6.3 6.2 6.1 6.0	7·3 7·2 7·1 6.9 6.8	8.3 8.1 8.0 7.8 7.7	9.2 9.0 8.8 8.7 8.5	9.9 9.7 9.5 9.4	10.8 10.6 10.4	11.9 11.7 11.5 11.2 11.0	12.6 12.4 12.1	13.7 13.5 13.2 13.0	0.92 .90 .88 .87 .85
1.20 1.22 1.25 1.28 1.30	0.8 .8 .8 .8	1.7 1.6 1.6 1.6	2.5 2.5 2.4 2.4 2.3	3·4 3·3 3·2 3·2 3.1	4.2 4.1 4.0 4.0 3.9	5.0 4.9 4.8 4.7 4.6	5·9 5·7 5.6 5·5 5·4	6.7 6.5 6.4 6.3 6.1	7·5 7·4 7·2 7·1 6.9	8.3 8.2 8.0 7.8 7.7	9.2 9.0 8.8 8.6 8.4	9.8	10.4	11.2	12.5 12.2 12.0 11.7 11.5	0.83 .82 .80 .78 .77
1.33 1.36 1.40 1.43 1.46	0.8 ·7 ·7 ·7 ·7	1.5 1.5 1.4 1.4	2.3 2.2 2.2 2.1 2.1	3.0 3.0 2.9 2.8 2.8	3.8 3.7 3.6 3.5 3.5	4·5 4·4 4·3 4·2 4·1	5.3 5.2 5.0 4.9 4.8	6.0 5.9 5.7 5.6 5.5	6.8 6.6 6.5 6.3 6.2	7·5 7·3 7·2 7·0 6.8	8.3 8.1 7.9 7.7 7.5	9.0 8.8 8.6 8.4 8.2	9.1 8.9	9.8	11.2 11.0 10.7 10.5 10.2	0.75 •73 •72 •70 •68
1.50 1.54 1.58 1.62 1.67	0.7 .7 .6 .6	1.3 1.3 1.2 1.2	2.0 2.0 1.9 1.9	2.7 2.6 2.6 2.5 2.4	3.4 3.3 3.2 3.1 3.0	4.0 3.9 3.8 3.7 3.6	4.7 4.6 4.5 4.3 4.2	5·3 5·2 5·1 4·9 4.8	6.0 5.9 5.7 5.6 5.4	6.7 6.5 6.3 6.2 6.0	7·3 7·2 7·0 6.8 6.6	8.0 7.8 7.6 7.4 7.2	8.7 8.4 8.2 8.0 7.8	8.9 8.6 8.4	9.7 9.5 9.2 9.0	0.67 .65 .63 .62 .60
1.71 1.76 1.82 1.88 1.94	0.6 .6 .6 .5	I.2 I.I I.I I.I	1.8 1.7 1.7 1.6 1.6	2.4 2.3 2.2 2.2 2.1	2.9 2.9 2.8 2.7 2.6	3·5 3·4 3·3 3·2 3.1	4.1 4.0 3.9 3.8 3.6	4·7 4·5 4·4 4·3 4·1	5·3 5.1 5.0 4.8 4·7	5.8 5.7 5.5 5.3 5.2	6.4 6.2 6.1 5.9 5.7	7.0 6.8 6.6 6.4 6.2	7.6 7.4 7.1 6.9 6.7	8.2 7.9 7.7 7.5 7.2	8.7 8.5 8.2 8.0 7.7	0.58 ·57 ·55 •53 •52
2.00 2.07 2.14 2.22 2.31	0.5 .5 .5 .5	1.0 1.0 0.9 .9	1.5 1.4 1.4 1.3	1.9 1.9 1.8	2.5 2.4 2.4 2.3 2.2	3.0 2.9 2.8 2.7 2.6	3·5 3·4 3·3 3·2 3·1	4.0 3.9 3.7 3.6 3.5	4·5 4·4 4·2 4·1 3·9	5.0 4.8 4.7 4.5 4.3	5.5 5.3 5.1 5.0 4.8	6.0 5.8 5.6 5.4 5.2	6.3	7.0 6.8 6.5 6.3 6.1	7.5 7.2 7.0 6.7 6.5	0.50 .48 .47 .45 .43
2.40 2.50 2.61 2.73 2.86	0.4 •4 •4 •4 •4	0.8 .8 .8 .7 .7	1.3 1.2 1.2 1.1	1.7 1.6 1.5 1.5	2.I 2.0 I.9 I.9	2.5 2.4 2.3 2.2 2.1	2.9 2.8 2.7 2.6 2.5	3·3 3·2 3·1 2·9 2.8	3.8 3.6 3.5 3.3 3.2	4.2 4.0 3.8 3.7 3.5	4.6 4.4 4.2 4.0 3.9	5.0 4.8 4.6 4.4 4.2	5.4 5.2 5.0 4.8 4.5	5.8 5.6 5.4 5.1 4.9	6.2 6.0 5.7 5.5 5.2	0.42 .40 .38 .37 .35
3.00 3.16 3.33 3.53 3.75	0.3 .3 .3 .3	°·7 .6 .6 .6 .5	1.0 1.0 0.9 .9	1.3 1.2 1.1 1.1	1.7 1.6 1.5 1.4	2.0 1.9 1.8 1.7 1.6	2.3 2.2 2.1 2.0 1.9	2.7 2.5 2.4 2.3 2.1	3.0 2.9 2.7 2.6 2.4	3.3 3.2 3.0 2.8 2.7	3.7 3.5 3.3 3.1 2.9	4.0 3.8 3.6 3.4 3.2		4.7 4.4 4.2 4.0 3.7	5.0 4.7 4.5 4.2 4.0	0.33 .32 .30 .28 .27
4.00 4.29 4.62 5.00 5.45	0.3	0.5 .5 .4 .4 .4	0.8 •7 •7 •6 •6	1.0 0.9 .9 .8 ·7	1.3 1.2 1.1 1.0 0.9	1.5 1.4 1.3 1.2	1.8 1.6 1.5 1.4 1.3	2.0 1.9 1.7 1.6 1.5	2.3 2.1 2.0 1.8 1.7	2.5 2.3 2.2 2.0 1.8	2.8 2.6 2.4 2.2 2.0	3.0 2.8 2.6 2.4 2.2	3.2 3.0 2.8 2.6 2.4	3.5 3.3 3.0 2.8 2.6	3.7 3.5 3.2 3.0 2.7	0.25 .23 .22 .20 .18
6.00 6.67 7.50 8.57 10.0	0.2 .2 .1 .1	0.3 .3 .3 .2	0.5 •5 •4 •4 •3	°·7 .6 ·5 ·5 ·4	0.8 .8 .7 .6 .5	1.0 0.9 .8 .7 .6	1.2 1.1 0.9 .8 ·7	1.3 1.2 1.1 0.9	1.5 1.4 1.2 1.1	1.7 1.5 1.3 1.2	1.8 1.7 1.5 1.3	2.0 1.8 1.6 1.4	2.2 2.0 1.7 1.5 1.3	2.3 2.1 1.9 1.6 1.4	2.5 2.2 2.0 1.7 1.5	0.17 .15 .13 .12
12.0 15.0 20.0 30.0 60.0	0.1 .I .0 .0	0.2 .I .I .I	0.3 .2 .2 .1	0.3 .3 .2 .1	0.4 ·3 ·3 ·2 ·1	0.5 .4 .3 .2 .1	0.6 ·5 ·4 ·2 ·1	0.7 .5 .4 .3 .1	0.8 .6 .5 .3 .2	0.8 •7 •5 •3 •2	0.9 .7 .6 .4 .2	0.8 .6 .4 .2	1.1 0.9 .6 .4 .2	1.2 0.9 ·7 ·5 .2	1.2 1.0 0.7 .5	0.08 .07 .05 .03 .02

<u>6ο′</u> Δ					Nu	mbe	er o	f M	inut	es o	of b					Δ
Δ	16′	17′	18′	19'	20′	21'	22′	23′	24'	25′	26′	27'	28′	29′	30′	60′
1.00 1.02 1.03 1.05 1.07	16.0 15.7 15.5 15.2 14.9	16.7 16.5	17.4 17.1	18.7 18.4 18.1	19.7	20.7 20.3 20.0	21.6	22.6 22.2 21.9	23.2	24.6	25.6 25.1 24.7	26.6 26.1	27. I 26. 6		29.0 28.5	1.00 0.98 •97 •95 •93
1.09 1.11 1.13 1.15 1.18	13.9	15.3 15.0 14.8 14.5	16.2 15.9 15.6 15.3	16.5 16.2	18.0 17.7 17.3	18.9 18.6 18.2 17.9	19.8 19.4 19.1 18.7	20.7 20.3 19.9 19.6	20.4	22.5 22.1 21.7 21.3	23.4 23.0 22.5 22.1	23.9 23.4 23.0	25.2 24.7 24.3	26. I 25. 6 25. I	27.0 26.5 26.0	0.92 .90 .88 .87 .85
1.20 1.22 1.25 1.28 1.30	12.8 12.5 12.3	13.9 13.6 13.3 13.0	14.4 14.1 13.8	15.5 15.2 14.9 14.6	16.0 15.7 15.3	17.2 16.8 16.5 16.1	17.6 17.2 16.9	18.8 18.4 18.0 17.6	19 6 19.2 18.8 18.4	20.4 20.0 19.6 19.2	20.8 20.4 19.9	22. I 21. 6 21. 2 20. 7	22.9 22.4 21.9 21.5	22.7	24.5 24.0 23.5 23.0	0.83 .82 .80 .78 .77
1.33 1.36 1.40 1.43 1.46	11.7 11.5 11.2	12.8 12.5 12.2 11.9 11.6	13.2 12.9 12.6 12.3	13.9 13.6 13.3 13.0	13.7	15.1 14.7 14.4	16.1 15.8 15.4 15.0	16.5 16.1 15.7	17.2 16.8 16.4	18.3 17.9 17.5 17.1	18.6 18.2 17.8	19.8 19.4 18.9 18.5	20.5 20.1 19.6 19.1	20.8 20.3 19.8	22.0 21.5 21.0 20.5	.73 .72 .70 .68
1.50 1.54 1.58 1.62 1.67	10.7 10.4 10.1 9.9 9.6	11.1	11.7	12.0		13.7 13.3 13.0	14.3 13.9 13.6 13.2	15.0 14.6 14.2	14.4	16.3 15.8 15.4 15.0	16.9 16.5 16.0	17.6 17.1 16.7 16.2	18.2 17.7 17.3	19.3 18.9 18.4 17.9 17.4	19.5 19.0 18.5	.65 .63 .62 .60
1.71 1.76 1.82 1.88 1.94	9.3 9.1 8.8 8.5 8.3	9.9 9.6 9.4 9.1 8.8	10.5 10.2 9.9 9.6 9.3	11.1 10.8 10.5 10.1 9.8	11.7 11.3 11.0 10.7 10.3	12.3 11.9 11.6 11.2 10.9	11.7		13.6 13.2 12.8	13.8	14.3	15.8 15.3 14.9 14.4 14.0	15.9 15.4 14.9	16.0	17.0 16.5 16.0	0.58 •57 •55 •53 •52
2.00 2.07 2.14 2.22 2.31	8.0 7.7 7.5 7.2 6.9	8.5 8.2 7.9 7.7 7.4	9.0 8.7 8.4 8.1 7.8	9.5 9.2 8.9 8.6 8.2	9.7 9.3 9.0 8.7	10.5 10.2 9.8 9.5 9.1	11.0 10.6 10.3 9.9 9.5	11.5 11.1 10.7 10.4 10.0	11.6	12.5 12.1 11.7 11.3 10.8		13.5 13.1 12.6 12.2 11.7	13.5 13.1 12.6		14.5 14.0 13.5	0.50 .48 .47 .45 .43
2.40 2.50 2.61 2.73 2.86	6.7 6.4 6.1 5.9 5.6	7.1 6.8 6.5 6.2 6.0	7.5 7.2 6.9 6.6 6.3	7.9 7.6 7.3 7.0 6.7	8.3 8.0 7.7 7.3 7.0	8.8 8.4 8.1 7.7 7.4	9.2 8.8 8.4 8.1 7.7	9.6 9.2 8.8 8.4 8.1	9.6	10.0	10.8 10.4 10.0 9.5 9.1	10.8	11.2 10.7 10.3	12.1 11.6 11.1 10.6 10.2	11.5	0.42 .40 .38 .37 .35
3.00 3.16 3.33 3.53 3.75	5·3 5·1 4.8 4·5 4·3	5.7 5.4 5.1 4.8 4.6	6.0 5.7 5.4 5.1 4.8	6.3 6.0 5.7 5.4 5.1	6.7 6.3 6.0 5.7 5.3	7.0 6.7 6.3 6.0 5.6	7·3 7·0 6.6 6.2 5·9	1	6.8		8.7 8.2 7.8 7.4 6.9	9.0 8.6 8.1 7.7 7.2	7.9	9·7 9·2 8·7 8·2 7·7	9.5 9.0 8.5 8.0	0.33 .32 .30 .28 .27
4.00 4.29 4.62 5.00 5.45	4.0 3.7 3.5 3.2 2.9	4·3 4·0 3·7 3·4 3.1	4.5 4.2 3.9 3.6 3.3	4.8 4.4 4.1 3.8 3.5	5.0 4.7 4.3 4.0 3.7	5·3 4·9 4·6 4·2 3·9	5.5 5.1 4.8 4.4 4.0	5.8 5.4 5.0 4.6 4.2	6.0 5.6 5.2 4.8 4.4	6.3 5.8 5.4 5.0 4.6	6.5 6.1 5.6 5.2 4.8	6.8 6.3 5.9 5.4 5.0	7.0 6.5 6.1 5.6 5.1	7·3 6.8 6.3 5.8 5·3	7.5 7.0 6.5 6.0 5.5	0.25 .23 .22 .20 .18
6.00 6.67 7.50 8.57 10.0	2.7 2.4 2.1 1.9 1.6	2.8 2.6 2.3 2.0	3.0 2.7 2.4 2.1 1.8	3.2 2.9 2.5 2.2 1.9	3.3 3.0 2.7 2.3 2.0	3.5 3.2 2.8 2.5 2.1	3.7 3.3 2.9 2.6 2.2	3.8 3.5 3.1 2.7 2.3	4.0 3.6 3.2 2.8 2.4	4.2 3.8 3.3 2.9 2.5	4·3 3·9 3·5 3.0 2.6	4.5 4.1 3.6 3.2 2.7	4·7 4·2 3·7 3·3 2.8	4.8 4.4 3.9 3.4 2.9	5.0 4.5 4.0 3.5 3.0	0.17 .15 .13 .12 .10
12.0 15.0 20.0 30.0 60.0	1.3 1.1 0.8 ·5 ·3	1.4 1.1 0.9 .6	1.5 1.2 0.9 .6	1.6 1.3 1.0 0.6 •3	1.7 1.3 1.0 0.7	1.8 1.4 1.1 0.7 .4	1.8 1.5 1.1 0.7 •4	1.9 1.5 1.2 0.8	2.0 1.6 1.2 0.8	2.1 1.7 1.3 0.8 •4	2.2 1.7 1.3 0.9 .4	2.3 1.8 1.4 0.9	2.3 1.9 1.4 0.9	2.4 1.9 1.5 1.0 0.5	2.5 2.0 1.5 1.0 0.5	0.08 .07 .05 .03 .02

60'					Nu	mbe	er o	f M	inut	es c	of b					Δ
Δ	31'	32'	33'	34'	35′	36′	37′	38′	39'	40′	41'	42'	43'	44'	45'	60'
1.00 1.02 1.03 1.05 1.07	31.0 30.5 30.0 29.5 28.9		32.5	34.0 33.4 32.9 32.3 31.7	33.8	35·4 34.8	36.4 35.8	37·4 36.7	38.4 37.7 37.1	40.0 39.3 38.7 38.0 37.3	40.3 39.6 39.0	41.3 40.6 39.9	41.6	43.3 42.5 41.8		1.00 0.98 •97 •95 •93
1.09 1.11 1.13 1.15 1.18	28.4 27.9 27.4 26.9 26.4	28.8 28.3 27.7	30.3 29.7 29.2 28.6 28.1	30.6		32.4 31.8	32.1	34.2 33.6 32.9	35.1 34.5 33.8	36.7 36.0 35.3 34.7 34.0	36.2 35.5	37.1 36.4	38.7 38.0	38.9 38.1	40.5 39.8	0.92 .90 .88 .87 .85
1.20 1.22 1.25 1.28 1.30	25.8 25.3 24.8 24.3 23.8	26.7 26.1 25.6 25.1 24.5	27.5 27.0 26.4 25.9 25.3		29.2 28.6 28.0 27.4 26.8	28.8 28.2		31.0 30.4 29.8	31.9 31.2 30.6	33·3 32·7 32·0 31·3 30·7	33·5 32.8	34·3 33.6 32.9	35.8 35.1 34.4 33.7 33.0	35.9 35.2 34.5	36.0 35.3	0.83 .82 .80 .78 •77
1.33 1.36 1.40 1.43 1.46	23.3 22.8 22.3 21.8 21.3	24.0 23.5 22.9 22.4 21.9	24.8 24.2 23.7 23.1 22.6	25.5 24.9 24.4 23.8 23.2	26.3 25.7 25.1 24.5 23.9	25.8 25.2	27.1 26.5	27.9 27.2	28.6 28.0 27.3	30.0 29.3 28.7 28.0 27.3	30.1 29.4	30.1	31.5 30.8 30.1	31.5	32.3	0.75 .73 .72 .70 .68
1.50 1.54 1.58 1.62 1.67	20.7 20.2 19.6 19.1 18.6	21.3 20.8 20.3 19.7 19.2	22.0 21.5 20.9 20.4 19.8	22.1	23.3 22.8 22.2 21.6 21.0	22.8	24. I	24.I 23.4	25.4 24.7 24.1	26.7 26.0 25.3 24.7 24.0		27.3 26.6 25.9	27.2 26.5	28.6 27.9		0.67 .65 .63 .62 60
1.71 1.76 1.82 1.88 1.94	18.1 17.6 17.1 16.5 16.0	18.7 18.1 17.6 17.1 16.5	19.3 18.7 18.2 17.6 17.1	19.8 19.3 18.7 18.1 17.6	20.4 19.8 19.3 18.7 18.1	20.4 19.8 19.2	21.0 20.4	21.5 20.9 20.3	22.1 21.5 20.8	23.3 22.7 22.0 21.3 20.7	22.6	23.8 23.1 22.4	25. I 24.4 23.7 22.9 22.2	24.9 24.2 23.5	24.8	0.58 •57 •55 •53 •52
2.00 2.07 2.14 2.22 2.31	15.5 15.0 14.5 14.0 13.4	16.0 15.5 14.9 14.4 13.9	16.5 16.0 15.4 14.9 14.3	17.0 16.4 15.9 15.3 14.7	17.5 16.9 16.3 15.8 15.2	17.4 16.8 16.2	17.9	18.4 17.7 17.1	18.9 18.2 17.6	20.0 19.3 18.7 18.0 17.3	19.8	20.3 19.6 18.9	21.5 20.8 20.1 19.4 18.6	21.3 20.5 19.8		0.50 •48 •47 •45 •43
2.40 2.50 2.61 2.73 2.86	12.9 12.4 11.9 11.4 10.9	13.3 12.8 12.3 11.7 11.2	13.8 13.2 12.7 12.1 11.6	13.0	14.6 14.0 13.4 12.8 12.3	14.4 13.8 13.2	14.2 13.6	15.2 14.6 13.9	14.3	16.7 16.0 15.3 14.7 14.0	15.7	16.1 15.4	17.9 17.2 16.5 15.8 15.1	16.9 16.1		0.42 •40 •38 •37 •35
3.00 3.16 3.33 3.53 3.75	9.8 9.8 9.3 8.8 8.3	10.7 10.1 9.6 9.1 8.5	11.0 10.5 9.9 9.4 8.8	10.8	11.7 11.1 10.5 9.9 9.3	11.4	11.7	12.0	12.4 11.7 11.1	13.3 12.7 12.0 11.3 10.7	13.0 12.3 11.6	13.3 12.6 11.9	12.2	13.9 13.2 12.5	13.5	0.33 .32 .30 .28 .27
4.00 4.29 4.62 5.00 5.45	7.8 7.2 6.7 6.2 5.7	8.0 7.5 6.9 6.4 5.9	8.3 7.7 7.2 6.6 6.1	8.5 7.9 7.4 6.8 6.2	8.8 8.2 7.6 7.0 6.4	9.0 8.4 7.8 7.2 6.6	9.3 8.6 8.0 7.4 6.8	9.5 8.9 8.2 7.6 7.0	9.8 9.1 8.5 7.8 7.2	9·3 8·7 8·0 7·3	9.6 8.9 8.2 7.5	9.8 9.1 8.4 7.7	10.8 10.0 9.3 8.6 7.9	11.0 10.3 9.5 8.8 8.1	11.3 10.5 9.8 9.0 8.3	0.25 .23 .22 .20 .18
6.00 6.67 7.50 8.57 10.0	5.2 4.7 4.1 3.6 3.1	5.3 4.8 4.3 3.7 3.2	5.5 5.0 4.4 3.9 3.3	5.7 5.1 4.5 4.0 3.4	5.8 5.3 4.7 4.1 3.5	6.0 5.4 4.8 4.2 3.6	6.2 5.6 4.9 4.3 3.7	6.3 5.7 5.1 4.4 3.8	6.5 5.9 5.2 4.6 3.9	6.7 6.0 5.3 4.7 4.0	6.8 6.2 5.5 4.8 4.1	7.0 6.3 5.6 4.9 4.2	7.2 6.5 5.7 5.0 4.3	7·3 6.6 5·9 5.1 4·4	7.5 6.8 6.0 5.3 4.5	0.17 .15 .13 .12
12.0 15.0 20.0 30.0 60.0	2.6 2.1 1.6 1.0 0.5	2.7 2.1 1.6 1.1 0.5	2.8 2.2 1.7 1.1 0.6	2.8 2.3 1.7 1.1 0.6	2.9 2.3 1.8 1.2 0.6	3.0 2.4 1.8 1.2 0.6	3.1 2.5 1.9 1.2 0.6	3.2 2.5 1.9 1.3 0.6	3·3 2.6 2.0 1.3	3·3 2·7 2·0 1·3 0·7	3·4 2·7 2·1 1·4 0·7	3·5 2.8 2.1 1.4 0.7	3.6 2.9 2.2 1.4 0.7	3.7 2.9 2.2 1.5 0.7	3.8 3.0 2.3 1.5 0.8	0.08 .07 .05 .03 .02

60'			-		Nu	mbe	er of	M	inut	es o	of b					Δ
Δ	46′	47'	48'	49′	50′	51 ′	52'	53′	54'	55′	56′	57'	58′	59′	60'	60′
1.00 1.02 1.03 1.05 1.07	45.2 44.5 43.7	47.0 46.2 45.4 44.7 43.9	47.2 46.4 45.6	48.2 47.4 46.6	49.2 48.3 47.5	50.2 49.3 48.5	51.1 50.3 49.4	52.1 51.2 50.4	53.1 52.2 51.2	54°1 53.2 54.3	55. I 54. I 53. 2	56.0 55.1 54.1	57.0 56.1	58.0 57.0 56.1	60.0 59.0 58.0 57.0 56.0	1.00 0.98 .97 .95 .93
1.09 1.11 1.13 1.15 1.18	41.4 40.6 39.9 39.1	42-3 41-5 40-7 40-0	43.2 42.4 41.6 40.8	44.1 43.3 42.5 41.7	45.6 44.2 43.3 42.5	45.9 45.1 44.2 43.4	45.9 45.1 44.2	47.7 46.8 45.9 45.1	48.6 47.7 46.8 45.9	47·7 46.8	50.4 49.5 48.5 47.6	51.3 50.3 49.4 48.4	52.2 51.2 50.3 49.3	52.1 51.1 50.2	53.0 52.0 51.0	.90 .88 .87 .85
1.20 1.22 1.25 1.28 1.30	37.6 36.8 36.0 35.3		39.2 38.4 37.6 36.8	39.2 38.4 37.6	40.8 40.0 39.2 38.3	41.7 40.8 40.0 39.1	42.5 41.6 40.7 39.9	43·3 42·4 41·5 40.6	44. I 43.2 42. 3 41. 4	44.9 44.0 43.1 42.2	45.7 44.8 43.9 42.9	46.5 45.6 44.6 43.7	47·4 46·4 45·4 44·5	48.2 47.2 46.2 45.2	49.0 48.0 47.0 46.0	.80 .78 .77
1.33 1.36 1.40 1.43 1.46	34.5 33.7 33.0 32.2 31.4	33.7 32.9 32.1	35.2 34.4 33.6 32.8	35.9 35.1 34.3 33.5	36.7 35.8 35.0 34.2	37·4 36.6 35·7 34·9	38.1 37.3 36.4 35.5	38.9 38.0 37.1 36.2	39.6 38.7 37.8 36.9	39·4 38·5 37·6	41.1 40.1 39.2 38.3	41.8 40.8 39.9 38.9	42.5 41.6 40.6 39.6	41.3	44.0 43.0 42.0 41.0	0.75 •73 •72 •70 •68
1.50 1.54 1.58 1.62 1.67	30.7 29.9 29.1 28.4 27.6	31.3 30.6 29.8 29.0 28.2	31.2 30.4 29.6 28.8	31.9 31.0 30.2 29.4	32.5 31.7 30.8 30.0	33.2 32.3 31.5 30.6	33.8 32.9 32.1 31.2	34·5 33.6 32·7 31.8	35.1 34.2 33.3 32.4	36.7 35.8 34.8 33.9 33.0	36.4 35.5 34.5 33.6	37.0 36.1 35.1 34.2	36.7 35.8 34.8	38.4 37.4 36.4 35.4		.63 .62 .60
1.71 1.76 1.82 1.88 1.94	26. I 25. 3 24. 5 23. 8	25.9 25.1 24.3	27.2 26.4 25.6 24.8	27.8 27.0 26.1 25.3	28.3 27.5 26.7 25.8	28.9 28.1 27.2 26.4	29.5 28.6 27.7 26.9	30.0 29.2 28.3 27.4	30.6 29.7 28.8 27.9	29.3 28.4	31.7 30.8 29.9 28.9	32.3 31.3 30.4 29.4	30.9 30.0	33.4 32.5 31.5 30.5	33.0 32.0 31.0	0.58 •57 •55 •53 •52
2.00 2.07 2.14 2.22 2.31	22.2 21.5 20.7 19.9	22.7 21.9 21.2 20.4	23.2 22.4 21.6 20.8	23.7 22.9 22.1 21.2	24.2 23.3 22.5 21.7	24.7 23.8 23.0 22.1	25. I 24. 3 23. 4 22. 5	25.6 24.7 23.9 23.0	26.1 25.2 24.3 23.4	23.8	27.1 26.1 25.2 24.3	27.5 26.6 25.6 24.7	27.1 26.1 25.1	28.5 27.5 26.6 25.6	29.0 28.0 27.0 26.0	0.50 .48 .47 .45 .43
2.40 2.50 2.61 2.73 2.86	16.9 16.1	18.8 18.0 17.2 16.5	17.6 16.8	19.6 18.8 18.0 17.2	19.2 18.3 17.5	19.6 18.7 17.9	20.8 19.9 19.1 18.2	21.2 20.3 19.4 18.6	21.6 20.7 19.8 18.9	22.9 22.0 21.1 20.2 19.3	22.4 21.5 20.5 19.6	22.8 21.8 20.9 19.9	23.2 22.2 21.3 20.3	23.6 22.6 21.6 20.7	24.0 23.0 22.0 21.0	0.42 .40 .38 .37 .35
3.00 3.16 3.33 3.53 3.75	15.3 14.6 13.8 13.0 12.3	14.9 14.1 13.3 12.5	13.6	15.5 14.7 13.9 13.1	15.8 15.0 14.2 13.3	16.2 15.3 14.5 13.6	15.6 14.7 13.9	16.8 15.9 15.0 14.1	17.1 16.2 15.3 14.4	14.7	17.7 16.8 15.9 14.9	18.0 17.1 16.1 15.2	18.4 17.4 16.4 15.5	18.7 17.7 16.7 15.7	19.0 18.0 17.0 16.0	0.33 .32 .30 .28 .27
4.00 4.29 4.62 5.00 5.45	9.2 8.4	9.4 8.6	9.6 8.8	11.4 10.6 9.8 9.0	11.7 10.8 10.0 9.2	11.1	12.1 11.3 10.4 9.5	12.4 11.5 10.6 9.7	11.7 10.8 9.9	11.0	13.1 12.1 11.2 10.3	13.3 12.3 11.4 10.4	12.6 11.6 10.6	13.8 12.8 11.8 10.8	12.0	0.25 .23 .22 .20 .18
6.00 6.67 7.50 8.57 10.0	7.7 6.9 6.1 5.4 4.6	7.8 7.1 6.3 5.5 4.7	8.0 7.2 6.4 5.6 4.8	8.2 7.4 6.5 5.7 4.9	8.3 7.5 6.7 5.8 5.0	8 5 7·7 6.8 6.0 5.1	8.7 7.8 6.9 6.1 5.2	8.8 8.0 7.1 6.2 5.3	9.0 8.1 7.2 6.3 5.4	9.2 8.3 7.3 6.4 5.5	9.3 8.4 7.5 6.5 5.6	9.5 8.5 7.6 6.6 5.7	9.7 8.7 7.7 6.8 5.8	9.8 8.9 7.9 6.9 5.9	9.0 8.0 7.0 6.0	0.17 .15 .13 .12
12.0 15.0 20.0 30.0 60.0	3.8 3.1 2.3 1.5 0.8	3.9 3.1 2.4 1.6 0.8	4.0 3.2 2.4 1.6 0.8	4.1 3.3 2.5 1.6 0.8	4.2 3.3 2.5 1.7 0.8	4·3 3·4 2.6 1.7 0.9	4·3 3·5 2.6 1.7 0.9	4·4 3·5 2·7 1.8 0.9	4.5 3.6 2.7 1.8 0.9	4.6 3.7 2.8 1.8 0.9	4·7 3·7 2.8 1.9 0.9	4.7 3.8 2.8 1.9	4.8 3.9 2.9 1.9	4.9 3.9 3.0 2.0 1.0	5.0 4.0 3.0 2.0 1.0	0.08 .07 .05 .03

1			<i>a</i> =	0° 0′			a = 0	° 30′				a =	1° 0′		\ c	\ a
B	h	d	$\frac{60'}{\Delta}$	Z^{t}	h	d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	Δ 60'	$c \setminus$	β
0 1 2 3 4	0 0 1 2 3 4	0 0 0	I	0 0 0 0 0 0 0	0 I 2 3 4	00000	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	0 30 30 30 30 30	.00	1 2 3 4	0000	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	i 0 0 0	.00	89 88 87 86	90.0 90.0 90.0 90.0 90.0
5 6 7 8 9	5 6 7 8 9	0 0 0 0	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	0 0 0	5 6 7 8 9	0 0 0	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	30 30 30 30 30	.00	5 6 7 8 9	0 0 0 0	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	1 0 0	0.00 .00 .02 .00	85 84 83 82 81	90.0 89.9 89.9 89.9
10 11 12 13 14	10 11 12 13 14	0 0 0	1 1 1 1	0 0 0	10 11 12 13 14	0 0 0 0	1 1 1	31 31 31 31 31	.00	10 11 12 13 14	00000	I I I I	I I 1 2 2	.00	80 79 78 77 76	89.9 89.9 89.9 89.9
15 16 17 18 19	15 16 17 18	00000	I I I	0 0 0 0	15 16 17 18	00000	1 1 1	31 31 31 32 32	0.00 .00 .02 .00	15 16 17 18 19	0 0 0 0	I I I	2 2 3 3 3	.00	75 74 73 72 71	89.9 89.9 89.8 89.8 89.8
20 21 22 23 24	20 21 22 23 24	00000	1 1 1	0 0 0 0	20 21 22 23 24	0 0 0 0	I I I I	32 32 32 33 33	0.00 .00 .02 .00	20 21 22 23 24	0 0 0 0	I I I I	4 4 5 5 6	0.00 .02 .00 .02	70 69 68 67 66	89.8 89.8 89.8 89.8
25 26 27 28 29	25 26 27 28 29	0 0 0 0	1 1 1	0 0 0 0	25 26 27 28 29	0 0 0 0	I I I I	33 33 34 34 34	0.00 .02 .00 .00	25 26 27 28 29	0 0 0 0	I I I I	6 7 7 8 9	0.02 .00 .02 .02	65 64 63 62 61	89.8 89.8 89.7 89.7 89.7
30 31 32 33 34	30 31 32 33 34	0 0 0 0	1 1 1	0 0 0 0	30 31 32 33 34	0 0 0 0	I I I I	35 35 35 36 36	0.00 .00 .02 .00	30 31 32 33 34	00000	I I I I	9 10 11 12 12	0.02 .02 .02 .00	60 59 58 57 56	89.7 89.7 89.7 89.7 89.7
35 36 37 38 39	35 36 37 38 39	0 0 0 0	I I I I	0 0 0 0	35 36 37 38 39	0 0 0 0	I I I I	37 37 38 38 39	0.00 .02 .00 .02	35 36 37 38 39	0 0 0 0	I I I I	13 14 15 16	0.02 .02 .02 .02	55 54 53 52 51	89.7 89.6 89.6 89.6 89.6
40 41 42 43 44	40 41 42 43 44	0 0 0 0	I I I	0 0 0 0	40 41 42 43 44	0 0 0 0	I I I I	39 40 40 41 42	0.02 .00 .02 .02		0 0 0 0 59	I I I I.02	18 19 21 22 23	0.02 .03 .02 .02	50 49 48 47 46	89.6 89.6 89.5 89.5
45	45	0		0	45	0		42		44	59		25		45	89.5
	a		<u>6ο'</u> Δ	b	a		<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	a		6ο' Δ	b	<u>Δ</u> 60'		a
t			d = 0)° 0′		($l = 0^{\circ}$	30′				d = 1	° 0′			

\ b			a = 0)° 0′				a = 0	° 3	D'				a = 1	1° 0	,		\ c	\ a
$B \setminus$	h	d	$\frac{60'}{\Delta}$	Z		h	d	<u>60'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{\epsilon_0}$	$C \setminus$	B
45 46 47 48 49	45 46 47 48 49	00000	I I I I	0 0		o 45 46 47 48 49	00000	I I I I	00	42 43 44 45 46	0.02 .02 .02 .02	° 44 45 46 47 48	59 59 59 59 59	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	I	25 26 28 30 31	0.02	45 44 43 42 41	89.5 89.5 89.5 89.4 89.4
50 51 52 53 54	50 51 52 53 54	0000	I I I I	0		50 51 52 53 54	0 0 0 0	1 1 1 1		47 48 49 50 51	0.02 .02 .02 .02	49 50 51 52 53	59 59 59 59	1 1 1		33 35 37 40 42	0.03 .03 .05 .03	40 39 38 37 36	89.4 89.4 89.3 89.3
55 56 57 58 59	55 56 57 58 59	00000	I I I I	0		55 56 57 58 59	00000	I I I I		52 54 55 57 58	0.03 .02 .03 .02	54 55 56 57 58	59 59 59 59	I I I I		45 47 50 53 56	0.03 .05 .05 .05	35 34 33 32 31	89.3 89.3 89.2 89.2 89.2
60 61 62 63 64	60 61 62 63 64	0 0 0 0	I I I I			60 61 62 63 64	00000	1 1 1	I	0 2 4 6 8	0.03 .03 .03 .03	59 60 61 62 63	59 59 59 59	I I I	2	0 4 8 12 17	0.07 .07 .07 .08	30 29 28 27 26	89.1 89.1 89.0 89.0
65 66 67 68 69	65 66 67 68 69	00000	O I O O O O O O O O O O O O O O O O O O			65 66 67 68 69	0 0 0 0	1 1 1 1		11 14 17 20 24	0.05 .05 .05 .07	64 65 66 67 68	59 59 59 59	I I I		22 27 33 40 47	0.08 .10 .12 .12	25 24 23 22 21	88.9 88.9 88.8 88.8 88.7
70 71 72 73 74	70 71 72 73 74	0 0 0 0	I I I	(70 71 72 73 74	0 0 0 0	1 1 1		28 32 37 43 49	0.07 .08 .10 .10	69 70 71 72 73	59 58 58 58	I.02 I I I I	3	55 4 14 25 37	0.15 .17 .18 .20	20 19 18 17 16	88.6 88.5 88.5 88.4 88.3
75 76 77 78 79	75 76 77 78 79	0 0 0 0		(75 76 77 78	59 59 59 59	I.02 I I I	2	56 4 13 24 37	0.13 .15 .18	74 75 76 77 78	58 58 58 57	I I I I.02 I	4 5	51 8 26 48 14	0.28 .30 .37 .43	15 14 13 12 11	88.1 88.0 87.8 87.6 87.4
80 81 82 83 84	80 81 82 83 84	O I O O O O O O O O O O O O O O O O O O				79 80 81 82 83	59 59 59 59	1 1	3 4	53 12 35 6 46		79 80 81 82 83	57 57 56 56 55	I I.02 I I.02 I.02	6 7 8 9	44 22 9 9 29		10 9 8 7 6	87.2 86.8 86.4 85.9 85.3
85 86 87 88 89	85 86 87 88 89	O I O O O O O O O O O O O O O O O O O O					59 58 58 56 53	1.02 1 1.03 1.05 1.62		43 8 28 2 34		88	35	1.02 1.05 1.07 1.22 2.40	11 14 18 26 45	20 3 27 34 0		5 4 3 2 1	84.3 82.9 80.5 76.0 63.4
90	90 === a		60'	b		-	30	60'	<u> </u>	o b	Δ	-	a a	60'		0 	Δ	0	0.0 a
t			Δ	0° 0′		-		d = 0			60'	_		$\frac{60'}{\Delta}$ $d = 1$			60'		•

1	ь			a = 1	° 30′				a = 1	2° 0′	,				a=2	° 30	,		c	a
B	\	h	d	6ο' Δ	Z	$\frac{\Delta}{60'}$	h	d	60' Δ	Z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	C	β
	0 0 1 2 3	0 0 1 2 3 4	00000	I I I I I	i 30 30 30 30 30	0.00	0 0 1 2 3 4	000000000000000000000000000000000000000	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	2	00000	0.00	0 0 1 2 3 4	0000	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII		30 30 30 30 30	0.00	90 89 88 87 86	90.0 90.0 89.9 89.9 89.9
	56 78 9	5 6 7 8 9	0 0 0	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	30 30 31 31 31	.00	5 6 7 8 9	0 0 0 0	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII		O I I I	.00	5 6 7 8	0 0 0 0 59	I I I I.02		31 31 31 31 32	0.00	85 84 83 82 81	89.8 89.8 89.8 89.7 89.7
10 12 12 12	2	10 11 12 13 14	0 0 0	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	31 32 32 32 33	.00	10 11 12 13	0 0 0 0 59	I I I I.02		2 2 3 4	0.00 .02 .00 .02	9 10 11 12 13	59 59 59 59	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII		32 33 33 34 35	0.02 .00 .02 .02	80 79 78 77 76	89.6 89.6 89.6 89.5 89.5
1; 16 17 18	7	15 16 17 18	0 0 0 0	1 1 1 1	33 34 34 35 35	0.02 .00 .02 .00 .02	14 15 16 17 18	59 59 59 59	I I I I		4 5 6 7	0.02 .00 .02 .02	14 15 16 17 18	59 59 59 59	1 1 1		35 36 37 38 39	0.02 .02 .02 .02	75 74 73 72 71	89.5 89.4 89.4 89.4 89.3
20 21 22 23 24	2	20 21 22 23	o o 59 59	I I I.02 I I	36 36 37 38 39	0.00	19 20 21 22 23	59 59 59 59	I I I I	l .	9 10 11	.00	19 20 21 22 23	59 59 59 59	I I I I I.02	4	10 11 12 13 14	0.02 .02 .02 .02	70 69 68 67 66	89.3 89.2 89.2 89.2 89.1
25 26 27 28 29	6 7 8	24 25 26 27 28	59 59 59 59	I I I I	39 40 41 42 43	0.02 .02 .02 .02	24 25 26 27 28	59 59 59 59	1 1 1		12 13 15 16	0.02 .03 .02 .02	24 25 26 27 28	58 58 58 58 58	I I I I	2	15 17 18 50 51	0.03 .02 .03 .02	65 64 63 62 61	89.1 89.0 89.0 88.9 88.9
30 31 32 33 34	2	29 30 31 32 33	59 59 59 59	1 1 1	44 45 46 47 49	0.02 .02 .02 .03	29 30 31 32 33	59 59 59 59	1 1 1 1		19 20 21 23 25	0.02 .02 .03 .03	29 30 31 32 33	58 58 58 58 58	I I I I		53 57 59 1	0.03 .03 .03 .03	60 59 58 57 56	88.8 88.8 88.8 88.7 88.7
35 36 37 38 39	7	34 35 36 37 38	59 59 59 59 59	1 1 1 1	50 51 53 54 56	0.02 .03 .02 .03	34 35 36 37 38	59 58 58 58	I.02 I I I I		26 28 30 32 34	0.03 .03 .03 .03	34 35 36 37 38	58 58 58 57 57	I I I.02 I I	1	3 5 8 10 13	0.03 .05 .03 .05	55 54 53 52 51	88.6 88.5 88.5 88.4 88.4
40 41 42 43 44	2 3	39 40 41 42 43		I I I I	57 59 2 I 3	0.03 .03 .03 .03	39 40 41	58 58 58	1 .1 .1		37 39 41 44 47		39 40 41 42		I I I	1 2	16 19 22 25 28	0.05 .05 .05 .05	50 49 48 47 46	88.3 88.3 88.2 ,88.1
45	- 1	44	- 1		7		44				50		44	- 1		3	32		45	88.0
		а		<u>6ο'</u> Δ	b	$\frac{\Delta}{\epsilon o'}$	a	ı	<u>60'</u> Δ	b		$\frac{\Delta}{60'}$	0	ı	<u>60'</u> Δ	b		Δ 60'		a
t		_	,	d=1	° 30′				d = 2	2° 0′	,				d = 2	° 30′				

\ b		a = 1	° 30′			•	a = 2	2° 0)′			(a = 2	° 30)′		C	a
$B \setminus$	h	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	*	<u>Δ</u> 6ο'	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$c \setminus$	β
9 45 46 47 48 49	44 59 45 59 46 59 47 59 48 59	I I I I	2 2 12 12 12	.03	44 45 46 47 48	58 58 58 58 58	1 1 1 1	3	50 53 56 59 3	0.05 .05 .05 .07	44 45 46 47 48	57 57 56 56 56	I I.02 I I I	3	32 36 40 44 48	0.07 .07 .07 .07 .08	° 45 44 43 42 41	88.0 87.9 87.9 87.8 87.7
50 51 52 53 54	49 59 50 59 51 58 52 58 53 58	I I.02 I I I	20 20 20 20 3	.05	49 50 51 52 53	58 57 57 57 57	I.02 I I I I		7 11 15 19 24	0.07 .07 .07 .08 .08	49 50 51 52 53	56 56 56 56	I I I I I.02	4	53 58 3 9	80.0 80. 01. 01.	40 39 38 37 36	87.6 87.5 87.4 87.3 87.2
55 56 57 58 59	54 58 55 58 56 58 57 58 58 58	I I I	32 4 4 50 5	.07	54 55 56 57 58	57 57 57 57 57	I I I I.02		29 34 40 46 53	0.08 .10 .10 .12	54 55 56 57 58	55 55 55 55	I I I I I,02		21 28 35 43 51	.12 .13 .13	35 34 33 32 31	87.1 87.0 86.9 86.8 86.7
60 61 62 63 64	59 58 60 58 61 58 62 58 63 58	I I I I,02	3 (.10 .10 .12	59 60 61 62 63	56 56 56 56 56	I I I I	4	7 15 24 33	0.12 .13 .15 .15	59 60 61 62 63	54 54 54 54 53	I I I I.02 I	5	9 19 30 41	0.15 .17 .18 .18	30 29 28 27 26	86.5 86.4 86.2 86.1 85.9
65 66 67 68 69	64 57 65 57 66 57 67 57 68 57	I I I I	3. 4 50 4	.15	64 65 66 67 68	56 55 55 55 55	I.02 I I I I.02	5	43 54 6 19 34	0.18 .20 .22 .25 .27	64 65 66 67 68	53 52 52 52 52	I I.02 I I I.02	6	54 23 39 57	0.23 .25 .27 .30 .32	25 24 23 22 21	85.7 85.5 85.3 85.1 84.8
70 71 72 73 74	69 57 70 57 71 56 72 56 73 56	I I.02 I I I	5 20	.25	69 70 71 72 73	54 54 54 53 53	I I.02 I I.02	6	50 7 27 49 13	0.28 ·33 ·37 ·40 ·47	69 70 71 72 73	51 50 49 49	I I.02 I.02 I I.02	7 8 9	16 38 30 0	0.37 .42 .45 .50 .58	20 19 18 17 16	84.5 84.2 83.9 83.5 83.1
75 76 77 78 79	74 56 75 55 76 55 77 54 78 54	I.02 I I.02 I I.02	6 I 39 7 I 49	·47 ·53 ·63	74 75 76 77 78	52 52 51 50 49	I I.02 I.02 I.02 I.02	8 9 10	41 13 50 32 22	0.53 .62 .70 .83	74 75 76 77 78	48 47 46 45 43	1.02 1.02 1.02 1.03 1.02	10 11 12	35 14 59 52 53	0.65 •75 .88 1.02 1.23	15 14 13 12	82.6 82.0 81.4 80.7 79.8
80 81 82 83 84	79 53 80 53 81 52 82 51 83 49	I I.02 I.02 I.03 I.03	8 3 9 30 10 30 12		79 80 81 82 83	48 47 45 43 41	1.02 1.03 1.03 1.03 1.07	11 12 14 15 18	22 35 5 59 28	,	79 80 81 82 83	42 40 37 34 30	1.03 1.05 1.05 1.07 1.09	14 15 17 19 22	7 36 25 43 40	·	9 8 7 6	78.8 77.6 76.1 74.1 71.6
85 86 87 88 89 90	84 47 85 44 86 39 87 30 88 12	1.05 1.09 1.18 1.43 3.33	16 4. 20 3 26 3 36 5. 56 19	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		37 32 24 10 46	1.09 1.15 1.30 1.67 4.29		50 36 43 1 27		84 85 86 87	25 17 6 48 18	1.15 1.22 1.43 2.00 5.00	26 32 39 51 68	13		5 4 3 2 1	68.3 63.5 56.3 45.0 26.6
	a	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	-	a	60' A	11	b	$\frac{\Delta}{60'}$	-	z	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{\epsilon o'}$	==	<u>а</u>
t		1	° 30′	1 30			d=2	2° 0	,	1 00			d=2	° 30	0′			

\ b		a = 1	3° 0′		Ī	_	a=3	° 30	0′				a = 4	ا° 0	,		\ c	a
$ _{B}$	h d	<u>εο'</u> Δ	Z	<u>Δ</u> 6ο'	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	6ο' Δ	Z	ŧ	$\frac{\Delta}{60'}$	C	β
0 0 1 2 3 4	0 0 1 0 2 0 3 0 4 0	I I I I I I I I I I I I I I I I I I I	3 0 0 0 0 0	0.00	° 0 1 2 3 4	100000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3		0.00	° 0 I 2 3	0000	I I I I.02 I	° 4	0000	0.00 .00 .00 .02	90 89 88 87 86	90.0 89.9 89.9 89.8 89.8
5 6 7 8 9	5 0 6 0 59 7 59 8 59	I I.02 I I	I I I 2 2	0.00 .00 .02 .00	5 6 7 8	59 59 59 59	I I I I		31 32 32 32 33	0.00 .02 .00 .02	4 5 6 7 8	59 59 59 59 59	I I I J		I 2 2 3	0.00 .02 .00 .02	85 84 83 82 81	89.7 89.6 89.6 89.5 89.4
10 11 12 13 14	9 59 10 59 11 59 12 59 13 59	1 1 1 1	3 3 4 5 5	.02	9 10 11 12 13	59 59 59 59 58	1 1 1 1.02		33 34 35 36 36	0.02 .02 .02 .00	9 10 11 12 13	59 58 58 58 58	I.02 I I I I		4 4 5 6 7	0.00 .02 .02 .02	80 79 78 77 76	89.4 89.3 89.3 89.2 89.1
15 16 17 18 19	14 59 15 59 16 59 17 58 18 58	1 1.02 1 1	6 7 8 9	0.02 .02 .02 .02	14 15 16 17 18	58 58 58 58 58	1 1 1 1		37 38 39 41 42	0.02 .02 .03 .02	14 15 16 17 18	58 58 57 57 57	I I.02 I I I		8 10 11 12 14	0.03 .02 .02 .03 .02	75 74 73 72 71	89.1 89.0 88.9 88.9 88.8
20 21 22 23 24	19 58 20 58 21 58 22 58 23 58	III	11 13 14 15	19 20 21 22 23	58 58 57 57 57	1 1.02 1 1		43 45 46 48 50	0.03 .02 .03 .03	19 20 21 22 23	57 57 57 56 56	I I I.02 I I		15 17 19 21 23	0.03 .03 .03 .03	70 69 68 67 66	88.7 88.7 88.6 88.5 88.4	
25 26 27 28 29	24 58 25 58 26 58 27 57 28 57	I I I.02 I I	18 20 22 24 26	0.03 .03 .03 .03	24 25 26 27 28	57 57 57 57 56	I I I I.02 I	4	52 54 56 58 0	0.03 .03 .03 .03	24 25 26 27 28	56 56 56 55	I I I I.02 I		25 27 29 32 34	0.03 .03 .05 .03	65 64 63 62 61	88.4 88.3 88.2 88.1 88.1
30 31 32 33 34	29 57 30 57 31 57 32 57 33 57	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	28 30 32 34 37	0.03 .03 .03 .05	29 30 31 32 33	56 56 56 56 56	1 1 1 1		2 5 8 10 13	0.05 .05 .03 .05	29 30 31 32 33	55 55 55 54	I I I I.02		37 40 43 46 49	0.05 .05 .05 .05	59 58 57 56	88.0 87.9 87.8 87.7 87.6
35 36 37 38 39	34 57 35 57 36 56 37 56 38 56	32 57 I 34 .c 33 57 I 37 .c 34 57 I 40 o.c 55 57 I.o2 42 .c 56 I 45 .c					I.02 I I I I		16 19 23 26 30	0.05 .07 .05 .07	34 35 36 37 38	54 54 54 53 53	1 1 1,02 1	5	53 56 0 4 8	0.05 .07 .07 .07	55 54 53 52 51	87.6 87.5 87.4 87.3 '87.2
40 41 42 43 44	39 56 40 56 41 56 42 56 43 55	I I I I.02 I	55 58 4 2 6	0.05 .07 .07 .07	37 38 39 40 41 42 43		1.02 1 1 1 1		34 38 42 47 52	0.07 .07 .08 .08		52	I I.02 I I		13 18 23 28 33	0.08	46	87.1 87.0 86.9 86.7 86.6
45	44 55	60'	14	Ι	44		601		57	Δ		52	60'	,	39	Δ	45	86.5
t	a	Δ	b	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$		b	<u>Δ</u> 60'	0	ı	Δ	1		60′		a
		d = 3	3° 0′				d = 3	° 30)′				d = 4	f _o O	'			

\ b		a = 3	3° C)′				a = 3	3° 3	0′				a = c	4° ()′		\ v	•
$B \setminus$	h d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	44 55 45 55 46 55 47 55 48 55	I I I I I.02	4	14 19 24 29 34	0.08	0 44 45 46 47 48	54 53 53 53 53	I.02 I I I I.02	6 4 5	57 2 7 13	0.08 .08 .10 .10	0 44 45 46 47 48	52 51 51 51 50	I.02 I I I.02	6	39 45 51 58 5	0.10 .10 .12 .12	° 45 44 43 42 41	86.5 86.4 86.3 86.1 86.0
50 51 52 53 54	49 54 50 54 51 54 52 54 53 54	I I I I I.02	5	40 46 52 59 6	0, IO .10 .12 .12	49 50 51 52 53	52 52 52 51 51	I I I.02 I I		26 33 40 48 56	0.12 .12 .13 .13	49 50 51 52 53	50 50 49 49	I I.02 I I I.02		13 21 29 38 47	0.13 .13 .15 .15	40 39 38 37 36	85.8 85.7 85.5 85.4 85.2
55 56 57 58 59	54 53 55 53 56 53 57 52 58 52	I I I.02 I I		13 21 30 39 49	0.13 .15 .15 .17	54 55 56 57 58	51 50 50 50 49	I.02 I I I.02 I	6	5 14 24 35 46	0.15 .17 .18 .18	54 55 56 57 58	48 48 47 47 46	I I.02 I I.02 I	7	57 8 19 31 44	0.18 .18 .20 .22 .23	35 34 33 32 31	85.0 84.8 84.6 84.4 84.2
60 61 62 63 64	59 52 60 52 61 51 62 51 63 50	I I.02 I 1.02 I	6	59 10 22 35 49	0.18 .20 .22 .23 .25	59 60 61 62 63	49 48 48 47 47	I.02 I I.02 I I.02	7	58 11 25 40 56	0.22 .23 .25 .27 .30	59 60 61 62 63	46 45 44 44 43	I.02 I.02 I I.02 I.02	8	58 13 28 45 4	0.25 .25 .28 .32 .33	30 29 28 27 26	84.0 83.7 83.5 83.2 82.9
65 66 67 68 69	64 50 65 49 66 49 67 48 68 48	1.02 I 1.02 I I.02	7 8	4 20 38 58 19	0.27 .30 .33 .35	64 65 66 67 68	46 46 45 44 43	I I.02 I.02 I.02 I.02	9	14 33 54 16 41	0.32 ·35 ·37 ·42 ·45	64 65 66 67 68	42 41 40 39 38	I.02 I.02 I.02 I.02 I.02	10	24 45 9 34 2	0.35 .40 .42 .47 .52	25 24 23 22 21	82.5 82.3 81.8 81.4 81.0
70 71 72 73 74	69 47 70 46 71 46 72 45 73 44	1.02 1 1.02 1.02 1.02	9	43 9 38 10 46	0.43 .48 .53 .60 .68	69 70 71 72 73	42 41 40 39 38	I.02 I.02 I.02 I.02 I.03	10 11 12	8 38 12 49 31	0.50 .57 .62 .70 .78	69 70 71 72 73	37 36 35 33 31	I.02 I.02 I.03 I.03 I.03	13	33 7 45 27 14	0.57 .63 .70 .78 .88	20 19 18 17 16	80.5 79.9 79.4 78.7 78.0
75 76 77 78 79	74 43 75 41 76 40 77 38 78 36	1.03 1.02 1.03 1.03	11 12 13 14 15	27 13 7 9 22	0.77 .90 I.03 I.22 I.43	74 75 76 77 78	36 35 33 30 28	I.02 I.03 I.05 I.03 I.05	13 14 15 16	18 11 13 24 46	0.88 1.03 1.18 1.37 1.63	74 75 76 77 78	29 27 25 22 18	1.03 1.03 1.05 1.07	15 16 17 18 20	7 16 35 8	1.00 1.15 1.32 1.55 1.80	15 14 13 12 11	77.2 76.2 75.2 74.0 72.6
80 81 82 83 84	79 34 80 31 81 28 82 23 83 18	1.05 1.05 1.09 1.09	16 18 20 23 26	48 31 38 16 38		79 80 81 82 83	25 21 16 11 3	1.07 1.09 1.09 1.15 1.18	19 21 23 26 30	24 21 43 39 20		79 80 81 82	14 9 4 57 48	1.09 1.09 1.13 1.18 1.25	21 24 26 29 33	56 5 41 51 47		10 9 8 7 6	70.9 68.9 66.5 63.6 59.9
85 86 87 88 89	84 10 85 0 45 86 24 50			55 2 20 35		84 85 86	54 41 23 58 22	1.28 1.43 1.71 2.50 7.50		4 15 27 17 4		83 84 85	36 21 0 32 53	1.33 1.54 1.88 2.86 8.57	38 45 53 63 75	44 4 11 29 59		5 4 3 2 1	55.1 48.9 40.6 29.8 10.0
90	87 0		90	0			30		90	0		86	0		90	0		0	0.0
t.	а	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $					ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	(ı	<u>6ο′</u> Δ		b	<u>∆</u> 60′		a
,					d=3	° 30	0′				d =	4° ()′						

								_			_						-	a .
	b	a = 4	4° 30′				a = 3	5° ()′				a = 5	5° 3	0′		$\setminus c$	\ a
B	h	$\frac{1}{\Delta} \frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	$C \setminus$	β
22 3	O I 2 2 5	1 0 1 0 1.02 9 1	4 30 30 30 30 31	.00	0 I 2		I I I.02 I I	5	0 0 0	0.00	0 I 2 3		I I.02 I I	5	30 30 30 30 31	.00	90 89 88 87 86	90.0 89.9 89.8 89.7 89.7
78	6 5 7 5 8 5	1 1 1 1.02 1	31 31 32 33 33	0.00 .02 .02 .00	4 5 6 7 8	59 58 58 58	I I.02 I I I		1 2 2 3 4	0.02 .00 .02 .02	4 5 6 7 8	59 58 58 58	I.02 I I I I.02		31 32 32 33 34	0.02 .00 .02 .02	85 84 83 82 81	89.6 89.5 89.4 89.3 89.2
10 11 12 13 14	10 5 11 5 12 5	8 I 8 I 8 I.02	34 35 36 37 38	.02	9 10 11 12 13	58 57 57 57 57	I.02 I I I I.02		5 6 7 8 9	0.02 .02 .02 .02	9 10 11 12 13	57 57 57 56 56	I I I.02 I		35 36 37 39 40	0.02 .02 .03 .02 .03	80 79 78 77 76	89.1 89.0 88.9 88.8 88.8
15 16 17 18 19	15 5 16 5 17 5	7 I 7 I 7 I.02	39 41 42 44 45	0.03 .02 .03 .02	14 15 16 17 18	56 56 56 56 55	I I I I.02		10 12 14 15	0.03 .03 .02 .03	14 15 16 17 18	56 55 55 55 55	I.02 I I I I.02		42 43 45 47 49	0.02 .03 .03 .03	75 74 73 72 71	88.7 88.6 88.5 88.4 88.3
20 21 22 23 24	19 50 20 50 21 50 22 50 23 5	I I I I I I I I I I I I I I I I I I I	47 49 51 53 55	0.03 .03 .03 .03	19 20 21 22 23	55 55 55 54 54	1 1 1.02 1 1		19 21 23 26 28	0.03 .03 .05 .03	19 20 21 22 23	54 54 54 53 53	I I I.02 I I	6	51 53 56 58 1	0.03 .05 .03 .05	70 69 68 67 66	88.2 88.1 88.0 87.9 87.8
25 26 27 28 29	24 5! 25 5! 26 5! 27 52 28 52	I I.02 I	58 5 0 3 6 9	0.03 .05 .05 .05	24 25 26 27 28	54 54 53 53 53	I I.02 I I I.02		31 34 37 40 43	0.05 .05 .05 .05	24 25 26 27 28	53 52 52 52 51	I.02 I I I.02 I		4 7 10 13 17	0.05 .05 .05 .07	65 64 63 62 61	87.7 87.6 87.5 87.3 87.2
30 31 32 33 34	29 54 30 54 31 53 32 53 33 53	I 1.02	12 15 18 22 25	0.05 .05 .07 .05	29 30 31 32 33	52 52 52 52 51	I I I I.02 I	6	46 50 53 57	0.07 .05 .07 .07	29 30 31 32 33	51 50 50 50 49	I.02 I I I.02 I		21 25 29 33 37	0.07 .07 .07 .07	59 58 57 56	87.1 87.0 86.9 86.8 86.6
35 36 37 38 39	34 53 35 52 36 52 37 52 38 51	I I I.02	29 33 38 42 47	0.07 .08 .07 .08	34 35 36 37 38	51 50 50 49	I I.02 I I.02 I		6 10 15 20 25	0.07 .08 .08 .08	34 35 36 37 38	49 49 48 48 47	I I.02 I I.02 I	7	42 47 52 58 4	80.0 80. 01. 01.	55 54 53 52 51	86.5 86.4 86.2 86.1 86.0
40 41 42 43 44	39 51 40 51 41 50 42 50 43 50	I.02 I I	52 57 6 3 9	0.08 .10 .10 .10	39 40 41 42 43	49 49 48 48 47	I I.02 I I.02 I		31 37 43 49 56	0.IO .IO .IO .I2	39 40 41 42 43	47 46 46 45 45	I.02 I I.02 I I.02		10 16 23 30 37	0.10 .12 .12 .12	50 49 48 47 46	85.8 85.7 85.5 85.4 85.2
45	44 49		21		44	47		7	3		44	44			45		45	85.0
4	а	$\frac{60'}{\Delta}$	b	<u>Δ</u> 60'	a		$\frac{\epsilon_{\mathbf{O'}}}{\Delta}$	l	b	<u>Δ</u> 6ο'	a		<u>6ο'</u> Δ	t		$\frac{\Delta}{60'}$		а
t		d = 4	° 30′				d = 5	° 0′	,			a	l=5	30)′			

10.39

11.43

N.																		1\	1
\ b		a = 4	° 3	0′	-			a = 8	5° 0) ′				a = 5	° 3	0′		$\setminus c$	a
$B \setminus$	h	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	$\frac{d}{}$	6ο' Δ	z	t	<u>Δ</u> 6ο'	$C \setminus$	β
° 45 46 47 48 49	0 / 44 49 45 49 46 49 47 48 48 48	I I I.02 I I.02	6	21 28 35 42 50	0.12 .12 .12 .13	° 44 45 46 47 48	47 46 46 45 45	I.02 I I.02 I I.02	7	3 11 19 27 36	0.13 .13 .13 .15	0 44 45 46 47 48	44 44 43 42 42	I I.02 I.02 I I.02	8	45 53 2 11 21	0.13 .15 .15 .17	° 45 44 43 42 41	85.0 84.8 84.7 84.5 84.3
50 51 52 53 54	49 47 50 47 51 46 52 46 53 45	I I.02 I I.02 I	7	59 8 17 27 38	0.15 .15 .17 .18	49 50 51 52 53	44 44 43 43 42	I I.02 I I.02 I.02	8	45 55 5 16 28	0.17 .17 .18 .20	49 50 51 52 53	41 40 39 38	I I.02 I.02 I.02 I	9	31 42 53 5 18	0.18 .18 .20 .22 .23	40 39 38 37 36	84.1 83.9 83.6 83.4 83.2
55 56 57 58 59	54 45 55 44 56 44 57 43 58 42	I.02 I I.02 I.02 I	8	49 I I 3 27 42	0.20 .20 .23 .25	54 55 56 57 58	41 40 39 38	I I.02 I.02 I.02 I.02	9	40 53 7 22 38	0.22 .23 .25 .27 .30	54 55 56 57 58	38 37 36 35 34	I.02 I.02 I.02 I.02 I.02	10	32 46 2 18 35	0.23 .27 .27 .28 .32	35 34 33 32 31	82.9 82.6 82.4 82.1 81.7
60 61 62 63 64	59 42 60 41 61 40 62 39 63 38	I.02 I.02 I.02 I.02 I.02	9	57 13 31 50 11	0.27 .30 .32 .35 .37	59 60 61 62 63	37 36 35 34 33	I.02 I.02 I.02 I.02 I.02	10	56 14 33 54 17	0.30 .32 .35 .38 .42	59 60 61 62 63	33 32 30 29 28	I.02 I.03 I.02 I.02 I.03	11	54 14 35 58 23	0.33 ·35 ·38 ·42 ·45	30 29 28 27 26	81.4 81.1 80.7 80.3 79.9
65 66 67 68 69	64 37 65 36 66 35 67 34 68 33	1.02 1.02 1.02 1.02 1.03	11	33 57 23 52 23	0.40 •43 •48 •52 •57	64 65 66 67 68	32 31 29 28 26	I.02 I.03 I.02 I.03 I.02	12	42 8 37 9 43	0.43 .48 .53 .57 .63	64 65 66 67 68	26 25 23 21 19	I.02 I.03 I.03 I.03 I.03	13 14 15	50 19 51 25 2	0.48 •53 •57 .62 .68	25 24 23 22 21	79.4 78.9 78.4 77.8 77.2
70 71 72 73 74	69 31 70 30 71 28 72 26 73 24	1.02 1.03 1.03 1.03 1.05	13 14 15	57 35 17 4 56	0.63 .70 .78 .87 .98	69 70 71 72 73	25 23 20 18 15	1.03 1.05 1.03 1.05 1.05	14 15 16 17	21 48 40 37	0.68 •77 .87 •95	69 70 71 72 73	17 15 12 9	1.03 1.05 1.05 1.05	16 17 18	43 28 18 14 15	0.75 .83 .93 1.02 1.15	20 19 18 17 16	76.5 75.8 75.0 74.1 73.1
75 76 77 78 79	74 21 75 18 76 15 77 12 78 8	1.05 1.05 1.05 1.07 1.09	16 18 19 20 22	55 1 17 44 25	1.10 1.27 1.45 1.68 1.97	74 75 76 77	9 5 1 56	1.05 1.07 1.07 1.09 1.11	18 19 21 22 24	41 53 15 49 38	1.20 1.37 1.57 1.82 2.10	74 75 76 77	3 59 54 49 43	1.07 1.09 1.09 1.11 1.13	20 21 23 24 26	24 42 10 51 47	1.30 1.47 1.68 1.93 2.23	15 14 13 12 11	72.0 70.7 69.3 67.7 65.9
80 81 82 83 84	79 3 57 80 50 81 41 82 30	1.11 1.13 1.18 1.22 1.28	24 26 29 32 36	23 42 29 51 59		78 79 80 81 82	50 43 34 24 12	1.13 1.18 1.20 1.25 1.36	26 29 32 35 39	44 13 9 40 56		78 79 80 81	36 28 18 6 52	1.15 1.20 1.25 1.30 1.43	29 31 34 38 42	37 41 19 39	2.60	10 9 8 7 6	63.7 61.2 58.2 54.6 50.3
85 86 87 88 89	83 17 59 84 36 85 5 23		42 48 56 66 77	5 27 23 5 30		83 84	56 36 10 37 54	1.50 1.76 2.22 3.53 10.0	45 51 59 68 78	7 26 7 15 43		82 83 84	34 12 44 9 25	1.58 1.88 2.40 3.75 12.0	47 54 61 70 79	51 28 5 44		5 4 3 2 1	45.1 38.7 31.0 21.8 11.3
90	30		90	0		85	0		90	0			30		90	0		0	0.0
4	а	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	1	b	<u>Δ</u> 60'	a	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
t		d=4° 30′						d =	5° ()′				d = 5	° 3	0′			

8		a = 0	6° 0′				$a = \epsilon$	3° 3	0′				a = '	7° 0	,		\ c	\ a
B	h	<u>6ο'</u> Δ	Z t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	1	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	0 0 1 0 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1.02 1 1 1 1.02	6 0	.00	0 I 2 3	0 59 59 58	I I.02 I I.02 I	6	30 30 30 31 31	.00	2 3	0 59 59 58	I I.02 I I.02 I	7	0 0 0 1 1	0.00	90 89 88 87 86	90.0 89.9 89.8 89.7 89.5
5 6 7 8 9	4 58 5 58 6 58 7 57 8 57	I I.02	1 2 3 4 5	0.02 .02 .02 .02	4 5 6 7 8	58 58 57 57 57	I I.02 I I I.02		31 32 33 34 35	0.02 .02 .02 .02	4 5 6 7 8	58 57 57 56 56	I.02 I I.02 I I.02		2 2 3 4 5	0.00 .02 .02 .02	85 84 83 82 81	89.4 89.3 89.2 89.1 89.0
10 11 12 13 14	9 57 10 56 11 56 12 56 13 55	I I I,02	6 7 8 9	0.02 .02 .02 .03	9 10 11 12 13	56 56 55 55 54	I I.02 I I.02 I		36 37 39 40 42	0.02 .03 .02 .03	9 10 11 12 13	55 55 54 54	I I.02 I I.02		6 8 9 11 13	0.03 .02 .03 .03	80 79 78 77 76	88.9 88.7 88.6 88.5 88.4
15 16 17 18 19	14 55 15 55 16 54 17 54 18 54	I.02 I I	13 14 16 18 21	0.02 .03 .03 .05	14 15 16 17 18	54 54 53 53 52	I I.02 I I.02 I		44 46 48 50 52	0.03 .03 .03 .03	14 15 16 17 18	53 53 52 52 51	I I.02 I I.02 I		15 17 19 21 24	0.03 .03 .03 .05	75 74 73 72 71	88.3 88.1 88.0 87.9 87.8
20. 21 22 23 24	19 53 20 53 21 52 22 52 23 52	I.02	23 25 28 31 34	0.03 .05 .05 .05	19 20 21 22 23	52 52 51 51 50	I I.02 I I.02 I	7	55 57 0 3 6	0.03 .05 .05 .05	19 20 21 22 23	51 50 50 49 49	I.02 I I.02 I I.02		27 30 33 36 39	0.05 .05 .05 .05	70 69 68 67 66	87.6 87.5 87.4 87.2 87.1
25 26 27 28 29	24 51 25 51 26 50 27 50 28 50	I.02 I	37 40 44 47 51	0.05 .07 .05 .07	24 25 26 27 28	50 49 49 48 48	I.02 I I.02 I I.02		10 13 17 21 25	0.05 .07 .07 .07	24 25 26 27 28	48 48 47 46 46	I I.02 I.02 I I.02		43 47 51 55 59	0.07 .07 .07 .07	65 64 63 62 61	87.0 86.8 86.7 86.6 86.4
30 31 32 33 34	29 49 30 49 31 48 32 48 33 47	I.02	55 59 7 4 9	0.07 .08 .08 .08	29 30 31 32 33	47 47 46 46 45	I I.02 I I.02 I		30 34 39 44 49	0.07 .08 .08 .08	29 30 31 32 33	45 45 44 43 43	I I.02 I.02 I I.02	8	4 9 14 20 26	80.0 80. 01. 01.	60 59 58 57 56	86.3 86.1 86.0 85.8 85.6
35 36 37 38 39	34 47 35 46 36 46 37 45 38 45	I.02	19 24 30 36 42	0.08 .10 .10 .10	34 35 36 37 38	45 44 43 43 42	I.02 I.02 I I.02 I.02	8	55 1 7 14 21	0.10 .10 .12 .12	34 35 36 37 38	42 41 41 40 39	I.02 I I.02 I.02 I		32 38 45 52 59	0.10 .12 .12 .12	55 54 53 52 51	85.5 85.3 85.1 84.9 84.8
40 41 42 43 44	39 44 40 44 41 43 42 42 43 42	I.02 I.02	49 56 8 3 11 19	0.12 .12 .13 .13	39 40 41 42 43	41 40 39 39	I I.02 I.02 I I.02	9	28 35 43 51 0			39 38 37 36 35	I.02 I.02 I.02 I.02 I.02	9	6 14 23 32 41	0.13 .15 .15 .15	50 49 48 47 46	84.6 84.4 84.2 84.0 83.8
45	44 41	1	27		44	38			9		44	34			51		45	83.5
$ _t$	а	$\frac{60'}{\Delta}$	b	<u>∆</u> 60′	а	ı	$\frac{60'}{\Delta}$	l	6	$\frac{\Delta}{60'}$		a	<u>6ο′</u> Δ	b		$\frac{\Delta}{60'}$		a
		d = 6	3° 0′				d = 6	° 30)′				d = 7	7° 0′	,			

8			a = 0	3° 0)′				a = 6	s° 30)′				<i>a</i> =	7° ()*		\ c	a
$B \setminus$	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	$c \setminus$	β
45 46 47 48 49	44 45 46 47 48	41 41 40 39 38	I I.02 I.02 I.02 I	8	27 36 46 56	0.15 .17 .17 .17	44 45 46 47 48	38 37 36 36 35	I.02 I.02 I I.02 I.02	9	9 19 29 40 51	0.17 .17 .18 .18	44 45 46 47 48	34 34 33 32 31	I I.02 I.02 I.02 I.02	9	51 1 12 24 36	0.17 .18 .20 .20	45 44 43 42 41	83.5 83.3 83.1 82.8 82.6
50 51 52 53 54	49 50 51 52 53	38 37 36 35 34	I.02 I.02 I.02 I.02 I.02	10	17 29 41 54 8	0.20 .20 .22 .23 .25	49 50 51 52 53	34 33 32 31 30	I.02 I.02 I.02 I.02 I.02	10	3 16 29 43 58	0.22 .22 .23 .25 .27	49 50 51 52 53	30 29 27 26 25	1.02 1.03 1.02 1.02 1.02	11	49 2 17 32 48	0.22 .25 .25 .27 .28	40 39 38 37 36	82.3 82.0 81.8 81.5 81.1
55 56 57 58 59	54 55 56 57 58	33 32 31 30 29	I.02 I.02 I.02 I.02 I.02	11	23 39 55 13 32	0.27 .27 .30 .32 .33	54 55 56 57 58	29 27 26 25 24	1.03 1.02 1.02 1.02 1.03	11	14 31 49 8 28	0.28 .30 .32 .33 .37	54 55 56 57 58	24 22 21 19 18	I.03 I.02 I.03 I.02 I.03	13	5 23 42 3 25	0.30 .32 .35 .37 .38	35 34 33 32 31	80.8 80.5 80.1 79.7 79.3
60 61 62 63 64	59 60 61 62 63	28 26 25 23 22	I.03 I.02 I.03 I.02 I.03	12	52 14 37 2 29	0.37 .38 .42 .45 .48	59 60 61 62 63	22 21 19 17 15	1.02 1.03 1.03 1.03 1.03	13	50 13 38 5 34	0.38 .42 .45 .48 .52	59 60 61 62 63	16 14 12 10 8	I.03 I.03 I.03 I.03	14	48 13 39 8 39	0.42 •43 •48 •52 •55	30 29 28 27 26	78.9 78.5 78.0 77.5 76.9
65 66 67 68 69	64 65 66 67 68	20 18 16 14	1.03 1.03 1.03 1.03 1.05	14 15 16	58 29 3 40 21	0.52 •57 .62 .68 •73	64 65 66 67 68	13 11 9 6 4	1.03 1.03 1.05 1.03 1.05	15 16 17	5 39 15 55 38	0.57 .60 .67 .72 .78	64 65 66	6 4 58 55	1.03 1.05 1.05 1.05	16 17 18	12 48 27 9 55	0.60 .65 .70 .77 .83	25 24 23 22 21	76.4 75.7 75.1 74.3 73.6
70 71 72 73 74	69 70 71 72	9 6 3 0 56	1.05 1.05 1.05 1.07	17 18 19 20	5 54 47 46 52	0.82 .88 .98 1.10	69 70 71 72	58 54 50 46	1.05 1.07 1.07 1.07 1.09	18 19 20 21 22	25 17 14 17 27	0.87 .95 1.05 1.17 1.30	68 69 70 71 72	52 48 44 39 34	1.07 1.07 1.09 1.09	19 20 21 22 24	45 40 40 47 1	0.92 1.00 1.12 1.23 1.37	20 19 18 17 16	72.7 71.8 70.8 69.7 68.5
75 76 77 78 79	73 74 75 76 77	52 47 42 36 29	1.09 1.09 1.11 1.13 1.15	22 23 25 26 28	6 29 3 49 51	1.38 1.57 1.77 2.03 2.33	73 74 75 76 77	41 36 30 23 15	1.09 1.11 1.13 1.15 1.18	23 25 26 28 30	45 13 52 43 50	1.47 1.65 1.85 2.12 2.43	73 74 75 76	29 23 16 8 59	1.11 1.13 1.15 1.18 1.20	25 26 28 30 32	23 55 38 34 46	1.53 1.72 1.93 2.20 2.50	15 14 13 12 11	67.1 65.6 63.9 62.0 59.8
80 81 82 83 84	78 79 80 81	21 12 1 47 31	1.18 1.22 1.30 1.36 1.46	31 33 37 40 45	54 4 47 9	2.72	78 79 80 81	6 55 42 28 10	1.22 1.28 1.30 1.43 1.58	33 36 39 43 47	16 4 18 4 28	2.80	77 78 79 80	49 37 23 7 47	1.25 1.30 1.36 1.50 1.62	35 38 41 45 49	16 8 25 13 36	2.87	10 9 8 7 6	57·3 54·4 51.1 47·3 42·9
85 86 87 88 89	82 83	12 48 18 41 55	1.67 2.00 2.61 4.29 12.0		20 26 32 38 34		82 83	48 22 51 12 25	1 4		35 31 20 58 17		81 82	24 57 23 43 56	1.82 2.31 3.00 4.62 15.0	54 60 66 74 81	38 24 55 8 55		5 4 3 2 1	37·7 31·7 24.8 17·1 8.8
90	84	0		90	0		-	30		90	0		83	0		90			0	0.0
$ _t$		a	<u>δο'</u> Δ		b	$\frac{\Delta}{60'}$		a	60' <u>∆</u>		b	$\frac{\Delta}{60'}$	L	a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
			<i>d</i> =	6° C)′				d = 6	3° 3	0′				d =	7° ()′		j.	

\	-														_			1
$\setminus b$		a = 7	° 30′				a = 3	8° ()′				a = 8	3° 3	0′		c	\ a
$B \setminus$	h d	6ο ′ Δ	Z	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	z	*	<u>Δ</u> 6ο'	h	d	$\frac{60'}{\Delta}$	Z	t	<u>∆</u> 60′	$C \setminus$	β
0 I 2 3 4	0 0 59 1 59 2 58 3 58	I.02 I I.02 I I.02	7 30 30 30 31 31	0.00	° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	59 59 58 58	I.02 I I.02 I I.02	8	0 0 0 I I	0.00 .00 .02 .00	0 1 2 3		I.02 I I.02 I.02	8	30 30 30 31 31	0.00 .00 .02 .00	90 89 88 87 86	90.0 89.9 89.7 89.6 89.4
5 6 7 8 9	4 57 5 57 6 56 7 56 8 55	I I.02 I I.02 I	32 32 33 34 35	0.00 .02 .02 .02	4 5 6 7 8	57 56 56 55	I.02 I I.02 I I.02		3 4 5 6	0.02 .02 .02 .02 .02	4 5 6 7 8	57 56 55 55 54	I.02 I.02 I I.02 I.02		32 33 34 35 36	0.02 .02 .02 .02	85 84 83 82 81	89.3 89.2 89.0 88.9 88.7
10 11 12 13 14	9 55 10 54 11 54 12 53 13 53	I.02 I I.02 I I.02	37 38 40 42 44	0.02 .03 .03 .03	9 10 11 12 13	54 53 53 52 52	I.02 I I.02 I I.02		7 9 11 13 15	0.03 .03 .03 .03	9 10 11 12 13	53 53 52 51 51	I I.02 I.02 I I.02		38 39 41 43 45	0.02 .03 .03 .03	80 79 78 77 76	88.6 88.5 88.3 88.2 88.0
15 16 17 18 19	14 52 15 52 16 51 17 50 18 50	I I.02 I.02 I I.02	46 48 50 53 56	0.03 .03 .05 .05	14 15 16 17 18	51 50 50 49 48	I.02 I I.02 I.02		17 19 22 24 27	0.03 .05 .03 .05	14 15 16 17 18	50 49 48 48 47	I.02 I.02 I I.02 I.02		48 50 53 56 59	0.03 .05 .05 .05	75 74 73 72 71	87.9 87.7 87.6 87.4 87.3
20 21 22 23 24	19 49 20 49 21 48 22 48 23 47	I I.02 I I.02 I.02	8 2 5 8 12	0.05 .05 .05 .07	19 20 21 22 23	48 47 46 46 45	I.02 I.02 I I.02 I.02		30 34 37 41 45	0.07 .05 .07 .07	19 20 21 22 23	46 46 45 44 43	I I.02 I.02 I.02 I.02	9	2 6 9 13	0.07 .05 .07 .07	70 69 68 67 66	87.1 86.9 86.8 86.6 86.5
25 26 27 28 29	24 46 25 46 26 45 27 44 28 44	I I.02 I.02 I I.02	16 20 24 29 34	0.07 .07 .08 .08	24 25 26 27 28	44 44 43 42 41	1 1.02 1.02 1.02	9	49 53 58 3	0.07 .08 .08 .08	24 25 26 27 28	42 42 41 40 39	I I.02 I.02 I.02 I.02		22 26 31 36 42	0.07 .08 .08 .10	65 64 63 62 61	86.3 86.1 85.9 85.8 85.6
30 31 32 33 34	29 43 30 42 31 42 32 41 33 40	1.02 1 1.02 1.02 1.02	39 44 49 55 9 1	0.08 .08 .10 .10	29 30 31 32 33	41 40 39 38 37	I.02 I.02 I.02 I.02		13 19 25 31 37	0.10 .10 .10 .10	29 30 31 32 33	38 37 36 36 35	I.02 I.02 I I.02 I.02	10	48 54 0 6 13	0.10 .10 .10 .12	59 58 57 56	85.4 85.2 85.0 84.8 84.6
35 36 37 38 39	34 39 35 39 36 38 37 37 38 36	1 1.02 1.02 1.02 1.02	8 15 22 29 37	0.12 .12 .12 .13	34 35 36 37 38	37 36 35 34 33	I.02 I.02 I.02 I.02 I.02	10	44 51 59 7 15	0.12 .13 .13 .13	34 35 36 37 38	34 33 32 31 30	1.02 1.02 1.02 1.02 1.03		20 28 36 44 53	0.13 .13 .13 .15	55 54 53 52 51	84.4 84.2 84.0 83.8 83.5
40 41 42 43 44	39 35 40 35 41 34 42 33 43 32	I I.02 I.02 I.02 I.02	45 54 10 3 12 22	0.15 .15 .15 .17	39 40 41 42 43	32 31 30 29 28	I.02 I.02 I.02 I.02 I.02	11	24 33 43 53 3	0.15 .17 .17 .17	39 40 41 42 43	28 27 26 25 24	1.02 1.02 1.02 1.02 1.03	11	2 12 22 33 44	0.17 .17 .18 .18	50 49 48 47 46	83.3 83.1 82.9 82.6 82.3
45	44 31		33		44	27			14		44	22			56		45	82.1
	а	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	a	ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	C	ı	$\frac{60'}{\Delta}$	1	,	$\frac{\Delta}{60'}$		a
t			° 30′				d = 8	3° 0)′				d=8	° 30) [']			

\ b			a = 7	° 3()′				a = 8	3° 0	,				a = 8	° 30)′		\ c	\ a
B	h	d	<u>6ο′</u> Δ	Z	1	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	Z	t	<u>Δ</u> 6ο'	h	d	$\frac{60'}{\Delta}$	Z	*	<u>Δ</u> 6ο'	$c \setminus$	β
9 45 46 47 48 49	0 44 45 46 47 48	31 30 29 28 26	I.02 I.02 I.02 I.03 I.02	10	33 44 56 8 21	0.18 .20 .20 .22 .23	0 44 45 46 47 48	27 26 24 23 22	1.02 1.03 1.02 1.02 1.03	12	14 26 39 52 6	0.20 .22 .22 .23 .23	0 44 45 46 47 48	22 21 20 18 17	I.02 I.02 I.03 I.02 I.03	1 I 1 2	56 9 22 36 50	0.22 .22 .23 .23 .25	° 45 44 43 42 41	82.1 81.8 81.5 81.2 80.9
50 51 52 53 54	49 50 51 52 53	25 24 23 21 20	1.02 1.02 1.03 1.02 1.03	12	35 49 4 20 37	0.23 .25 .27 .28	49 50 51 52 53	20 19 18 16 14	1.02 1.02 1.03 1.03 1.02	13	20 35 52 9 27	0.25 .28 .28 .30 .32	49 50 51 52 53	15 14 12 10 9	1.02 1.03 1.03 1.02 1.03	13	5 22 39 57 16	0.28 .28 .30 .32 .33	40 39 38 37 36	80.6 80.2 79.9 79.5 79.2
55 56 57 58 59	54 55 56 57 58	18 17 15 13	1.02 1.03 1.03 1.02 1.03	13	56 15 35 57 20	0.32 •33 •37 •38 •42	54 55 56 57 58	13 11 9 7 5	1.03 1.03 1.03 1.03 1.03	14	46 6 28 51 16	0.33 .37 .38 .42 .43	54 55 56 57	7 5 3 0 58	1.03 1.03 1.05 1.03	15	36 58 21 45	0.37 .38 .40 .43 .47	35 34 33 32 31	78.8 78.3 77.9 77.4 77.0
60 61 62 63 64	59 60 61 62 63	10 8 5 3	1.03 1.05 1.03 1.03 1.05	15	45 12 40 10 43	0.45 .47 .50 .55 .58	59 60 61 62	3 58 56 53	1.03 1.05 1.03 1.05 1.05	16	42 10 40 12 47	0.47 .50 .53 .58 .62	58 59 60 61 62	56 53 50 47 44	1.05 1.05 1.05 1.05	17	39 8 39 13 50	0.48 •52 •57 •62 •65	30 29 28 27 26	76.4 75.9 75.3 74.7 74.1
65 66 67 68 69	64 65 66 67	58 55 52 49 46	1.05 1.05 1.05 1.05 1.07	17 18 19 20	18 56 37 22 10	0.63 .68 .75 .80	63 64 65 66 67	50 47 43 39 35	1.05 1.07 1.07 1.07 1.07	18 19 20 21	24 4 47 34 25	0.67 •72 •78 •85 •92	63 64 65 66 67	41 37 33 29 25	1.07 1.07 1.07 1.07 1.09	19 20 21 22	29 11 56 45 38	0.70 .75 .82 .88 .97	25 24 23 22 21	73.4 72.6 71.8 71.0 70.1
70 71 72 73 74	68 69 70 71 72	42 38 33 28 22	1.07 1.09 1.09 1.11	21 22 23 24 25	3 1 5 15 32	0.97 1.07 1.17 1.28 1.43	68 69 70 71 72	31 26 21 16	1.09 1.09 1.09 1.11 1.13	22 23 24 25 27	20 21 27 40 1	1.02 1.10 1.22 1.35 1.48	68 69 70 71	20 15 9 3 56	1.09 1.11 1.11 1.13 1.15	23 24 25 27 28	36 39 48 4 28	1.05 1.15 1.27 1.40 1.53	20 19 18 17 16	69.1 68.0 66.8 65.5 64.1
75 76 77 78 79	73 74 75 76	16 9 1 53 43	1.13 1.15 1.15 1.20 1.25	26 28 30 32 34	58 33 20 20 36	1.58 1.78 2.00 2.27 2.57	73 74 75 76	3 55 46 37 26	1.15 1.18 1.18 1.22 1.28	28 30 32 34 36	30 9 0 4 23	1.65 1.85 2.07 2.32 2.60	72 73 74 75 76	48 40 30 20 8	1.15 1.20 1.20 1.25 1.30	30 31 33 35 38	0 42 36 43 4	1.70 1.90 2.12 2.35 2.65	15 14 13 12	62.6 60.8 58.9 56.8 54.4
80 81 82 83 84	77 78 79 80	31 18 3 45 24	1.28 1.33 1.43 1.54 1.67	37 40 43 47 51	10 5 25 13 33	2.92 3·33	77 78 79 80	13 59 42 23 1	1.30 1.40 1.46 1.58 1.76	38. 41 45 49 53	59 56 17 4 22	2.95 3·35	77 78 79	54 39 21 0 37	1.33 1.43 1.54 1.62 1.88	40 43 47 50 55	43 41 2 48 2	2.97 3.35 3.77	10 9 8 7 6	51.7 48.7 45.3 41.4 37.1
85 86 87 88 89	81 82	0 30 56 14 26	2.00 2.31 3.33 5.00 15.0	56 62 68 75 82	30 5 19 9 27		81	35 4 28 45 56	2.07 2.50 3.53 5.45 15.0	58 63 69 76 82	12 36 35 3 55		80 81	9 37 59 16 27	2.14 2.73 3.53 5.45 20.0		45 59 42 51 20		5 4 3 2 1	32.2 26.7 20.6 14.1 7.1
90		30	6-1	90	0		82	0		90	0			30		90	0		0	0.0
$ _t$	0		<u>δο'</u> Δ		b	$\frac{\Delta}{60'}$	0	ι	<u>6ο′</u> Δ		b	$\frac{\Delta}{60'}$	(a	$\frac{60'}{\Delta}$		<i>b</i>	$\frac{\Delta}{60'}$		a
			d = 7	° 30)′				d = 3	8° 0	'	1			d = 8	° 30	0′			

65

E

8			a = 9	9° 0	,				a = 9	° 30)′				a = 1	0° 0	r		c	a
$B \setminus$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	\overline{z}	t	$\frac{\Delta}{60'}$	h	d	6ο' Δ	Z	t	$\frac{\Delta}{60'}$	c	β
0 I 2 3 4	0 0 1 2 3	59 59 58 57	I.02 I I.02 I.02 I.02	9	0 0 0 I I	0.00 .00 .02 .00	0 0 1 2 3	59 58 57 57	I.02 I.02 I.02 I	°9	30 30 30 31 31	0.00 .00 .02 .00	0 I 2 3	59 58 57 56	I.02 I.02 I.02 I.02 I.02	10	0 0 0 1 1	.00	90 89 88 87 86	90.0 89.8 89.7 89.5 89.3
5 6 78 9	4 5 6 7 8	56 56 55 54 53	I I.02 I.02 I.02	5 1	2 3 4 5 7	.02	4 5 6 7 8	56 55 54 53 53	I.02 I.02 I.02 I		32 33 34 35 37	.02 .02 .02 .03	4 5 6 7 8	55 54 53 52	I I.02 I.02 I.02 I.02		2 3 4 6 7	.02 .03 .02 .03	85 84 83 82 81	89.2 89.0 88.8 88.7 88.5
10 11 12 13 14	9 10 11 12 13	53 52 51 50 49	1.02 1.02 1.02 1.02		8 10 12 14 16	0.03 .03 .03 .03	9 10 11 12 13	52 51 50 49 48	I.02 I.02 I.02 I.02 I.02		39 41 43 45 47	0.03 .03 .03 .03	9 10 11 12 13	51 50 49 48 47	I.02 I.02 I.02 I.02 I.02		9 11 13 15	0.03 .03 .03 .05	80 79 78 77 76	88.3 88.1 88.0 87.8 87.6
15 16 17 18 19	14 15 16 17 18	49 48 47 46 45	I.02 I.02 I.02 I.02		19 21 24 27 30	0.03 .05 .05 .05	14 15 16 17 18	47 46 46 45 44	I.02 I I.02 I.02 I.02	10	50 53 56 59 2	0.05 .05 .05 .05	14 15 16 17 18	46 45 44 43 42	1.02 1.02 1.02 1.02 1.02		21 24 27 30 34	0.05 .05 .05 .07	75 74 73 72 71	87.5 87.3 87.1 86.9 86.7
20 21 22 23 24	19 20 21 22 23	45 I 30 0 0 45 I.02 34 0.0 0 44 I.02 38 0 43 I.02 42 0 44 I.02 50 0 41 I.02 55 0.0 30 I.02 IO 0				0.07 .07 .07 .07 .08	19 20 21 22 23	43 42 41 40 39	I.02 I.02 I.02 I.02 I.02		6 10 14 18 23	0.07 .07 .07 .08	19 20 21 22 23	41 40 39 38 37	I.02 I.02 I.02 I.02 I.02		38 42 46 51 56	0.07 .07 .08 .08	70 69 68 67 66	86.6 86.4 86.2 86.0 85.8
25 26 27 28 29	24 25 26 27 28	0 44 1.02 38 1 43 1.02 42 2 42 1.02 46 3 41 1.02 50 5 39 1.02 10 0 7 38 1.02 10 3 37 1.02 10				0.08	24 25 26 27 28	38 37 36 35 34	1.02 1.02 1.02 1.02 1.02		28 33 38 44 50	0.08	24 25 26 27 28	36 35 33 32 31	1.02 1.03 1.02 1.02 1.02	II	1 6 12 18 24	0.08 .10 .10 .10	65 64 63 62 61	85.6 85.4 85.2 85.0 84.8
30 31 32 33 34	29 30 31 32 33	36 35 34 33 32	1.02 1.02 1.02 1.02 1.03		22 28 35 42 49	0.10 .12 .12 .12	29 30 31 32 33	33 32 31 29 28	1.02 1.02 1.03 1.02 1.02	11	56 3 10 17 25	0.12 .12 .12 .13	29 30 31 32 33	30 29 27 26 25	1.02 1.03 1.02 1.02 1.02	12	31 38 45 52 0	0.12 .12 .12 .13	59 58 57 56	84.6 84.3 84.1 83.9 83.6
35 36 37 38 39	34 35 36 37 38	31 34 1.02 35 .1 32 33 1.03 42 .1 33 32 1.03 49 .1 34 30 1.02 57 0.1 35 29 1.02 11 5 .1 36 28 1.02 13 .1					34 35 36 37 38	27 26 25 23 22	1.02 1.02 1.03 1.02 1.02	12	33 41 50 59	0.13 .15 .15 .17	34 35 36 37 38	24 22 21 19 18	1.03 1.02 1.03 1.02 1.03		9 18 27 37 47	0.15 .15 .17 .17	55 54 53 52 51	83.4 83.2 82.9 82.7 82.4
40 41 42 43 44		25 23 22 21 19		12	0.17 .18 .18 .20	39 40 41 42 43	21 19 18 16	1.03 1.02 1.03 1.02 1.03	13	19 30 41 53	0.18 .18 .20 .22	42		1.02 1.03 1.02 1.03 1.03	13	58 9 21 33 46	0.18 .20 .20 .22 .23	50 49 48 47 46	82.1 81.8 81.5 81.3 80.9	
45	44	18	i		38		44	13			19		44	8		14	0		45	80.6
t		a	6 <u>ο'</u> Δ		b	$\frac{\Delta}{60'}$		a	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
			d =	9° C)′				d = 9)° 3	0′				d = 3	10°	0′			

6		a =	9° 0′	:			a = 9	° 3()′				a=1	0° (0′		c	a
B	h	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	h	d	60' ▲	Z	t	$\frac{\Delta}{60'}$	h	$\frac{d}{}$	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	C	β
45 46 47 48 49	0 44 18 45 16 46 15 47 13 48 12		12 38 51 13 5 19 34	0.22 .23 .23 .25 .28	44 45 46 47 48	13 12 10 8 6	I.02 I.03 I.03 I.03 I.03	13	19 33 47 2 18	0.23 .23 .25 .27 .28	44 45 46 47 48	8 6 4 2 0	I.03 I.03 I.03 I.03 I.03	14	0 15 30 46 3	0.25 .25 .27 .28	° 45 44 43 42 41	80.6 80.3 80.0 79.6 79.3
50 51 52 53 54	49 10 50 8 51 6 52 4 53 2	1.03	51 14 8 26 45 15 5	0.28 .30 .32 .33 .35	49 50 51 52	4 0 58 56	1.03 1.03 1.03 1.03	15	35 53 12 32 53	•.30 •32 •33 •35 •38	49 50 51 52	58 56 54 52 49	1.03 1.03 1.03 1.05 1.03	16	20 39 59 20 42	·32 ·33 ·35 ·37 ·38	40 39 38 37 36	78.9 78.5 78.1 77.6 77.2
55 56 57 58 59	54 0 58 55 56 56 53 57 51	1.03 1.03 1.05 1.03 1.05	26 49 16 13 39 17 6	0.38 .40 .43 .45 .48	53 54 55 56 57	54 51 49 46 43	1.05 1.03 1.05 1.05	16 17 18	16 40 5 32 0	•42 •45 •47 •50	53 54 55 56 57	47 44 41 38 35	1.05 1.05 1.05 1.05	17	5 30 56 24 54	0.42 •43 •47 •50 •53	35 34 33 32 31	76.7 76.2 75.7 75.2 74.6
60 61 62 63 64	58 48 59 45 60 42 61 39 62 36	1.05 1.05 1.05 1.05 1.07	18 6 39 19 14 52	• 55 • 58 • 63 • 68	58 59 60 61 62	40 37 33 30 26	1.05 1.07 1.05 1.07	19	30 37 14 54	0.55 •57 •62 •67 •70	58 59 60 61 62	32 28 24 20 16	1.07 1.07 1.07 1.07	19 20 21	26 59 35 14 55	0.55 .60 .65 .68	30 29 28 27 26	74.0 73.4 72.8 72.1 71.3
65 66 67 68 69	63 32 64 28 65 24 66 19 67 14	1.07 1.07 1.09 1.09	20 33 21 17 22 4 55 23 51	0.73 .78 .85 .93	63 64 6 5 66 67	22 18 13 8 2	1.07 1.09 1.09 1.11	21 22 23 24 25	36 22 11 4 2	0.77 .82 .88 .97 I.03	63 64 65 66	7 2 56 50	1.09 1.09 1.11 1.11	22 23 24 25 26	39 26 17 12	0.78 .85 .92 1.00	25 24 23 22 21	70.5 69.8 68.8 67.8 66.7
70 71 72 73 74	68 9 69 3 57 70 50 71 42		24 51 25 56 27 8 28 27 29 53	1.08 1.20 1.32 1.43 1.58	68 69 70 71	56 50 43 36 27	1.11 1.13 1.13 1.18 1.18	26 27 28 29 31	4 12 26 47 16	1.13 1.23 1.35 1.48 1.62	67 68 69 70 71	44 37 29 21 12	I.13 I.15 I.15 I.18 I.20	27 28 29 31 32	16 26 43 6 36	1.17 1.28 1.38 1.50 1.67	20 19 18 17 16	65.6 64.4 63.1 61.6 60.1
75 76 77 78 79	72 34 73 24 74 14 75 2 49	1.20 1.25 1.28	31 28 33 13 35 9 37 18 39 42	1.75 1.93 2.15 2.40 2.67	72 73 74 75	18 8 57 44 30	1.20 1.22 1.28 1.30 1.36	32 34 36 38 41	53 40 39 50 15	1.78 1.98 2.18 2.42 2.68	72 73 74 75	2 51 39 26 11	1.22 1.25 1.28 1.33 1.40	34 36 38 40 42	16 5 5 18 44	1.82 2.00 2.22 2.43 2.70	15 14 13 12 11	58.4 56.5 54.4 52.2 49.7
80 81 82 83 84	76 35 77 18 59 78 37 79 12	1.58	42 22 45 21 48 42 52 25 56 35	2.98 3.35 3.72	76 77 78	14 57 36 13 47	1.40 1.54 1.62 1.76 2.00	43 46 50 53 58	56 56 15 56	3.00 3.32 3.68 4.08	76 77 78	54 35 13 49 21	1.46 1.58 1.67 1.88 2.07	45 48 51 55 59	26 25 43 21 20	2.98 3.30 3.63 3.98	10 9 8 7 6	46.9 43.8 40.4 36.6 32.5
85 86 87 88 89	80 9 31 47 57	2.73 3.75 6.00	61 11 66 14 71 43 77 34 83 43		79 80	17 42 3 18 27	2.40 2.86 4.00 6.67 20.0	62 67 72 78 84	29 22 38 13	-	79	50 14 34 48 57	2.50 3.00 4.29 6.67 20.0	63 68 73 78 84	42 25 28 48 21		5 4 3 2 1	27.9 23.0 17.6 11.9 6.0
90	81 0	60'	90 O	Δ	-	30	60'	90		Δ		0	60'	-	, o	Δ	0	0.0
t	a	Δ	9° 0′	60'	-	ı	$\frac{\Delta}{d=9}$		b 	60'	_	<i>1</i>	d=1		b — O'	$\frac{\Delta}{60'}$		a

\ b		a = 1	0° 30	,			a = 1	1° (0′			(a=1	1° 3	0′			\ a
$B \setminus$	h	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	<u>Δ</u> 60'	C	β
0 I 2 3 4	0 0 59 1 58 2 57 3 56	1.02 1.02 1.02 1.02 1.02	10 30 30 30 31 33	0 .00	0 I 2 3	59 58 57 56	I.02 I.02 I.02 I.02 I.03	II	0 0 0 1 2	0.00 .00 .02 .02	0 1 2 3	59 58 56 55	1.02 1.02 1.03 1.02 1.02	II	30 30 30 31 32	0.00 .00 .02 .02	90 89 88 87 86	90.0 89.8 89.6 89.4 89.2
5 6 78 9	4 55 5 54 6 53 7 52 8 51	I.02 I.02 I.02 I.02 I.02	3: 3: 3: 3:	3 .03	4 5 6 7 8	54 53 52 51 50	I.02 I.02 I.02 I.02 I.02		3 4 5 6 8	0.02 .02 .02 .03	4 5 6 7 8	54 53 52 50 49	I.02 I.02 I.03 I.02 I.02		33 34 35 37 38	.02 .03 .02 .03	85 84 83 82 81	89.0 88.9 88.7 88.5 88.3
10 11 12 13 14	9 50 10 49 11 48 12 47 13 46	I,02 I,02 I,02 I,02 I,02	4: 4: 4: 4:	2 .03 1 .03 5 .05	9 10 11 12 13	49 48 47 45 44	I.02 I.02 I.03 I.02 I.02		10 12 14 17 20	0.03 .03 .05 .05	9 10 11 12 13	48 47 45 44 43	1.02 1.03 1.02 1.02 1.02		40 42 45 48 51	0.03 .05 .05 .05	80 79 78 77 76	88.1 87.9 87.7 87.5 87.3
15 16 17 18	14 45 15 44 16 42 17 41 18 40	I.02 I.03 I.02 I.02 I.02		.05	14 15 16 17 18	43 42 41 39 38	I.02 I.02 I.03 I.02 I.02		23 26 29 33 37	0.05 .05 .07 .07	14 15 16 17 18	42 40 39 38 36	1.03 1.02 1.02 1.03 1.02	12	54 57 1 5 9	0.05 .07 .07 .07	75 74 73 72 71	87.1 86.9 86.7 86.5 86.2
20 21 22 23 24	19 39 20 38 21 37 22 36 23 34	I.02 I.02 I.02 I.03 I.02	10 12 13 22 23	.08	19 20 21 22 23	37 36 35 33 32	1.02 1.02 1.03 1.02 1.02	12	41 46 51 56 1	0.08 .08 .08 .08	19 20 21 22 23	35 34 32 31 29	1.02 1.03 1.02 1.03 1.02		13 18 23 28 33	0.08 .08 .08 .08	70 69 68 67 66	86.0 85.8 85.6 85.4 85.1
25 26 27 28 29	24 33 25 32 26 31 27 29 28 28	I.02 I.02 I.03 I.02 I.02	3: 3: 4: 5:	.10	24 25 26 27 28	31 29 28 27 25	1.03 1.02 1.02 1.03 1.02		6 12 18 25 32	0.10 .10 .12 .12	24 25 26 27 28	28 26 25 23 22	1.03 1.02 1.03 1.02 1.03	13	39 45 52 59 6	0.10 .12 .12 .12	65 64 63 62 61	84.9 84.7 84.5 84.2 84.0
30 31 32 33 34	29 27 30 26 31 24 32 23 33 21	I.02 I.03 I.02 I.03 I.02	12 20 21 31	3 .13	29 30 31 32 33	24 22 21 19 18	1.03 1.02 1.03 1.02 1.03	13	39 47 55 3	0.13 .13 .13 .15	29 30 31 32 33	20 19 17 15	1.02 1.03 1.03 1.02 1.03		13 21 29 38 47	0.13 .13 .15 .15	60 59 58 57 56	83.7 83.5 83.2 82.9 82.7
35 36 37 38 39	34 20 35 18 36 17 37 15 38 14	I.03 I.02 I.03 I.02 I.03	13	1 .17 1 .17 1 .18	34 35 36 37 38	16 14 13 11	1.03 1.02 1.03 1.03	14	21 31 41 51	0.17 .17 .17 .18	34 35 36 37 38	12 10 8 6 4	1.03 1.03 1.03 1.03	14	57 7 18 29 40	0.17 .18 .18 .18	55 54 53 52 51	82.4 82.1 81.8 81.5 81.2
40 41 42 43 44	39 12 40 10 41 9 42 7 43 5	1.03 1.02 1.03 1.03	39 14 14 1 2	3 .20	39 40 41 42	7 5 3 1 59	I.03 I.03 I.03 I.03	15	14 27 40 53 7	0.22 .22 .22 .23	39 40 41 42	2 0 58 56 54	1.03 1.03 1.03 1.03	15	52 5 19 33 48	0.22 .23 .23 .25 .25	50 49 48 47 46	80.9 80.6 80.3 79.9 79.6
45	44 3		4	1	43	57			22		43	52		16	3		45	79.2
	а	<u>60'</u> Δ	b	$\frac{\Delta}{60'}$	a	ı	<u>6ο′</u> Δ	1	b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$	b)	$\frac{\Delta}{60'}$		a
t	C		0° 30′				d = 1	1° (0′	1		á	l = 11	l° 3	0′			

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6		a = 2	12° 0′			C	ı = 12	2° 3	0′	,			a = 1	13° C	ľ		\ c	a
$B \setminus$	h d	$\frac{60'}{\Delta}$	Z	<u>Δ</u> 6ο'	h	$\frac{d}{}$	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 6ο'	C	β
0 I 2 3 4	0 0 59 1 57 2 56 3 55	1.02 1.03 1.02 1.02 1.03	0 / 12 0 0 0 1 2	0.00	O I 2 3	59 57 56 54	I.02 I.03 I.02 I.03 I.02	12	30 30 30 31 32	0.00	0 I 2 3		I.03 I.02 I.03 I.02 I.03	13	0 0 0 0 1 2	0.00 .00 .02 .02	90 89 88 87 86	90.0 89.8 89.6 89.4 89.1
5 6 78 9	4 53 5 52 6 51 7 49 8 48	1.02 1.02 1.03 1.02 1.02	3 4 5 7 9	0.02 .02 .03 .03	4 5 6 7 8	53 51 50 49 47	I.03 I.02 I.02 I.03 I.02		33 34 35 37 39	0.02 .02 .03 .03	4 5 6 7 8	52 51 49 48 46	1.02 1.03 1.02 1.03 1.03		3 4 6 8 10	.03 .03 .03 .03	85 84 83 82 81	88.9 88.7 88.5 88.3 88.0
10 11 12 13 14	9 47 10 45 11 44 12 43 13 41	1.03 1.02 1.02 1.03 1.02	11 13 16 19 22	0.03 .05 .05 .05	10	46 44 43 41 40	1.03 1.02 1.03 1.02 1.03		41 43 46 49 52	0.03 .05 .05 .05	9 10 11 12 13	44 43 41 40 38	I.02 I.03 I.02 I.03 I.03		12 14 17 20 23	0.03 .05 .05 .05	80 79 78 77 76	87.8 87.6 87.4 87.1 86.9
15 16 17 18 19	14 40 15 38 16 37 17 36 18 34	1.03 1.02 1.02 1.03 1.02	25 28 32 36 40	•••5 ••7 ••7 ••8	14 15 16 17 18	38 37 35 34 32	1.02 1.03 1.02 1.03 1.03	13	56 59 3 7 12	0.05 .07 .07 .08	14 15 16 17 18	36 35 33 31 30	I.02 I.03 I.03 I.02 I.03		26 30 34 39 43	.07 .08 .08	75 74 73 72 71	86.7 86.4 86.2 86.0 85.7
20 21 22 23 24	19 33 20 31 21 30 22 28 23 27	1.03 1.02 1.03 1.02 1.03	45 50 55 13 0 6	0.08	19 20 21 22 23	30 29 27 25 24	1.02 1.03 1.03 1.02 1.03		17 22 27 33 39	0.08 .08 .10 .10	19 20 21 22 23	28 26 24 23 21	1.03 1.03 1.02 1.03 1.03	14	48 53 59 11	0.08	70 69 68 67 66	85.5 85.3 85.0 84.8 84.5
25 26 27 28 29	24 25 25 23 26 22 27 20 28 18	1.03 1.02 1.03 1.03 1.02	12 18 25 32 40	0.10 .12 .12 .13	24 25 26 27 28	22 20 19 17	1.03 1.02 1.03 1.03	14	45 51 58 6 14	0.10 .12 .13 .13	24 25 26 27 28	19 17 15 13	1.03 1.03 1.03 1.03	-	17 24 31 39 47	0.12 .12 .13 .13	65 64 63 62 61	84.2 84.0 83.7 83.4 83.2
30 31 32 33 34	29 17 30 15 31 13 32 11 33 10	1.03 1.03 1.03 1.02 1.03	48 56 14 4 13 23	0.13 .13 .15 .17	29 30 31 32 33	.13 11 9 7 5	1.03 1.03 1.03 1.03		22 30 39 48 58	0.13 .15 .15 .17	29 30 31 32 33	9 7 5 3 1	1.03 1.03 1.03 1.03	15	56 14 24 34	0.15 .15 .17 .17	60 59 58 57 56	82.9 82.6 82.3 82.0 81.7
35 36 37 38 39	34 8 35 6 36 4 37 2 38 0	1.03 1.03 1.03 1.03 1.05	33 43 54 15 6 18	0.17 .18 .20 .20	34 35 36 37	3 59 57 55	1.03 1.03 1.03 1.03	15	9 20 31 43 55	0.18 .18 .20 .20	34 35 36 37	59 56 54 52 49	1.05 1.03 1.03 1.05	16	44 55 7 20 33	0.18 .20 .22 .22 .22	55° 54 53 52° 51	81.4 81.1 80.7 80.4 80.1
40 41 42 43 44,	57 39 55 40 53 41 51 42 48	1.03 1.03 1.03 1.05 1.05	31 44 58 16 12 28	0.22 .23 .23 .27 .27	4I	52 50 47 45 42	1.03 1.05 1.03 1.05	16	8 22 37 52 8	0.23 .25 .25 .27 .28		47 44 41 39 36	1.05 1.05 1.03 1.05	17	46 0 15 31 48	0.23 .25 .27 .28 .28	50 49 48 47 46	79.7 79.3 79.0 78.6 78.2
45	43046	,	44		43	39			25		43	33		18	5.		45	77.8
$egin{bmatrix} z_{t} \\ t \end{bmatrix}$	a	60' Δ	√ <i>b</i>	<u>Δ</u> 6ο'	а	,	$\frac{60'}{\Delta}$	0.	b	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$	b		<u>Δ</u> 60'	.)	a
		d=1	2° 0′ -	11		O	l = 12	2° 3	0′				d = 1	3° 0	-			

-	_						_						_							ī
b			a = 1	12°	0′			C	a=12	2° 3	0′				a = 1	.3° (0′		$\setminus c$	a
B	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
45 46 47 48 49	43 44 45 46 47	46 43 40 38 35	1.05 1.05 1.03 1.05 1.05	16	44 1 19 37 57	0.28 .30 .30 .33 .35	43 44 45 46 47	39 37 34 31 28	1.03 1.05 1.05 1.05	17	25 42 0 20 40	0.28 .30 .33 .33	43 44 45 46 47	33 30 27 24 20	1.05 1.05 1.05 1.07 1.05	18	5 23 42 2 23	0.30 .32 .33 .35 .37	° 45 44 43 42 41	77.8 77.4 76.9 76.5 76.0
50 51 52 53 54	48 49 50 51 52	22	1.05 1.05 1.07 1.05 1.07	19	18 40 3 27 53	0.37 .38 .40 .43 .45	48 49 50 51 52	24 21 18 14 10	1.05 1.05 1.07 1.07	20	2 24 48 13 40	0.37 ·.40 ·42 ·45 ·47	48 49 50 51 52	17 13 9 5	I.07 I.07 I.07 I.07 I.07	20 21	45 9 33 59 27	•.40 •43 •47 •48	40 39 38 37 36	75.5 75.0 74.5 74.0 73.4
55 56 57 58 59	53 54 55 56	15 11 7 3 59	1.07 1.07 1.07 1.07 1.09	20 21 22	20 49 19 51 26	•.48 •50 •53 •58 •60	53 54 55 56	6 2 58 53 48	1.07 1.07 1.09 1.09	2I 22 23	8 38 9 42 17	•.50 •52 •55 •58 •63	53 54 55 56	57 53 48 43 38	1.07 1.09 1.09 1.09	22 23 24	56 26 58 33 9	•.50 •53 •58 •60 •63	35 34 33 32 31	72.8 72.2 71.6 70.9 70.2
60 61 62 63 64	57 58 59 60 61		1.09	23 24 25	2 41 22 5 52	0.65 .68 .72 .78 .83	57 58 59 60 61	43 38 33 27 21	1.09 1.09 1.11 1.11 1.13	24 25 26	55 35 17 2 50	0.67 •70 •75 •80 •85	57 58 59 60 61	33 27 21 15	I.II I.II I.II I.I3 I.I3	25 26 27	47 28 11 57 46	•.68 • 7 2 •77 .82 .88	30 29 28 27 26	69.5 6 .7 67.9 67.0 66.1
65 66 67 68 69	62 63 64 65	26 20 13 5 57	1.11 1.13 1.15 1.15 1.15	26 27 28 29 30	42 36 33 34 40	0.90 •95 1.02 1.10 1.20	62 63 64 65	14 7 59 51 42	1.13 1.15 1.15 1.18 1.18	27 28 29 30 31	41 36 34 37 45	0.92 .97 I.05 I.13 I.20	62 63 64 65	53 45 37 28	I.15 I.15 I.15 I.18 I.20	28 29 30 31 32	39 35 35 39 47	0.93 1.00 1.07 1.13 1.23	25 24 23 22 21	65.1 64.1 63.0 61.8 60.6
70 71 72 73 74	66 67 68 69 70	39 29 18	1.18 1.20 1.22 1.25 1.28	31 33 34 36 37	52 8 31 1 38	1.27 1.38 1.50 1.62 1.77	66 67 68 69	33 23 12 0 48	1.20 1.22 1.25 1.25 1.30	32 34 35 37 38	57 15 39 10 49	1.30 1.40 1.52 1.65 1.77	66 67 68 69	18 7 55 43 30	I.22 I.25 I.25 I.28 I.33	34 35 36 38 39	1 20 46 18 57	1.32 1.43 1.53 1.65 1.78	20 19 18 17 16	59·3 57·8 56·3 54·7 53·0
75 76 77 78 79	71 72 73		1.33 1.33 1.40 1.46 1.54	39 41 43 45 48	24 18 23 38 5	1.90 2.08 2.25 2.45 2.67	70 71 72 73	34 19 2 44 24	1.33 1.40 1.43 1.50 1.58	40 42 44 46 49	35 30 35 50 17	1.92 2.08 2.25 2.45 2.65	70 71 72 73	15 59 42 23	1.36 1.40 1.46 1.54 1.62	41 43 45 48 50	44 40 45 0 26	1.93 2.08 2.25 2.43 2.62	15 14 13 12 11	51.1 49.0 46.8 44.5 41.9
80 81 82 83 84	74 75 76	2 37	1.67 1.71 1.94 2.14 2.40	50 53 56 60 63	45 39 47 10 49	2.90 3.13 3.38 3.65 3.88	74 75 76	2 38 12 42 9	1.67 1.76 2.00 2.22 2.50	51 54 57 61 64	56 48 53 12 45	2.87 3.08 3.32 3.55 3.78	74 75	39 14 46 16 42	1.71 1.88 2.00 2.31 2.61	53 55 58 62 65	3 53 55 10 38	2.83 3.03 3.25 3.47 3.68	10 9 8 7 6	39.2 36.2 33.0 29.6 25.9
85 86 87 88 89		1 22 38 50 58	2.86 3.75 5.00 7.50 30.0		42 50 10 41 18	4.13 4.33 4.52 4.62	77	33 53 9 21 28	3.00 3.75 5.00 8.57 30.0	68 72 76 81 85	32 32 43 30	4.45	76	5 25 40 51 58	3.00 4.00 5.45 8.57 30.0		19 11 14 24 41	3.87 4.05 4.17 4.28 4.32	5 4 3 2 1	22.0 17.9 13.6 9.2 4.6
90	78	0		90	0			30	1	90	0		77	0		90	0		0	0.0
		$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $				$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	(ı	<u>60'</u> Δ		b	<u>Δ</u> 6ο'		a
t			d = 1	2° ()′	1	_	(d=1	2° 3	30′				d = 1	3° (0′	1		

b		a=1	3° 3 0′			a	= 1	4° (0′			(<i>i</i> = 1	4° 3	30′		\ c	a
B	h	<u>6ο′</u> Δ	Z^{t}	Δ 60'	h	d	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 1 2 3 4	58 1 57 2 55 3 53	1.02	13 30 30 30 31 32	.00	2	58 56 55	1.03 1.03 1.02 1.03	14		0.00 .00 .02 .02	0 0 1 2 3	58 56 54 52	1.03 1.03 1.03 1.03	14		0.00 .02 .00 .02	90 89 88 87 86	90.0 89.8 89.5 89.3 89.0
5 6 7 8 9	4 52 5 50 6 48 7 47 8 45		33 34 36 38 40	0.02 .03 .03 .03	5 4 6 4 7 4	49 1 47 1 46 1	1.03 1.03 1.02 1.03		3 4 6 8 10	0.02 .03 .03 .03	4 5 6 7 8	50 48 47 45 43	I.03 I.02 I.03 I.03 I.03		33 35 36 38 40	0.03 .02 .03 .03	85 84 83 82 81	88.8 88.5 88.3 88.1 87.8
10 11 12 13 14	9 43 10 42 11 40 12 38 13 36	I.02 I.03 I.03 I.03 I.02	42 45 48 51 54	•.05 •05 •05 •05	IO 2 II 3 I2	40 1 38 1 36 1	1.03 1.03 1.03 1.02		12 15 18 21 25	0.05 .05 .05 .07	9 10 11 12 13	41 39 37 35 33	1.03 1.03 1.03 1.03 1.03		43 46 49 52 55	•.05 •05 •05 •05	80 79 78 77 76	87.6 87.3 87.1 86.8 86.5
15 16 17 18 19	14 35 15 33 16 31 17 29 18 27	1.03 1.03 1.03 1.03 1.03	58 14 2 6 10	•.07 •07 •07 •08 •08	15 3 16 2	31 1 29 1 27 1	1.03 1.03 1.03 1.03		28 32 37 41 46	0.07 .08 .07 .08	14 15 16 17 18	31 29 27 24 22	I.03 I.03 I.05 I.03 I.03	15	59 3 8 13 18	.08 .08 .08	75 74 73 72 71	86.3 86.0 85.8 85.5 85.2
20 21 22 23 24	19 25 20 24 21 22 22 20 23 18	I.02 I.03 I.03 I.03 I.03	20 25 31 37 43	0.08 .10 .10 .10	20 2 21 1 22 1	21 I 19 I 17 I	1.03 1.03 1.03 1.03	15	52 57 3 9 16	0.08 .10 .10 .12	19 20 21 22 23	20 18 16 14	I.03 I.03 I.03 I.05 I.05		23 29 35 42 48	0.10 .10 .12 .10	70 69 68 67 66	85.0 84.7 84.4 84.1 83.9
25 26 27 28 29	24 16 25 14 26 12 27 10 28 8	1.03 1.03 1.03 1.03 1.05	50 57 15 5 13 21	0.12 .13 .13 .13		8 1	1.05 1.03 1.03 1.03		23 30 38 46 55	0.12 .13 .13 .15	24 25 26 27 28	9 7 4 2 0	1.03 1.05 1.03 1.03	16	55 3 11 19 28	0.13 .13 .13 .15	65 64 63 62 61	83.6 83.3 83.0 82.7 82.4
30 31 32 33 34	29 5 30 3 31 1 59 32 56	1.03 1.03 1.03 1.05 1.03	30 39 48 58 16 9	0.15 .15 .17 .18	30 5 31 5	59 I 57 I 54 I	1.03	16	4 13 23 33 44	0.15 .17 .17 .18	29 30 31 32	57 55 52 49 47	1.03 1.05 1.05 1.03 1.05	17	37 47 57 8	0.17 .17 .18 .18	59 58 57 56	82.0 81.7 81.4 81.1 80.7
35 36 37 38 39	33 54 34 51 35 49 36 46 37 44	1.05 1.03 1.05 1.03 1.05	20 32 44 57 17 10	0.20 .20 .22 .22	34 4 35 4 36 4	16 I 14 I 11 I	1.05	17	56 8 20 33 47	0.20 .20 .22 .23	33 34 35 36 37	44 41 38 35 32	1.05 1.05 1.05 1.05	18	31 44 57 10 24	0.22 .22 .22 .23 .25	55 54 53 52 51	80.4 80.0 79.7 79.3 78.9
40 41 42 43 44	38 41 39 38 40 35 41 32 42 29		24 39 54 18 10 27		39 3	32 I 29 I 26 I		18	2 17 33 50 7	0.25 .27 .28 .28	38 39 40 41 42	29 26 23 19 16	1.05 1.05 1.07 1.05 1.07	19	39 55 11 28 46	0.27 .27 .28 .30 .32	50 49 48 47 46	78.5 78.1 77.7 77.3 76.9
45	43 26		45		43 I	19			25		43	12	1	20	5		45	76.4
+	а	<u>6ο'</u> Δ	b	<u>Δ</u> 60'	a		δο' Δ	l	5	<u>Δ</u> 60'	a.		<u>6ο′</u> Δ	l	6	$\frac{\Delta}{60'}$		a
t		d = 13	3° 30′			d	= 14	۱° C)′			0	l=1	4° 3	30′			

4.011

8		a=13	3° 3	0′				a = 1	4° (0′			C	ı = 14	4° 3	0′		\ c	a
B	h d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	60' Δ	Z	*	Δ 60'	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	43 26 44 23 45 20 46 16 47 13	1.05 1.05 1.07 1.05 1.07	18 19 20	45 4 24 44 6	0.32 •33 •33 •37 •38	43 44 45 46 47	19 16 12 8 4	1.05 1.07 1.07 1.07	19	25 45 5 26 48	0.33 .33 .35 .37	43 44 45 46	8 4 0 56	1.07 1.07 1.07 1.07	20	5 25 46 8 31	0.33 .35 .37 .38	° 45 44 43 42 41	76.4 75.9 75.5 75.0 74.4
50 51 52 53 54	48 9 49 5 50 1 57 51 53	1.07 1.07 1.07 1.07 1.09	2I 22	29 53 18 45 13	•42 •45 •47 •50	48 49 50 51	56 52 48 43	1.07 1.07 1.07 1.09 1.09	2I 22	37 30 59	•43 •45 •48 •52	47 48 49 50 51	52 48 43 38 33	1.07 1.09 1.09 1.09 1.09	22	55 20 47 15 45	•45 •47 •50 •52	40 39 38 37 36	73.9 73.4 72.8 72.2 71.6
55 56 57 58 59	52 48 53 43 54 38 55 33 56 28	1.09 1.09 1.09 1.11	23 24 25	43 14 47 22 0	•55 •58 •63	52 53 54 55 56	38 33 28 22 16	1.09 1.11 1.11 1.11	23 24 25	30 2 36 12 50	•.53 •57 •60 •63 •67	52 53 54 55 56	28 23 17 11 5	1.09	24 25 26	16 49 24 1 40	0.55 .58 .62 .65	35 34 33 32 31	70.9 70.3 69.6 68.8 68.1
60 61 62 63 64	57 22 58 16 59 9 60 2 55	I.II I.I3 I.I3 I.I3 I.I3	26 27 28	39 21 5 52 42	•.7° •73 •78 •83 •9°	57 58 59 60	10 4 57 50 42	1.11 1.13 1.13 1.15 1.15	26 27 28 29	30 13 59 47 38	•.72 •77 .80 .85	57 58 59 60	59 52 45 37 29	1.13 1.13 1.15 1.15	27 28 29 30	21 5 51 40 32	•.73 •77 .82 .87 •93	30 29 28 27 26	67.3 66.4 65.5 64.6 63.6
65 66 67 68 69	61 48 62 40 63 31 64 22 65 12	1.15 1.18 1.18 1.20 1.20	29 30 31 32 33	36 33 34 39 49	0.95 1.02 1.08 1.17 1.25	61 62 63 64	34 25 16 7 56	1.18 1.18 1.18 1.22 1.22	30 31 32 33 34	32 31 33 39 50	0.98 1.03 1.10 1.18 1.25	61 62 63	20 II I 51 40	1.18 1.20 1.20 1.22 1.25	31 32 33 34 35	28 27 30 37 49	0.98 1.05 1.12 1.20 1.28	25 24 23 22 21	62.6 61.5 60.3 59.1 57.8
70 71 72 73 74	66 2 50 67 38 68 25 69 11	1.25 1.25 1.28 1.30 1.36	35 36 37 39 41	4 24 51 24 3	1.33 1.45 1.55 1.65 1.80	65 66 67 68	45 33 20 7 52	1.25 1.28 1.28 1.33 1.36	36 37 38 40 42	5 27 54 27 8	1.37 1.45 1.55 1.68 1.80	65 66 67 68	28 16 2 48 32	1.25 1.30 1.30 1.36 1.40	37 38 39 41 43	6 28 56 30 11	1.37 1.47 1.57 1.68 1.80	20 19 18 17 16	56.4 54.9 53.3 51.6 49.8
75 76 77 78 79	55 70 39 71 21 72 1 39	1.36 1.43 1.50 1.58 1.67	42 44 46 49 51	51 47 52 6 31	1.93 2.08 2.23 2.42 2.60	69 70 71 72	36 18 59 38 16	1.43 1.46 1.54 1.58 1.71	43 45 47 50 52	56 52 57 11 35	1.93 2.08 2.23 2.40 2.57	69 70 71	15 57 37 16 52	1.43 1.50 1.54 1.67 1.71	44 46 48 51 53	59 55 59 12 35	1.93 2.07 2.22 2.38 2.53	15 14 13 12	47.9 45.9 43.7 41.3 38.8
80 81 82 83 84	73 15 49 74 21 49 75 15	1.76 1.88 2.14 2.31 2.73	54 56 59 63 66	7 55 54 5 28	2.80 2.98 3.18 3.38 3.58	73 74	51 24 55 23 48	1.82 1.94 2.14 2.40 2.86	55 57 60 63 67	9 54 50 57 15	2.75 2.93 3.12 3.30 3.48	72 73 74	27 59 29 56 20	1.88 2.00 2.22 2.50 2.86	56 58 61 64 67	7 50 43 46 59	2.72 2.88 3.05 3.22 3.38	10 9 8 7 6	36.1 33.2 30.2 26.9 23.5
85 86 87 88 89	37 56 76 11 21 28				3.75 3.90 4.03 4.12 4.15	75	9 27 41 52 58	3·33 4·29 5·45 10.0 30.0		44 22 9 2 0	3.63 3.78 3.88 3.97 4.00	75	41 58 12 22 28	3.53 4.29 6.00 10.0 30.0		22 54 34 19	3.53 3.67 3.75 3.82 3.87	5 4 3 2 1	19.9 16.1 12.2 8.2 4.1
90	30		90	0		76 —	0		90	0			30		90	0		0	0.0
t	а	60' <u>∆</u>	1	5	$\frac{\Delta}{60'}$	a	ı	<u>60'</u> Δ		ь	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	l	b	$\frac{\Delta}{60'}$		a
	d	l = 13	3° 3	0′				d = 1	4° ()′			d	l = 14	1° 3	0′			

В		a = 1	5° 0′			a=1	5° 3	30′			a = 1	16° 0′		\	\ a
B	h d	<u>6ο′</u> Δ	Z	$\frac{\Delta}{60'}$	h	$\frac{60'}{\Delta}$	Z	*	<u>Δ</u> 60'	A	$\frac{1}{\Delta} \frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	$C\setminus$	β
o o i 2 3 4	0 0 58 1 56 2 54 3 52	1.03 1.03 1.03 1.03	0 / 15 0 0 1 1 2	0.00	58 1 56 2 53 3 51	1.03	15	30 30 31 31 32	0.00	5 I 5 2 5 3 5	5 1.03	16 0 0 1 1 2	0.00	90 89 88 87 86	90.0 89.7 89.5 89.2 88.9
5 6 7 8 9	4 50 5 48 6 46 7 44 8 41	I.03 I.03 I.03 I.05 I.05	3 5 7 9	0.03 .03 .03 .03	4 49 5 47 6 45 7 42 8 40	1.03 1.03 1.05 1.03 1.03		33 35 37 39 41	•••3 ••3 ••3 ••5	4 4 5 4 6 4 7 4 8 3	6 1.03 4 1.05 1 1.03	3 5 7 9	•.03 •03 •03 •03 •05	85 84 83 82 81	88.7 88.4 88.1 87.8 87.6
10 11 12 13 14	9 39 10 37 11 35 12 33 13 31	1.03 1.03 1.03 1.03	13 16 19 22 26	•••5 ••5 ••7	9 38 10 36 11 33 12 31 13 29	I.03 I.05 I.03 I.03		44 47 50 53 57	0.05 .05 .05 .07	9 3 10 3 11 3 12 2 13 2	1.03 2 1.05 9 1.03	14 17 20 24 28	0.05 .05 .07 .07	80 79 78 77 76	87.3 87.0 86.7 86.5 86.2
15 16 17 18 19	14 29 15 26 16 24 17 22 18 20	1.05 1.03 1.03 1.03	30 35 39 44 49	0.08 .07 .08 .08	14 27 15 24 16 22 17 20 18 17	1.05 1.03 1.03 1.05 1.03	16	1 5 10 15 21	0.07 .08 .08 .10	14 2 15 2 16 1 17 1 18 1	2 1.05 9 1.03 7 1.05	32 37 42 47 52	0.08 .08 .08	75 74 73 72 71	85.9 85.6 85.3 85.0 84.7
20 21 22 23 24	19 17 20 15 21 13 22 10 23 8	1.03 1.03 1.05 1.03	16 I 7 14 21	0.10 .10 .12 .12	19 15 20 12 21 10 22 7 23 5	1.05 1.03 1.05 1.03 1.05		27 33 39 46 53	0.10 .10 .12 .12	2I 22	2 1.05 1.05 1.03 1.05 1.05	58 17 4 11 18 26	0.10 .12 .12 .13	70 69 68 67 66	84.4 84.1 83.8 83.5 83.2
25 26 27 28 29	24 6 25 3 26 I 58 27 55	1.05 1.03 1.05 1.05	28 36 44 53 17 2	0.13 .13 .15 .15	24 2 59 25 57 26 54 27 51	1.05 1.03 1.05 1.05	17	9 17 26 35	0.13 .13 .15 .15	24 5 25 5 26 5 27 4	5 1.05 2 1.03 1.05	34 42 50 59 18 9	0.13 .13 .15 .17	65 64 63 62 61	82.9 82.6 82.2 81.9 81.6
30 31 32 33 34	28 53 29 50 30 47 31 44 32 42	1.05 1.05 1.05 1.03 1.05	12 22 32 43 55	0.17 .17 .18 .20	28 48 29 45 30 42 31 39 32 36	1.05 1.05 1.05 1.05	18	45 56 7 18 30	0.18 .18 .18 .20	28 4 29 4 30 3 31 3 32 3	1 1.07 7 1.05 4 1.05	19 30 41 53 19 5	0.18 .18 .20 .20	60 59 58 57 56	81.2 80.9 80.5 80.2 79.8
35 36 37 38 39	33 39 34 36 35 33 36 29 37 26	1.05 1.05 1.07 1.05 1.05	18 7 20 33 47 19 1	0.22 .22 .23 .23	33 33 34 30 35 27 36 23 37 20	1.07	19	42 55 9 23 38	0.22 .23 .23 .25 .27	33 2 34 2 35 2 36 I 37 I	4 1.05 1 1.07 7 1.07	18 31 45 20 0	0.22 .23 .25 .25 .27	55 54 53 52 51	79.4 79.0 78.6 78.2 77.8
40 41 42 43 44	38 23 39 19 40 16 41 12 42 9	1.07 1.05 1.07 1.05 1.07	17 33 50 20 7 26	0.27 .28 .28 .32 .32	38 16 39 13 40 9 41 5 42 1	1.07	20 2I	54 11 28 46 5	0.28 .28 .30 .32 .33	40	6 1.07 2 1.07 8 1.07	31 48 21 6 25 44	0.28 .30 .32 .32 .33	50 49 48 47 46	77·4 76.9 76.5 76.0 75·5
45	43 5		45		57			25		42 4	9	22 4		45	75.0
	a	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	а	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$	а	<u>60'</u> Δ	b	$\frac{\Delta}{60'}$		a
$\parallel t$		d = 1	5° 0′			d = 1	5° 3	30′			d = 1	16° 0′			

\. b	0.1	a = 1	5° 0′	1 5 1		(a=1	5° 3	30%	d,		1	a = 1	6° (0′		c	a
B	h d	$\frac{60'}{\Delta}$	Z	<u>Δ</u> 60'	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{6o'}{\Delta}$	Z	t	<u>Δ</u> 6ο'	C	$\beta \backslash$.
45 46 47 48 49	43 5 44 I 57 45 53 46 48	1.07 1.07 1.07 1.09 1.07	20 45 21 6 27 49 22 13	.35 .38 .40	42 43 44 45 46	57 53 49 44 39	1.07 1.07 1.09 1.09	2I 22	25 46 8 31 55	0.35 .37 .38 .40 .42	42 43 44 45 46	49 45 40 35 30	1.07 1.09 1.09 1.09	22	4 26 48 12 37	0•37 •37 •40 •42 •43	° 45 44 43 42 41	75.0 74.5 74.0 73.5 72.9
50 51 52 53 54	47 44 48 39 49 34 50 29 51 24		38 23 4 31 24 0	.45 .48	47 48 49 50 51	34 29 24 19	1.09 1.09 1.09 1.11	23 24 25	20 47 15 44 15	0.45 .47 .48 .52 .55	47 48 49 50 51	25 20 15 9 3	1.09 1.09 1.11 1.11	24 25 26	30 59 29	0.45 .48 .50 .52 .57	39 38 37 36	72.3 71.7 71.1 70.5 69.8
55 56 57 58 59	52 18 53 12 54 6 55 C	1.11 1.11 1.13 1.13	25 2 36 26 12 49 27 29	62 .67	52 53 54 55	7 55 48 41	I.II I.II I.I3 I.I3 I.I3	26 27 28	48 23 59 37 18	0.58 .60 .63 .68	52 53 54 55	57 50 43 36 29	1.13 1.13 1.13 1.13 1.15	27 28 29	34 9 46 25 6	0.58 .62 .65 .68 .73	35 34 33 32 31	69.1 68.4 67.6 66.8 66.0
60 61 62 63 64	56 46 57 39 58 31 59 23 60 15	I.15 I.15 I.15	28 11 56 29 43 30 33 31 26	.78 .83 .88	56 57 58 59 60	34 26 18 10	1.15 1.15 1.15 1.18 1.20	30 31 32	1 46 34 25 19	0.75 .80 .85 .90	56 57 58 59	21 13 4 55 46	1.15 1.18 1.18 1.18 1.20	30 31 32 33	50 36 25 17	0.77 .82 .87 .90 .97	30 29 28 27 26	65.2 64.3 63.3 62.3 61.3
65 66 67 68 69	61 6 56 62 46 63 35 64 23	I.20 I.20 I.22 I.25 I.25	32 23 33 23 34 27 35 35 36 47	1.07 1.13 1.20	61 62 63 64	51 41 30 19	1.20 1.22 1.22 1.25 1.28	33 34 35 36 37	16 17 22 31 44	1.02 1.08 1.15 1.22 1.30	60 61 62 63	36 25 14 2 49	I.22 I.22 I.25 I.28 I.28	34 35 36 37 38	9 11 17 26 40	1.03 1.10 1.15 1.23 1.30	25 24 23 22 21	60.2 59.0 57.8 56.5 55.2
70 71 72 73 74	65 11 58 66 44 67 29 68 12		38 2 39 27 40 50 42 30 44 11	1.48 1.57 1.68	65 66 67	54 40 25 9 52	1.30 1.33 1.36 1.40 1.43	39 40 41 43 45	2 25 54 29 11	1.38 1.48 1.58 1.70 1.80	64 65 66	36 21 6 49 31	1.33 1.33 1.40 1.43 1.46	39 41 42 44 46	58 22 52 27 8	1.40 1.50 1.58 1.68 1.80	20 19 18 17 16	53·7 52·2 50·6 48·8 47·0
75 76 77 78 79	55 69 36 70 15 53 71 28	1.46 1.54 1.58 1.71 1.76	45 -59 47 5 49 59 52 13 54 3	2.07 2.22 2.35	68 69 70 71	34 14 52 29 4	1.50 1.58 1.62 1.71 1.82	46 48 50 53 55	59 54 57 8 28	1.92 2.05 2.18 2.33 2.48	68 69 70	12 52 30 6 40	1.50 1.58 1.67 1.76 1.88	47 49 51 54 56	56 51 53 3 21	1.92 2.03 2.17 2.30 2.45	15 14 13 12 11	45.1 43.0 40.8 38.5 36.0
80 81 82 83 84	72 2 34 73 3 29 52	2.31	57 59 4 62 3 65 3 68 4	2.83 2.98 2.3.15	72 73	37 8 3 6 2	1.94 2.14 2.31 2.73 3.00	57 60 63 66 69	57 34 21 17 21	2.62 2.78 2.93 3.07 3.20	71 72	12 42 9 34 56	2.00 2.22 2.40 2.73 3.16	58 61 64 66 69	48 23 7 59 59	2.58 2.73 2.87 3.00 3.12	10 9 8 7 6	33·4 30·7 27·7 24·7 21·5
85 86 87 88 89	74 12 29 43 52 58	4.29 6.67	71 59 75 2 78 57 82 3 86 16	3.53 3.63	74	44 0 13 22 28	3.75 4.62 6.67 10.0 30.0			3.33 3.43 3.52 3.57 3.60	73	15 31 44 53 58	3.75 4.62, 6.67 12.0 30.0	73 76 79 83 86	6 20 39 4 31	3.23 3.32 3.42 3.45 3.48	5 4 3 2 1	18.1 14.7 11.1 7.4 3.7
90	75 C		90 0			30		90	0		74 —	0	1	90	0	1	0	0.0
t	a	$\frac{60'}{\Delta}$	√ b .	Δ 60'	3.0	ı	$\frac{60'}{\Delta}$	4.7	<i>b</i>	<u>Δ</u> 60'	0	ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	ξ.	a
		d = 1	15° 0′	٠,		C	l=1	5°.3	0′	- ·		ļ	d = 1	6° (0′	-		

8	a	ı = 16	5° 30′			a=1	7° C)′			a	ı = 17	7° 30)′		c	a
B	$h \stackrel{d}{\downarrow}$	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	h d	<u>6ο'</u> Δ	\overline{z}	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	3
0 0 1 2 3 4	0 0 58 1 55 2 53 3 50	1.03 1.05 1.03 1.05 1.03	16 30 30 31 31 32	0.00	0 0 57 1 55 2 52 3 49	1.05 1.03 1.05 1.05 1.03	17	0 0 1 1 2	0.00 .02 .00 .02	° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	57 54 52 49	1.05 1.05 1.03 1.05	17	30 30 31 31 32	0.00 .02 .00 .02	90 89 88 87 86	90.0 89.7 89.4 89.1 88.8
5 6 78 9	4 48 5 45 6 43 7 40 8 38	1.05 1.03 1.05 1.03 1.05	34 35 37 39 42	0.02 .03 .03 .05	4 47 5 44 6 42 7 39 8 36	1.05 1.03 1.05 1.05 1.03		4 5 7 9	•••• ••• ••• ••• •••	4 5 6 7 8	46 43 40 38 35	1.05 1.05 1.03 1.05 1.05		34 35 37 40 42	0.02 .03 .05 .03	85 84 83 82 81	88.5 88.2 87.9 87.6 87.3
10 11 12 13 14	9 35 10 33 11 30 12 27 13 25	1.03 1.05 1.05 1.03 1.05	45 48 51 55 59	•.05 •05 •07 •07	9 34 10 31 11 28 12 25 13 23	1.05 1.05 1.05 1.03 1.05		15 18 21 25 29	•.05 •07 •07 •08	9 10 11 12 13	32 29 26 23 20	1.05 1.05 1.05 1.05 1.05	18	45 48 52 56 0	0.05 .07 .07 .07	80 79 78 77 76	87.0 86.7 86.4 86.1 85.8
15 16 17 18 19	14 22 15 19 16 17 17 14 18 11	1.05 1.03 1.05 1.05 1.03	17 3 8 13 18	0.08	14 20 15 17 16 14 17 11 18 8	1.05 1.05 1.05 1.05 1.05		34 39 44 49 55	0.08 .08 .08	14 15 16 17 18	17 14 11 8 5	1.05 1.05 1.05 1.05 1.05		5 10 15 21 27	0.08	75 74 73 72 71	85.5 85.2 84.9 84.6 84.3
20 21 22 23 24	19 9 20 6 21 3 22 0 57	1.05 1.05 1.05 1.05	30 36 43 50 58	.I2 .I2	19 5 20 2 59 21 56 22 53	1.05 1.05 1.05 1.05	18	8 15 22 30	0.12 .12 .12 .13	19 20 21 22	2 59 56 53 49	1.05 1.05 1.05 1.07 1.05	19	33 40 47 54 2	0.12 .12 .12 .13	70 69 68 67 66	83.9 83.6 83.3 82.9 82.6
25 26 27 28 29	23 54 24 51 25 48 26 45 27 42	1.05 1.05 1.05 1.05	18 6 14 23 33 43	.15	23 50 24 47 25 44 26 41 27 37	1.05 1.05 1.05 1.07 1.05	19	38 47 56 6	0.15 .15 .17 .17	23 24 25 26 27	46 43 39 36 32	1.05 1.07 1.05 1.07 1.05		11 20 29 39 49	0.15 .15 .17 .17	65 64 63 62 61	82.2 81.9 81.5 81.2 80.8
30 31 32 33 34	28 39 29 36 30 32 31 29 32 25	1.05 1.07 1.05 1.07 1.05	53 19 4 15 27 40	.18	28 34 29 30 30 27 31 23 32 20	1.07 1.05 1.07 1.05 1.07	20	27 38 50 2 15	0.18 .20 .20 .22	28 29 30 31 32	29 25 21 18 14	1.07 1.07 1.05 1.07	20	0 12 24 36 49	0.20 .20 .20 .22 .23	59 58 57 56	80.4 80.0 79.6 79.2 78.8
35 36 37 38 39	33 22 34 18 35 15 36 11 37 7	1.07 1.05 1.07 1.07	53 20 7 21 36 52	.23	33 16 34 12 35 8 36 4 37 0	1.07 1.07 1.07 1.07	21	28 42 57 12 28	0.23 .25 .25 .27 .28	33 34 35 36	10 6 2 58 53	1.07 1.07 1.07 1.09 1.07	2I 22	3 18 33 49 5	0.25 .25 .27 .27	55 54 53 52 51	78.4 78.0 77.6 77.1 76.7
40 41 42 43 44	38 3 59 39 55 40 50 41 46	1.07 1.07 1.09 1.07 1.09	2I 9 26 44 22 3 23	.30	56 38 52 39 47 40 42 41 38	1.09		22 41	0.30 .32 .32 .35	40	49 44 39 34 29	1.09 1.09 1.09 1.09		22 40 59 19 40		49 48 47	76.2 75.7 75.2 74.7 74.2
45	42 41		44	-	42 33			23		42	24		24	2		45	73.7
4	a	6ο' Δ	b	$\frac{\Delta}{60'}$	a	$\frac{6o'}{\Delta}$		b	$\frac{\Delta}{60'}$	(a	6ο' Δ		b	$\frac{\Delta}{60'}$		а
t		d=1	6° 30′	1		d = 1	7° (0′				d = 1	7° 3	80′			

b		C	z = 16	3° 3	0′				a = 1	7° ()′			(<i>i</i> = 17	7° 3	0′		C	a
$B \setminus$	h	d	<u>6ο'</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	*	$\frac{\Delta}{60'}$	$C \setminus$	β
° 45 46 47 48 49	42 43 44 45 46	41 36 31 26 21	1.09 1.09 1.09 1.09	22 23 24	44 6 29 53 18	0.37 .38 .40 .42 .43	42 43 44 45 46	33 28 23 18	1.09 1.09 1.09 1.11	23	23 45 9 33 5 9	0.37 .40 .40 .43 .45	42 43 44 45 46	24 19 14 8 2	1.09 1.09 1.11 1.11	24	2 25 49 14 40	0.38 .40 .42 .43 .47	45 44 43 42 41	73.7 73.2 72.6 72.0 71.4
50 51 52 53 54	47 48 49 50	16 10 4 58 52	1.11	25 26	44 12 42 12 45	•.47 •5° •5° •55 •57	47 48 49 50	6 0 54 48 41	1.11 1.11 1.11 1.13 1.13	25 26 27	26 55 25 56 29	•.48 •5° •52 •55 •58	47 48 49 50	56 50 44 37 30	I.II I.II I.I3 I.I3 I.I3	26 27 28	8 37 7 39 13	•.48 •5° •53 •57 •58	40 39 38 37 36	70.8 70.1 69.5 68.8 68.1
55 56 57 58 59	51 52 53 54 55	46 39 32 24 16	1.13 1.13 1.15 1.15	27 28 29	19 55 32 12 54	0.60 .62 .67 .70 .75	51 52 53 54 55	34 27 20 12 4	1.13 1.13 1.15 1.15 1.18	28 29 30	4 40 18 59 42	0.60 .63 .68 .72 .75	51 52 53 54	23 15 7 59 50	1.15 1.15 1.15 1.18 1.18	29 30 31	48 25 4 45 28	0.62 .65 .68 .72 .77	35 34 33 32 31	67.3 66.6 65.8 64.9 64.1
60 61 62 63 64	56 57 58 59	8 0 51 41 31	1.15 1.18 1.20 1.20 1.22	30 31 32 33 34	39 26 15 7 3	0.78 .82 .87 .93 .98	56 57 58 59	55 46 36 26 16	I.18 I.20 I.20 I.20 I.22	31 32 33 34	27 14 4 57 53	0.78 .83 .88 .93 1.00	55 56 57 58 59	4I 32 22 II O	1.18 1.20 1.22 1.22 1.25	32 33 34 35	14 2 53 47 44	•.80 •.85 •90 •95	30 29 28 27 26	63.1 62.2 61.2 60.2 59.1
65 66 67 68 69	60 61 62 63	20 9 57 45 32	1.22 1.25 1.25 1.28 1.33	35 36 37 38 39	2 4 10 20 35	1.03 1.10 1.17 1.25 1.32	60 61 62 63	5 53 41 28 14	1.25 1.25 1.28 1.30 1.33	35 36 38 39 40	53 56 3 13 28	1.05 1.12 1.17 1.25 1.33	60 61 62	48 36 23 10 55	1.25 1.28 1.28 1.33 1.33	36 37 38 40 41	44 47 54 5 20	1.05 1.12 1.18 1.25 1.33	25 24 23 22 21	57.9 56.7 55.4 54.1 52.7
70 71 72 73 74	64 65 66 67	17 2 46 29 10	1.33 1.36 1.40 1.46 1.50	40 42 43 45 47	54 18 47 22 3	1.40 1.48 1.58 1.68 1.80	64 65 66	59 43 26 8 49	1.36 1.40 1.43 1.46 1.50	41 43 44 46 47	48 12 42 17 58	1.40 1.50 1.58 1.68 1.78	63 64 65 66	40 23 6 47 27	1.40 1.40 1.46 1.50 1.54	42 44 45 47 48	40 5 35 10 50	1.42 1.50 1.58 1.67 1.78	20 19 18 17 16	51.2 49.7 48.0 46.3 44.4
75 76 77 78 79	68 69 70	50 29 6 42 15	1.54 1.62 1.67 1.82 1.88	48 50 52 54 57	51 46 47 56 13	1.92 2.02 2.15 2.28 2.40	67 68 69	29 7 43 18 50	1.58 1.67 1.71 1.88 1.94	49 51 53 55 58	45 39 39 47 2	1.90 2.00 2.13 2.25 2.37	67 68 69	6 43 19 53 25	1.62 1.67 1.76 1.88 2.00	50 52 54 56 58	37 30 30 36 49	1.88 2.00 2.10 2.22 2.35	15 14 13 12	42.5 40.5 38.3 36.0 33.6
80 81 82 83 84	71 72	47 16 43 7 28	2.07 2.22 2.50 2.86 3.16	59 62 64 67 70	37 10 50 38 34	2.55 2.67 2.80 2.93 3.03	70 71 72	21 50 16 39 0	2.07 2.31 2.61 2.86 3.33	60 62 65 68 71	24 54 31 16 7	2.50 2.62 2.75 2.85 2.97	70 71	55 23 49 12 32	2.14 2.31 2.61 3.00 3.53	61 63 66 68 71	10 37 11 52 40	2.45 2.57 2.68 2.80 2.88	9 8 7 6	31.1 28.4 25.7 22.8 19.8
85 86 87 88 89	73	47 2 14 23 28	7 4.00 73 36 3.15 2 5.00 76 45 3.23 4 6.67 79 59 3.30 3 12.0 83 17 3.35 8 30.0 86 38 3.37		3.23 3.30 3.35		18 33 45 53 58	4.00 5.00 7.50 12.0 30.0	74 77 80 83 86	5 9 17 29 44	3.07 3.13 3.20 3.25 3.27	72	49 4 15 23 28	4.00 5.45 7.50 12.0 30.0	74 77 80 83 86	33 32 35 41 50	2.98 3.05 3.10 3.15 3.17	5 4 3 2 1	16.7 13.5 10.2 6.8 3.4	
90		30		90	0		73	0		90	0			30		90	0		0	0.0
,	0	$b \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60'} \right $					0	ı	<u>6ο'</u> Δ	1	b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	i	b	<u>Δ</u> 6ο'		a
t			d=10	6° 3	0′				d = 1	7° ()′			à	l = 17	7° 3	0′			

0	\ b			a = 1	8° (0′		- *	a	ı = 18	3° 3	0′				a=1	9° ()′ ·		\ c	a
	B	h	d	$\frac{60'}{\Delta}$	z	t	<u>Δ</u> 66'	h	d	<u>6ο'</u> Δ	z	*	Δ 60'	h	d	$\frac{60'}{\Delta}$	Z	*	* <u>Δ</u> 6ο'	$C \setminus$	β
	0 1 2 3 4	I 5	7 4 1 8	1.05 1.05 1.05 1.05	.18	0 0 1 1 2	.00	0 I 2 3	57 54 51 48	1.05 1.05 1.05 1.05	18	30 30 31 32 33	0.00 .02 .02 .02	0 I 2 3	57 54 50 47	1.05 1.05 1.07 1.05 1.05	19	0 0 1 2 3	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.7 89.4 89.0 88.7
	5 6 7 8 9	5 4 6 3 7 3	5 2 9 6 3	1.05 1.05 1.05 1.05		4 6 8 10 13	0.03 .03 .03 .05	4 5 6 7 8	45 41 38 35 32	1.07 1.05 1.05 1.05		34 36 38 40 43	0.03 .03 .03 .05	4 5 6 7 8	44 40 37 34 30	1.07 1.05 1.05 1.07		6 8 10 13	0.03 .03 .03 .05	85 84 83 82 81	88.4 88.1 87.8 87.4 87.1
	10 11 12 13 14	IO 2 II 2 I2 2	7 4 1 8	1.05 1.05 1.05 1.05		16 19 23 27 31	0.05 .07 .07 .07	9 10 11 12 13	29 26 22 19 16	1.05 1.07 1.05 1.05 1.07	19	46 49 53 57	0.05 .07 .07 .07	9 10 11 12 13	27 24 20 17 13	1.05 1.07 1.05 1.07 1.05		16 20 24 28 32	0.07 .07 .07 .07	80 79 78 77 76	86.8 86.5 86.1 85.8 85.5
	15 10 17 18 19	15 I 16	5 2 9 6 2	1.05 1.05 1.05 1.07 1.05		36 41 46 52 58	0.08	14 15 16 17	9 6 2 59	1.05 1.05 1.07 1.05 1.05		6 11 17 23 29	0.08 .10 .10 .10	14 15 16	10 6 3 59 56	1.07 1.05 1.07 1.05	20	37 42 48 54 1	0.08 .10 .10 .12	75 74 73 72 71	85.1 84.8 84.5 84.1 83.8
	20 21 22 23 24	19 5 20 5 21 4	96295	1.05 1.07 1.05 1.07 1.05	19	4 11 19 27 35	0.12 .13 .13 .13	18 19 20 21 22	56 52 49 45 41	1.07 1.05 1.07 1.07 1.05	20	36 43 51 59 7	0.12 .13 .13 .13	18 19 20 21 22	52 48 45 41 37	1.07 1.05 1.07 1.07		8 15 22 30 39	0.12 .12 .13 .15	70 69 68 67 66	83.4 83.1 82.7 82.3 82.0
	25 26 27 28 29	24 3 25 3 26 3	2 8 5 1	1.07 1.05 1.07 1.07 1.05	20	43 52 2 12 23	0.15 .17 .17 .18 .18	23 24 25 26 27	38 34 30 26 22	1.07 1.07 1.07 1.07		16 25 35 45 56	0.15 .17 .17 .18	23 24 25 26 27	33 29 25 21 17	1.07 1.07 1.07 1.07	21	48 58 8 18 29	0.17 .17 .18 .20	65 64 63 62 61	81.6 81.2 80.8 80.4 80.0
	30 31 32 33 34	29 2 30 I	40628	1.07 1.07 1.07 1.07	21	34 46 58 11 24	0.20 .20 .22 .22 .23	28 29 30 31 32	18 14 10 6 2	1.07 1.07 1.07 1.07 1.09	21	7 19 32 45 59	0.20 .22 .22 .23 .23	28 29 30 31	13 9 4 0 55	1.07 1.09 1.07 1.09	22	53 6 19 33	0.20 .22 .22 .23 .25	59 58 57 56	79.6 79.2 78.8 78.4 77.9
	35 36 37 38 39	34 5 35 5	4 9 5 0 6	1.09 1.07 1.09 1.07 1.09	22	38 53 8 24 41	0.25 .25 .27 .28 .30	33 34 35 36	57 53 48 43 38	1.07 1.09 1.09 1.09	23	13 28 44 1 18	0.25 .27 .28 .28	32 33 34 35 36	51 46 41 36 31	1.09 1.09 1.09 1.09	23	48 3 19 36 54	0.25 .27 .28 .30	55 54 53 52 51	77.5 77.0 76.6 76.1 75.6
	40 41 42 43 44	38 3 39 3 40 2	46 1.09 41 .3 41 1.09 59 0.3 36 1.09 23 18 .3 31 1.09 37 .3 26 1.09 57 .3 21 1.09 24 18 .3			0.32 •32 •33 •35 •38		33 28 23 18	1.09 1.09 1.11 1.09	24	36 55 14 35 57	0.32 .32 .35 .37		26 20 15 9 3	1.11 1.09 1.11 1.11	24 25	12 32 52 13 35	0.33 •33 •35 •37 •38	50 49 48 47 46	75.1 74.6 74.1 73.5 73.0	
	45	42 I	6			41		42	7		25	19			57	Í		58		45	72.4
	t	а		$\frac{60'}{\Delta}$		b	<u>Δ</u> 60'	a	ı	<u>6ο'</u> Δ		b.	$\frac{\Delta}{60'}$	0	ı ·	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$		a
100 000			(d = 1	8° ()′			a	l=18	3° 3	0′				d = 1	9° ()′	0		

-	6			a = 1	8° ()′		200	(a = 18	3° 3	0′	11	,		a = 1	9°	0′	-	\ c	a
	$B \setminus$	h	d	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	**	Δ 60'	$C \setminus$	$\beta \setminus$
	45 46 47 48 49	42 43 44 45	16 10 4 58 52	1.11 1.11 1.11 1.11	24 25 26	41 4 28 54 21	0.38 .40 .43 .45 .47	42 43 44 45	7 1 55 49 42	I.II I.II I.II I.I3 I.I3	25 26 27	19 43 8 34 1	0.40 .42 .43 .45	41 42 43 44 45	57 51 45 39 32	1.11 1.11 1.11 1.13 1.13	25 26 27	58 22 47 14 42	0.40 .42 .45 .47	° 45 44 43 42 41	72.4 71.8 71.2 70.6 69.9
	50 51 52 53 54	46 47 48 49 50	46 39 32 25 18	1.13 1.13 1.13 1.13 1.15	27 28	49 18 49 22 56	0.48 •52 •55 •57 •60	46 47 48 49 50	35 28 21 14 6	1.13 1.13 1.13 1.15 1.15	28 29	30 0 31 4 39	•.50 •52 •55 •58 •60	46 47 48 49	25 18 10 2 54	1.13 1.15 1.15 1.15 1.15	28 29 30	11 41 13 47 22	• 53 • 57 • 58 • 62	40 39 38 37 36	69.3 68.6 67.9 67.2 66.4
	55 56 57 58 59	51 52 53 54	10 2 54 46 37	1.15 1.15 1.15 1.18 1.20	29 30 31 32	32 10 49 31 15	0.63 .65 .70 .73 .77	51 52 53 54	58 50 41 32 23	1.15 1.18 1.18 1.18 1.20	30 31 32 33	15 54 34 16	0.65 .67 .70 .75 .77	50 51 52 53 54	46 37 28 18	I.18 I.18 I.20 I.20 I.20	31 32 33	59 37 18 1 46	0.63 .68 .72 .75 .78	35 34 33 32 31	65.6 64.8 64.0 63.1 62.2
	60 61 62 63 64	55 56 57 58	27 17 7 56 44	1.20 1.20 1.22 1.25 1.25	33 34 35 36	50 41 35 33	0.82 .85 .90 .97	55 56 57 58	13 51 40 28	I.22 I.22 I.22 I.25 I.28	34 35 36 37	47 37 29 23 21	0.83 .87 .90 .97 I.02	55 56 57 58	58 47 36 24	1.22 1.22 1.25 1.28 1.28	34 35 36 37 38	33 23 16 11 9	0.83 .88 .92 .97	30 29 28 27 26	61.2 60.2 59.2 58.1 57.0
	65 66 67 68 69	59 60 61 62	32 19 6 52 37	1.28 1.28 1.30 1.33 1.36	37 38 39 40 42	33 37 45 56	I.07 I.13 I.18 I.27 I.33	59 60 61 62	15 2 48 33 18	1.28 1.30 1.33 1.33 1.40	38 39 40 41 43	22 26 34 46 2	1.07 1.13 1.20 1.27 1.33	59 60 61	58 44 30 15 58	1.30 1.30 1.33 1.40 1.40	39 40 41 42 43	10 15 23 35 51	1.08 1.13 1.20 1.27 1.33	25 24 23 22 21	55.8 54.5 53.2 51.9 50.4
	70 71 72 73 74	63 64 65 66	45 45 26 6	1.40 1.46 1.46 1.50 1.58	43 44 46 48 49	32 56 26 1 42	1.40 1.50 1.58 1.68	63 64 65	1 43 25 5 44	1.43 1.43 1.50 1.54 1.62	44 45 47 48 50	22 47 17 51 31	1.42 1.50 1.57 1.67 1.77	62 63 64 65	4I 23 4 43 2I	1.43 1.46 1.54 1.58 1.62	45 46 48 49 51	36 6 40 19	1.42 1.50 1.57 1.65	20 19 18 17 16	48.9 47.3 45.7 43.9 42.1
	75 76 77 78 79	67 68 69	44 20 55 29 0	1.67 1.71 1.76 1.94 2.07	51 53 55 57 59	28 20 18 23 35	i.87 i.97 2.08 2.20 2.30	66 67 68	21 57 31 4 35	1.67 1.76 1.82 1.94 2.14	52 54 56 58 60	17 8 5 8 18	1.85 1.95 2.05 2.17 2.27	66 67 68	58 33 7 39 9	1.71 1.76 1.88 2.00 2.14	53 54 56 58 61	4 55 51 53 0	1.85 1.93 2.03 2.12 2.23	15 14 13 12	40.2 38.2 36.0 33.8 31.5
	80 81 82 83 84	70 71	29 56 21 44 3	2.22 2.40 2.61 3.16 3.53	61 64 66 69 72	53 18 49 26 10	2.42 2.52 2.62 2.73 2.82	69 70	30 54 16 35	2.22 2.50 2.73 3.16 3.53	62 64 67 69 72	34 57 25 59 39	2.38 2.47 2.57 2.67 2.75	69 70	37 3 27 48 7	2.31 2.50 2.86 3.16 3.75	63 65 68 70 73	14 34 0 31 7	2.33 2.43 2.52 2.60 2.68	9 8 7 6	29.1 26.5 23.9 21.2 18.3
	85 86 87 88 89		20 35 46 54 58	4.00 5.45 7.50 15.0 30.0	74 77 80 83 86	59 53 51 52 55	2.90 2.97 3.02 3.05 3.08	71	52 5 16 24 28	4.62 5.45 7.50 15.0 30.0	75 78 81 84 87	24 13 7 3 1	2.82 2.90 2.93 2.97 2.98		23 36 46 54 58	4.62 6.00 7.50 15.0 30.0	75 78 81 84 87	48 33 22 13 6	2.75 2.82 2.85 2.88 2.90	5 4 3 2 1	15.4 12.4 9.4 6.3 3.1
	90	72	0		90	0			30		90	0		71	0		90	0		0	0.0
	t	_	a	60' Δ		ь	$\frac{\Delta}{60'}$	(a	$\frac{60'}{\Delta}$	1	6	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	1	Ь	$\frac{\Delta}{60'}$		a
				d = 1	8° ()′				d = 18	3° 3	0′				d=1	9°′	0′			

					/						2.0/5							,	
$\setminus b$	a = 19° 30′						a = 20° 0′						a = 20° 30′						a
$B \setminus$	h	$\frac{\epsilon o'}{\Delta}$	Z	t	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	z	*	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 6ο'	$C \setminus$	B
0 I 2 3 4	0 0 57 1 53 2 50 3 46	1.05 1.07 1.05 1.07 1.05	19	30 30 31 32 33	0.00 .02 .02 .02	° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	56 53 49 46	1.07 1.05 1.07 1.05 1.07	20	0 0 1 2 3	0.00 .02 .02 .02	0 I 2 3	6 56 52 49 45	1.07 1.07 1.05 1.07	20	30 30 31 32 33	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.7 89.3 89.0 88.6
5 6789	4 43 5 39 6 36 7 32 8 29	1.07 1.05 1.07 1.05 1.07		34 36 38 41 44	•••3 ••5 ••5 ••5	4 5 6 7 8	42 38 35 31 27	1.07 1.05 1.07 1.07		4 6 8 11 14	.03 .03 .05 .05	4 5 6 7 8	41 37 33 29 26	1.07 1.07 1.07 1.05 1.07		34 36 38 41 44	0.03 .03 .05 .05	85 84 83 82 81	88.3 87.9 87.6 87.2 86.9
10 11 12 13 14	9 25 10 22 11 18 12 15 13 11	1.05 1.07 1.05 1.07 1.07	20	47 50 54 58 3	.05 .07 .08 .08	9 10 11 12 13	23 20 16 12 8	1.05 1.07 1.07 1.07 1.05		17 21 25 29 34	0.07 .07 .08 .08	9 10 11 12 13	22 18 14 10 6	1.07 1.07 1.07 1.07	21	47 51 55 0 5	.07 .08 .08 .08	80 79 78 77 76	86.5 86.2 85.8 85.5 85.1
15 16 17 18 19	14 7 15 4 16 0 56 17 52	1.05 1.07 1.07 1.07		8 13 19 25 32	0.08 .10 .10 .12	14 15 16 17	5 57 53 49	1.07 1.07 1.07 1.07 1.07	21	39 44 50 56 3	0.08 .10 .10 .12	14 15 16 17	2 58 54 49 45	1.07 1.07 1.09 1.07		10 15 21 28 35	0.08 .10 .12 .12	75 74 73 72 71	84.8 84.4 84.0 83.7 83.3
20 21 22 23 24	18 48 19 45 20 41 21 37 22 33	1.05 1.07 1.07 1.07 1.07	21	39 46 54 2	0.12 .13 .13 .15	18 19 20 21 22	45 41 37 32 28	1.07 1.07 1.09 1.07 1.07		10 18 26 34 43	0.13 .13 .13 .15	18 19 20 21 22	4I 37 32 28 24	1.07 1.09 1.07 1.07 1.09	22	42 50 58 6	0.13 .13 .13 .15	70 69 68 67 66	82.9 82.5 82.1 81.7 81.3
25 26 27 28 29	23 29 24 25 25 20 26 16 27 12	1.07 1.09 1.07 1.07 1.09	22	20 30 40 51 2	0.17 .17 .18 .18	23 24 25 26 27	24 20 15 11 6	1.07 1.09 1.07 1.09 1.07	22	53 3 13 24 36	0.17 .17 .18 .20	23 24 25 26 27	19 15 10 5 0	1.07 1.09 1.09 1.09 1.09	23	25 35 46 57 9	0.17 .18 .18 .20	65 64 63 62 61	80.9 80.5 80.1 79.7 79.3
30 31 32 33 34	28 7 29 3 58 30 54 31 49	1.07 1.09 1.07 1.09 1.09	23	14 27 40 54 8	0.22 .22 .23 .23 .25	28 29 30 31	57 52 47 42	1.09 1.09 1.09 1.09	23	48 I 14 28 42	0.22 .22 .23 .23 .25	28 29 30 31	5.5 50 4.5 40 35	1.09 1.09 1.09 1.09	24	21 34 48 2 17	0,22 .23 .23 .25 .25	60 59 58 57 56	78.8 78.4 77.9 77.5 77.0
35 36 37 38 39	3 ² 44 33 39 34 34 35 29 36 23	1.09 1.09 1.09 1.11 1.09	24	23 39 55 12 30	0.27 .27 .28 .30 .32	32 33 34 35 36	37 32 26 21 15	1.09 1.11 1.09 1.11 1.11	24	57 13 30 48 6	0.27 .28 .30 .30 .32	32 33 34 35 36	30 24 19 13 7	1.11 1.09 1.11 1.11	25	32 48 5 23 42	0.27 .28 .30 .32 .32	55 54 53 52 51	76.5 76.0 75.5 75.0 74.5
40 41 42 43 44	37 18 38 12 39 6 40 0 54	1.11 1.11 1.11 1.11			0.32 •35 •35 •38 •38	40	9 3 57 51 45	1.11 1.11 1.11 1.11	26	25 45 6 27 50	0.33 .35 .35 .38	39	55 49 42 36	1.11 1.11 1.13 1.11 1.13	26	1 21 42 5 28	• 35 • 38 • 38 • 40	50 49 48 47 46	74.0 73.4 72.9 72.3 71.7
45	41 48			36		41	39		27	14		41	29			52		45	71.1
$ _t$	$a \left \frac{60'}{\Delta} \right $		$b \mid \frac{\Delta}{60'}$		$\frac{\Delta}{60'}$	а		$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		а		$b \left \frac{\Delta}{60'} \right $			a	
		d=19° 30′						d = 20° 0′						d = 20° 30′					

Λ -	1				1						1						1\	1.
1	a	a=19	9° 30′				a=2	0°	0′			C	a=20)° 3	0′		\ c	a
B	h	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	d	60' Δ	Z	t	<u>Δ</u> 6ο'	$c \setminus$	$\beta \setminus$
45 46 47 48 49	41 48 42 42 43 35 44 28 45 21	I.II I.I3 I.I3 I.I3 I.I3	26 31 27 28 2	1 .42 5 .45 3 .48	41 42 43 44 45	39 32 25 18	1.13 1.13 1.13 1.15 1.15	27 28 29	14 39 5 33 1	0.42 •43 •47 •47 •50	41 42 43 44	29 22 15 7 59	I.13 I.13 I.15 I.15	27 28 29	52 17 44 12 41	0.42 •45 •47 •48 •50	45 44 43 42 41	71.1 70.5 69.9 69.2 68.5
50 51 52 53 54	46 14 47 6 58 48 50 49 42	1.15 1.15 1.15 1.15 1.18	5 29 2: 30 2: 31	2 .53	46 47 48 49	2 54 46 38 29	1.15 1.15 1.15 1.18 1.18	30 31	31 36 10 46	0.53 •55 •57 •60 •63	45 46 47 48 49	51 43 34 25 16	1.15 1.18 1.18 1.18	30 31 32	11 43 16 51 28	0.53 •55 •58 •62 •63	40 39 38 37 36	67.8 67.1 66.4 65.6 64.8
55 56 57 58 59	50 33 51 24 52 14 53 4 54	1.18 1.20 1.20 1.20 1.20	32 2 33 4 34 3	.68 2 .72 5 .77	50 51 52 53	20 10 0 50 39	I.20 I.20 I.20 I.22 I.22	32 33 34 35	24 3 45 29 15	0.65 .70 .73 .77	50 51 52 53	7 57 46 35 24	I.20 I.22 I.22 I.22 I.22	33 34 35	6 46 28 12 59	•.67 •7° •73 •78 •80	35 34 33 32 31	64.0 63.1 62.2 61.3 60.3
60 61 62 63 64	54 43 55 32 56 20 57 8 55	1.22 1.25 1.25 1.28 1.30		.88 2 .92 7 .98	54 55 56 57	28 16 4 51 38	1.25 1.25 1.28 1.28 1.30	36 37 38 39	3 54 47 43 42	0.85 .88 .93 .98 1.03	54 55 56 57	13 48 34 20	1.25 1.28 1.30 1.30 1.30	36 37 38 39 40	47 38 32 29 28	•.85 •90 •95 •98	30 29 28 27 26	59.3 58.3 57.2 56.1 55.0
65 66 67 68 69	58 41 59 27 60 12 56 61 39	1.30 1.33 1.36 1.40 1.43	39 5 41 42 1 43 2 44 3	3 I.13 I.20 3 I.27	58 59 60 61	24 9 53 36 19	1.33 1.36 1.40 1.40	40 41 42 44 45	44 49 58 11 27	1.08 1.15 1.22 1.27 1.33	58 59 60	6 50 34 17 59	1.36 1.36 1.40 1.43 1.46	41 42 43 44 46	30 35 44 57 13	1.08 1.15 1.22 1.27 1.33	25 24 23 22 21	53.7 52.5 51.1 49.7 48.3
70 71 72 73 74	62 21 63 2 42 64 21 59	1.46 1.50 1.54 1.58 1.67	46 0 47 24 48 5 50 2 52 0	1.48	62 63 64	1 41 21 59 36	1.50 1.50 1.58 1.62 1.71	46 48 49 51 52	47 11 40 14 52	1.40 1.48 1.57 1.63 1.72	61 62 63 64	40 20 59 36 12	1.50 1.54 1.62 1.67 1.71	47 48 50 51 53	33 57 26 59 36	1.40 1.48 1.55 1.62 1.70	20 19 18 17 16	46.8 45.2 43.5 41.8 40.0
75 76 77 78 79	65 35 66 9 42 67 14 43	1.76 1.82 1.88 2.07 2.14	53 50 55 40 57 3 59 3 61 4	1.92 2.00 2.10	65 66 67	11 45 18 48 17	1.76 1.82 2.00 2.07 2.22	54 56 58 60 62	35 23 17 16 20	1.80 1.90 1.98 2.07 2.17	65 66	47 21 53 23 51	1.76 1.88 2.00 2.14 2.31	55 57 58 60 62	18 6 58 55 58	1.80 1.87 1.95 2.05 2.12	15 14 13 12 11	38.1 36.1 34.0 31.9 29.6
80 81 82 83 84	68 11 36 59 69 20 38	2.40 2.61 2.86 3.33 3.75	63 5 66 16 68 3 71 73 3	2.38 3 2.47 2.53	68 69	44 9 31 51 9	2.40 2.73 3.00 3.33 3.75	64 66 69 71 73	30 45 5 29 59	2.25 2.33 2.40 2.50 2.55	67 68	17 41 3 23 41	2.50 2.73 3.00 3.33 4.00	65 67 69 71 74	5 18 35 57 23	2.22 2.28 2.37 2.43 2.50	10 9 8 7 6	27.3 24.8 22.3 19.7 17.1
85 86 87 88 89	70 7 17 24 29	4.62 6.00 8.57 12.0 60.0	76 10 78 5 81 30 84 2: 87 1	2.75 5 2.77 2 2.82		25 37 47 54 59	5.00 6.00 8.57 12.0 60.0		32 9 49 31 15	2.62 2.67 2.70 2.73 2.75	69		5.00 6.67 8.57 12.0 60.0		53 26 2 40 20	2.55 2.60 2.63 2.67 2.67	5 4 3 2	14.3 11.6 8.7 5.8 2.9
90	30		90 (70	0		90	0			30		90	0		0	0.0
	a	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	a		<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	a	ı	<u>6ο'</u> Δ	1	b	$\frac{\Delta}{60'}$		a
t	à	l = 19	° 30′				d = 2	0° ()′			C	l=20)° 3	0′			

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									2.5							/3				
1	1	4	a = 2	1° ()′			a	2 = 2	l° 3	0′	÷-			a = 2	2° (0′		c	a
B	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	h	d	6ο' Δ	Z	*	∆ 60'	h	d	60' Δ	Z	t	<u>Δ</u> 60'	$C \setminus$	$\beta \setminus$
0 0 1 2 3 4	0 I 2 3	56 52 48 44	1.07 1.07 1.07 1.07 1.07	21	0 0 1 2 3	0.00 .02 .02 .02	0 I 2 3	6 56 52 47 43	1.07 1.07 1.09 1.07	21	30 30 31 32 33	0.00 .02 .02 .02	0 I 2 3	56 51 47 42	1.07 1.09 1.07 1.09	22	0 0 1 2 3	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.6 89.3 88.9 88.5
5 6789	4 5 6 7 8	40 36 32 28 24	1.07 1.07 1.07 1.07		4 6 9 11 14	•••3 •••5 •••5 •••7	4 5 6 7 8	39 35 31 26 22	1.07 1.07 1.09 1.07		34 36 39 42 45	0.03 .05 .05 .05	4 5 6 7 8	38 34 29 25 20	1.07 1.09 1.07 1.09 1.07		5 7 9 12 15	0.03 .03 .05 .05	85 84 83 82 81	88.2 87.8 87.4 87.1 86.7
10 11 12 13 14	9 10 11 12 13	20 16 12 7 3	1.07 1.07 1.09 1.07		18 22 26 30 35	.07 .07 .08 .08	9 10 11 12 13	18 14 9 5 0	1.07 1.09 1.07 1.09	22	48 52 56 1	.07 .08 .08 .08	9 10 11 12	16 11 7 2 58	1.09 1.07 1.09 1.07 1.09		18 22 26 31 36	.07 .08 .08	80 79 78 77 76	86.3 85.9 85.5 85.2 84.8
15 16 17 18 19	14 15 16 17	59 55 50 46 42	1.07 1.09 1.07 1.07 1.09	22	40 46 52 59 6	0, IO .IO .I2 .I2	14 15 16 17	56 52 47 43 38	1.07 1.09 1.07 1.09 1.09	-	11 17 23 30 37	0.10 .10 .12 .12	13 14 15 16	53 48 44 39 34	1.09 1.09 1.09 1.09	23	42 48 54 1 8	0.10 .10 .12 .12	75 74 73 72 71	84.4 84.0 83.6 83.2 82.8
20 21 22 23 24	18 19 20 21 22	37 33 28 24 19	1.07 1.09 1.07 1.09		13 21 29 38 47	0.13 .13 .15 .15	18 19 20 21 22	33 29 24 19 14	1.07 1.09 1.09 1.09	23	45 53 1 10 20	0.13 .13 .15 .17	18 19 20 21 22	29 24 19 14 9	1.09 1.09 1.09 1.09		16 24 33 42 52	0.13 .15 .15 .17	70 69 68 67 66	82.4 82.0 81.6 81.2 80.7
25 26 27 28 29	23 24 25 26	9 4 59 54	1.09 1.09 1.09 1.09	23	57 8 19 30 42	0.18 .18 .18 .20	23 24 25 26	9 4 59 54 49	1.09 1.09 1.09 1.09	24	30 40 51 3 15	0.17 .18 .20 .20	23 24 25 26	59 54 48 43	1.09 1.11 1.09 1.11	24	2 12 23 35 48	0.17 .18 .20 .22	65 64 63 62 61	80.3 79.9 79.4 79.0 78.5
30 31 32 33 34	27 28 29 30 31	49 44 39 34 2 8	1.09 1.09 1.09 1.11	24	54 7 21 36 51	0.22 .23 .25 .25 .27	27 28 29 30 31	43 38 33 27 21	1.09 1.09 1.11 1.11	25	28. 41 55 10 25	0.22 .23 .25 .25 .27	27 28 29 30 31	37 32 26 20 14	1.09 1.11 1.11 1.11	25	1 14 28 43 59	0.22 .23 .25 .27 .27	59 58 57 56	78.1 77.6 77.1 76.6 76.1
35 36 37 38 39	32 33 34 35	23 17 11 5 59	I.II I.II I.II I.II	25 26	7 23 40 58 17	0.27 .28 .30 .32 .33	32 33 34 35	1 5 9 3 57 50	1.11 1.11 1.11 1.13 1.11	26	41 58 15 33 53	0.28 .28 .30 .33	32 33 34 35	8 1 55 48 42	1.13 1.11 1.13 1.11 1.13	26 27	32 50 9 28	0.28 .30 .32 .32 .33	55 54 53 52 51	75.6 75.1 74.6 74.0 73.5
40 41 42 43 44		53 46 40 33 26	1.13 1.11 1.13 1.13 1.13	27 28	4 ² 5	0.35 •35 •38 •38 •42	40	44 37 30 23 16	1.13 1.13 1.13 1.13 1.15	28	13 34 56 18 42	0.35 .37 .37 .40 .42	36 37 38 39 40		1.13 1.13 1.15 1.13 1.15		48 10 32 55 19	0.37 .37 .38 .40 .42	50 49 48 47 46	72.9 72.3 71.7 71.1 70.5
45	41	19			30		41	8		29	7			58			44		45	69.9
4		a	$\frac{60'}{\Delta}$		b	<u>Δ</u> 6ο'	(ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$		a	6ο' Δ	l	b	$\frac{\Delta}{60'}$		a
t			d=2	21°	0′			0	<i>l</i> = 2	1° 8	30′				d = 2	2°	0′			

			_			-		1	-					-				_		1	ī.
1	b	/		a=2	21°	0′				a = 2	1° 3	0′				a=2	22°	0′		$\setminus c$	a
B	/	h	$\frac{d}{}$	60'	Z	t	$\frac{\Delta}{60'}$	h	d	60' A	z	t	$\frac{\Delta}{60'}$	h	$\frac{d}{}$	<u>6ο′</u> Δ	Z	t	$\frac{\Delta}{60'}$	$c \setminus$	β
4 4 4 4	7	42 43	19 11 4 56 48	1.15 1.13 1.15 1.15	28 29 30	30 55 22 50 20	0.42 •45 •47 •50 •52	41 42 43 44	8 1 53 45 36	1.13 1.15 1.15 1.18 1.18	29 30	7 33 1 29 59	0.43 •47 •47 •50 •52	40 41 42 43 44	58 50 42 33 24	1.15 1.15 1.18 1.18 1.18	29 30 31	44 11 39 8 38	0.45 •47 •48 •50 •52	45 44 43 42 41	69.9 69.2 68.5 67.8 67.1
5 5 5 5 5	I 2 3	46 47	40 31 22 13	1.18 1.18 1.18 1.20 1.20	31 32 33	51 23 57 32 9	0.53 ·57 ·58 ·62 ·65	45 46 47 48	27 18 9 0 50	1.18 1.18 1.18 1.20 1.22	31 32 33	30° 37 12 50°	0.55 •57 •58 •63	45 46 47 48	56 46 36	I.18 I.20 I.20 I.20 I.22	32 33 34	9 42 17 53 30	0.55 .58 .60 .62 .67	40 39 38 37 36	66.4 65.6 64.9 64.1 63.2
5. 5. 5. 5. 5.	5 7 8	50 . 51	53 43 32 21	1.20 1.22 1.22 1.25 1.25	34 35 36	48 28 11 55 42	0.67 •72 •73 •78 •82	49 50 51 52	39 28 17 6 54	1.22 1.22 1.22 1.25 1.28	34 35 36 37	29 10 53 38 25	0.68 •72 •75 •78 •82	49 50 51 52	25 14 2 50 38	I.22 I.25 I.25 I.25 I.28	35 36 37 38	10 51 34 19 7	0.68 •72 •75 •80 •82	35 34 33 32 31	62.4 61.5 60.6 59.6 58.6
6: 6: 6: 6:	2	54 · 55 ·	57 44 31 17	1.28 1.28 1.30 1.30 1.33	37 38 39 40 41	31 22 16 13	0.85 .90 .95 1.00	53 54 55 56	41 28 14 0 45	1.28 1.30 1.30 1.33 1.36	38 39 40 41	14 6 0 57 57	0.87 .90 .95 1.00	53 54 55 56	25 11 57 42 27	1.30 1.30 1.33 1.33	39 40 41 42	56 48 43 40 40	0.87 .92 .95 1.00	30 29 28 27 26	57.6 56.5 55.4 54.3 53.1
60 60 60 60	7 8	58	48 32 15 57 39	1.36 1.40 1.43 1.43 1.50	42 43 44 45 46	15 21 30 42 58	1.10 1.15 1.20 1.27 1.33	57 58 59 60	29 12 55 37 18	1.40 1.40 1.43 1.46 1.50	42 44 45 46 47	59 5 14 26 42	1.10 1.15 1.20 1.27 1.33	57 58 59	54 36 17 57	1.40 1.43 1.46 1.50 1.54	43 44 45 47 48	43 49 58 10 26	1.10 1.15 1.20 1.27 1.32	25 24 23 22 21	51.8 50.5 49.2 47.8 46.3
70 71 72 73 74	2	62 63	19 58 36 13	1.54 1.58 1.62 1.67 1.76	48 49 51 52 54	18 42 10 42 19	1.40 1.47 1.53 1.62 1.70	61 62 63	58 37 14 51 26	1.54 1.62 1.62 1.71 1.82	49 50 51 53 55	2 26 53 25 1	1.40 1.45 1.53 1.60 1.68	60 61 62 63	36 14 51 27 2	1.58 1.62 1.67 1.71 1.82	49 51 52 54 55	45 8 35 7 42	1.38 1.45 1.53 1.58 1.65	20 19 18 17 16	44.8 43.2 41.6 39.8 38.0
7: 7: 7: 7: 7: 7: 7:	5 7 8	65	23 56 27 57 25	1.82 1.94 2.00 2.14 2.40	56 57 59 61 63	1 47 38 34 34	1.77 1.85 1.93 2.00 2.10	64 65	59 32 2 31 58	1.82 2.00 2.07 2.22 2.40	56 58 60 62 64	42 27 16 10 9	1.75 1.82 1.90 1.98 2.07	64 65	35 7 37 5 32	1.88 2.00 2.14 2.22 2.50	57 59 60 62 64	5 53 46 43	1.73 1.80 1.88 1.95 2.02	15 14 13 12 11	36.2 34.2 32.2 30.1 27.9
80 81 82 83 84	2	67	50 14 36 55 12	2.50 2.73 3.16 3.53 4.29	65 67 70 72 74	40 50 4 23 46	2.17 2.23 2.32 2.38 2.43	66 67	23 46 8 26 43	2.61 2.73 3.33 3.53 4.29	66 68 70 72 75	13 20 32 48 8	2.12 2.20 2.27 2.33 2.38	66 67	56 19 40 58 14	2.61 2.86 3.33 3.75 4.29	66 68 71 73 75	44 50 0 13 30	2.10 2.17 2.22 2.28 2.33	10 9 8 7 6	25.7 23.4 21.0 18.5 16.0
81 83 83 83	7		26 38 48 55 59	5.00 6.00 8.57 15.0 60.0	84 87		2.50 2.53 2.57 2.60 2.60	68	57 9 18 25 29	5.00 6.67 8.57 15.0 60.0	87	31 57 26 56 28	2.43 2.48 2.50 2.53 2.53		59	5.45 6.67 8.57 15.0 60.0	87	50 12 37 4 32	2.37 2.42 2.45 2.47 2.47	5 4 3 2 1	13.4 10.8 8.1 5.4 2.7
90	0	69	0		90	0			30		90	0		68	0		90	0		0	0.0
$\Big\ _{t}$		a		<u>6ο'</u> Δ	1	5	<u>Δ</u> 60'	0	ı	<u>6ο′</u> Δ	6	b -	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$		b	<u>Δ</u> 60'		a
1			,	d=2	1° ()′			(d = 2	i° 3	0′				d=2	2°	0′			

7															7
b		a=2	2° 30′			a = 2	23° 0)′			a=2	3° 30′		$\setminus c$	1
$B \setminus$	h d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	$\frac{1}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	C	β
0 I 2 3 4	0 0 55 1 51 2 46 3 42	1.09 1.07 1.09 1.07 1.09	22 30 30 31 32 33	0.00 .02 .02 .02	5 I 5 2 4 3 4	1 1.09 6 1.09		0 0 1 2 3	0.00 .02 .02 .02	55 1 50 2 45 3 40	1.09	23 30 30 31 32 33	.02	90 89 88 87 86	90.0 89.6 89.2 88.8 88.4
5 6 78 9	4 37 5 33 6 28 7 23 8 19	1.07 1.09 1.09 1.07 1.09	35 37 39 42 45	0.03 .03 .05 .05	4 3 5 3 6 2 7 2 8 1	1 1.09 6 1.07 2 1.09		5 7 9 12 15	0.03 .03 .05 .05	4 35 5 30 6 25 7 20 8 15	1.09	35 37 39 42 46	0.03 .03 .05 .07	85 84 83 82 81	88.0 87.6 87.3 86.9 86.5
10 11 12 13 14	9 14 10 9 11 4 12 0 55	1.09 1.09 1.07 1.09 1.09	49 53 57 23 2 7	0.07 .08 .08		7 1.09 2 1.09 7 1.09		19 23 27 32 38	0.07 .07 .08 .10	9 10 10 5 11 0 54 12 49	1.09	49 53 58 24 3	0.07 .08 .08 .08	80 79 78 77 76	86.1 85.7 85.3 84.8 84.4
15 16 17 18 19	13 50 14 45 15 40 16 35 17 30	1.09 1.09 2.5 1.09 3.9 1.09 4.7 0 1.09 5.5 1.09 1.09 1.11 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.			13 4 14 4 15 3 16 3 17 20	2 1.09 7 1.09 2 1.11	24	43 49 56 3	0.10 .12 .12 .13	13 44 14 39 15 33 16 28 17 22	1.09 1.11 1.09 1.11	14 20 27 34 42	0.10 .12 .12 .13	75 74 73 72 71	84.0 83.6 83.2 82.8 82.3
20 21 22 23 24	18 25 19 20 20 15 21 10 22 4	1.09	55 24 4 14	0.13 .15 .17 .17	18 2 19 10 20 10 21	1.11		19 27 36 45 55	0.13 .15 .15 .17	18 17 19 11 20 6 21 0	1.11	50 58 25 7 17 27	0.13 .15 .17 .17	70 69 68 67 66	81.9 81.5 81.0 80.6 80.1
25 26 27 28 29	59 23 54 24 48 25 42 26 37	1.09	34 45 56 25 8 21	0.18 .18 .20 .22	22 54 23 48 24 42 25 36 26 30	3 1.11 2 1.11 5 1.11		6 17 28 40 53	0.18 .18 .20 .22 .23	22 48 23 42 24 36 25 30 26 24	I.II I.II I.II I.II	38 49 26 I 13 26	0.18 .20 .20 .22 .23	65 64 63 62 61	79.7 79.2 78.7 78.3 77.8
30 31 32 33 34	27 31 28 25 29 19 30 13 31 7	1.11	34 48 26 2 17 33	0.23 .23 .25 .27 .28	27 22 28 18 29 12 30 5	1.11		7 21 35 51 7	0.23 .23 .27 .27 .28	27 18 28 11 29 5 58 30 51	1.13 1.11 1.13 1.13	40 54 27 9 24 40	0.23 .25 .25 .27 .28	59 58 57 56	77.3 76.8 76.3 75.8 75.2
35 35 37 38 39	32 0 54 33 47 34 40 35 33	1.11 1.13 1.13 1.13	50 27 7 25 44 28 4	0.28 .30 .32 .33	31 52 32 45 33 38 34 31 35 24	1.13	28	24 41 59 18 38	0.28 .30 .32 .33 .35	31 44 32 37 33 30 34 23 35 15	1.13 1.13 1.13 1.15 1.15	57 28 15 34 53 29 14	0.30 .32 .32 .35	55 54 53 52 51	74.7 74.2 73.6 73.0 72.4
40 41 42 43 44	1	1.13 1.15 1.15 1.15	24 45 29 8 32 56	0.35 .38 .40 .40 .43	36 17 37 9 38 1 39 45	1.15	30	59 21 44 8 33	0.37 .38 .40 .42 .43	36 7 59 37 51 38 43 39 34	1.15 1.15 1.15 1.18 1.15		0.37 .38 .40 .42 .43	50 49 48 47 46	71.8 71.2 70.6 70.0 69.3
45	40 47		30 22		40 37			59		40 26		35		45	68.7
t	a	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	a	<u>6ο'</u> Δ	b		$\frac{\Delta}{60'}$	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$		a
	d	=22	° 30′			d=2	3° 0′	,		(l=23	3° 30′			

\ b		a	=22	2° 3	0′			(a=2	3° ()′			a	ı = 23	3° 3	0′		c	a
B	h	d	<u>6ο'</u> Δ	z	t	<u>Δ</u> 60'	h	d	<u>6ο′</u> Δ	z	t	<u>Δ</u> 6ο'	h	d	<u>60'</u> Δ	Z	*	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
45 46 47 48 49	40 41 42 43 44	47 39 31 22 13	1.15 1.15 1.18 1.18 1.20	30° 31 32	22 48 16 45 16	0.43 .47 .48 .52 .53	40 41 42 43 44	37 28 19 10	1.18 1.18 1.18 1.20 1.20	30 31 32	59 26 54 23 54	0.45 •47 •48 •52 •53	40 41 42 43	26 17 7 58 48	1.18 1.20 1.18 1.20 1.20	31 32 33	35 3 31 1 32	0.47 •47 •50 •52 •55	45 44 43 42 41	68.7 68.0 67.3 66.5 65.8
50 51 52 53 54	45 46 47 48	3 53 43 33 22	I.20 I.20 I.20 I.22 I.22	33 34 35	48 21 56 32 10	0.55 .58 .60 .63	45 46 47 48	50 40 30 19	I.20 I.20 I.22 I.22 I.25	33 34 35	26 0 35 12 50	0.57 .58 .62 .63	44 45 46 47	38 27 16 5 54	I.22 I.22 I.22 I.22 I.25	34 35 36	5 39 14 51 30	0.57 .58 .62 .65	40 39 38 37 36	65.0 64.2 63.4 62.6 61.7
55 56 57 58 59	49 50 51 52	59 47 35 22	1.25 1.25 1.25 1.28 1.30	36 37 38	50 32 15 1 48	0.70 •72 •77 •78 •83	49 50 51 52	56 44 32 19	1.25 1.25 1.28 1.28 1.30	36 37 38 39	30 12 56 42 30	0.70 •73 •77 .80 .83	48 49 50 51	42 29 16 3 49	1.28 1.28 1.28 1.30 1.30	37 38 39 40	10 52 36 22 10	•.7° •73 •77 .8° .85	35 34 33 32 31	60.8 59.9 59.0 58.0 57.0
60 61 62 63 64	53 54 55 56	8 54 40 24 8	1.30 1.30 1.36 1.36 1.40	2 40 31 .90 41 25 .97 42 23 1.00 43 23 1.05 44 26 1.08 45 31 1.15 46 40 1.27 49 8 1.32 2 50 27 1.38 5 51 50 1.45 5 53 17 1.50 5 54 47 1.57 1.57		53 54 55	52 37 22 6 49	1.33 1.33 1.36 1.40 1.40	40 41 42 43 44	20 12 7 5 5	0.87 .92 .97 1.00	52 53 54 55	35 20 4 48 31	1.33 1.36 1.36 1.40 1.43	41 42 43 44	53 48 46 46	0.87 .92 .97 1.00 1.05	30 29 28 27 26	55.9 54.8 53.7 52.5 51.3	
65 66 67 68 69	57 58 59	51 34 16 56 36	1.40 1.43 1.50 1.50 1.54	45 46 47	31 40 52	1.15 1.20 1.27	56 57 58 59	32 14 55 35 15	1.43 1.46 1.50 1.50 1.58	45 46 47 48 49	8 13 22 34 50	1.08 1.15 1.20 1.27 1.30	56 57 58	13 54 35 15 53	1.46 1.46 1.50 1.58 1.58	45 46 48 49 50	49 55 3 15 30	1.10 1.13 1.20 1.25 1.32	25 24 23 22 21	50.0 48.7 47.4 46.0 44.5
70 71 72 73 74	60 61 62	15 52 29 4 38	1.62 1.62 1.71 1.76 1.82	51 53 54	50 17 47	1.45 1.50 1.57	60 61 62	53 30 6 41 14	1.62 1.67 1.71 1.82 1.88	51 52 53 55 57	8 31 57 27 0	1.38 1.43 1.50 1.55 1.63	59 60 61	31 8 43 17 50	1.62 1.71 1.76 1.82 1.94	51 53 54 56 57	49 11 36 5 38	1.37 1.42 1.48 1.55 1.60	20 19 18 17 16	43.0 41.4 39.7 38.0 36.3
75 76 77 78 79	63 64 65	11 42 11 39 5	1.94 2.07 2.14 2.31 2.50	40 43 23 1.05 40 44 26 1.08 43 45 31 1.15 50 46 40 1.20 54 47 52 1.27 54 49 8 1.32 62 50 27 1.38 62 51 50 1.45 71 53 17 1.50 76 54 47 1.57 82 56 21 1.65 94 58 0 1.72 97 59 43 1.78 14 61 30 1.85 31 63 21 1.92		63 64	46 16 45 13 38	2.00 2.07 2.14 2.40 2.50	58 60 62 63 65	38 19 5 54 48	1.68 1.77 1.82 1.90 1.95	62 63 64	21 51 19 46 11	2.00 2.14 2.22 2.40 2.61	59 60 62 64 66	14 55 39 27 18	1.68 1.73 1.80 1.85 1.93	15 14 13 12 11	34·4 32·5 30.6 28·5 26·4	
80 81 82 83 84	66	29 51 11 29 45	2.73 3.00 3.33 3.75 4.29	67 69 71 73 75	15 19 26 36 50	2.07 2.12 2.17 2.23 2.28	65 66	2 23 43 1 16	2.86 3.00 3.33 4.00 4.62	67 69 71 73 76	45 46 51 59	2.02 2.08 2.13 2.18 2.23	65	34 56 15 32 47	2.73 3.16 3.53 4.00 4.62	68 70 72 74 76	15 21	1.98 2.03 2.10 2.13 2.18	10 9 8 7 6	24.3 22.1 19.8 17.4 15.1
85 86 87 88 89	67	59 10 19 25 29	5.45 6.67 10.0 15.0 60.0	85	7 26 48 11 35	2.32 2.37 2.38 2.40 2.42		29 40 49 55 59	5.45 6.67 10.0 15.0 60.0	85	24 40 58 18 39	2.27 2.30 2.33 2.35 2.35	66	0 11 19 25 29	5.45 7.50 10.0 15.0 60.0	78 80 83 85 87	40 53 8 25 42	2.22 2.25 2.28 2.28 2.30		12.ó 10.1 7.6 5.1 2.6
òo		30	$\left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $			Δ	67		60'	90	0	Δ		30	601		0		0	0.0
t		<i>a</i>				60'			$\frac{60'}{\Delta}$		<i>b</i>	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	-	1	$\frac{60'}{\Delta}$		<i>b</i>	<u>∆</u>		-12
		C	l = 2:	2° 3	0′				d=2	3°	0′			0	<i>l</i> = 23	3° 3	0′			

	b	Ī		a	= 2	24°	0′		T		a = 2	24°	30′		T		a = 1	25°	0′		1\0	
	\	1	-	l I	601		t	Δ	- -	à	_	11	t	Δ	+	d	1 .		t	ΙΛ	- \ \	\ a
B	/	h	/	1	Δ	Z	. 1	60	h		Δ	2	- \	60	h		$\frac{1}{\Delta}$	Z	-	<u>Δ</u> 60	$C \setminus$	β
	0 I	C	5.	5 1	1.09 1.09	24		.02		55		24	4 30 30		0	54		11 .	5 0		89	90.0
1 3	3	3	2 44	4 1	1.11		3	.02	2		1.11		31 32 33	.0:	2 2	1 49 2 43 3 38	1.00		2 3	.02	87	89.2 88.8 88.3
1		4	29) 1	1.09	-	5	.05	5	27	1.11		35 37	0.03		1 32 5 26	1.11	11	5		84	87.9 87.5 87.1
8		7 8		3 1	.09		13 16	.05	1 2		1.11		40 43 46	.05	1 2		1.09		10 13 16	.05	83	87.1 86.7 86.2
10 I I		9	2	1 5	.11		20 24	0.07	10	ō	1.09		50 54	0.07		57	1.11		20 24	.08	80 79	85.8 85.4
12 13 14	3	I I I 2		1 1	.09		28 33 39	80.	I I I 2		1.11	25	59 4 9	.08	11	46	1.11 1.11 1.11		29 34 40	.10	1 /	85.0 84.5 84.1
15 16	5	13	35	1.	.11		45	0.10	13 14		1.09		15	0.12	14	. 28	1,11		46 53	.12	75	83.7 83.2
17 18 19	1	15 16 17	29 24 18	1.	.09	25	58 5 13	.13	15 16 17	26 20 14	1.11		29 36 44	.13	15 16 17	16	1.11	26	7	.13	73 72 71	82.8 82.3 81.9
20 2 I	1	18	I 2 7	I.	.09		21 30	0.15	18 19	8	1.11	26		0.15	18	3 57	1.11		23 32	0.15	70 69	81.4 81.0
22 23 24	ı	20 21	55 49	Ι.	11.		39 49 59	.17 .17	20 21	56 50 43	1.11		10 20 31	.17 .18	19 20 21		1.13	27	42 52 3	.17	68 67 66	80.5 80.0 79.5
25 26	ŀ	22 23	43 37	1.	11	26	10 21	0.18	22 23	37 31	1.11		42 53	0.18	22 23	31 25	1.11		14 25	0.18	65 64	79.1 78.6
27 28 29	1	24 25 26	30 24 17	1.	13		33 46 5 9	.22	24 25 26	24 17 11	1.13	27	18 31	.22	24 25 26	18 11 4	I.13 I.13	28	37 50 4	.23	63 62 61	78.1 77.6 77.1
30		27 28	11	1.	13	27	I 3 27	0.23	27	4 57	1.13	28	45 O	0.25	27	57 50	1.13		18 33 48	0.25	60 59	76.5 76.0
32 33 34		29 30	57 50 43	ı.	13 13	28	42 58 14	.27 .27 .28	28 29 30	50 43 35	I.13 I.15 I.13		15 31 48	.27 .28	28 29 30	42 35 27	I.13 I.15 I.15	29	48 4 21	.27 .28	58 57 56	75.5 74.9 74.4
35 36		3 I 3 2	36 29	ı.	13		31 49	0.30	31 32	28 20	1.15	29	5 23	o.30	31 32	19	1.15		39 58	0.32	55 54	73.8 73.2
37 38 39	13	33 34 35	21 13 5	1.	15 15	29	28 49	•33 •35 •35	33 34	12 4 56	1.15 1.15 1.15	30	43 3 24	•33 •35 •35	33 34	3 55 47	1.15	30	37 58	-33 -35 -37	53 52 51	72.6 72.0 71.4
40		36	57 49	I.	15	30	10 32	°.37	36	48 39	1.18	31	45	°•37	35 36	38 29	1.18	31	20 43	0.38	50 49	70.8 70.2
42 43 44	3	38	41 32 23	I.	18	31	56 20 45	.40 .42 .45	37 38 39	30 21 12	1.18	32	31 56 21	.42 .42 .45	37 38	20 II I	1.18 1.20 1.20	32	7 31 57	.40 .43 .45	48 47 46	69.5 68.9 68.2
45		to			- 11	32			40	3			48			51	1	33			45	67.5
		а		<u>6α</u>	7	t		<u>Δ</u> 6ο'	a		<u>6ο'</u> Δ	b		Δ 60'	a		<u>6ο'</u> Δ	t		<u>Δ</u> 6ο'	Y	a
t			(-	24	°C)'	- /1		d	= 24	l° 3	0'			0	l=2	5° 0	y'	Υ.		
	1							7.1														

1	, [a = 2	10 0)'		1		<i>i</i> = 2	1.º c	20'				a = 2	50	n'		1	\
/	-	. 7		14			_		1	4 6	_				1	10		1 2	\ c	a
R	1	h d	<u>6ο'</u> Δ	Z	*	<u>Δ</u> 6ο'	h	d	$\frac{60'}{\Delta}$	Z	1	$\frac{\Delta}{6\sigma'}$	h	d	$\frac{60'}{\Delta}$	Z	1	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
45 46 47 48 49	4	0 14 11 5 55 12 45 13 35	1.18 1.20 1.20 1.20 1.20	33	12 39 8 38 10	0.45 .48 .50 .53	40 41 42 43	3 53 43 33 22	1.20 1.20 1.20 1.22 1.22	32 33 34	48 16 45 15 47	0.47 .48 .50 .53 .55	39 40 41 42 43	51 41 31 20 9	I.20 I.20 I.22 I.22 I.22	33 34 35	24 52 22 52 24	0.47 .50 .50 .53 .55	45 44 43 42 41	67.5 66.8 66.0 65.3 64.5
50 51 52 53 54	2	14 25 15 14 16 3 51 17 39	1.22 1.22 1.25 1.25 1.25	35	43 17 53 30 9	0.57 .60 .62 .65	44 45 46 47	11 0 49 37 25	1.22 1.22 1.25 1.25 1.25	35 36 37	20 55 31 8 47	0.58 .60 .62 .65	44 45 46 47	58 47 35 22 9	1.22 1.25 1.28 1.28 1.28	36 37 38	57 32 8 46 26	0.58 .60 .63 .67	40 39 38 37 36	63.7 62.9 62.0 61.2 60.3
55 56 57 58 59		48 27 49 14 50 1 47 51 33	1.28 1.30 1.30 1.33	38 39 40	49 32 16 2 50	0.72 .73 .77 .80 .85	48 49 50 51	12 58 44 30 15	1.30 1.30 1.30 1.33	38 39 40 41	28 11 55 42 30	.72 .73 .78 .80 .85	48 49 50	56 42 28 14 59	1.30 1.30 1.30 1.33 1.36	39 40 41 42	7 49 34 21	0.70 •75 •78 •80 •85	35 34 33 32 31	59·4 58·4 57·4 56·4 55·4
61 62 63 64		52 18 53 2 46 54 29 55 11	1 1.30 39 16 47 1.30 40 2 33 1.33 50 18 1.36 41 41 0 2 1.36 42 34 46 1.40 43 29 29 1.43 44 27 1 11 1.43 45 27 1 53 1.46 46 30 1 34 1.50 47 35 1 14 1.54 48 44 1 53 1.58 49 55 1 31 1.62 51 10 1 8 1.67 52 28 1		0.88 .92 .97 1.00	52 53 54	0 44 27 10 52	1.36 1.40 1.40 1.43 1.46	42 43 44 45 46	21 14 9 7	0.88 .92 .97 1.00	51 52 53 54	43 26 9 51 33	1.40 1.43 1.43 1.50	43 44 45 46	53 48 46 46	0.88 .92 .97 1.00	30 29 28 27 26	54·3 53·2 52·0 50·9 49·6	
65 66 67 68 69		53 56 34 57 14 53 58 31	2 1.36 42 34 16 1.40 43 29 29 1.43 44 27 1 11 1.43 45 27 1 13 1.46 46 30 1 14 1.50 47 35 1 15 1.54 48 44 1 15 1.62 51 10 1 8 1.67 52 28 1 14 1.71 53 49 1 19 1.76 55 14 1				55 56 57 58	33 14 53 32 9	1.46 1.54 1.54 1.62 1.62	47 48 49 50 51	10 15 24 35 49	1.08 1.15 1.18 1.23 1.30	55 56 57	13 53 32 10 47	1.50 1.54 1.58 1.62 1.67	47 48 50 51 52	49 54 2 13 27	1.08 1.13 1.18 1.23 1.28	25 24 23 22 21	48.4 47.0 45.7 44.3 42.8
70 71 72 73 74	6	59 8 44 50 19 51 25	1.71	1.35 1.42 1.47 1.53 1.60	59 60 61	46 22 56 29	1.67 1.76 1.82 1.88 2.00	53 54 55 57 58	7 28 52 19 50	1.35 1.40 1.45 1.52 1.57	58 59 60	23 58 32 5 36	1.71 1.76 1.82 1.94 2.00	53 55 56 57 59	44 5 .28 55 25	1.35 1.38 1.45 1.50 1.55	20 19 18 17 16	41.3 39.7 38.1 36.4 34.7		
75 76 77 78 79	6	56 52 26 54 53 20 44	2.00 2.14 2.31 2.50 2.61	61 63 64	50 29 12 58 48	1.65 1.72 1.77 1.83	62 63	31 O 27 53 17	2.07 2.22 2.31 2.50 2.73	60 62 63 65 67	24 24 44 29 17	1.63 1.70 1.75 1.80 1.87	61 62	6 34 1 26 50	2.14 2.22 2.40 2.50 2.73	60 62 64 65 67	58 35 15 58 45	1.62 1.67 1.72 1.78 1.83	15 14 13 12 11	32.9 31.0 29.1 27.1 25.1
80 81 82 83 84	1	54 7 28 47 55 3 18	2.86 3.16 3.75 4.00 4.62	70 72 74	42 39 39 42 47	1.95 2.00 2.05 2.08 2.13	64	39 0 18 35 49	2.86 3.33 3.53 4.29 4.62	69 71 73 75 77	9 3 1 2 5	1.90 1.97 2.02 2.05 2.08	63 64	32 50 6 20	3.00 3.33 3.75 4.29 5.00	69 71 73 75 77	35 27 23 21 22	1.87 1.93 1.97 2.02 2.05	10 9 8 7 6	23.6 20.9 18.7 16.5 14.2
85 86 87 88 89		31 41 49 55 59	6.00 7.50 10.0 15.0 60.0	81	55 6 18 31 45	2.18 2.20 2.22 2.23 2.25	65	2 12 20 25 29	6.00 7.50 12.0 15.0 60.0		10 18 27 37 48	2.13 2.15 2.17 2.18 2.20		32 42 50 56 59	6.00 7.50 10.0 20.0 60.0	79 81 83 85 87	25 30 36 43 51	2.08 2.10 2.12 2.13 2.15	5 4 3 2 1	9.6 7.2 4.8 2.4
90	===	66 o		90	0			30		90	0		65 —	0		90	0		0	0.0
l.		a	<u>6ο'</u> Δ	b	,	$\frac{\Delta}{60'}$	a	ı	6ο' Δ		b	$\frac{\Delta}{60'}$	(ı	$\frac{60'}{\Delta}$		Ь	$\frac{\Delta}{60'}$		a
	-		d=2	4° ()′			d	=24	4° 3	0′	-	•		d = 2	5° (0′	•		- i

\ b		a=25	5° 30′			a = 2	6° 0′			a	=26	5° 30′		_c	\ a
B	h d	$\left \frac{60'}{\Delta} \right $	Z	$\frac{\Delta}{60'}$	$\frac{d}{h}$	6ο' Δ	Z	Δ 60'	h	d	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	$c \setminus$	β
0 0 1 2 3 4	0 0 54 1 48 2 43 3 37	1.11	25 30 30 31 32 33	0.00 .02 .02 .02 .03	0 0 54 1 48 2 42 3 36	I.II I.II I.II I.II	26 0 0 1 2 3	0.00 .02 .02 .02		ó 54 47 41 35	1.11 1.13 1.11 1.11	26 30 30 31 32 33	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.6 89.1 88.7 88.2
5 6 7 8 9	4 31 5 25 6 19 7 13 8 7	1.11 1.11 1.11 1.11	35 37 40 43 47	0.03 .05 .05 .07	4 30 5 23 6 17 7 11 8 5	1.13 1.11 1.11 1.11	5 7 10 13 17	0.03 .05 .05 .07	4 5 6 7 8	28 22 16 9 3	1.11 1.13 1.11 1.13	35 37 40 43 47	0.03 .05 .05 .07	85 84 83 82 81	87.8 87.4 86.9 86.5 86.1
10 11 12 13	11 43	1.11	51 55 26 0 5	0.07 .08 .08 .10	59 9 53 10 46 11 40 12 34	1.11 1.13 1.11 1.11	21 25 30 35 41	0.07 .08 .08 .10	9 10 11 12	56 50 43 37 30	1.11 1.13 1.11 1.13 1.11	51 56 27 1 6	.08	80 79 78 77 76	85.6 85.1 84.7 84.2 83.8
15 16 17 18	15 18 16 12	1.11	17 24 31 38 46	0.12 .12 .12 .13	13 27 14 21 15 14 16 8 17 1	1.11 1.13 1.11 1.13 1.13	47 54 27 I 9 17	0.12 .12 .13 .13	13 14 15 16	24 17 10 3 56	I.13 I.13 I.13 I.13	18 25 32 40 48	.12	75 74 73 72 71	83.3 82.8 82.4 81.9 81.4
20 21 22 23 24	18 52 19 46 20 39	1.11	55 27 4 13 23 34	.17	54 18 47 19 40 20 33 21 2 6	1.13 1.13 1.13 1.13 1.13	26 35 45 55 28	.17	17 18 19 20 21	49 42 35 28 21	1.13 1.13 1.13 1.13 1.15	28 6 16 26 37	.17	70 69 68 67 66	80.9 80.4 80.0 79.5 79.0
25 26 27 28 29	23 18 24 11 25 4	1.13	45 57 28 10 23 37	.22	22 19 23 12 24 5 57 25 50	1.13 1.13 1.15 1.13 1.15	17 29 42 55 29	.22	22 23 24 25	13 6 58 51 43	1.13 1.15 1.13 1.15 1.15	29 1 29 1 27 41	.22	65 64 63 62 61	78.4 77.9 77.4 76.9 76.3
31 32 33 34	27 42 28 3 29 2	1.13	29 6 22 38 55	.27 .27 .28	26 42 27 34 28 26 29 18 30 10	1.15 1.15 1.15 1.15 1.15	30 11 28	.27	29	35 27 19 10 2	1.15 1.15 1.18 1.15 1.18	30 II 20 31	.27	57	75.8 75.2 74.7 74.1 73.5
3. 3. 3. 3. 3. 3. 3.	32 7 8 33 4	3 1.18 1 1.18 5 1.18	30 13 31 51 31 11 32	·33 ·33 ·35	31 2 53 32 45 33 36 34 27	1.18 1.15 1.18 1.18 1.18	31 2 4 32	33	31 32 33	26	1.18 1.18 1.18 1.18 1.20	39 39 32 4	9 ·33 9 ·33 9 ·37 1 ·38	54 53 52 51	72.9 72.3 71.7 71.1 70.5
4444	36 I 37 3 38	8 1.18 9 1.18 0 1.20		3 .40 2 .42 7 .43		I.20 I.20 I.20 I.20 I.20		2 .42		7 57 47 37 26	I.20 I.20 I.20 I.22 I.22	2 5 34 I	7 .43	49 48 47	69.8 69.1 68.5 67.8 67.1
4	39 4		34		39 28	-	31	-	39	15	1	35 1	1	45	56.3
	a	60' Δ	В	Δ 60'	G	60' Δ	b	00°		а	60' Δ	b	$\frac{\Delta}{60'}$		a
		d = 2	5° 30′		·	d = 2	26° 0′				d=2	6° 30′			

1	l 	a = 2	5° 30′				a=2	6°	0′			C	<i>i</i> = 2	6° 3	30′		C	a
$B \setminus$	h	β <u>60'</u> Δ	Z	$\frac{\Delta}{60'}$	h	d	6ο' Δ	Z	t	<u>Δ</u> 6ο'	h	d	<u>6ο′</u> Δ	z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
o 45 46 47 48 49	39 40 40 29 41 18 42 7	I.22 I.22 I.22	34 28 58 35 29 36 1	.50	39 40 41 42	28 17 6 55 43	I.22 I.22 I.22 I.25 I.25	34 35 36	36 4 34 5 37	0.47 .50 .52 .53 .57	39 40 41 42	15 4 53 41 29	I.22 I.22 I.25 I.25 I.25	35 36 37	11 40 10 41 14	0.48 .50 .52 .55	° 45 44 43 42 41	66.3 65.6 64.8 64.0 63.2
50 51 52 53 54	43 45 44 33 45 26 46 3	I.28 I.28 I.28	35 37 10 46 38 24 39 4	.63	43 44 45 46	31 18 5 52 39	1.28 1.28 1.28 1.28 1.30	37 38 39	11 46 23 1 41	0.58 .62 .63 .67	43 44 45 46	17 4 51 37 23	1.28 1.28 1.30 1.30 1.30	38 39 40	48 23 0 38 18	0.58 .62 .63 .67	39 38 37 36	62.4 61.6 60.7 59.8 58.9
55 56 57 58 59	47 41 48 27 49 12 57 50 41	1.33 1.33 1.36	45 40 28 41 13 59 42 48	0.72 •75 •77 .82 .85	47 48 49 50	25 10 55 40 24	1.33 1.33 1.33 1.36 1.40	40 41 42 43	23 6 51 38 26	0.72 •75 •78 •80 •85	47 48 49 50	9 54 38 22 6	1.33 1.36 1.36 1.36 1.40	41 42 43 44	0 43 28 15 4	0.72 •75 •78 •82 •85	35 34 33 32 31	58.0 57.0 56.0 54.9 53.9
60 61 62 63 64	51 25 52 8 50 53 32 54 13	1.43 1.43 1.46	43 39 44 32 45 27 46 25 47 25	0.88 •92 •97 1.00	51 52 53	7 49 31 13 53	1.43 1.43 1.43 1.50 1.50	44 45 46 47 48	17 10 6 3 3	0.88 •93 •95 1.00 1.03	51 52 53	49 31 12 53 33	1.43 1.46 1.46 1.50 1.54	45 46 47 48	55 48 43 41 41	0.88 .92 .97 1.00 1.03	30 29 28 27 26	52.8 51.7 50.5 49.3 48.1
65 66 67 68 69	53 55 33 56 11 49 57 25	1.58	48 28 49 33 50 41 51 51 53 5	1.08 1.13 1.17 1.23 1.27	54 55 56 57	33 12 50 27 3	1.54 1.58 1.62 1.67 1.71	49 50 51 52 53	5 10 18 28 42	1.08 1.13 1.17 1.23 1.27	54 55 56	50 28 4 40	1.58 1.58 1.67 1.67 1.71	49 50 51 53 54	43 48 55 5 18	1.08 1.12 1.17 1.22 1.25	25 24 23 22 21	46.8 45.4 44.1 42.7 41.2
70 71 72 73 74	58 I 35 59 8 40 60 II	1.82 1.88 1.94	54 21 55 41 57 4 58 30 59 59		58 59	38 12 44 16 46	1.76 1.88 1.88 2.00 2.07	54 56 57 59 60	58 17 39 4 32	I.32 I.37 I.42 I.47 I.52	57 58 59	15 48 20 51 21	1.82 1.88 1.94 2.00 2.14	55 56 58 59 61	33 51 13 37 4	1.30 1.37 1.40 1.45 1.50	20 19 18 17 16	39·7 38.1 36.5 34·9 33·2
75 76 77 78 79	61 8 35 62 22	2.22 2.50 2.61	61 31 63 6 64 45 66 27 68 12	1.58 1.65 1.70 1.75 1.80	60 61	15 42 8 32 55	2.22 2.31 2.50 2.61 2.86	62 63 65 66 68	37 14 55 38	1.57 1.62 1.68 1.72 1.77	60 61	49 16 41 5 28	2,22 2,40 2,50 2,61 3.00	62 64 65 67 69	34 7 43 22 4	1.55 1.60 1.65 1.70 1.73	15 14 13 12 11	31.4 29.6 27.8 25.9 23.9
80 81 82 83 84	63 4 21 37 51	3.53 3.75 4.29	70 0 71 51 73 44 75 40 77 38	1.85 1.88 1.93 1.97 2.02	62 63	16 35 53 8 22	3.16 3.33 4.00 4.29 5.45	70 72 74 75 77	24 13 4 58 54	1.82 1.85 1.90 1.93 1.97	62	48 7 24 39 53	3.16 3.53 4.00 4.29 5.45	70 72 74 76 78	48 35 24 16	1.78 1.82 1.87 1.90 1.92	9 8 7 6	21.9 19.9 17.8 15.6 13.5
85 86 87 88 89	64 3 20 26 29	8.57 10.0 20.0	79 39 81 41 83 44 85 49 87 54	2.08		33 43 50 56 59	6.00 8.57 10.0 20.0 60.0	79 81 83 85 87	52 52 53 55 57	2.00 2.02 2.03 2.03 2.05	63	-	6.67 8.57 10.0 20.0 60.0		52000	1.95 1.97 2.00 2.00 2.00	5 4 3 2 1	9.1 6.8 4.6 2.3
90	30		90 0		64	0		90	0			30		90	0		0	0.0
_	а	60' <u>∆</u>	b	$\frac{\Delta}{60'}$	0	ı	<u>6ο'</u> Δ		ь	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$		ь	<u>Δ</u> 6ο'		a
t		d = 2	5° 30′				d = 2	6° ()′			d	= 26	3° 3	0′			

b	,	a = 2	27° 0′			a=2	7° 3	0′	1			a=2	8° (0′	(\ c	a
B	h	<u>60'</u> Δ	Z	$\frac{\Delta}{60'}$	h d	$\frac{60'}{\Delta}$	z	t	<u>Δ</u> 60'	h	d	6ο' Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	53 1 47 2 40 3 34	1.13 1.11 1.13 1.11 1.13	27 0 0 1 2 3		53 1 46 2 40 3 33	1.13	27	30 30 31 32 33	0.00 .02 .02 .02	0 I 2 3	53 46 39 32	I.13 I.13 I.13 I.13	28	0 0 1 2 3	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.5 89.1 88.6 88.2
5 6 7 8 9	4 27 5 21 6 14 7 7 8 1	1.11 1.13 1.13 1.11 1.13	5 8 11 14 17	0.05 .05 .05 .05	4 26 5 19 6 12 7 5 59	1.13 1.13 1.11		35 38 41 44 48	0.05 .05 .05 .07	4 5 6 7	25 18 11 4 56	I.13 I.13 I.13 I.15 I.13		5 8 11 14 18	0.05 .05 .05 .07	85 84 83 82 81	87.7 87.2 86.8 86.3 85.8
10 11 12 13 14	54 9 47 10 41 11 34 12 27	1.13 1.11 1.13 1.13 1.13	21 26 31 36 42	0.08 .08 .08 .10	8 52 9 45 10 38 11 31 12 23	1.13 1.13 1.15	28	52 56 1 7	0.07 .08 .10 .10		49 42 35 27 20	I.13 I.15 I.15 I.13		22 27 32 37 43	0.08 .08 .08 .10	80 79 78 77 76	85.3 84.9 84.4 83.9 83.4
15 16 17 18 19	13 20 14 13 15 6 59 16 52	1.13 1.13 1.13 1.13	49 56 28 3 11 19	0.12 .12 .13 .13	13 16 14 9 15 2 55 16 47	1.13 1.13 1.15		19 26 34 42 50	0.12 .13 .13 .13	13 14 15 16	13 58 50 42	1.15 1.13 1.15 1.15	29	50 57 4 12 21	0.12 .12 .13 .15	75 74 73 72 71	82.9 82.5 82.0 81.5 81.0
20 21 22 23 24	17 45 18 37 19 30 20 22 21 15	1.15 1.13 1.15 1.13 1.15	28 37 47 58 29 9	0.15 .17 .18 .18	17 40 18 32 19 24 20 17 21 9	1.15 1.13 1.15	29	59 9 19 30 41	0.17 .17 .18 .18	17 18 19 20 21	35 27 19 11 3	1.15 1.15 1.15 1.15	30	30 40 50 1	0.17 .17 .18 .18	70 69 68 67 66	80.5 79.9 79.4 78.9 78.4
25 26 27 28 29	22 7 23 0 52 24 44 25 36	1.13 1.15 1.15 1.15 1.18	33 46 59 30 13	0.20 .22 .22 .23	22 I 53 23 45 24 37 25 28	1.15	30	53 5 18 32 46	0.20 .22 .23 .23	22 23 24 25	55 46 38 29 21	1.18 1.15 1.18 1.15 1.15	31	24 37 50 3 18	0.22 .22 .22 .25 .25	65 64 63 62 61	77.8 77.3 76.8 76.2 75.6
30 31 32 33 34	26 27 27 19 28 11 29 2 53	1.15 1.15 1.18 1.18 1.18	28 44 31 0 17 35	0.27 .27 .28 .30 .30	26 20 27 11 28 2 53 29 44	1.18	31	1 16 33 50 8	0.25 .28 .28 .30	26 27 28 29	3 54 45 35	1.18 1.18 1.18 1.20 1.18	32	33 49 5 22 40	0.27 .27 .28 .30 .32	60 59 58 57 56	75.1 74.5 73.9 73.3 72.7
35 36 37 38 39	30 44 31 35 32 26 33 16 34 6	1.18 1.18 1.20 1.20 1.20	32 12 32 53 33 15	0.32 -33 -35 -37 -38	30 35 31 26 32 16 33 6 56	1.20	33	26 46 6 27 49	0.33 .33 .35 .37	30 31 32 33	26 16 6 56 46	I,20 I,20 I,20 I,20 I,22	33 34	59 19 39 1 23	0.33 .33 .37 .37 .38	55 54 53 52 51	72.1 71.5 70.8 70.2 69.5
40 41 42 43 44	56 35 46 36 36 37 25 38 14		38 34 I 26 52 35 I9	0.38 .42 .43 .45 .47		I.22 I.22	34 35	12 36 1 27 54	0.40 •42 •43 •45 •47		35 24 13 2 50	1.22 1.22 1.22 1.25 1.25	35 36	46 10 35 1 28	0.40 •42 •43 •45 •48	50 49 48 47 46	68.8 68.1 67.4 66.7 66.0
45	39 3		47		51		36	22		38	38	6.1		57		45	65.2
$ _t$	a	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	а	<u>6ο'</u> Δ		b	Δ 60'	a	,	<u>6ο'</u> Δ	. 1	b	<u>Δ</u> 6ο'	-	a
		d = 2	27° 0′			d=2	7° 3	80′				d=2	28° () [′]	,		

\ b	, ,	a = 2	27° 0′				a = 2	7° 8	30′				a=2	8°	0′		\ c	a
$B \setminus$	h d	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	39 3 52 40 40 41 28 42 15	I.22 I.25 I.25 I.28 I.28	35 47 36 16 46 37 17 50	50 52 55	38 39 40 41 42	51 39 27 14 1	1.25 1.25 1.28 1.28 1.28	36 37 38	22 51 21 53 26	0.48 .50 .53 .55 .57	38 39 40 41	38 26 13 0 47	I.25 I.28 I.28 I.28 I.28	36 37 38 39	57 26 56 28 1	0.48 .50 .53 .55	45 44 43 42 41	65.2 64.4 63.7 62.9 62.0
50 51 52 53 54	43 2 49 44 36 45 22 46 7	1.28 1.28 1.30 1.33 1.33	38 24 39 0 40 1 55	.62	43 44 45	48 35 21 6 51	1.28 1.30 1.33 1.33	39 40 41	36 13 52 32	0.60 .62 .65 .67	42 43 44 45	34 20 5 50 35	1.30 1.33 1.33 1.33 1.36	40 41 42	36 12 49 28 8	0.60 .62 .65 .67	40 39 38 37 36	61.2 60.3 59.4 58.5 57.6
55 56 57 58 59	52 47 37 48 21 49 5 48	1.33 1.36 1.36 1.40 1.43	41 37 42 20 43 5 44 41	.75 .78 .82	46 47 48 49	36 20 4 47 29	1.36 1.36 1.40 1.43	42 43 44 45	14 57 42 29 18	0.72 •75 •78 •82 •85	46 47 48 49	19 3 46 29 11	1.36 1.40 1.40 1.43 1.46	43 44 45	50 34 19 6 55	0.73 •75 •78 •82 •85	35 34 33 32 31	56.6 55.6 54.6 53.5 52.5
60 61 62 63 64	50 30 51 12 53 52 33 53 13	1.43 1.46 1.50 1.50 1.58	45 32 46 25 47 21 48 18 49 18	·95	50 51 52	52 33 13 52	1.46 1.46 1.50 1.54 1.58	46 47 48 49	9 2 57 54 54	0.88 .92 .95 I.00 I.03	50 51 52	52 33 13 53 31	1.46 1.50 1.50 1.58 1.58	46 47 48 49 50	46 38 33 30 30	0.87 .92 .95 1.00	30 29 28 27 26	51.3 50.2 49.0 47.8 46.6
65 66 67 68 69	51 54 29 55 6 42 56 17	1.58 1.62 1.67 1.71 1.76	50 20 51 22 52 31 53 41 54 53	I.12 I.17 I.20	53 54 55	30 8 44 20 54	1.58 1.67 1.67 1.76 1.76	50 52 53 54 55	56 0 7 16 27	1.07 1.12 1.15 1.18 1.25	53 54 55	9 46 22 57 31	1.62 1.67 1.71 1.76 1.82	51 52 53 54 56	31 35 41 50 1	1.07 1.10 1.15 1.18 1.23	25 24 23 22 21	45·3 44·0 42·6 41·2 39·7
70 71 72 73 74	51 57 24 56 58 26 ->55	1.82 1.88 2.00 2.07 2.14	56 8 57 25 58 46 60 6 61 35	1.35 1.38 1.43	56 57 58	28 0 31 1 30	1.88 1.94 2.00 2.07 2.22	56 57 59 60 62	42 59 18 41 6	1.28 1.32 1.38 1.42 1.47	56 57 58	4 36 7 36 4	1.88 1.94 2.07 2.14 2.22	57 58 59 61 62	15 31 50 12 36	1.27 1.32 1.37 1.40 1.45	20 19 18 17 16	38.2 36.7 35.1 33.5 31.8
75 76 77 78 79	59 23 50 60 15 38 61 0	2.22 2.40 2.61 2.73 3.00	63 2 64 36 66 11 67 48 69 28	1.58 1.62 1.67	59 60	57 23 48 11 32	2.31 2.40 2.61 2.86 3.00	63 65 66 68 69	34 5 38 14 52	1.52 1.55 1.60 1.63 1.68	59 60	31 57 21 44 5	2.31 2.50 2.61 2.86 3.16	64 65 67 68 70	3 32 4 39 16	1.48 1.53 1.58 1.62 1.65	15 14 13 12 11	30.1 28.4 26.6 24.7 22.8
80 81 82 83 84	20 39 56 62 10 23	3.16 3.53 4.29 4.62 5.00	71 11 72 56 74 4. 76 3. 78 22	1.78 1.83 1.85	61	52 10 27 41 54	3.33 3.53 4.29 4.62 5.45	71 73 75 76 78	33 16 2 50 39	1.72 1.77 1.80 1.82 1.85	61	24 42 58 12 25	3·33 3·75 4·29 4.62 5·45	71 73 75 77 78	55 36 20 6 53	1.68 1.73 1.77 1.78 1.82	10 9 8 7 6	20.9 18.9 16.9 14.9 12.8
85 86 87 88 89	35 44 51 56 59	6.67 8.57 12.0 20.0 60.0		1.93	62	5 14 21 26 29				1.87 1.90 1.90 1.92 1.92			7.50 8.57 12.0 20.0 60.0		42 32 23 15 7	1.83 1.85 1.87 1.87 1.88	5 4 3 2 1	10.7 8.6 6.5 4.3 2.2
90	63 0		90 (30	1	90	0		62 ==	0		90	0		0	0.0
t	а	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	0	ı	<u>60'</u> Δ	,	b	<u>Δ</u> 60'	0	ı	<u>6ο′</u> Δ		Ь	$\frac{\Delta}{60'}$		a.
		d = 2	2 7° 0′	- c		0	l=2	7° 3	0′				d = 2	8° ()′	-		

b	a	i = 28	3° 30)′				a = 2	9° ()′			a	= 29)° 3	0′		\ c	a
B	h	$\left \frac{\epsilon_{\mathbf{O'}}}{\Delta} \right $	z	t	<u>Δ</u> 6ο'	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	h	d	$\frac{6o'}{\Delta}$	Z	t	<u>Δ</u> 6ο'	$C \setminus$	β
0 I 2 3 4	0 0 53 1 46 2 38 3 31	I.13 I.13 I.15 I.13 I.13		30 30 31 32 34	.02	2	52 45 37 30	1.15 1.13 1.15 1.13	29	0 0 1 2 4	0.00 .02 .02 .03	0 I 2 3	0 52 44 37 29	1.15 1.15 1.13 1.15 1.15	29	30 30 31 32 34	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.5 89.0 88.5 88.1
5 6 78 9	4 24 5 16 6 9 7 2 54	1.15 1.13 1.13 1.15 1.15		36 38 41 44 48	.03 .05 .05 .07	6	22 15 7 59 52	1.13 1.15 1.15 1.13 1.15		6 8 11 14 18	0.03 .05 .05 .07	4 5 6	21 13 5 57 49	1.15 1.15 1.15 1.15 1.15		36 38 41 44 48	0.03 .05 .05 .07	85 84 83 82 81	87.6 87.1 86.6 86.1 85.6
10 11 12 13 14	8 47 9 39 10 32 11 24 12 17	1.15 1.13 1.15 1.13 1.15	29	52 57 2 8 14	.08 .10 .10	8 9 10 11 12	44 36 29 21	1.15 1.13 1.15 1.15		22 27 32 38 44	0.08 .08 .10 .10	8 9 10 11 12	41 33 25 17 9	1.15 1.15 1.15 1.15	30	53 58 3 9	0.08 .08 .10 .10	80 79 78 77 76	85.1 84.6 84.1 83.6 83.1
15 16 17 18 19	13 9 14 1 53 15 45 16 37	1.15 1.15 1.15 1.15 1.15		21 0 28 35 43 52	.12 .13 .15		5 57 49 41 33	1.15 1.15 1.15 1.15 1.18	30	51 58 6 14 23	0.12 .13 .13 .15	13 14 15 16	53 45 36 28	1.15 1.15 1.18 1.15 1.15		22 29 37 45 54	0.12 .13 .13 .15	75 74 73 7 ² 71	82.6 82.1 81.6 81.0 80.5
20 21 22 23 24	17 29 18 21 19 13 20 5 57	1.15 1.15 1.15 1.15 1.18		I 6 II 2I 32 44	.17 .18 .20	17 18 19	24 16 8 59 50	1.15 1.15 1.18 1.18	31	32 42 52 3 15	0.17 .17 .18 .20	17 18 19	19 11 2 53 44	1.15 1.18 1.18 1.18 1.18	31	3 13 24 35 46	0.17 .18 .18 .18	70 69 68 67 66	80.0 79.5 78.9 78.4 77.8
25 26 27 28 29	2I 48 22 40 23 3I 24 22 25 I3	1.15 1.18 1.18 1.18	31	56 8 21 35 50	0.20 .22 .23 .25	21 22 23 24 25	41 32 23 14 5	1.18 1.18 1.18 1.18 1.18	32	27 40 53 7 22	0.22 .22 .23 .25	21 22 23 24	35 26 16 7 57	1.18 1.20 1.18 1.20 1.18	32	58 11 25 39 54	0.22 .23 .23 .25 .27	65 64 63 62 61	77.3 76.7 76.1 75.5 75.0
30 31 32 33 34	26 4 55 27 45 28 36 29 26	1.18 1.20 1.18 1.20 1.20		5 21 38 55 13	0.27 .28 .28 .30	26 27 28 29	56 47 37 27 17	I.18 I.20 I.20 I.20 I.20	33	37 53 10 28 46	0.27 .28 .30 .30 .32	25 26 27 28 29	48 38 28 18 7	I.20 I.20 I.20 I.22 I.22	33	10 26 43 0	0.27 .28 .28 .32 .32	60 59 58 57 56	74·4 73·8 73·1 72·5 71·9
35 36 37 38 39	30 16 31 6 56 32 45 33 34	I.20 I.20 I.22 I.22 I.22	34°	32 52 13 34 57	• 33 • 35 • 35 • 38 • 38	30 31 32 33	7 56 46 35 24	I.22 I.20 I.22 I.22 I.22	34 35	5 25 46 7 30	0.33 .35 .35 .38	30 31 32 33	57 46 35 24 13	I.22 I.22 I.22 I.22 I.25	35 36	38 58 19 41 3	0.33 -35 -37 -37 -40	55 54 53 52 51	71.3 70.6 69.9 69.3 68.6
40 41 42 43 44	34 23 35 12 36 1 49 37 37	I.22 I.22 I.25 I.25 I.25	36	20 44 9 36 3	0.40 •42 •45 •45 •47	34 35 36 37	13 1 49 37 25	I.25 I.25 I.25 I.25 I.25	36 37	53 18 43 10 37	0.42 .42 .45 .45	34 35 36 37	1 49 37 25 12	1.25 1.25 1.25 1.28 1.28	3 <i>7</i> 38	27 51 17 44 11	0.40 •43 •45 •45 •48	50 49 48 47 46	67.9 67.1 66.4 65.7 64.9
45	38 25			31		38	12		38	5			59			40		45	64.1
	а	<u>6ο'</u> Δ	b	•	<u>Δ</u> 6ο'	а	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	(a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
t		l=2	8° 30	0′				d=2	29° (0′				d = 2	9° 8	30′			

\ b		C	ı = 28	8° 3	0′				a=2	9°	0′		Π		a = 2	9° 8	30′		\ c	a
$B \setminus$	h	d	6ο' Δ	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	C	β
45 46 47 48 49	38 39 40 41	25 13 0 47 33	1.25 1.28 1.28 1.30 1.30	37 38 39	31 31 31 33 37	0.50 .50 .53 .57 .57	38 39 40 41	59 46 32 18	1.28 1.28 1.30 1.30	38 39 40	5 35 6 38 11	0.50 .52 .53 .55 .58	37 38 39 40 41	59 46 32 18 4	1.28 1.30 1.30 1.30 1.33	38 39 40	40 10 41 13 46	0.50 .52 .53 .55 .58	° 45 44 43 42 41	64.1 63.3 62.5 61.7 60.9
50 51 52 53 54	42 43 44 45	19 5 50 35 19	1.30 1.33 1.33 1.36 1.36	40 41 42	11 47 24 3 44	0.60 .62 .65 .68	42 43 44 45	4 49 34 18 2	1.33 1.33 1.36 1.36 1.36	41 42 43	46 22 0 39 19	0.60 .63 .65 .67	42 43 44	49 34 18 2 46	1.33 1.36 1.36 1.36 1.40	41 42 43	21 57 35 14 54	0.60 .63 .65 .67	40 39 38 37 36	60.0 59.1 58.2 57.2 56.3
55 56 57 58 59	46 47 48	3 46 29 11 53	1.40 1.40 1.43 1.43 1.46	43 44 45 46	26 9 55 42 31	0.72 •77 •78 •82 •85	46 47 48	46 29 11 53 34	1.40 1.43 1.43 1.46 1.50	44 45 46 47	45 30 17 6	0.73 .75 .78 .82 .85	45 46 47 48	29 11 53 34 15	1.43 1.43 1.46 1.46 1.50	44 45 46 47	36 20 5 52 41	0.73 .75 .78 .82 .85	35 34 33 32 31	55·3 54·3 53·3 52·2 51·1
60 61 62 63 64	49 50 51 52	34 14 53 32 10	1.50 1.54 1.54 1.58 1.58	47 48 49 50 51	22 14 9 6 5	0.87 .92 .95 .98	49 50 51	14 54 33 12 49	1.50 1.54 1.54 1.62 1.62	48 49 50 51	57 50 44 41 40	0.88 .90 .95 .98	49 50 51	55 34 13 51 28	1.54 1.54 1.58 1.62 1.67	48 49 50 51 52	32 25 19 15 14	0.88 .90 .93 .98	30 29 28 27 26	50.0 48.8 47.6 46.4 45.2
65 66 67 68 69	53 54 55	48 24 59 34 8	1.67 1.71 1.71 1.76 1.88	52 53 54 55 56	6 16 24 35	1.07 1.10 1.13 1.18 1.22	52 53 54	26 2 37 11 44	1.67 1.71 1.76 1.82 1.88	52 53 54 55 57	41 44 49 57 7	1.05 1.08 1.13 1.17 1.20	52 53 54	4 40 14 48 21	1.67 1.76 1.76 1.82 1.94	53 54 55 56 57	14 17 22 29 39	1.05 1.08 1.12 1.17 1.20	25 24 23 22 21	43.9 42.6 41.2 39.8 38.4
70 71 72 73 74	56 57	40 12 42 11 39	1.88 2.00 2.07 2.14 2.31	57 59 60 61 63	48 3 21 42 5	I.25 I.30 I.35 I.38 I.43	55 56 57	16 47 17 46 13	1.94 2.00 2.07 2.22 2.31	58 59 60 62 63	19 34 52 12 34	I.25 I.30 I.33 I.37 I.40	55 56	52 23 52 20 47	1.94 2.07 2.14 2.22 2.31	58 60 61 62 64	51 5 21 40 2	1.23 1.27 1.32 1.37 1.38	20 19 18 17 16	36.9 35.4 33.8 32.2 30.6
75 76 77 78 79	58 59	5 30 54 16 37	2.40 2.50 2.73 2.86 3.16	64 65 67 69 70	31 59 29 2 38	1.47 1.50 1.55 1.60 1.63	58 59	39 4 27 49 9	2.40 2.61 2.73 3.00 3.16	64 66 67 69 71	58 25 54 26 0	1.45 1.48 1.53 1.57 1.60	5 <i>7</i> 58	13 37 0 21 41	2.50 2.61 2.86 3.00 3.16	65 66 68 69 71	25 51 19 49 22	1.43 1.47 1.50 1.55 1.57	15 14 13 12 11	28.9 27.2 25.5 23.7 21.8
80 81 82 83 84	60	56 14 29 43 56	3.33 4.00 4.29 4.62 6.00	72 73 75 77 79	16 56 37 21 6	1.67 1.68 1.73 1.75 1.78	60	28 45 0 14 26	3.53 4.00 4.29 5.00 6.00	72 74 75 77 79	36 14 54 36 19	1.63 1.67 1.70 1.72 1.75	59	0 17 32 45 57	3.53 4.00 4.62 5.00 6.00	72 74 76 77 79	56 33 11 51 32	1.62 1.63 1.67 1.68 1.70	9 8 7 6	20.0 18.1 16.2 14.2 12.2
85 86 87 88 89	61	6 15 21 26 29	6.67 10.0 12.0 20.0 60.0			1.80 1.82 1.82 1.83 1.85			6.67 10.0 12.0 20.0 60.0				60	7 15 22 26 29	7.50 8.57 15.0 20.0 60.0			1.73 1.75 1.75 1.77 1.77	5 4 3 2 1	10.2 8.2 6.2 4.1 2.1
90		30		90	0		61	0		90	0		_	30		90	0		0	0.0
t	(ı	$\frac{60'}{\Delta}$		b	<u>Δ</u> 6ο'	a	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	1	b	$\frac{\Delta}{60'}$		G.
ι	d=28° 30′								d=2	9° ()′			C	l = 29	9° 3	0′			

\ b		a=3	0° 0′		1	a = 30	0° 3	30′				a=3	1° (D′		\ c	
$B \setminus$	h d	$\left \frac{60'}{\Delta} \right $	Z t	$\frac{\Delta}{60'}$	h d	6ο' Δ	Z	t	<u>Δ</u> 6ο'	h	$\frac{d}{}$	60' Δ	Z	t	$\frac{\Delta}{60'}$	$c \setminus$	3
0 0 1 2 3 4	0 0 52 1 44 2 36 3 28	1.15 1.15 1.15 1.15 1.15	30 0 0 1 2 4	0.00 .02 .02 .03	0 0 52 1 43 2 35 3 27	1.15 1.18 1.15 1.15	30	30 30 31 32 34	0.00 .02 .02 .03	2	6 51 43 34 26	1.18 1.15 1.18 1.15 1.15	31	0 0 1 2 4	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.5 89.0 88.5 88.0
5 6 78 9	4 20 5 12 6 4 55 7 47	1,15 1,15 1,18 1,15 1,15	6 8 11 15 19	0.03 .05 .07 .07	4 18 5 10 6 2 53 7 45	1.15 1.15 1.18 1.15 1.18		36 38 41 45 49	0.03 .05 .07 .07	5	17 8 0 51 43	1.18 1.15 1.18 1.15 1.18	1	6 8 11 15	0.03 .05 .07 .07	85 84 83 82 81	87.5 86.9 86.4 85.9 85.4
10 11 12 13 14	8 39 9 31 10 22 11 14 12 6	1.15 1.18 1.15 1.15 1.18	23 28 33 39 45	0.08 .08 .10 .10	8 36 9 28 10 19 11 11 12 2	1.15 1.18 1.15 1.18 1.18	31	53 58 3 9	0.08 .08 .10 .12	9 10 11	34 25 16 7 58	1.18 1.18 1.18 1.18		23 28 34 40 46	0.08 .10 .10	80 79 78 77 76	84.9 84.4 83.8 83.3 82.8
15 16 17 18 19	57 13 49 14 40 15 31 16 23	1.15 1.18 1.18 1.15 1.15	52 59 31 7 16 25	0.12 .13 .15 .15	53 13 44 14 35 15 26 16 17	1.18 1.18 1.18 1.18		23 30 38 46 55	0.12 •13 •13 •15 •17	13 14 15	49 40 31 22 12	1.18 1.18 1.18 1.20 1.18	32	53 1 9 17 26	0.13 .13 .13 .15	75 74 73 72 71	82.3 81.7 81.2 80.6 80.1
20 21 22 23 24	17 14 18 5 56 19 47 20 37	1.18 1.18 1.18 1.20 1.18	34 44 55 32 6 18	0.17 .18 .18 .20	17 8 59 18 50 19 41 20 31	1.18 1.18 1.18 1.20 1.20	32	5 15 26 37 49	0.17 .18 .18 .20	18	3 53 44 34 24	I.20 I.18 I.20 I.20 I.20	33	36 46 57 8 20	0.17 .18 .18 .20	70 69 68 67 66	79.5 79.0 78.4 77.8 77.3
25 26 27 28 29	21 28 22 19 23 9 59 24 49	I.18 I.20 I.20 I.20 I.20	30 43 57 33 11 26	0.22 .23 .23 .25	2I 2I 22 II 23 I 5I 24 4I	I.20 I.20 I.20 I.20 I.20	33	1 14 28 42 57	0.22 .23 .23 .25 .27	22	14 54 44 33	I.20 I.20 I.20 I.22 I.22	34	33 46 0 14 29	0.22 .23 .23 .25 .27	65 64 63 62 61	76.7 76.1 75.5 74.9 74.3
30 31 32 33 34	25 39 26 29 27 19 28 9 58	I.20 I.20 I.20 I.22 I.22	41 58 34 15 33 51	0.28 .28 .30 .30	25 31 26 21 27 10 59 28 48	I.20 I.22 I.22 I.22 I.22	34	13 30 47 5 24	0.28 .28 .30 .32 .32	26 27	23 12 1 50 39	I.22 I.22 I.22 I.22 I.25	35	45 2 19 37 56	0.28 .28 .30 .32 .33	59 58 57 56	73.7 73.0 72.4 71.8 71.1
35 36 37 38 39	29 47 30 36 31 25 32 13 33 1	I.22 I.22 I.25 I.25 I.25	35 11 31 52 36 14 37	0.33 •35 •37 •38 •38	29 37 30 26 31 14 32 2 50	I.22 I.25 I.25 I.25 I.25	36 37	43 4 25 47 10	0.35 .35 .37 .38 .40	30 31	27 15 3 51 39	I.25 I.25 I.25 I.25 I.28	36 37	16 36 57 20 43	0.33 •35 •38 •38 •40	55 54 53 52 51	70.4 69.8 69.1 68.4 67.7
40 41 42 43 44	49 34 37 35 25 36 12 59	1.25 1.25 1.28 1.28 1.28	37 0 25 51 38 17 45	0.42 •43 •43 •47 •48	33 38 34 25 35 12 59 36 46	1.28 1.28 1.28 1.28 1.30	38 39	34 58 24 51	•43 •45 •47 •48	34 35		1.28 1.28 1.30 1.28 1.30		7 31 57 24 52	•43 •45 •47 •48	50 49 48 47 46	66.9 66.2 65.4 64.7 63.9
45	37 46		39 14		37 32			48		37	19		40	21		45	63.1
	а	<u>60'</u> Δ	b	<u>Δ</u> 60'	a	<u>6ο'</u> Δ		b	<u>Δ</u> 6ο'	a		$\frac{60'}{\Delta}$	1	b	$\frac{\Delta}{60'}$		a
t		d = 3	0° 0′			d=3	0° 3	 30′				d = 3	1°	0′			

\ b			a=3	0° ()′			C	<i>i</i> = 30	0° 3	0′				a = 3	31°	0′	5.	c	a
B	h	d	6ο' Δ	z	*	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	Z	t	<u>Δ</u> 6ο'	h	d	60' Δ	Z	*	$\frac{\Delta}{60'}$	$C \setminus$	B
9 45 40 47 48 49	37 38 39 40	46 32 18 4 49	1.30 1.30 1.30 1.33 1.33	39 40 41	14 44 15 47 21	0.50 .52 .53 .57	37 38 39 40	32 18 4 49 34	1.30 1.30 1.33 1.33	39 40 41	48 18 49 21 55	0.50 •52 •53 •57 •58	37 38 39 40	19 4 49 34 19	1.33 1.33 1.33 1.33 1.36	41 42	21 52 23 55 29	0.52 .52 .53 .57	45 44 43 42 41	63. 1 62.3 61.4 60.6 59.7
50 51 52 53 54	41 42 43 44	34 18 2 46 29	1.36 1.36 1.36 1.40 1.43	42 43 44	56 32 10 49 29	0.60 .63 .65 .67	41 42 43 44	18 2 46 29 12	1.36 1.36 1.40 1.40	42 43 44 45	30 6 44 23 4	0.60 .63 .65 .68	41 42 43	3 46 29 12 54	1.40 1.40 1.40 1.43 1.43	43 44 45	40 18 57 38	0.60 .63 .65 .68	40 39 38 37 36	58.8 57.9 57.0 56.0 55.1
55 56 57 58 59	45 46 47	53 35 16 56	1.43 1.43 1.46 1.50 1.50	45 46 47 48	55 40 27 16	0.73 •75 •78 •82 •83	45 46 47	54 35 16 57 37	1.46 1.46 1.46 1.50 1.54	46 47 48	46 30 15 2 50	0.73 .75 .78 .80 .83	44 45 46 47	36 17 58 38 17	1.46 1.46 1.50 1.54 1.54	46 47 48 49	20 4 49 35 24	0.73 .75 .77 .82 .83	35 34 33 32 31	54.1 53.0 52.0 50.9 49.8
60 61 62 63 64	48 49 50 51	36 15 53 30 7	1.54 1.58 1.62 1.62 1.67	49 50 51 52	6 59 53 49 48	0.88 .90 .93 .98	48 49 50	16 54 32 9 45	1.58 1.58 1.62 1.67 1.71	49 50 51 52 53	40 33 27 23 21	0.88 .90 .93 .97	48 49 50	56 34 11 48 24	1.58 1.62 1.62 1.67 1.71	50 51 52 53	14 6 0 56 53	0.87 .90 .93 .95 1.00	30 29 28 27 26	48.7 47.5 46.3 45.1 43.9
65 66 67 68 69	52 53	43 18 52 25 57	1.71 1.76 1.82 1.88 1.94	53 54 55 57 58	48 50 55 1	1.03 1.08 1.10 1.15 1.18	51 52 53	20 55 29 1 33	1.71 1.76 1.88 1.88	54 55 56 57 58	21 23 27 33 41	1.03 1.07 1.10 1.13 1.18	51 52 53	59 33 6 38 9	1.76 1.82 1.88 1.94 2.00	54 55 56 58 59	53 55 58 3	1.03 1.05 1.08 1.13 1.17	25 24 23 22 21	42.6 41.3 39.9 38.5 37.1
70 71 72 73 74	54 55 56	28 58 27 55 21	2.00 2.07 2.14 2.31 2.40	59 60 61 63 64	21 35 51 9 29	I.23 I.27 I.30 I.33 I.37	54 55	4 33 2 29 55	2.07 2.07 2.22 2.31 2.40	59 61 62 63 64	52 4 19 36 55	1.20 1.25 1.28 1.32 1.37	54 55	39 8 36 3 29	2.07 2.14 2.22 2.31 2.50	60 61 62 64 65	21 33 47 3 21	1.20 1.23 1.27 1.30 1.35	20 19 18 17 16	35.6 34.2 32.6 31.1 29.5
75 76 77 78 79	5 <i>7</i>	58 2.07 60 35 1 27 2.14 61 51 1 55 2.31 63 9 1 5 21 2.40 64 29 1 46 2.50 65 51 1 10 2.61 67 16 1 33 2.86 68 43 1 54 3.16 70 12 1					56 57	20 43 5 26 45	2.61 2.73 2.86 3.16 3.33	66 67 69 70 72	17 40 6 33 3	1.38 1.43 1.45 1.50 1.52	56 57	53 16 38 58 17	2.61 2.73 3.00 3.16 3.33	66 68 69 70 72	42 4 29 55 23	1.37 1.42 1.43 1.47 1.50	15 14 13 12 11	27.8 26.2 24.5 22.7 21.0
80 81 82 83 84	59	31 48 3 16 28	3.53 4.00 4.62 5.00 6.00	73 74 76 78 79	16 50 27 5 44	1.57 1.62 1.63 1.65 1.68	58	3 19 34 47 58	3.75 4.00 4.62 5.45 6.00	73 75 76 78 79	34 7 42 18 56	1.55 1.58 1.60 1.63 1.65	58	35 51 5 18 29	3.75 4.29 4.62 5.45 6.67	73 75 76 78 80	53 24 57 32 8	1.52 1.55 1.58 1.60 1.62	9 8 7 6	19.2 17.3 15.5 13.6 11.7
85 86 87 88 89		38 46 52 56 59	7.50 10.0 15.0 20.0 60.0	81 83 84 86 88	25 7 49 32 16	1.70 1.70 1.72 1.73 1.73	59	8 16 22 26 29	7.50 10.0 15.0 20.0 60.0	81 83 84 86 88	35 15 55 36 18	1.67 1.68 1.70 1.70		38 46 52 56 59	7.50 10.0 15.0 20.0 60.0	81 83 85 86 88	45 23 I 40 20	1.63 1.63 1.65 1.67 1.67	5 4 3 2 1	9.8 7.8 5.9 3.9 2.0
90	60	0		90	0		_	30		90	0		59	0		90	0		0	0.0
$ _{t}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	_	a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	-	a
			d = 3	30°	0′				d = 3	0° 3	30′				d = 3	31° ()′			

\ b	C	<i>i</i> = 3	1° 30′			a=3	2° (0′			a=3	2° 30′		\ c	a
$B \setminus$	h	$\frac{60'}{\Delta}$	Z^{t}	$\frac{\Delta}{60'}$	h d	<u>6ο′</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	$\frac{1}{\Delta}$	Z	$\frac{\Delta}{60'}$	$C \setminus$	β
0 1 2 3 4	0 0 51 1 42 2 34 3 25	1.18 1.18 1.15 1.18	31 30 30 31 32 34	0.00	0 0 51 1 42 2 33 3 23	1.18 1.18 1.18 1.20 1.18	32	0 0 1 2 4	0.00 .02 .02 .03	5 1 4 2 3 3 2	1.18	32 30 30 31 32 32	.02	90 89 88 87 86	90.0 89.5 88.9 88.4 87.9
5 6 78 9	4 16 5 7 58 6 49 7 40	1.18 1.18 1.18 1.18	36 38 41 45 49	0.03 .05 .07 .07	4 14 5 5 56 6 47 7 37	1.18 1.18 1.18 1.20 1.18		6 8 11 15 19	0.03 .05 .07 .07	4 I 5 5 6 4 7 3	1.18 1.20 1.18	39 42 41 49	.05	85 84 83 82 81	87.3 86.8 86.3 85.7 85.2
10 11 12 13 14	8 31 9 22 10 13 11 4 54	1.18 1.18 1.18 1.20 1.18	54 59 32 4 10 17	0.08 .08 .10 .12	8 28 9 19 10 9 11 0 50	1.18 1.20 1.18 1.20 1.18		24 29 34 40 47	0.08 .08 .10 .12	8 2 9 10 10 6 11 40	I.20 I.20 I.20	33	.10	80 79 78 77 76	84.7 84.1 83.6 83.0 82.5
15 16 17 18 19	12 45 13 36 14 26 15 17 16 7	1.18 1.20 1.18 1.20 1.20	24 31 39 48 57	0.12 .13 .15 .15	12 41 13 31 14 21 15 12 16 2	1.20 1.20 1.18 1.20 1.20	33	54 2 10 18 27	0.13 .13 .13 .15	12 30 13 20 14 10 15 0	1.20 1.20 1.20	22 32 49 55	.13	75 74 73 72 71	81.9 81.4 80.8 80.2 79.7
20 21 22 23 24	57 17 47 18 37 19 27 20 17	I.20 I.20 I.20 I.20 I.20	33 7 17 28 39 51	0.17 .18 .18 .20	52 17 42 18 31 19 21 20 11	I.20 I.22 I.20 I.20 I.20	34	37 48 59 10 22	0.18 .18 .18 .20	16 4 17 3 18 2 19 1 20	5 1.22 5 1.22	34 19 30 4 51	.18	70 69 68 67 66	79.1 78.5 77.9 77.3 76.7
25 26 27 28 29	2I 7 57 22 47 23 36 24 25	I.20 I.20 I.22 I.22 I.22	34 4 17 31 46 35 1	0.22 .23 .25 .25	2I 0 49 22 38 23 27 24 16	I.22 I.22 I.22 I.22 I.22	35	35 48 2 19 33	0.22 .23 .25 .27 .27	5 2I 4 22 3 23 2 24	2 1.22 I 1.22	34	1 .25	65 64 63 62 61	76.1 75.5 74.9 74.3 73.6
30 31 32 33 34	25 14 26 3 52 27 40 28 29	1.22 1.22 1.25 1.22 1.25	17 34 51 36 9 28	0.28 .28 .30 .32 .33	25 5 54 26 42 27 30 28 18	I.22 I.25 I.25 I.25 I.25	36 37	49 6 23 41 0	0.28 .28 .30 .32 .33	5 25 4 26 3 27 2 28	5 1.25 3 1.25	37 1 33 33 35 35 35 35 35 35 35 35 35 35 35	7 .30 5 .30 3 .32	59 58 57 56	73.0 72.3 71.7 71.0 70.3
35 36 37 38 39	29 17 30 5 53 31 40 32 27	1.25 1.25 1.28 1.28 1.28	48 37 9 30 52 38 15	0.35 -35 -37 -38 -40	29 6 54 30 41 31 28 32 15	1.25 1.28 1.28 1.28 1.28	38	20 41 2 25 48	0.35 •35 •38 •38 •40	5 29 4 30 3 31 1 32	3 1.28	38 I 38 I 39 2	3 ·37 5 ·37 7 ·40	55 54 53 52 51	69.6 68.9 68.2 67.5 66.8
40 41 42 43 44	33 14 34 1 47 35 33 36 19	1.28 1.30 1.30 1.30 1.30	39 39 5 31 58 40 26	0.43 .43 .45 .47	33 2 48 34 34 35 20 36 6		39 40	37 4 31 59	0.42 •45 •45 •47 •48	33. 3 34. 2 35. 5	6 1.30	40 10	·43 ·47 4 ·47	50 49 48 47 46	66.0 65.3 64.5 63.7 62.9
45	37 5		5.5		51		41	28		36 3		42	1	45	62.1
	а	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	а	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	а	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$		a
t	-1-	d = 3	1° 30′			d = 3	2° (0′			d = 3	2° 30′			

\ b		a=3	1° 30′				a=3	2° (0′			(a=3	2° 3	0′		\ c	a
$B \setminus$	h d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
45 40 47 48 49	37 5 50 38 35 39 19 40 3	1.33 1.33 1.36 1.36 1.36	40 5 41 2 5 42 2 43	5 .52	36 37 38 39	51 36 20 4 48	1.33 1.36 1.36 1.36 1.40	41 42 43	28 58 30 2 36	0.50 •53 •53 •57 •58	36 37 38 39	37 21 5 49 32	1.36 1.36 1.36 1.40 1.40	43 44	31 36 10	0.50 •53 •55 •57 •58	° 45 44 43 42 41	62.1 61.2 60.4 59.5 58.6
50 51 52 53 54	47 41 30 42 13 55 43 37	1.40 1.43 1.43 1.46	44 I. 5 45 3 46 I	4 .63 2 .65 1 .68	40 41 42 43	31 14 56 38 19	1.40 1.43 1.43 1.46 1.46	44 45 46	48 26 5 45	0.62 .63 .65 .67	40 41 42 43	15 57 39 21 2	1.43 1.43 1.43 1.46 1.50	45 46 47	45 21 59 38 18	0.60 .63 .65 .67	40 39 38 37 36	57.7 56.8 55.9 54.9 53.9
55 56 57 58 59	44 18 59 45 39 46 19 58	1.46 1.50 1.50 1.54 1.58	47 3 48 2 49 5	7 .75 .78 .80	44 45 46	0 40 20 59 38	1.50 1.50 1.54 1.54 1.58	47 48 49 50	27 10 55 42 30	0.72 •75 •78 •80 •83	44 45 46	42 22 I 40 I8	1.50 1.54 1.54 1.58 1.62	48 49 50 51	0 43 28 15 3	0.72 •75 •78 •80 •83	35 34 33 32 31	52.9 51.8 50.8 49.7 48.6
60 61 62 63 64	47 36 48 13 50 49 26 50 1	1.62 1.62 1.67 1.71 1.71	50 4 51 3 52 3 53 2 54 2	9 .9c 3 .92 8 .95	47 48 49	16 53 29 5 40	1.62 1.67 1.67 1.71 1.76	51 52 53 54	20 12 5 0 57	0.87 .88 .92 .95 .98	47 48 49	55 32 8 43 17	1.62 1.67 1.71 1.76 1.76	52 53 54 55	53 44 37 32 28	0.85 .88 .92 .93 .97	30 29 28 27 26	47.5 46.3 45.1 43.9 42.6
65 66 67 68 69	36 51 10 42 52 14 45	1.76 1.88 1.88 1.94 2.00	55 2 56 2 57 2 58 3 59 4	1.05 1.08 1.12	50 51 52	14 47 19 50 21	1.82 1.88 1.94 1.94 2.07	55 56 57 59 60	56 56 59 4	1.00 1.05 1.08 1.10	50 51	51 24 56 27 56	1.82 1.88 1.94 2.07 2.07	56 57 58 59 60	26 27 29 33 39	1.02 1.03 1.07 1.10	25 24 23 22 21	41.3 40.0 38.7 37.3 35.9
70 71 72 73 74	53 15 44 54 11 38 55 3	2.07 2.22 2.22 2.40 2.50	60 50 62 63 1. 64 30 65 4	I I.22 4 I.27 D I.28	53 54	50 18 45 11 36	2.14 2.22 2.31 2.40 2.50	61 62 63 64 66	18 29 41 56 12	1.18 1.20 1.25 1.27 1.30	52 53 54	25 53 20 46 10	2.14 2.22 2.31 2.50 2.61	61 62 64 65 66	46 56 8 21 36	I.17 I.20 I.22 I.25 I.28	20 19 18 17 16	34·5 33.0 31·5 30.0 28.4
75 76 77 78 79	27 50 56 11 31 49	2.61 2.86 3.00 3.33 3.53	67 68 2: 69 50 71 1 72 4	1.42 5 1.45	55 56	0 22 43 3 21	2.73 2.86 3.00 3.33 3.53	67 68 70 71 73	30 50 12 36 1	1.33 1.37 1.40 1.42 1.45	55	33 55 16 35 53	2.73 2.86 3.16 3.33 3.53	67 69 70 71 73	53 12 33 56 20	1.32 1.35 1.38 1.40 1.42	15 14 13 12 11	26.8 25.2 23.5 21.9 20.1
80 81 82 83 84	57 6 22 36 49 58 0	3.75 4.29 4.62 5.45 6.67	74 I 75 4 77 I: 78 4 80 I	1 1.52 2 1.55 5 1.57	5 <i>7</i>	38 53 7 19 30	4.00 4.29 5.00 5.45 6.67	74 75 77 78 80	28 57 27 58 30	1.48 1.50 1.52 1.53 1.57	56 5 <i>7</i>	10 25 38 50 1	4.00 4.62 5.00 5.45 6.67	74 76 77 79 80	45 12 41 10 41	1.45 1.48 1.48 1.52 1.53	10 9 8 7 6	18.4 16.6 14.9 13.0 11.2
85 86 87 88 89	9 16 22 27 29	8.57 10.0 12.0 30.0 60.0	81 54 83 30 85 4 86 4 88 2:	1.62 7 1.62 1 1.63		39 47 53 57 59	7.50 10.0 15.0 30.0 60.0			1.57 1.58 1.58 1.60		10 17 23 27 29	8.57 10.0 15.0 30.0 60.0			1.53 1.55 1.57 1.57 1.57	5 4 3 2 1	9·4 7·5 5·6 3·8 1·9
90	30		90		58	0		90	0			30		90	0		0	0.0
=	a	<u>6ο'</u> Δ	b	$\frac{\Delta}{\epsilon o'}$	a	ı	<u>6ο′</u> Δ	1	b	Δ 60'	0	ı	<u>6ο'</u> Δ	1	5	<u>Δ</u> 60'		a
t	(d=3	l° 30′	1			d=3	2° () _′			C	l=32	2° 3	0′			

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1	i				1									1/	1
b	,	a=3	33° 0′			a=3	3° 8	30′			a = 3	84° 0′		$\setminus c$	a
$B \setminus$	h d	<u>6ο′</u> Δ	Z	$\frac{\Delta}{60'}$	h d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h d	60' <u>A</u>	Z	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	0 0 50 1 41 2 31 3 21	I.20 I.18 I.20 I.20 I.18	33 0	.02	0 0 50 1 40 2 30 3 20	I.20 I.20 I.20	33		0.00	0 0 50 1 39 2 29 3 19	I.22 I.20 I.20		0.00 0.02 1.02 2.03 4.03	90 89 88 87 86	90.0 89.4 88.9 88.3 87.8
5 6 78 9	4 12 5 2 52 6 42 7 32	I.20 I.20 I.20 I.20 I.20	12	.05	4 10 5 0 50 6 40 7 30	I.20 I.20 I.20		36 39 42 46 50	0.05 .05 .07 .07	4 58 5 48 6 38 7 27	I.20	100	2 .07	85 84 83 82 81	87.2 86.7 86.1 85.6 85.0
10 11 12 13 14	8 22 9 12 10 2 52 11 42	I.20 I.20 I.20 I.20 I.20	24 29 35 41 48	.IO .IO	8 20 9 9 59 10 49 11 38	1.22	34	54 59 5 11 18	0.08 .10 .10 .12	8 17 9 6 56 10 45 11 34	I.22 I.22	30 31 41 48	.08	80 79 78 77 76	84.4 83.9 83.3 82.7 82.2
15 16 17 18 19	12 32 13 22 14 12 15 1 51	I.20 I.20 I.22 I.20 I.22	34 3 11 20 29	.13	12 28 13 17 14 7 56 15 45	I.22 I.20 I.22 I.22 I.22	35	33 41 50 0	0.13 .13 .15 .17	12 23 13 13 14 2 51 15 40	I.22 I.22	35 2 12 21 30	1 .13 2 .15 1 .15	75 74 73 72 71	81.6 81.0 80.4 79.8 79.2
20 21 22 23 24	16 40 17 29 18 19 19 8 57	I.22 I.20 I.22 I.22 I.22	35 49 35 12 24	.18	16 34 17 23 18 12 19 1 50	I.22 I.22 I.22 I.22 I.25		10 20 31 43 55	0.17 .18 .20 .20	16 28 17 17 18 6 54 19 42	I.22 I.22 I.25 I.25 I.25	36 2 26	.18	70 69 68 67 66	78.6 78.0 77.4 76.8 76.2
25 26 27 28 29	20 46 21 34 22 23 23 11 59	1.25 1.22 1.25 1.25 1.25	37 51 36 20 36	.25	20 38 21 27 22 15 23 3 51	I.22 I.25 I.25 I.25 I.25	36 37	8 22 36 51 7	0.23 .23 .25 .27	20 30 21 18 22 6 54 23 42	1.25 1.25 1.25 1.25 1.25	37 37 23 38	.25	65 64 63 62 61	75.6 74.9 74.3 73.6 73.0
30 31 32 33 34	24 47 25 35 26 23 27 11 58	1.25 1.25 1.25 1.28 1.28	45	.30	24 39 25 26 26 13 27 0 47	1.28 1.28 1.28 1.28 1.28	38	23 40 58 17 36	0.28 .30 .32 .32 .33	24 29 25 16 26 3 50 27 37	1.28 1.28 1.28 1.28 1.28	38 12 30 49 39	30 .32	60 59 58 57 56	72.3 71.7 71.0 70.3 69.6
35 36 37 38 39	28 45 29 32 30 19 31 5 51	11 1.28 45 .3 58 1.28 38 4 .3 45 1.28 24 0.3 32 1.28 45 .3 19 1.30 39 7 .3 5 1.30 30 .3			28 34 29 21 30 7 53 31 39	1.28 1.30 1.30 1.30 1.30	39 40	56 17 39 2 25	0.35 .37 .38 .38 .42	28 24 29 10 56 30 42 31 27	1.30 1.30 1.30 1.33 1.33	28 49 40 11 34 57	·37 ·38 ·38	55 54 53 52 51	68.9 68.1 67.4 66.7 65.9
40 41 42 43 44	32 37 33 23 34 8 53 35 38	1.30 1.33 1.33 1.33 1.36	40 17 43 41 9 36 42 5	.48	32 25 33 10 55 34 40 35 24		4I 42	50 15 41 9 37	0.42 •43 •47 •47 •48	32 12 57 33 42 34 26 35 10	1.33 1.33 1.36 1.36 1.40		·45 ·45 ·48	50 49 48 47 46	65.2 64.4 63.6 62.8 61.9
45	36 22	12	34		36 8	- 1	43	6		53		39)	45	61.1
	a	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	а	60' Δ	1	b	$\frac{\Delta}{60'}$	а	60' Δ	b	$\frac{\Delta}{60'}$		a
t	d	l=33	3° 0′	,	(d=33	3° 3	0′			d=3	4° 0′			

					_						_	==		_			1	1.
$\setminus b$		a = 3	3° 0′			a	= 38	3° 3	0′				a=3	4° ()′		$\setminus c$	a
B	h d	6ο' Δ	Z	$t \mid \frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	z	t	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	Z	t	<u>∆</u> 60'	$C \setminus$	$\beta \setminus$
9 45 46 47 48 49	36 22 37 6 50 38 33 39 16	1.36 1.36 1.40 1.40	43 3	4 0.50 4 .53 6 .55 9 .57 .3	36 37 38 39	8 52 35 18 0	1.36 1.40 1.40 1.43 1.43	43 44 45	6 37 8 41 15	0.52 .52 .55 .57	35 36 37 38	53 36 19 2 44	I.40 I.40 I.40 I.43	43 44 45	39 9 41 14 48	• 53 • 55 • 57 • 58	° 45 44 43 42 41	61.1 60.3 59.4 58.5 57.6
50 51 52 53 54	59 40 41 41 22 42 3 44	1.43 1.46 1.46 1.46 1.50	46 3 47 I	4 .63 2 .65	40 41 42	42 24 5 45 25	1.43 1.46 1.50 1.50	46 47 48	50 27 4 43 23	0.62 .62 .65 .67	39 40 41 42	26 7 48 28 7	1.46 1.46 1.50 1.54 1.54	46 47 48	23 59 37 16 56	0.60 .63 .65 .67	40 39 38 37 36	56.7 55.7 54.8 53.8 52.8
55 56 57 58 59	43 24 44 3 42 45 20 58	1.54 1.54 1.58 1.58 1.62	48 3 49 1 50 4 51 3	6 .75 I .77 7 .80	43 44 45	5 44 22 0 37	1.54 1.58 1.58 1.62 1.62	49 50 51 52	5 48 33 19 7	•.72 •.75 •.77 •.80	43 44 45	46 25 3 40 17	1.54 1.58 1.62 1.62 1.67	49 50 51 52	37 20 5 51 38	•.72 •75 •77 •78 •82	35 34 33 32 31	51.8 50.7 49.6 48.5 47.4
60 61 62 63 64	46 35 47 11 46 48 21 55	1.67 1.71 1.71 1.76 1.82	55		46 47 48	50 25 59 33	1.67 1.71 1.76 1.76 1.88	53 54 55 56	56 47 39 33 29	0.85 .87 .90 .93	46 47 48	53 28 3 37 10	1.71 1.71 1.76 1.82 1.88	53 54 55 56	27 18 10 4 59	0.85 .87 .90 .92 .95	30 29 28 27 26	46.3 45.1 43.9 42.7 41.5
65 66 67 68 69	49 28 50 I 32 51 2 32	1.82 1.94 2.00 2.00 2.07		7 1.02	49 50 51	37 8 38 7	1.88 1.94 2.00 2.07 2.14	57 58 59 60 61	26 26 27 30 34	1.00 1.02 1.05 1.07 1.10	49 50	42 14 44 14 43	1.88 2.00 2.00 2.07 2.22	57 58 59 60 62	56 55 57	0.98 1.00 1.03 1.07 1.10	25 24 23 22 21	40.2 38.9 37.6 36.2 34.8
70 71 72 73 74	52 1 28 54 53 19 43	2.22 2.31 2.40 2.50 2.61	64 3 65 4	3 1.15 2 1.18 3 1.22 6 1.23 0 1.27	52 53	35 28 28 53	2.22 2.31 2.40 2.50 2.73	62 63 64 66 67	40 48 58 10 24	1.13 1.17 1.20 1.23 1.25	51 52	37 3 27 50	2.22 2.31 2.50 2.61 2.73	63 64 65 66 67	7 14 23 34 46	1.12 1.15 1.18 1.20 1.23	20 19 18 17 16	33.4 32.0 30.5 29.0 27.5
75 70 77 78 79	54 6 28 48 55 7 25	2.73 3.00 3.16 3.33 3.75	69 3 70 5 72 I	6 1.30 4 1.33 4 1.35 5 1.38 1.40	54	39 1 21 39 56	2.73 3.00 3.33 3.53 3.75	68 69 71 72 73	39 55 14 34 55	1.27 1.32 1.33 1.35 1.38	53 54	33 53 11 28	2.86 3.00 3.33 3.53 3.75	69 70 71 72 74	0 16 33 52 12	1.27 1.28 1.32 1.33 1.37	15 14 13 12 11	25.9 24.3 22.7 21.1 19.4
80 81 82 83 84	41 56 56 9 21 31	4.00 4.62 5.00 6.00 6.67	77 5 79 2	2 I.42 7 I.45 4 I.47 2 I.48 I I.50	55 56	12 27 40 52 2	4.00 4.62 5.00 6.00 7.50	75 76 78 79 81	18 42 7 34 2	1.40 1.42 1.45 1.47 1.47	55	44 58 11 22 32	4.29 4.62 5.45 6.00 6.67	75 76 78 79 81	34 57 21 46 12	1.38 1.40 1.42 1.43 1.43	10 9 8 7 6	17.7 16.0 14.3 12.5 10.8
85 86 87 88 89	40 47 53 57 59	8.57 10.0 15.0 30.0 60.0	83 5 85 2 86 5	1 1.52 1.52 1.53 1.53 1.55		10 17 23 27 29	8.57 10.0 15.0 30.0 60.0	82 83 85 86 88	30 59 29 59 29	1.48 1.50 1.50 1.50 1.50		41 48 53 57 59	8.57 12.0 15.0 30.0 60.0	82 84 85 87 88	38 6 34 2 31	1.47 1.47 1.47 1.48 1.48	5 4 3 2 1	9.0 7.2 5.4 3.6 1.8
90	57 0		90	0		30		90	0		56	0		90	0		0	0.0
$ _t$	a _.	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	(ı	6ο' Δ		b	<u>Δ</u> 6ο'	(a	$\frac{60'}{\Delta}$		b	<u>Δ</u> 6ο'	1	a
		d = 3	3° 0′			(d = 3	3° 3	30′				d=3	4°	0′			

\ b	1 0	a=3	4° 3	80′				a=3	5°	0′				i = 3	5° 9	30′		\setminus_{c}	\ a
	d	60'		t	Δ	_	\overline{d}	60'		$\frac{1}{t}$	Δ	-	d	60'		t	Δ	\'	
$B\setminus$	h	Δ	$ z\rangle$		60'	h	/	Δ	Z	<u>`</u>	60'	h	13.	Δ	z	/	60'	$C \setminus$	$\beta \setminus$
0 1 2 3 4	0 0 49 1 39 2 28 3 18	I.22 I.20 I.22 I.20 I.22	34	30 30 31 32 34	0.00 .02 .02 .03	0 I 2 3	49 38 27 17	I.22 I.22 I.22 I.20 I.20	35	0 0 1 2 4	0.00 .02 .02 .03	0 I 2 3	49 38 27 15	I.22 I.22 I.22 I.25 I.25	35	30 30 31 32 34	0.00	90 89 88 87 86	90.0 89.4 88.9 88.3 87.7
5 6789	4 7 57 5 46 6 35 7 24	I.20 I.22 I.22 I.22 I.20		36 39 42 46 50	.05 .05 .07 .07	4 5 6 7	55 44 33 22	I.22 I.22 I.22 I.22 I.22		6 9 12 16 20	0.05 .05 .07 .07	4 5 6 7	4 53 42 30 19	I.22 I.22 I.25 I.22 I.22		36 39 42 46 50	0.05 .05 .07 .07	85 84 83 82 81	87.1 86.6 86.0 85.4 84.8
10 11 12 13 14	8 14 9 3 52 10 41 11 30	I.22 I.22 I.22 I.22 I.22	35	55 6 12 19	0.08 .10 .10 .12	9 10 11	0 48 37 26	I.22 I.25 I.22 I.22 I.25		25 30 36 42 49	0.08 .10 .10 .12	9 10 11	8 56 45 33 22	I.25 I.22 I.25 I.22 I.25	36	55 0 6 12 19	0.08 .10 .10 .12	80 79 78 77 76	84.2 83.6 83.0 82.5 81.9
15 16 17 18 19	12 19 13 8 57 14 45 15 34	I.22 I.22 I.25 I.22 I.25	36	26 34 42 51	0.13 .13 .15 .17	12 13 14 15	3 51 40 28	I.22 I.25 I.22 I.25 I.25	36	56 4 13 22 31	0.13 .15 .15 .15	13 14 15	58 46 34 22	I.25 I.25 I.25 I.25 I.25	37	27 35 43 52 2	0.13 .13 .15 .17	75 74 73 72 71	81.3 80.7 80.1 79.4 78.8
20 21 22 23 24	16 22 17 11 59 18 47 19 35	1.22 1.25 1.25 1.25 1.25		11 22 33 45 57	0.18 .18 .20 .20	16 17 18 19	16 4 52 40 28	1.25 1.25 1.25 1.25 1.25	37	41 52 4 16 28	0.18 .20 .20 .20	16 17 18 19	10 58 45 33 20	1.25 1.28 1.25 1.28 1.28		12 23 34 46 59	0.18 .18 .20 .22	70 69 68 67 66	78.2 77.6 77.0 76.3 75.7
25 26 27 28 29	20 23 21 11 58 22 46 23 33	1.25 1.28 1.25 1.28 1.28	37	10 24 39 54 10	0.23 .25 .25 .27 .27	20 21 22 23	3 50 37 24	1.25 1.28 1.28 1.28 1.28	38	41 55 10 25 41	0.23 .25 .25 .27 .27	20 21 22 23	7 54 41 28 15	1.28 1.28 1.28 1.28 1.30	38	12 26 41 56 12	0.23 .25 .25 .27 .28	65 64 63 62 61	75.0 74.4 73.7 73.0 72.4
30 31 32 33 34	24 20 25 7 54 26 40 27 26	1.28 1.28 1.30 1.30 1.30	39	26 43 1 20 40	0.28 .30 .32 .33 .33	24 25 26 27	57 44 30 16	1.30 1.28 1.30 1.30 1.30	39 40	57 15 33 52 11	0.30 •30 •32 •32 •33	24 25 26 27	1 47 33 19 5	I.30 I.30 I.30 I.30 I.33	40	29 46 4 23 43	0.28 .30 .32 .33	59 58 57 56	71.7 71.0 70.3 69.6 68.9
35 36 37 38 39	28 12 58 29 44 30 29 31 14	1.30 1.33 1.33 1.33	40	0 21 43 6 30	0.35 •37 •38 •40 •40	28 29 30 31	2 47 32 17 2	1.33 1.33 1.33 1.33 1.36	41 42	31 52 14 37	0.35 •37 •38 •40 •42	28 29 30	50 35 20 5 49	1.33 1.33 1.33 1.36 1.36	41	3 24 46 9 33	0.35 .37 .38 .40 .42	55 54 53 52 51	68.1 67.4 66.6 65.9 65.1
40 41 42 43 44	59 32 44 33 28 34 12 56	1.33 1.36 1.36 1.36 1.40	42	54 19 46 13 42	•45 •45 •48 •48	32 33 34	46 30 14 58 41	1.36 1.36 1.36 1.40 1.40		26 51 18 45 14	0.42 •45 •45 •48 •48	31 32 33 34	33 17 0 43 26	1.36 1.40 1.40 1.40 1.40	43 44	58 23 50 17 45	0.42 •45 •45 •47	50 49 48 47 46	64.3 63.5 62.7 61.9 61.0
45	35 39		44	11		35	24		H	43		35	9		45	15		45	60.2
,	a	$\left\ \frac{60'}{\Delta} \right\ b \left\ \frac{\Delta}{60'} \right\ $					a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a	60' Δ		b	$\frac{\Delta}{60'}$		a
$\mid t \mid$		d=3	4° 3	0′				d=3	5°	0′				d=3	5° 3	30′			

\ b	a	a = 34	1° 30′				a=3	5° (0′			0	i = 3	5° 3	80′		\ c	a
$B \setminus$	h	$\frac{60'}{\Delta}$	Z t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
o 45 46 47 48 49	35 39 36 22 37 4 46 38 28	1.40 1.43 1.43 1.43	44 11 42 45 13 46 46 20	0.52 .52 .55 .57 .58	35 36 37 38	24 6 48 30 11	1.43 1.43 1.43 1.46 1.46	44 45 46	43 14 45 18 52	0.52 .52 .55 .57 .58	35 36 37	9 51 33 14 55	1.43 1.43 1.46 1.46 1.50	45 46 47	15 45 17 50 24	0.50 •53 •55 •57 •58	° 45 44 43 42 41	60.2 59.3 58.4 57.5 56.6
50 51 52 53 54	39 9 50 40 30 41 10 49	1.46 1.50 1.50 1.54 1.54	55 47 31 48 9 48 49 28	0.60 .63 .65 .67	39 40 41	52 32 12 52 31	1.50 1.50 1.50 1.54 1.58	47 48 49	27 3 41 19 59	0.60 .63 .63 .67	38 39 40 41	35 15 54 33 12	1.50 1.54 1.54 1.54 1.58	48 49 50	59 35 12 51 31	0.60 .62 .65 .67	40 39 38 37 36	55.6 54.7 53.7 52.7 51.7
55 56 57 58 59	42 28 43 6 43 44 20 56	1.58 1.62 1.62 1.67 1.67	50 9 52 51 36 52 22 53 9	0.72 •73 •77 •78 .82	42 43 44	9 47 24 0 36	1.58 1.62 1.67 1.67 1.71	50 51 52 53	41 23 7 53 40	0.70 •73 •77 •78 •80	42 43 44	50 27 4 40 15	1.62 1.62 1.67 1.71	51 52 53 54	54 38 23 10	•.70 •73 •75 •78 •80	35 34 33 32 31	50.7 49.6 48.5 47.4 46.3
60 61 62 63 64	45 32 46 7 41 47 15 48	1.71 1.76 1.76 1.82 1.88	58 54 48 55 40 56 33 57 28	0.83 .87 .88 .92 .95	45 46 4 7	11 46 20 53 25	1.71 1.76 1.82 1.88 1.94	54 55 56 57	28 18 10 3 57	0.83 .87 .88 .90 .93	45 46 47	50 24 57 30 2	1.76 1.82 1.82 1.88 1.94	55 56 57 58	58 48 39 32 26	0.83 .85 .88 .90	30 29 28 27 26	45.2 44.0 42.8 41.6 40.4
65 66 67 68 69	48 20 51 49 21 50 50 18	1.94 2.00 2.07 2.14 2.22	58 25 59 23 60 23 61 25 62 28	0.97 1.00 1.03 1.05 1.08	48 49	56 27 56 25 53	1.94 2.07 2.07 2.14 2.22	58 59 60 61 62	53 51 50 51 54	0.97 .98 I.02 I.05 I.07	48 49	33 32 1 28	2.00 2.07 2.07 2.22 2.22	59 60 61 62 63	21 18 17 18 20	0.95 .98 1.02 1.03 1.05	25 24 23 22 21	39.1 37.8 36.5 35.2 33.8
70 71 72 73 74	45 51 11 36 52 0 23	2.31 2.40 2.50 2.61 2.73	63 33 64 39 65 47 66 57 68 9	I.10 I.13 I.17 I.20 I.22	50 51	20 46 10 34 57	2.31 2.50 2.50 2.61 2.86	63 65 66 67 68	58 4 11 20 31	1.10 1.12 1.15 1.18 1.20	50 51	55 20 44 8 30	2.40 2.50 2.50 2.73 2.86	64 65 66 67 68	23 28 35 43 52	1.08 1.12 1.13 1.15 1.18	20 19 18 17 16	32.4 31.0 29.5 28.1 26.6
75 76 77 78 79	53 6 25 43 54 0	2.86 3.16 3.33 3.53 4.00	69 22 70 37 71 53 73 10 74 29	1.25 1.27 1.28 1.32 1.33	52 53	18 38 57 15 31	3.00 3.16 3.33 3.75 4.00	69 70 72 73 74	43 56 11 28 45	1.22 1.25 1.28 1.28 1.32	52 53	51 11 30 47 3	3.00 3.16 3.53 3.75 4.00	70 71 72 73 75	30 30 45	1.22 1.23 1.25 1.27 1.30	15 14 13 12 11	25.0 23.5 21.9 20.3 18.7
80 81 82 83 84	15 29 42 53 55 3	4.29 4.62 5.45 6.00 7.50	75 49 77 11 78 33 79 57 81 21	I.37 I.37 I.40 I.40 I.42	54	46 0 13 24 33	4.29 4.62 5.45 6.67 7.50	76 77 78 80 81	4 24 46 8 31	1.33 1.37 1.37 1.38 1.38	54	18 31 43 54 4	4.62 5.00 5.45 6.00 7.50	76 77 78 80 81	19 38 58 18 40	I.32 I.33 I.33 I.37 I.37	10 9 8 7 6	17.1 15.4 13.8 12.1 10.4
85 86 87 88 89	11 18 23 27 29	8.57 12.0 15.0 30.0 60.0	82 46 84 12 85 39 87 6 88 33	I.43 I.45 I.45 I.45 I.45		41 48 53 57 59	8.57 12.0 15.0 30.0 60.0	82 84 85 87 88	54 19 44 9 34	I.42 I.42 I.42 I.42 I.43		12 18 23 27 29	10.0 12.0 15.0 30.0 60.0				5 4 3 2 1	8.7 7.0 5.2 3.5 1.7
90	30		90 0		55	0		90	0			30		90	0		0	0.0
4	a	$\left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60'} \right $				ı	60' ∆		b	$\frac{\Delta}{60'}$	0	ı	6ο' Δ		b	<u>Δ</u> 6ο'		a
t	0	l=34	4° 30′				d=3	5° ()′			d	l=38	5° 3	0′	1		

\ b		a = 3	6° 0)′			C	a = 3	6° 8	30′				a=3	7°	0′		\ c	a
$B \setminus$	h d	<u>6ο'</u> Δ	z	-	0/1	h	d	<u>6ο′</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 0 1 2 3 4	0 0 49 1 37 2 26 3 14	1.22 1.25 1.22 1.25 1.25	36	O	00 02 02 03	0 I 2 3	0 48 36 25 13	I.25 I.25 I.22 I.25 I.25	36	30 30 31 32 34	0.00	° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	0 48 36 24 12	1.25 1.25 1.25 1.25 1.25	37°	0 0 1 2 4	0.00	90 89 88 87 86	90.0 89.4 88.8 88.2 87.6
5 6 7 8 9	4 3 51 5 39 6 28 7 16	1.25 1.25 1.22 1.25 1.25		12 .	05 05 07 07 08	4 5 6 7	1 49 37 25 13	I.25 I.25 I.25 I.25 I.25		36 39 42 46 50	0.05 .05 .07 .07	4 5 6 7	59 47 35 23	1.25 1.25 1.25 1.25 1.25		6 9 12 16 20	0.05 .05 .07 .07	85 84 83 82 81	87.0 86.4 85.8 85.2 84.6
10 11 12 13 14	8 5 53 9 41 10 29 11 17	1.25 1.25 1.25 1.25 1.25		36 . 43 ·	08 10 12 12	9 10 11	1 49 37 25 13	I.25 I.25 I.25 I.25 I.25	37	55 1 7 13 20	0.10 .10 .10 .12	8 9 10	58 46 34 21 8	1.25 1.25 1.28 1.28 1.25		25 31 37 43 50	0.10 .10 .10 .12	80 79 78 77 76	84.0 83.4 82.8 82.2 81.6
15 16 17 18 19	12 5 53 13 41 14 29 15 16	1.25 1.25 1.25 1.28 1.28	37	13 .	13 13 15 17	13 14 15	0 48 36 23 10	I.25 I.25 I.28 I.28 I.28	38	27 35 44 53 3	0.13 .15 .15 .17	12 13 14 15	56 43 30 17 4	1.28 1.28 1.28 1.28 1.28	38	57 5 14 23 33	0.13 15 .15 .17	75 74 73 72 71	80.9 80.3 79.7 79.1 78.4
20 21 22 23 24	16 4 51 17 38 18 25 19 12	5 4 1.28 43 5 5 1 1.28 54 7 38 1.28 38 5 8 25 1.28 17 1 12 1.28 30 5 9 1.28 43 0 5 9 1.28 57 3 3 1.30 39 12					57 44 31 18	1.28 1.28 1.28 1.28 1.28	39	13 24 36 48 1	0.18 .20 .20 .22 .22	16 17 18	51 38 25 11 57	1.28 1.28 1.30 1.30 1.30	39	44 55 6 18 31	0.18 .18 .20 .22	70 69 68 67 66	77.8 77.1 76.5 75.8 75.2
25 26 27 28 29	20 46	1.28	39	57 · · · · · · · · · · · · · · · · · · ·	23 25 25 27 28	20 21 22	52 38 24 10 56	1.30 1.30 1.30 1.30	40	14 28 43 58 14	0.23 .25 .25 .27 .28	19 20 21 22	43 29 15 1 47	1.30 1.30 1.30 1.30	40	45 59 13 29 45	0.23 .23 .27 .27 .28	65 64 63 62 61	74.5 73.8 73.1 72.5 71.8
30 31 32 33 34	51 24 37 25 23 26 9 54	1.30 1.30 1.30 1.33 1.33		35 54	28 30 32 33	23 24 25 26	42 27 13 58 43	I.33 I.30 I.33 I.33	41	31 48 6 25 45	0.28 .30 .32 .33 .35	23 24 25 26	32 17 2 47 32	1.33 1.33 1.33 1.33 1.36	4I 42	19 37 56 16	0.28 .30 .32 .33 .35	59 58 57 56	71.0 70.3 69.6 68.9 68.1
35 36 37 38 39	27 39 28 24 29 8 52 30 36	1.33 1.36 1.36 1.36 1.36	42	18 .	37 37 38 38 38	27 28 29 30	28 12 56 40 24	1.36 1.36 1.36 1.36 1.40	42	6 27 49 12 36	0.35 .37 .38 .40 .42	27 28 29 30	16 0 44 27 10	1.36 1.36 1.40 1.40	43	37 58 20 43 7	0.35 .37 .38 .40 .42	55 54 53 52 51	67.4 66.6 65.9 65.1 64.3
40 41 42 43 44	31 20 32 3 46 33 29 34 12	1.40 1.40 1.40 1.40 1.43	44	49	43 47 47 47	31 32 33	7 50 33 15 57	1.40 1.43 1.43 1.43	44	1 26 53 20 49	0.42 •45 •45 •48 •48	31 32 33	53 36 18 0 42	1.40 1.43 1.43 1.43 1.46	45 46	32 58 24 52 20	0.43 .43 .47 .47 .48	50 49 48 47 46	63.5 62.7 61.8 61.0 60.1
45	9 54		, ,	46		34	39		46	18	,	34	23		ď	49		45	59-3
	a	<u>€o'</u> Δ	b	6	2	a	t	$\frac{60'}{\Delta}$	1. 1	b	$\frac{\Delta}{60'}$	- 0	ı	$\frac{60'}{\Delta}$	1	Ь	<u>Δ</u> 6ο'		a
t	:	d = 3	6° 0	, ₁			á	l=3	6° 3	30′				d=3	7° (0′	0		

8			a = 3	6° ()′			a	ı = 36	3° 3	0′				a=3	7° (0′		\ c	\\ \ \ \ \ \ \ \ \ \ \ \ \ \
$B \setminus$	h	d	<u>6ο'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	C	$\beta \setminus$
45 46 47 48 49	34 35 36 37	54 35 16 57 38	1.46 1.46 1.46 1.46	45 46 47	46 17 49 21 55	0.52 •53 •53 •57 •58	34 35 36 37	39 20 1 41 21	1.46 1.46 1.50 1.50	46 47 48	18 48 20 53 26	0.50 •53 •55 •55 •55	34 35 36 37	23 4 44 24 4	1.46 1.50 1.50 1.50	46 47 48		0.52 .52 .55 .55	9 45 44 43 42 41	59·3 58·4 57·5 56.6 55.6
50 51 52 53 54	38 39 40	18 57 36 15 53	1.54 1.54 1.58 1.62	48 49 50 51	30 6 43 22 2	0.60 .62 .65 .67	38 39 40	1 40 18 56 34	1.54 1.58 1.58 1.58 1.62	49 50 51	37 14 52 32	0.60 .62 .63 .67	38 39 40	43 22 0 38 15	1.54 1.58 1.58 1.62 1.62	49 50 51 52	32 8 45 23 3	0.60 .62 .63 .67	39 38 37 36	54·7 53·7 52·7 51·7 50·7
55 56 57 58 59	41 42 43	30 7 43 19 54	1.62 1.67 1.67 1.71 1.71	52 53 54	43 25 9 54 40	•.7° •73 •75 •77 .8°	41 42 43	11 47 23 58 33	1.67 1.67 1.71 1.71 1.76	52 53 54 55	13 55 39 24 10	•.7° •73 •75 •77 •78	41 42 43	52 28 3 38 12	1.67 1.71 1.71 1.76 1.76	53 54 55	43 25 8 53 39	0.70 •72 •75 •77 •78	35 34 33 32 31	49.7 48.6 47.5 46.4 45.3
60 61 62 63 64	44 45 46	29 2 35 7 39	1.82 1.82 1.88 1.88 2.00	55 56 57 58	28 17 8 0 54	0.82 .85 .87 .90	44 45 46	7 40 13 45 16	1.82 1.82 1.88 1.94 2.00	56 57 58 59	57 46 36 28 21	0.82 .83 .87 .88	44 45	46 19 51 22 52	1.82 1.88 1.94 2.00 2.00	56 57 58 59	26 15 5 56 49	0.82 .83 .85 .88	30 29 28 27 26	44.1 43.0 41.8 40.6 39.4
65 66 67 68 69	47 48 49	9 39 8 36 3	2.00 2.07 2.14 2.22 2.31	59 60 61 62 63	49 46 44 44 45	0.95 •97 1.00 1.02 1.05	47 48	46 15 43 11 38	2.07 2.14 2.14 2.22 2.40	60 61 62 63 64	16 12 10 9 10	0.93 .97 .98 1.02	46 47 48	22 51 19 46 13	2.07 2.14 2.22 2.22 2.40	60 61 62 63 64	43 39 36 34 34	0.93 •95 •97 1.00 1.02	25 24 23 22 21	38.1 36.8 35.5 34.2 32.8
70 71 72 73 74	50	29 54 18 41 3	2.40 2.50 2.61 2.73 2.86	2.00 54 .92 2.00 59 49 0.95 2.07 60 46 .97 2.14 61 44 1.00 2.22 62 44 1.02 2.31 63 45 1.05 2.40 64 48 1.07 2.50 66 58 1.12 2.73 68 5 1.15				3 28 52 14 36	2.40 2.50 2.73 2.73 3.00	65 66 67 68 69	12 15 20 26 34	1.05 1.08 1.10 1.13 1.15	49 50	38 2 26 48 9	2,50 2,50 2,73 2,86 3.00	65 66 67 68 69	35 38 42 48 55	1.05 1.07 1.10 1.12 1.13	20 19 18 17 16	31.5 30.1 28.6 27.2 25.7
75 76 77 78 79	52	24 43 1 18 34	3.16 3.33 3.53 3.75 4.00	70 71 72 74 75	24 35 48 2 17	1.18 1.22 1.23 1.25 1.27	51 52	56 15 33 50 6	3.16 3.33 3.53 3.75 4.29	70 71 73 74 75	43 54 5 18 33	1.18 1.18 1.22 1.25 1.25	51	29 48 6 22 37	3.16 3.33 3.75 4.00 4.29	71 72 73 74 75	3 12 23 35 47	I.15 I.18 I.20 I.20 I.23	15 14 13 12 11	24.3 22.7 21.2 19.7 18.1
80 81 82 83 84	53	49 2 14 25 34	4.62 5.00 5.45 6.67 7.50	76 77 79 80 81	33 51 9 29 49	1.30 1.30 1.33 1.33	53	20 33 45 56 5	4.62 5.00 5.45 6.67 7.50	76 78 79 80 81	48 4 21 39 58	1.27 1.28 1.30 1.32 1.32	52	51 4 16 26 35	4.62 5.00 6.00 6.67 7.50	77 78 79 80 82	1 16 32 49 6	1.25 1.27 1.28 1.28 1.30	10 9 8 7 6	16.5 14.9 13.3 11.7 10.0
85 86 87 88 89		42 49 54 57 59	34 7.50 81 49 1.35 42 8.57 83 10 1.35 49 12.0 84 31 1.37 54 22.0 85 53 1.37 57 30.0 87 15 1.37 59 60.0 88 37 1.38					13 19 24 27 29	10.0 12.0 20.0 30.0 60.0	83 84 85 87 88	17 37 57 18 39	I.33 I.33 I.35 I.35 I.35		43 49 54 57 59	10.0 12.0 20.0 30.0 60.0	83 84 86 87 88	24 43 2 21 40	1.32 1.32 1.32 1.32 1.33	5 4 3 2 1	8.4 6.7 5.0 3.4 1.7
90	54	0		90	0			30		90	0		53	0		90	0		0	0.0
t		a	$\frac{60'}{\Delta}$		ь	<u>Δ</u> 6ο'		ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	11 6	a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	١.	a
			d=3	6° (0′			(d = 3	6° 3	80′	7			d = 3	87°	0′			.: .: .:

b		a=3	7° 3	0′				a = 3	88°	0′				a=3	8° 3	30′		c	\ a
$B \setminus$	h	<u>6ο'</u> Δ	z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	h	d	$\frac{\epsilon o'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$c \setminus$	β
0 I 2 3 4	0 0 48 1 35 2 23 3 10	1.25 1.28 1.25 1.28 1.25	37	30 30 31 32 34	0.00	0 I 2 3	6 47 35 22 9	1.28 1.25 1.28 1.28 1.28	38	0 0 1 2 4	0.00 .02 .02 .03	0 I 2 3	47 34 21 8	1.28 1.28 1.28 1.28 1.28	38	30 30 31 32 34	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.4 88.8 88.2 87.5
5 6 7 8 9	58 4 46 5 33 6 20 7 8	1.25 1.28 1.28 1.25 1.25		36 39 42 46 51	0.05 .05 .07 .08	4 5 6 7	56 44 31 18	1.25 1.28 1.28 1.28 1.28		6 9 12 16 21	0.05 .05 .07 .08	4 5 6 7	55 42 28 15 2	1.28 1.30 1.28 1.28 1.28		36 39 42 46 51	0.05 .05 .07 .08	85 84 83 82 81	86.9 86.3 85.7 85.1 84.4
10 11 12 13 14	55 8 42 9 30 10 17 11 4	1.28 1.25 1.28 1.28 1.28	38	56 1 7 13 20	0.08 .10 .10 .12	8 9 10	52 39 26 13 59	1,28 1,28 1,28 1,30 1,28		26 31 37 43 50	0.08 .10 .10 .12	8 9 10	49 35 22 8 55	1.30 1.28 1.30 1.28 1.30	39	56 1 7 14 21	0.08 .10 .12 .12	80 79 78 77 76	83.8 83.2 82.5 81.9 81.3
15 16 17 18 19	51 12 38 13 25 14 12 58	1.28 1.28 1.28 1.30 1.28	39	28 36 45 54 4	0.13 .15 .15 .17	11 12 13 14	46 33 19 6 52	1.28 1.30 1.28 1.30 1.30	39	58 6 15 24 34	0.13 .15 .15 .17	11 12 13 14	41 28 14 0 46	1.28 1.30 1.30 1.30 1.30	40	28 36 45 54 4	0.13 .15 .15 .17	75 74 73 72 71	80.6 80.0 79.3 78.7 78.0
20 21 22 23 24	15 45 16 31 17 17 18 3 49	1.30 1.30 1.30 1.30	40	14 25 37 49 2	0,18 .20 .20 .22 .22	15 16 17 18	38 24 10 56 42	1.30 1.30 1.30 1.30	40	44 55 7 19 32	0.18 .20 .20 .22 .23	15 16 17 18	32 17 3 48 34	I.33 I.30 I.33 I.30 I.33	41	15 26 38 50 3	0.18 .20 .20 .22 .22	70 69 68 67 66	77.4 76.7 76.0 75.4 74.7
25 26 27 28 29	19 35 20 21 21 7 52 22 37	1.30 1.30 1.33 1.33	41	15 29 44 0 16	0.23 .25 .27 .27 .28	19 20 21 22	27 13 58 43 28	1.30 1.33 1.33 1.33	41	46 0 15 30 46	0.23 .25 .25 .27 .28	19 20 21 22	19 4 49 34 18	1.33 1.33 1.36 1.36	42	16 30 45 1	0.23 .25 .27 .27 .28	65 64 63 62 61	74.0 73.3 72.6 71.9 71.2
30 31 32 33 34	23 22 24 7 52 25 36 26 20	1.33 1.33 1.36 1.36 1.36	42	33 50 8 27 47	0.28 .30 .32 .33 .35	23 24 25 26	12 57 41 25	1.33 1.36 1.36 1.36	42	39 58 18	0.30 .30 .32 .33	23 24 25	2 46 30 14 57	1.36 1.36 1.36 1.40 1.40	43	34 52 10 29 49	0.30 .30 .32 .33	60 59 58 57 56	70.4 69.7 69.0 68.2 67.4
35 36 37 38 39	27 4 48 28 31 29 14 57	1.36 1.40 1.40 1.40	43 44	8 29 51 14 38	0.35 •37 •38 •40 •42	27 28 29	52 35 18 1 44	I.40 I.40 I.40 I.40	44	39 0 22 45 9	0.35 .37 .38 .40 .42	26 27 28 29	40 23 6 48 30	1.40 1.43 1.43 1.43	44	10 31 53 16 40	0.35 .37 .38 .40 .42	55 54 53 52 51	66.7 65.9 65.1 64.3 63.5
40 41 42 43 44	30 40 31 22 32 4 45 33 26	0 1.43 45 3 0.42 2 1.43 28 44 4 1.46 55 47 5 1.46 46 23 47 1.46 51 48				30 31 32 33	26 8 49 30 11	1.43 1.46 1.46 1.46 1.46	46 47	34 0 26 53 22	•43 •45 •48 •48	31	54 35 16 56	1.43 1.46 1.46 1.50 1.50	46 47	5 31 57 24 53	•43 •45 •48 •48	50 49 48 47 46	62.7 61.8 61.0 60.1 59.3
45	34 7		47	20			52			51		33	36		48	22		45	58.4
t	a	$\frac{60'}{\Delta}$	l	,	$\frac{\Delta}{60'}$	а		$\frac{60'}{\Delta}$	i	6	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	1	5	$\frac{\Delta}{60'}$		a
	C	d = 37° 30′						d=3	8° ()′			d	1=38	3° 3	0′			

	b		C	a = 3	7° 8	80′				a = 3	88°	0′			(<i>i</i> = 3	8° 3	30′		C	a
	B	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
I	45 46 47 48 49	34 35 36	7 48 28 8 47	1.46 1.50 1.50 1.54 1.54	47 48 49	20 51 22 55 28	0.52 •52 •55 •55 •58	33 34 35 36	52 32 12 51 30	1.50 1.50 1.54 1.54 1.58	47 48 49	51 22 53 25 59	0.52 .52 .53 .57	33 34 35 36	36 16 55 34 12	1.50 1.54 1.54 1.58 1.58	48 49 50	22 52 24 56 29	0.50 •53 •53 •55 •58	45 44 43 42 41	58.4 57.5 56.6 55.6 54.7
	50 51 52 53 54	37 38 39	26 4 42 19 56	1.58 1.58 1.62 1.62 1.62	50 51 52	3 39 16 54 33	0.60 .62 .63 .65	37 38 39	8 46 23 0 36	1.58 1.62 1.62 1.67 1.67	50 51 52 53	33 9 46 24 3	0.60 .62 .63 .65	37 38 39	50 28 5 41 17	1.58 1.62 1.67 1.67 1.71	51 52 53	4 39 16 53 32	0.58 .62 .62 .65	40 39 38 37 36	53·7 52.8 51.8 50.8 49·7
	55 56 57 58 59	40 41 42	32 8 43 17 51	1.67 1.71 1.76 1.76 1.82	53 54 55 56	13 55 38 22 8	0.70 •72 •73 •77 •78	40 41 42	12 47 22 56 29	1.71 1.71 1.76 1.82 1.82	54 55 56	43 24 7 51 36	0.68 •72 •73 •75 •78	40 41 42	52 27 1 35 8	1.71 1.76 1.76 1.82 1.88	54 55 56 57	54 36 20 5	0.70 .70 .73 .75 .77	35 34 33 32 31	48.7 47.6 46.5 45.4 44.3
	60 61 62 63 64	43 44 45	24 56 28 59 29	1.88 1.88 1.94 2.00 2.07	57 58 59 60	55 43 32 23 16	0.80 .82 .85 .88	43 44 45	34 5 36 6	1.88 1.94 1.94 2.00 2.07	57 58 59 60	23 11 0 50 42	0.80 .82 .83 .87	43 44	40 12 43 13 42	1.88 1.94 2.00 2.07 2.07	58 59 60 61	51 38 27 17 8	0.78 .82 .83 .85 .88	30 29 28 27 26	43.2 42.0 40.8 39.6 38.4
	65 66 67 68 69	46 47	58 27 55 21 47	2.07 2.14 2.31 2.31 2.40	9 4 59 58	0.92 •95 •97 •98 1.02	46 47	35 30 56 22	2.14 2.22 2.31 2.31 2.50	61 62 63 64 65	35 30 26 23 22	0.92 •93 •95 •98	45 46	38 5 31 56	2.22 2.22 2.31 2.40 2.50	62 63 64 65	55 50 47 45	0.90 .92 .95 .97	25 24 23 22 21	37.1 35.9 34.6 33.3 31.9	
	70 71 72 73 74	48 49	12 36 59 21 42	2.50 2.61 2.73 2.86 3.00	1.03 1.05 1.08 1.10 1.12	48 49	46 10 33 54 15	2.50 2.61 2.86 2.86 3.16	66 67 68 69 70	22 23 25 29 34	1.02 1.03 1.07 1.08 1.10	47 48	20 44 6 27 47	2.50 2.73 2.86 3.00 3.16	66 67 68 69 70	44 44 46 49 53	1.00 1.03 1.05 1.07	20 19 18 17 16	30.6 29.2 27.8 26.4 25.0		
	75 76 77 78 79	50	2 20 38 54 9	3.33 3.33 3.75 4.00 4.29	71 72 73 74 76	22 30 40 50 2	I.I3 I.I7 I.I7 I.20 I.22	50	34 52 9 25 40	3·33 3·53 3·75 4·00 4·29	71 72 73 75 76	40 48 56 6	1.13 1.13 1.17 1.18 1.18	49 50	6 24 41 57 12	3·33 3·53 3·75 4.00 4.62	71 73 74 75 76	58 5 13 21 31	1.12 1.13 1.13 1.17 1.17	15 14 13 12 11	23.5 22.0 20.5 19.0 17.5
	80 81 82 83 84	52	23 36 47 57 6	4.62 5.45 6.00 6.67 8.57	77 78 79 80 82	15 29 43 58 14	I.23 I.23 I.25 I.27 I.28	51	54 6 17 27 36	5.00 5.45 6.00 6.67 8.57	77 78 79 81 82	28 41 54 8 23	I.22 I.22 I.23 I.25 I.25	51	25 37 48 58	5.00 5.45 6.00 7.50 8.57	77 78 80 81 82	41 52 4 17 31	I.18 I.20 I.22 I.23 I.23	9 8 7 6	16.0 14.4 12.9 11.3 9.7
	85 86 87 88 89		1 3 10.0 83 31 1.2 14 1.3 10.0 19 12.0 24 20.0 27 30.0 29 60.0 88 42 1.3 30 90 0						43 49 54 57 59	10.0 12.0 20.0 30.0 60.0	87	38 54 10 26 43	1.27 1.27 1.27 1.28 1.28		13 19 24 27 29	10.0 12.0 20.0 30.0 60.0	86	29	I.23 I.25 I.25 I.25 I.27	5 4 3 2 1	8.1 6.5 4.9 3.2 1.6
	90	_	30		90	0		52 —	0		90	0			30		90	0		0	0.0
	t	a	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $						ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$	1	b	$\frac{\Delta}{60'}$		a
			à	l=37	7° 3	0′				d=3	8° ()′			á	=38	3° 3	0′			

8		a = 3	9° 0′			a = 3	9° 3	0′			C	i = 4	0° ()′		\ c	\ a
B	h d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	$d \frac{60'}{\Delta}$	Z	t	<u>∆</u> 60′	h	d	$\frac{60'}{\Delta}$	Z	t	<u>Δ</u> 6ο'	C	β
0 0 1 2 3 4	° ′ ′ ° ′ ° ′ ° ′ ° ′ ° ′ ° ′ ° ′ ° ′ °	1.28 1.30 1.28 1.28 1.30	39 0 0 1 2 4	1	1 3	0 1.30 16 1.28 33 1.30 1.30 5 1.30	39°	30 30 31 32 34	0.00 .02 .02 .03	I	0 46 32 18	1.30 1.30 1.30 1.30	4°	0 0 1 2 4	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.4 88.7 88.1 87.5
5 6 78 9	53 4 40 5 26 6 13 59	1.28 1.30 1.28 1.30 1.30	6 9 13 17 21	.07	4 3 5 2 6 I	1 1.28 38 1.30 24 1.30 1.30 1.30		36 39 43 47 51	0.05 .07 .07 .07	4 5 6	50 36 21 7 53	1.30 1.33 1.30 1.30		6 9 13 17 21	0.05 .07 .07 .07	85 84 83 82 81	86.8 86.2 85.5 84.9 84.2
10 11 12 13 14	7 45 8 32 9 18 10 4 50	1.28 1.30 1.30 1.30 1.30	26 31 37 44 51	0.08 .10 .12 .12	8 2 9 I 10	12 1.30 28 1.30 14 1.30 0 1.30 16 1.33	40	56 7 14 21	0.08 .10 .12 .12	7 8 9	39 24 10 55 41	1.33 1.30 1.33 1.30		26 31 37 44 51	0.08 .10 .12 .12	80 79 78 77 76	83.6 83.0 82.3 81.6 81.0
15 16 17 18 19	11 36 12 22 13 8 54 14 40	1.30 1.30 1.30 1.30	59 40 7 16 25 35	.15	12 1	31 1.30 17 1.33 2 1.30 18 1.33 1.33	41	29 37 46 55	0.13 .15 .15 .17	11 12 13 14	26 11 56 41 26	I.33 I.33 I.33 I.33 I.33	41	59 7 16 25 35	0.13 .15 .15 .17 .18	75 74 73 72 71	80.3 79.7 79.0 78.3 77.6
20 21 22 23 24	15 25 16 10 55 17 40 18 25	1.33 1.33 1.33 1.33 1.33	45 56 41 8 20	.20	16 4	18 1.33 3 1.33 48 1.33 33 1.33 1.36	42	16 27 39 51 4	0.18 .20 .20 .22	15 16 17 18	11 56 41 25	1.33 1.33 1.36 1.36 1.36	42	46 57 9 21 34	0.18 .20 .20 .22 .23	70 69 68 67 66	77.0 76.3 75.6 74.9 74.2
25 26 27 28 29	19 10 55 20 40 21 24 22 8	1.33 1.33 1.36 1.36 1.36	47 42 1 16 32 48	.25	20 3	2 1.36 46 1.36 30 1.36 14 1.36 58 1.36	43	17 31 46 2 18	0.23 .25 .27 .27 .28	19 20 21	53 37 21 5 48	1.36 1.36 1.36 1.40 1.40	43	48 2 17 33 49	0.23 .25 .27 .27 .28	65 64 63 62 61	73.5 72.8 72.0 71.3 70.6
30 31 32 33 34	52 23 36 24 19 25 2 45	1.36 1.40 1.40 1.40	43 5 22 41 44 0 20	32 .32	23 2 24	42 1.40 25 1.40 8 1.40 51 1.40 34 1.43	44	35 53 11 30 50	0.30 .30 .32 .33	22 23 24 25	31 14 57 40 22	I.40 I.40 I.43 I.43	44	6 23 42 I 21	0.28 •32 •32 •33 •33	60 59 58 57 56	69.8 69.1 68.3 67.6 66.8
35 36 37 38 39	26 28 27 11 53 28 35 29 17	1.40 1.43 1.43 1.43 1.46	45 2 45 2 47 46 11	-37 -38 -40	27	1.43 58 1.43 40 1.43 22 1.46	46	32 54	0.35 .37 .38 .40 .42	26 27 28	4 46 27 8 49	1.43 1.46 1.46 1.46 1.46	46 47	41 3 25 48 12	0.37 .37 .38 .40	55 54 53 52 51	66.0 65.2 64.4 63.6 62.7
40 41 42 43 44	58 30 39 31 20 32 0 40	1.46 1.46 1.50 1.50	47 1 28 48 23	•45 •45 •47	30 2 31	1.46 25 1.50 5 1.50 45 1.50 25 1.54	48	58 58 25 54	.48	30	30 10 50 30 9	1.50 1.50 1.50 1.54 1.54		36 28 55 24	•43 •45 •48		61.9 61.1 60.2 59.3 58.4
45	33 20		52		33	4	49	23			48			53	1	45	57.5
t	а	6ο' Δ	b	$\frac{\Delta}{60'}$	a	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$	0	a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
		d = 3	9° 0′			d=3	9° 3	30′				d = 4	10°	0′			

b	0	(a = 3	9° ()′			a	<i>i</i> = 39	9° 3	0′				a = 4	0° (0′		$\setminus c$	a
B	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	z	t	<u>Δ</u> 60'	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
45 46 47 48 49	33 34 35	20 59 38 17 55	1.54 1.54 1.54 1.58 1.62	48 49 50	52 23 54 26 59	0.52 .52 .53 .55 .57	33 34 35	4 43 21 59 37	1.54 1.58 1.58 1.58 1.62	49 50 51	23 53 24 56 29	0.50 .52 .53 .55	32 33 34 35	48 26 4 42 19	1.58 1.58 1.58 1.62 1.62	49 50 51	53 23 54 26 59	0.50 .52 .53 .55	° 45 44 43 42 41	57.5 56.6 55.7 54.8 53.8
50 51 52 53 54	36 37 38	32 9 46 22 57	1.62 1.62 1.67 1.71	51 52 53 54	33 9 45 23 2	.60 .63 .65	36 37 38	14 51 27 3	1.62 1.67 1.67 1.71 1.76	52 53 54	39 15 52 30	0.60 .60 .62 .63	36 37 38	56 32 8 43 18	1.67 1.67 1.71 1.71 1.76	52 53 54	33 8 44 21 59	0.58 .60 .62 .63	39 38 37 36	52.8 51.9 50.9 49.8 48.8
55 56 57 58 59	39 40 41	32 7 41 14 46	1.71 1.76 1.82 1.88 1.88	55 56 57	41 22 4 48 33	•.68 •7° •73 •75 •77	39 40 41	12 46 19 52 24	1.76 1.82 1.82 1.88 1.88	55 56 57 58	10 51 33 16 0	o.68 •7° •72 •73 •77	39 40 41	52 26 59 31	1.76 1.82 1.88 1.88	55 56 57 58	39 19 1 44 28	0.67 •7° •72 •73 •75	35 34 33 32 31	47.7 46.7 45.6 44.5 43.4
60 61 62 63 64	42 43 44	18 49 20 50	1.94 1.94 2.00 2.07 2.14	58 59 60 61	19 6 54 43 34	0.78 .80 .82 .85	42	56 27 57 26 54	1.94 2.00 2.07 2.14 2.14	59 60 61 62	46 32 20 9	0.77 .80 .82 .85	42 43	34 34 33 31	2.00 2.00 2.07 2.14 2.22	59 60 61 62	13 59 47 35 25	0.77 .80 .80 .83 .85	30 29 28 27 26	42.2 41.1 39.9 38.7 37.5
65 66 67 68 69	45 46	47 14 40 6 31	2.22 2.31 2.31 2.40 2.50	62 63 64 65 66	26 20 15 11 8	0.90 .92 .93 .95	44 45 46	22 49 15 41 5	2.22 2.31 2.31 2.50 2.50	63 64 65 66	51 44 38 34 30	•.88 •90 •93 •93 •97	44 45	58 25 51 16 40	2.22 2.31 2.40 2.50 2.61	63 64 65 66	16 8 2 57 53	0.87 .90 .92 .93 .95	25 24 23 22 21	36.2 35.0 33.7 32.4 31.1
70 71 72 73 74	47 48	39 3.33 72 16 15 77 3.75 73 22 149 13 3.75 74 29 1					47	29 51 12 33 53	2.73 2.86 2.86 3.00 3.33	67 68 69 70 71	28 27 27 28 31	0.98 1.00 1.02 1.05 1.05	46 47	3 25 46 6 26	2.73 2.86 3.00 3.00 3.33	67 68 69 70 71	50 48 47 47 49	0.97 .98 1.00 1.03 1.03	20 19 18 17 16	29.8 28.4 27.1 25.7 24.3
75 76 77 78 79	49	57	3.75	73	22	1.10 1.12 1.12 1.15 1.15	48 49	11 29 45 0 14	3·33 3·75 4·00 4·29 4·62	72 73 74 75 76	34 39 44 51 58	1.08 1.08 1.12 1.12 1.13	48	44 1 17 32 46	3.53 3.75 4.00 4.29 5.00	72 73 75 76 77	51 55 0 5	1.07 1.08 1.08 1.10 1.12	15 14 13 12 11	22.8 21.4 19.9 18.5 17.0
80 81 82 83 84	50	43 4.62 76 45 1. 56 5.00 77 54 1. 50 8 5.45 79 4 1. 19 6.00 80 15 1. 29 7.50 81 27 1. 37 8.57 82 39 1.						27 39 50 59 7	5.00 5.45 6.67 7.50 8.57	78 79 80 81 82	6 15 25 35 46	1.15 1.17 1.17 1.18 1.20	49	58 10 20 29 37	5.00 6.00 6.67 7.50 8.57	78 79 80 81 82	18 26 35 44 54	1.13 1.15 1.15 1.17	9 8 7 6	15.5 14.0 12.5 10.9 9.4
85 86 87 88 89		44 10.0 83 52 1.2 85 5 1.2 86 18 1.2 57 30.0 59 60.0 88 46 1.2 51 0 90 0						14 20 24 27 29	10.0 15.0 20.0 30.0 60.0	83 85 86 87 88	58 10 22 34 47	1.20 1.20 1.20 1.22 1.22		44 50 54 57 59	10.0 15.0 20.0 30.0 60.0	84 85 86 87 88	4 15 26 37 48	1.18 1.18 1.18 1.18 1.20	5 4 3 2 1	7.8 6.3 4.7 3.1 1.6
90	51	0		90	0			30		90	0		50	0		90	0	1	0	0.0
	$a \left \frac{60'}{\Delta} \right b \left \frac{4}{60'} \right $							а	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$, (a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
t		y	d = 3	9°	0′	١,		. (d=3	9° 3	0′			,	d=4	0°	0′			

8		a = 4	0° ٤	30′				a = 4	1° (0′			0	i = 4	1° 3	0′		\ c	\ a
$B \setminus$	h	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	$\frac{d}{d}$	6ο' Δ	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	$\stackrel{t}{\swarrow}$	$\frac{\Delta}{60'}$	$C \setminus$	3
o I 2 3 4	0 0 46 1 31 2 17 3 2	1.30 1.33 1.30 1.33 1.30	40	30 30 31 32 34	0.00 .02 .02 .03	0 I 2 3	6 45 31 16 1	1.33 1.30 1.33 1.33 1.33	41	0 0 1 2 4	0.00 .02 .02 .03	0 I 2 3	6 45 30 15 0	I.33 I.33 I.33 I.33 I.33	41	30 30 31 32 34	0.00	90 89 88 87 86	90.0 89.3 88.7 88.0 87.4
5 6 78 9	48 4 34 5 19 6 5 50	1.30 1.33 1.30 1.33 1.33		36 39 43 47 51	0.05 .07 .07 .07	4 5 6	46 31 17 2 47	1.33 1.30 1.33 1.33 1.33		6 9 13 17 21	0.05 .07 .07 .07	4 5 6	45 29 14 59 44	1.36 1.33 1.33 1.33 1.36		36 39 43 47 51	0.05 .07 .07 .07	85 84 83 82 81	86.7 86.1 85.4 84.7 84.1
10 11 12 13 14	7 35 8 21 9 6 51 10 36	1.30 1.33 1.33 1.33	41	56 8 14 21	0.10 .10 .10 .12	7 8 9	32 17 2 47 31	1.33 1.33 1.33 1.36 1.33		26 32 38 44 51	0.10 .10 .10 .12	7 8 9	28 13 58 42 26	1.33 1.33 1.36 1.36 1.36	42	56 2 8 14 21	0.10 .10 .10 .12	80 79 78 77 76	83.4 82.7 82.1 81.4 80.7
15 16 17 18 19	11 21 12 6 51 13 35 14 20	1.33 1.33 1.36 1.33 1.36	42	29 37 46 55 5	0.13 .15 .15 .17	11 12 13 14	16 0 45 29 13	1.36 1.33 1.36 1.36 1.36	42	59 7 16 26 36	0.13 .15 .17 .17	11 12 13 14	55 39 23 7	1.36 1.36 1.36 1.36 1.36	43	29 37 46 56 6	0.13 .15 .17 .17	75 74 73 72 71	80.0 79.3 78.7 78.6 77.3
20 21 22 23 24	15 4 49 16 33 17 17 18 1	1 1.33		0.18 .20 .20 .22 .23	15 16 17	57 41 25 9 53	1.36 1.36 1.36 1.36 1.40	43	46 57 9 22 35	0.18 .20 .22 .22	15 16 17	51 34 18 1 44	1.40 1.36 1.40 1.40	44	17 28 40 52 5	0.18 .20 .20 .22 .23	70 69 68 67 66	76.6 75.9 75.2 74.4 73.7	
25 26 27 28 29	45 19 29 20 12 55 21 38	1.36 27		0.23 .25 .27 .27 .28	18 19 20 21	36 19 2 45 28	I.40 I.40 I.40 I.40 I.43	44	48 3 18 33 49	0.25 .25 .25 .27 .28	18 19 20 21	27 10 53 35 17	I.40 I.40 I.43 I.43	45	19 33 48 4 20	0.23 .25 .27 .27 .28	65 64 63 62 61	73.0 72.3 71.5 70.8 70.0	
30 31 32 33 34	22 21 23 4 46 24 28 25 10	1.43	45	54	0.30 .30 .32 .33	22 23 24	10 52 34 16 58	I.43 I.43 I.43 I.43 I.46	45 46	6 24 43 2 22	0.30 .32 .32 .33	22 23 24	59 41 23 4 45	1.43 1.43 1.46 1.46	46	37 55 13 32 52	0.30 .30 .32 .33 .33	59 58 57 56	69.3 68.5 67.7 66.9 66.1
35 36 37 38 39	52 26 33 27 14 55 28 36	4 1.43 54 54 6 1.43 8 1.43 51 51 51 51 51 6 6 6 6 6 6 6 6 6 6 6 6			0.35 .37 .38 .40 .42	25 26 27 28	39 20 I 41 21	1.46 1.46 1.50 1.50 1.50	47 48	42 3 25 48 12	0.35 .37 .38 .40 .42	25 26 27 28	26 7 47 27 7	1.46 1.50 1.50 1.50 1.50	47 48	34 56 19 42	0.37 .37 .38 .38 .42	55 54 53 52 51	65.3 64.5 63.7 62.9 62.0
40 41 42 43 44	29 16 56 30 35 31 14 53	1.50 1.54 1.54 1.54 1.54	48	7 32 58 25 54	0.42 •43 •45 •48	29 30 31	1 41 20 59 37	1.50 1.54 1.54 1.58 1.58	49 50	37 28 55 23	•43 •45 •47 •48	29 30 31	47 26 5 43 21	1.54 1.54 1.58 1.58	49 50	7 32 58 25 53	0.42 •43 •45 •47 •48	50 49 48 47 46	61.2 60.3 59.4 58.5 57.6
45	32 32		50	23		32	15			52			59		51	22		45	56.7
t	a	$\frac{60'}{\Delta}$	t	$\frac{\Delta}{60'}$	а		$\frac{\epsilon_{\mathbf{O'}}}{\Delta}$	t		$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$	l		$\frac{\Delta}{60'}$		a	
	(l = 40)° 3	0′				d = 4	1° ()′			d	=41	° 3	0′			

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1	b		(<i>a</i> = 4	0° 3	30′				a=4	1° (0′				a = 4	1° 8	30′		\ c	a
B	/	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	z	t	$\frac{\Delta}{60'}$	C	β
4 4 4	• 15	32 33 34 35	32 10 47 24 1	1.58 1.62 1.62 1.62 1.62	50° 51 52	23 53 24 55 28	0.50 •52 •52 •55 •55	32 33 34	15 53 30 7 43	1.58 1.62 1.62 1.67 1.67	50 51 52	52 22 53 25 57	0.50 .52 .53 .53 .57	31 32 33 34	59 36 13 49 25	1.62 1.62 1.67 1.67	51 52 53	22 52 22 54 26	0.50 .50 .53 .53	° 45 44 43 42 41	56.7 55.8 54.9 53.9 53.0
555	1 2 3 4	36 37	38 14 49 24 58	1.67 1.71 1.71 1.76 1.76	53 54 55	2 37 13 50 28	0.58 .60 .62 .63	35 36 37	55 30 4 38	1.67 1.71 1.76 1.76 1.82	53 54 55	31 6 42 18 56	0.58 .60 .60 .63	35 36 37	36 10 44 18	1.71 1.76 1.76 1.76 1.82	54 55 56	0 35 10 46 24	0.58 .58 .60 .63	40 39 38 37 36	52.0 51.0 50.0 49.0 47.9
5 5 5	56 78 9	38 39 40	32 5 37 9 40	1.82 1.88 1.88 1.94 1.94	56 57 58	7 47 28 11 54	0.67 .68 .72 .72 .75	38 39 40	11 44 16 48 19	1.82 1.88 1.88 1.94 2.00	56 57 58 59	35 15 56 38 21	0.67 .68 .70 .72 .75	38 39	51 23 55 26 56	1.88 1.88 1.94 2.00 2.00	57 58 59	3 42 23 5 48	0.65 .68 .70 .72 .73	35 34 33 32 31	46.9 45.8 44.7 43.6 42.5
666	1 2 3 4	41 42 43	11 41 11 39 7	2.00 2.00 2.14 2.14 2.22	59 60 61 62	39 25 12 0 50	0.77 .78 .80 .83 .83	41 42	49 18 47 15 43	2.07 2.07 2.14 2.14 2.31	60 61 62 63	6 51 38 25 14	0.75 .78 .78 .82 .83	40 41 42	26 55 24 52 19	2.07 2.07 2.14 2.22 2.31	60 61 62 63	32 17 3 50 38	0.75 .77 .78 .80 .83	30 29 28 27 26	41.3 40.2 39.0 37.8 36.6
666	56 78 9	44	34 0 25 50 14	2.31 2.40 2.40 2.50 2.73	63 64 65 66 67	40 32 25 19 14	0.87 .88 .90 .92 .95	43 44	9 35 0 24 48	2.31 2.40 2.50 2.50 2.73	64 65 66 67	4 55 48 41 36	0.85 .88 .88 .92	43 44	45 10 35 59 22	2.40 2.40 2.50 2.61 2.73	64 65 66 67	28 19 10 3 57	0.85 .85 .88 .90	25 24 23 22 21	35·4 34·2 32·9 31·6 30·3
777	1 2 3 4	46	36 58 19 39 58	2.73 2.86 3.00 3.16 3.33	68 69 70 71 72	8 6 6 7	0.95 .97 1.00 1.02 1.02	45 46	10 32 52 12 30	2.73 3.00 3.00 3.33 3.33	68 69 70 71 72	31 28 26 25 25	0.95 .97 .98 1.00	45 46	44 5 25 45 3	2.86 3.00 3.00 3.33 3.53	68 69 70 71 72	52 48 45 43 42	0.93 •95 •97 •98	20 19 18 17 16	29.0 27.7 26.3 25.0 23.6
777	5 6 78 9	47 48	16 33 48 3 17	3.53 4.00 4.00 4.29 5.00	73 74 75 76 77	8 11 15 19 24	1.05 1.07 1.07 1.08 1.10	47	48 5 20 35 48	3.53 4.00 4.00 4.62 5.00	73 74 75 76 77	25 27 30 33 37	1.03 1.05 1.05 1.07 1.08	47	20 37 52 6 19	3.53 4.00 4.29 4.62 5.00	73 74 75 76 77	42 42 44 47 50	1.00 1.03 1.05 1.05	15 14 13 12 11	22.2 20.8 19.4 18.0 16.5
8 8	3 4	49	29 41 51 0 8	5.00 6.00 6.67 7.50 8.57	78 79 80 81 83	30 37 45 53 1	1.12 1.13 1.13 1.13 1.15	48	0 12 22 31 39	5.00 6.00 6.67 7.50 10.0	78 79 80 82 83	42 48 54 1 9	1.10 1.10 1.12 1.13 1.13	48	31 42 52 1	5.45 6.00 6.67 7.50 10.0	78 79 81 82 83	54 58 3 9 16	I.07 I.08 I.10 I.12 I.12	9 8 7 6	15.0 13.6 12.1 10.6 9.1
8 8	56 78 9		15 20 24 27 29	12.0 15.0 20.0 30.0 60.0	84 85 86 87 88	10 20 30 40 50	I.17 I.17 I.17 I.17		45 50 54 57 59	12.0 15.0 20.0 30.0 60.0	88	51	I.13 I.13 I.15 I.15		15 20 24 27 29	.12.0 15.0 20.0 30.0 60.0	84 85 86 87 88	23 30 37 44 52	I.12 I.12 I.12 I.13 I.13	5 4 3 2 1	7.6 6.1 4.6 3.0 1.5
9	0		30	601	90	0		49		601	90				30	601	90		Δ.	0	0.0
	t		$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $						ı	$\frac{60'}{\Delta}$)	$\frac{\Delta}{60'}$	- 0		$\frac{60'}{\Delta}$		b	<u>Δ</u> 6ο'	•	a
			d = 40° 30′							d = 4	11°	0′			(d = 4	1° 3	0′			

	$\setminus b$			a=4	ł2°	0′			a	i = 4	2° 8	30′				a = 4	3° ()′		$\setminus c$	a
	B	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
	0 I 2 3 4	0 0 I 2	ó 45 29 14 58	1.33 1.36 1.33 1.36 1.33	42		0.00 .02 .02 .03	0 I 2	ó 44 29 13 57	1.36 1.33 1.36 1.36 1.36	42	30 30 31 32 34	0.00	0 I 2	ó 44 28 12 55	1.36 1.36 1.36 1.40 1.36	43	0 0 1 2 4	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.3 88.6 88.0 87.3
	5 6 7 8 9	5	43 27 12 56 41	1.36 1.33 1.36 1.33 1.36		6 9 13 17 21	0.05 .07 .07 .07	3 4 5 6	41 25 9 53 37	1.36 1.36 1.36 1.36 1.36		36 39 43 47 51	0.05 .07 .07 .07	3 4 5 6	39 23 7 51 34	1.36 1.36 1.36 1.40 1.36		6 9 13 17 21	0.05 .07 .07 .07	85 84 83 82 81	86.6 85.9 85.3 84.6 83.9
	10 11 12 13 14	7 8 9 10	25 9 53 37 21	1.36 1.36 1.36 1.36 1.36		26 32 38 45 52	0.10 .10 .12 .12	7 8 9 10	21 5 49 33 16	1.36 1.36 1.36 1.40 1.36	43	56 8 15 22	0.10 .10 .12 .12	7 8 9 10	18 1 45 28 11	1.40 1.36 1.40 1.40 1.36		26 32 38 45 52	0.10 .10 .12 .12	80 79 78 77 76	83.2 82.5 81.8 81.1 80.4
	15 16 17 18 19	11 12 13 14	5 49 33 17	1.36 1.36 1.36 1.40 1.36	43	59 8 17 26 36	0.15 .15 .15 .17	11 12 13	0 44 27 10 53	1.36 1.40 1.40 1.40	44	30 38 47 56 6	0.13 .25 .15 .17	11 12 13	55 38 21 4 46	1.40 1.40 1.40 1.43 1.40	44	0 8 17 26 36	0.13 .15 .15 .17	75 74 73 72 71	79.7 79.0 78.3 77.6 76.9
	20 21 22 23 24	15 16	44 27 10 53 36	1.40 1.40 1.40 1.40 1.40	44	47 58 10 22 35	0, 18 .20 .20 .22 .23	14 15 16	36 19 2 45 27	I.40 I.40 I.40 I.43 I.43	45	17 28 40 52 5	0.18 .20 .20 .22 .23	14 15 16 17	29 12 54 36 18	I.43 I.43 I.43 I.43	45	47 58 10 22 35	0.18 .20 .20 .22 .23	70 69 68 67 66	76.2 75.5 74.7 74.0 73.3
	25 26 27 28 29	19	19 1 43 25 7	I.43 I.43 I.43 I.43 I.43	45	49 3 18 34 50	0.23 .25 .27 .27 .28	18 19 20	9 51 33 15 57	1.43 1.43 1.43 1.43 1.46	46	19 33 48 4 20	0.23 .25 .27 .27 .28	18 19 20	0 42 24 5 46	1.43 1.43 1.46 1.46 1.46	46	49 3 18 34 50	0.23 .25 .27 .27 .28	65 64 63 62 61	72.5 71.8 71.0 70.2 69.5
	30 31 32 33 34	22 23	49 30 11 52 33	1.46 1.46 1.46 1.46 1.46	46 47	7 25 43 2 22	0.30 .30 .32 .33	21 22 23 24	38 19 0 41 21	1.46 1.46 1.46 1.50 1.50	47	37 55 13 32 52	0.30 .30 .32 .33	21 22 23 24	27 8 48 28 8	1.46 1.50 1.50 1.50 1.50	47	7 25 43 2 22	0.30 .30 .32 .33	60 59 58 57 56	68.7 67.9 67.1 66.3 65.5
	35 36 37 38 39	26 27	14 54 34 14 53	1.50 1.50 1.50 1.54 1.54	48 49	42 4 26 49 12	0.37 .37 .38 .38 .42	25 26 27	1 41 21 0 39	1.50 1.50 1.54 1.54 1.58	48 49	12 33 55 18 42	0.35 .37 .38 .40	25 26 27	48 28 7 46 24	1.50 1.54 1.54 1.58 1.58	49	42 3 25 48 12	0.35 .37 .38 .40 .40	55 54 53 52 51	64.7 63.9 63.0 62.2 61.3
2	40 41 42 43 44	29	27	1.54 1.58 1.58 1.58 1.58	50	37 28 55 23	•43 •45 •47 •47	28 29 30	17 55 33 11 48	1.58 1.58 1.58 1.62 1.62	50	6 31 57 24 52	•.42 •43 •45 •47 •48	28 29 30	2 40 18 55 32	1.58 1.58 1.62 1.62 1.62	51	36 1 27 54 21	0.42 •43 •45 •45 •48	50 49 48 47 46	60.5 59.6 58.7 57.8 56.9
	45		42			51		31	25		52	21		31	9		-	50		45	56.0
	t	. a	$a \left\ \frac{60'}{\Delta} \right\ b \left\ \frac{\Delta}{60} \right\ $							$\frac{60'}{\Delta}$	t	5	<u>Δ</u> 6ο'	0	ı	$\frac{60'}{\Delta}$	b		$\frac{\Delta}{60'}$		a
	ı		C	l=4	2° ()′			d	= 42	2° 3	0′			(d = 4	3° ()′			

b		a = 4	ŀ2° 0′			C	a=4	2° 3	0′				a = 4	3° (0′		\ c	a
$B \setminus$	h	$\frac{l}{\Delta}$	Z^{t}	$\frac{\Delta}{60'}$	h	$\stackrel{d}{\swarrow}$	<u>6ο'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	60' Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	31 4 32 1 5 33 3 34	5 1.67	51 51 52 21 52 53 23 55	0.50 .52 .52 .53 .57	31 32 33	25 2 38 13 48	1.62 1.67 1.71 1.71	52 53 54	21 50 20 52 24	0.48 .50 .53 .53	3 ¹ 3 ² 33	9 45 20 55 30	1.67 1.71 1.71 1.71 1.76	52 53 54	50 19 49 20 52	0.48 •50 •52 •53 •55	° 45 44 43 42 41	56.0 55.0 54.1 53.1 52.1
50 51 52 53 54	35 I 35 2 36 2 5	7 1.76 I 1.82 4 1.82	54 29 55 3 38 56 15 52	0.57 .58 .62 .62 .63	34 35 36	23 57 31 4 37	1.76 1.76 1.82 1.82 1.88	55 56 57	57 31 6 42 19	0.57 .58 .60 .62 .63	343536	38 11 44 17	1.76 1.82 1.82 1.82 1.94	55 56 57	25 59 34 10 47	0.57 .58 .60 .62 .62	40 39 38 37 36	51.2 50.2 49.2 48.1 47.1
55 56 57 58 59	- 3	2 I.94 3 I.94 4 2.00	57 30 58 9 50 59 31 60 14	0.65 .68 .68 .72 .72	37 38 39	9 41 12 42 12	1.88 1.94 2.00 2.00 2.07	58 59 60	57 36 17 58 40	0.65 .68 .68 .70 .72	37 38	48 19 50 20 49	1.94 1.94 2.00 2.07 2.07	58 59 60 61	24 3 43 24 5	0.65 .67 .68 .68	35 34 33 32 31	46.0 45.0 43.9 42.8 41.7
60 61 62 63 64	3	2.22	57 61 42 62 28 63 15 64 2	0.75 .77 .78 .78 .82	40 41	41 9 37 4 30	2.14 2.14 2.22 2.31 2.31	61 62 63 64	23 7 52 39 26	0.73 .75 .78 .78 .78	39 40 41	18 46 13 40 6	2.14 2.22 2.22 2.31 2.40	62 63 64	48 32 17 2 49	0.73 .75 .75 .78 .80	30 29 28 27 26	40.5 39.4 38.2 37.0 35.8
65 66 67 68 69	42 20 44 43 10 3 5	2.40 2.61 2.61	51 65 41 66 32 67 25 68 18	0.83 .85 .88 .88	42 43	56 21 45 8 30	2.40 2.50 2.61 2.73 2.86	65 66 67 68	15 4 54 46 39	0.82 .83 .87 .88	42 43	31 55 19 42 4	2.50 2.50 2.61 2.73 2.86	65 66 67 68	37 26 16 7 59	0.82 .83 .85 .87	25 24 23 22 21	34.6 33.4 32.1 30.9 29.6
70 71 72 73 74	44 I 35 45 I 3	3.00 3.16 8 3.33	69 12 70 7 71 3 72 1 59	0.92 •93 •97 •97 •98	44 45	51 12 31 50 8	2.86 3.16 3.16 3.33 3.53	69 70 71 72 73	32 26 22 18 15	0.90 •93 •93 •95 •98	44	25 45 4 22 40	3.00 3.16 3.33 3.33 3.53	69 70 71 72 73	52 45 40 36 32	0.88 .92 .93 .93	20 19 18 17 16	28.3 27.0 25.7 24.3 23.0
75 76 77 78 79	46 ⁵ 2 3 5	4.00 4.29 8.4.62	73 58 74 58 75 58 77 0 78 2	1.00 1.03 1.03 1.05	46	25 40 55 9 22	4.00 4.00 4.29 4.62 5.00	74 75 76 77 78	14 13 13 13	0.98 1.00 1.00 1.02 1.03	45	57 12 27 41 53	4.00 4.00 4.29 5.00 5.00	74 75 76 77 78	29 27 26 26 26	0.97 .98 I.00 I.00	15 14 13 12 11	21.6 20.3 18.9 17.5 16.1
80 81 82 83 84	47 I 2 3 3	3 6.67 2 8.57	79 5 80 9 81 13 82 18 83 23	1.07 1.07 1.08 1.08	47	34 44 54 2	6.00 6.00 7.50 7.50 10.0	79 80 81 82 83	16 19 22 26 30	1.05 1.05 1.07 1.07 1.07	46	5 15 24 32 40	6.00 6.67 7.50 7.50 10.0	79 80 81 82 83	27 29 31 33 36	1.03 1.03 1.03 1.05 1.05	9 8 7 6	14.6 13.2 11.8 10.3 8.8
85 86 87 88 89	4 5 5 5 5	1 15.0 5 20.0 8 60.0	84 28 85 34 86 40 87 47 88 53	I.10 I.12 I.10 I.12		16 21 25 28 29	12.0 15.0 20.0 60.0 60.0	84 85 86 87 88	34 39 44 49 54	1.08 1.08 1.08 1.08		46 51 5 5 58 59	12.0 15.0 20.0 60.0 60.0	84 85 86 87 88	5 I	1.07 1.07 1.07 1.08 1.07	5 4 3 2 1	7·4 5·9 4·4 3.0 1.5
90	48	0	90 0			30		90	0		47	0		90	0		0	0.0
t	а	$\left \frac{6o'}{\Delta} \right b \left \frac{\Delta}{6o'} \right $				ı	60' Δ		b	<u>A</u> 60'	(ı	<u>6ο′</u> Δ	1	Ь	$\frac{\Delta}{60'}$		a ·
l		d = d	42° 0′			C	l=4	2° 3	0′				d = 4	3° (D′			

$\setminus b$	a	= 43	3° 30′				a = 4	4 ° (0′			C	a = 4	4° 3	0′		\ c	a
$B \setminus$	h d	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	<u>Δ</u> 60'	$C \setminus$	B
0 0 1 2 3 4	0 0 44 1 27 2 11 54	1.36 1.40 1.36 1.40 1.36	43 30 30 31 32 32	.02 I .02 2 .03	0 0 I 2	ó 43 26 10 53	1.40 1.40 1.36 1.40 1.40	44	0 0 1 2 4	0.00 .02 .02 .03	0 0 1 2	ó 43 26 8 51	1.40 1.40 1.43 1.40 1.40	44	30 30 31 32 34	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.3 88.6 87.9 87.2
5 6 78 9	3 38 4 21 5 4 48 6 31	1.40 1.40 1.36 1.40 1.40	39 39 44 47 5	9 .07 3 .07 7 .07 1 .08	3 4 5 6	36 19 2 45 28	1.40 1.40 1.40 1.40		6 9 13 17 21	.05 .07 .07 .07 .08	3 4 5 6	34 17 59 42 24	1.40 1.43 1.40 1.43 1.40		36 39 43 47 51	0.05 .07 .07 .07	85 84 83 82 81	86.5 85.8 85.1 84.4 83.7
10 11 12 13 14	7 14 57 8 40 9 23 10 6	1.40 1.40 1.40 1.40		2 .10 8 .12 5 .12	7 8 9 10	53 36 19	1.43 1.40 1.40 1.43 1.40		26 32 38 45 52	0.10 .10 .12 .12	7 8 9	7 49 32 14 56	1.43 1.40 1.43 1.43	45	56 8 15 22	0.10 .10 .12 .12	80 79 78 77 76	83.0 82.3 81.6 80.9 80.2
15 16 17 18 19	49 11 32 12 15 57 13 40	1.40 1.40 1.43 1.40 1.43	39 34 45	8 .15	11 12	44 26 8 50 32	1.43 1.43 1.43 1.43 1.43	45	8 17 26 36	0.13 .15 .15 .17	10 11 12	38 20 2 44 26	1.43 1.43 1.43 1.43 1.46	46	30 38 47 56 6	0.13 .15 .15 .17	75 74 73 72 71	79.5 78.7 78.0 77.3 76.5
20 21 22 23 24	14 22 15 4 46 16 28 17 10	1.43 1.43 1.43 1.43 1.46	1 2 4 5 46	8 .20	14 15 16 17	14 56 38 19	1.43 1.43 1.46 1.43 1.46	46	47 58 10 22 35	0.18 .20 .20 .22 .23	14 15 16	7 49 30 11 52	1.43 1.46 1.46 1.46 1.46	47	17 28 40 52 5	0.18 .20 .20 .22 .23	70 69 68 67 66	75.8 75.1 74.3 73.6 72.8
25 26 27 28 29	51 18 32 19 13 54 20 35	1.46 1.46 1.46 1.46 1.46			18 19 20	42 23 4 44 25	1.46 1.46 1.50 1.46 1.50	47	49 3 18 34 50	0.23 .25 .27 .27 .28	17 18 19 20	33 13 54 34 14	1.50 1.46 1.50 1.50 1.50	48	19 33 48 4 20	0.23 .25 .27 .27 .28	65 64 63 62 61	72.1 71.3 70.5 69.7 68.9
30 31 32 33 34	21 16 56 22 36 23 16 56	1.50 1.50 1.50 1.50		5 .30	21 22 23	5 45 25 4 43	1.50 1.50 1.54 1.54 1.54	48 49	7 25 43 2 21	0.30 .30 .32 .32 .35	21 22 23	54 33 12 51 30	1.54 1.54 1.54 1.54 1.54	49	37 54 12 31 51	0.28 .30 .32 .33	59 58 57 56	68.1 67.3 66.5 65.7 64.9
35 36 37 38 39	24 35 25 14 53 26 32 27 10	1.54 1.54 1.54 1.58 1.58	3 50 I	2 0.35 3 .37 5 .38 8 .38 1 .40	25 26	22 39 17 55	1.54 1.58 1.58 1.58 1.62	50	42 3 25 47	0.35 .37 .37 .40	24 25 26	9 47 25 3 40	1.58 1.58 1.58 1.62 1.62	50	32 54 17 40	0.35 .37 .38 .38 .40	55 54 53 52 51	64.1 63.2 62.4 61.5 60.6
40 41 42 43 44	48 28 25 29 2 39 30 15	1.62 1.62 1.62 1.67 1.67	52 2	5 0.42 0 .43 6 .45 3 .45 0 .48	28 29	32 9 46 23 59	1.67		35 0 25 52 19	0.42 .42 .45 .45 .47	28 29	17 54 30 6 42	1.62 1.67 1.67 1.67 1.71	53	48	1	47 46	59.8 58.9 58.0 57.1 56.1
45	51		53 1	9	30	34			47		30	17		54	16		45	55.2
	а	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		æ
			3° 30	,			d = 4	4°	0′				d = 4	4° 3	30′			

\ b		-	i = 4	3° 3	0′		1		a = 4	4°	0′			0	i = 4	4° ?	30′		\ c	\ a
	-	d	60'		t	Δ	-	\overline{d}	60'	<u></u>	$\frac{1}{t}$	Δ	7	$\frac{d}{d}$	60'		$\frac{1}{t}$	Δ		
$B \setminus$	h	/	Δ	Z		60'	h`	/	Δ	z	/	60'	h		Δ	Z	/	60'	$C \setminus$	$\beta \setminus$
45 46 47 48 49	30 31 32 33	51 27 2 37 11	1.67 1.71 1.71 1.76 1.76	53 54 55	19 48 18 49 21	0.48 .50 .52 .53	30 31 32	34 10 45 19 53	1.67 1.71 1.76 1.76 1.82	53 54 55	47 16 46 17 49	0.48 •50 •52 •53 •53	30 31 32	17 52 26 0 34	1.71 1.76 1.76 1.76 1.76	54 55 56	16 45 14 45 16	0.48 .48 .52 .52 .55	45 44 43 42 41	55.2 54.3 53.3 52.4 51.4
50 51 52 53 54	34 35	45 19 52 24 56	1.76 1.82 1.88 1.88	56 57 58	53 27 2 37 13	0.57 .58 .58 .60 .63	33 34 35	26 59 32 4 35	1.82 1.82 1.88 1.94 1.94	56 57 58	21 55 29 4 40	••57 •57 •58 •60 •62	33 34 35	7 40 12 44 15	1.82 1.88 1.88 1.94 2.00	57 58 59	49 22 56 31 7	0.55 .57 .58 .60 .62	40 39 38 37 36	50.4 49.4 48.4 47.3 46.3
55 56 57 58 59	36 37 38	27 58 28 58 27	1.94 2.00 2.00 2.07 2.14	59 60 61	51 30 9 49 31	0.65 .65 .67 .70	36 37 38	6 36 6 35 4	2.00 2.00 2.07 2.07 2.14	59 60 61	17 56 35 15 56	0.65 .65 .67 .68	36 37	45 15 44 13 41	2.00 2.07 2.07 2.14 2.14	60 61 62	44 21 0 40 21	0.62 .65 .67 .68	35 34 33 32 31	45.2 44.2 43.1 42.0 40.9
60 61 62 63 64	39 40	55 23 50 16 41	2.14 2.22 2.31 2.40 2.40	62 63 64 65	13 56 41 26 12	•.72 •.75 •.75 •.77 •.80	39 40	32 59 26 52 17	2.22 2.22 2.31 2.40 2.50	62 63 64 65	38 21 4 49 35	0.72 .72 .75 .77 .78	38 39	9 36 2 27 52	2.22 2.31 2.40 2.40 2.50	63 64 65	2 44 28 12 57	0.70 •73 •73 •75 •78	30 29 28 27 26	39·7 38·6 37·4 36·3 35·1
65 66 67 68 69	41 42	6 2.50 66 0 0.8 30 2.61 48 .8 53 2.61 67 37 .8 16 2.86 68 28 .8 37 2.86 69 19 .8 58 3.00 70 11 0.8 18 3.16 71 4 .9 37 3.33 58 .9 55 3.33 72 53 .9		0.80 .82 .85 .85	4I 42	41 5 28 50 11	2.50 2.61 2.73 2.86 3.00	66 67 68 69	22 10 58 48 38	0.80 .80 .83 .83	40 41	16 40 2 24 45	2.50 2.73 2.73 2.86 3.00	66 67 68 69	44 31 19 8 58	0.78 .80 .82 .83 .85	25 24 23 22 21	33.9 32.7 31.4 30.2 28.9		
70 71 72 73 74	43 44	53 2.61 67 37 .8 16 2.86 68 28 .8 37 2.86 69 19 .8 58 3.00 70 11 0.8 18 3.16 71 4 .9 37 3.33 58 .9 55 3.33 72 53 .9 13 3.75 73 48 .9 29 4.00 74 45 0.9		0.88 .90 .92 .92	43	31 51 10 28 45	3.00 3.16 3.33 3.53 3.75	70 71 72 73 74	30 22 15 9 4	0.87 .88 .90 .92 .93	42 43	5 24 43 0 17	3.16 3.16 3.53 3.53 3.75	70 71 72 73 74	49 40 33 26 20	0.85 .88 .88 .90	20 19 18 17 16	27.7 26.4 25.1 23.8 22.4		
75 76 77 78 79	45	29 44 58 12 24	4.00 4.29 4.29 5.00 5.45	74 75 76 77 78	45 42 40 39 38	0.95 •97 •98 •98	44	1 16 30 43 55	4.00 4.29 4.62 5.00 5.45	75 76 77 78	56 53 51 49	0.93 •95 •97 •97 •98	44	33 48 1 14 26	4.00 4.62 4.62 5.00 5.45	75 76 77 78 79	15 10 6 3 1	0.92 •93 •95 •97 •97	15 14 13 12 11	21.1 19.7 18.4 17.0 15.6
80 81 82 83 84	46	5 12 5.00 77 39 .9 24 5.45 78 38 1.0 35 5.45 79 38 1.0 46 6.67 80 38 1.0 55 7.50 81 39 1.0 6 3 8.57 82 41 1.0				1.00 1.02 1.03 1.03 1.03	45	6 16 26 34 41	6.00 6.00 7.50 8.57 10.0	79 80 81 82 83	48 48 48 48 49	I.00 I.00 I.00 I.02 I.02	45	37 47 56 4	6.00 6.67 7.50 8.57	80 81 82 83	59 57 56 56 56	0.97 0.98 1.00 1.00	9 8 7 6	14.2 12.8 11.4 10.0 8.6
85 86 87 88 89		16 12.0 84 45 1.0 21 15.0 85 48 1.0 25 20.0 86 51 1.0 28 60.0 87 54 1.0		1.05 1.05 1.05 1.05 1.05		47 51 55 58 59	15.0 15.0 20.0 60.0 60.0		50 52 54 56 58	1.03 1.03 1.03 1.03 1.03		17 21 25 28 29	15.0 15.0 20.0 60.0 60.0	84 85 86 87 88	56 56 57 58 59	I.00 I.02 I.02 I.02 I.02	5 4 3 2 1	7.2 5.7 4.3 2.9 1.4		
90		30		90	0		46	0		90	0			30		90	0		0	0.0
t	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $						(a	$\frac{60'}{\Delta}$	i	b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
	d=43° 30′								d = 4	4° (0′			á	l=44	4° 3	80′			

$\setminus b$		a = 4	ŀ5° C)′			(a = 4	5° 8	30′				a = 4	6° (D′		\ c	a
$B \setminus$	h d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	0 0 0 42 1 25 2 7 50	I.40 I.43 I.40	45	, 0 0 1 2 4	0.00 .02 .02 .03	0 0 I 2	0 42 24 6 48	I.43 I.43 I.43 I.43 I.43	45	30 30 31 32 34	0.00	O I 2		1.43 1.46 1.43 1.43 1.46	46	0 0 1 2 4	0.00	90 89 88 87 86	90.0 89.3 88.6 87.9 87.1
5 0 7 8 9	3 32 4 14 57 5 39 6 21	I.40 I.43 I.43	l	6 9 13 17 21	0.05 .07 .07 .07	3 4 5 6	30 12 54 36 18	I.43 I.43 I.43 I.43 I.43		36 39 43 47 51	0.05 .07 .07 .07	3 4 5 6	28 10 51 33 14	1.43 1.46 1.43 1.46 1.43		6 9 13 17 21	0.05 .07 .07 .07	85 84 83 82 81	86.4 85.7 85.0 84.3 83.6
10 11 12 13 14	7 3 45 8 27 9 9 51	I.43 I.43 I.43		26 32 38 45 52	0.10 .10 .12 .12	7 8 9	0 41 23 4 46	1.46 1.43 1.46 1.43 1.46	46	56 2 8 15 22	0.10 .10 .12 .12	7 8 9	56 37 18 59 40	1.46 1.46 1.46 1.46 1.46		26 32 38 45 52	0.10 .10 .12 .12	80 79 78 77 76	82.8 82.1 81.4 80.7 79.9
15 16 17 18	10 33 11 15 56 12 37 13 18	3		10 11 12 13	27 8 49 30 11	1.46 1.46 1.46 1.46 1.46	47	30 38 47 56	0.13 .15 .15 .17	10 11 12 13	21 2 43 24 4	1.46 1.46 1.46 1.50 1.46	47	0 8 17 26 36	0.13 .15 .15 .17	75 74 73 72 71	79.2 78.4 77.7 77.0 76.2		
20 21 22 23 24	59 14 40 15 21 16 2 43	1.46 1.46 1.46	47	58	.20	14 15 16	52 33 13 54 34	1.46 1.50 1.46 1.50 1.50	48	17 28 40 52 5	0.18 .20 .20 .22 .23	14 15 16	45 25 5 45 25	1.50 1.50 1.50 1.50	48	47 58 10 22 35	0.18 .20 .20 .22 .23	70 69 68 67 66	75.4 74.7 73.9 73.2 72.4
25 26 27 28 29	17 23 18 3 43 19 23 20 3	1.50	48	49 18 33 49	0.23 .25 .25 .27 .28	17 18 19	14 54 33 13 52	1.50 1.54 1.50 1.54 1.54	49	19 33 48 3 19	0.23 .25 .25 .27 .28	17 18 19	5 44 23 2 41	I.54 I.54 I.54 I.54 I.54	49	49 3 17 33 49	0.23 .23 .27 .27 .28	65 64 63 62 61	71.6 70.8 70.0 69.2 68.4
30 31 32 33 34	42 21 21 22 0 39 23 18	1.54	50	6 24 42 1 20	0.30 .30 .32 .32 .35	20 21 22 23	31 10 48 26 4	1.54 1.58 1.58 1.58 1.58	50	36 54 12 30 50	0.30 .30 .30 .33	20 21 22	20 58 36 14 52	1.58 1.58 1.58 1.58 1.62	50	6 23 41 0	0.28 .30 .32 .32 .33	60 59 58 57 56	67.6 66.8 66.0 65.1 64.3
35 36 37 38 39	56 24 34 25 11 48 26 25	1.58 1.62 1.62 1.62 1.62	51	41 2 23 46 9	0.35 .35 .38 .38 .40	24 25 26	42 20 57 34 11	1.58 1.62 1.62 1.62 1.62	51 52	10 31 53 15 38	0.35 .37 .37 .38 .40	23 24 25	29 6 43 19 55	1.62 1.62 1.67 1.67 1.67	52 53	39 0 22 44 7	• 35 • 37 • 37 • 38 • 40	55 54 53 52 51	63.5 62.6 61.7 60.9 60.0
40 41 42 43 44	28 14 50 29 25	25 1.62 2 1.67 38 1.67 14 1.67 50 1.71 25 1.71		33 58 23 49 16	0.42 .42 .43 .45 .47	27 28 29	47 23 58 33 8	1.67 1.71 1.71 1.71 1.71	53 54	2 26 52 18 45	•43 •43 •45 •45	26 27 28	31 7 42 17 51	1.67 1.71 1.71 1.76 1.76	54 55	31 55 20 46 13	0.40 .42 .43 .45	50 49 48 47 46	59.1 58.2 57.3 56.4 55.4
45	30 0	1	4	44			43		55	12		29	25			40		45	54·5 ———
t	а	$\frac{60'}{\Delta}$	b		$\frac{\Delta}{60'}$	a	ı	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	1	b	$\frac{\Delta}{60'}$		a
ι		d = 4	5° 0	,			a	=4	5° 3	0′				d = 4	6° ()′			

\ b			a = 4	50 (γ			~	=48	ç o	n'				a = 4	6° ()′			\
	_			5 (_	_			, 3						0 (1 .	C	a
B	h	d	<u>6ο'</u> Δ	z	$\frac{t}{t}$	<u>Δ</u> 6ο'	h	$\frac{d}{}$	$\frac{60'}{\Delta}$	z	t	<u>Δ</u> 6ο'	h	$\frac{d}{d}$	$\frac{60'}{\Delta}$	z	*	<u>Δ</u> 6ο'	$C\setminus$	$\beta \setminus$
45 46 47 48 49	3° 31 32	ó 34 8 42 15	1.76 1.76 1.76 1.82 1.82	54 55 56	44 13 42 13 44	0.48 .48 .52 .52 .53	29 30 31	43 17 50 23 56	1.76 1.82 1.82 1.82 1.88	55 56 57	12 41 10 40 11	0.48 .48 .50 .52 .53	29 30 31	25 59 32 5 37	1.76 1.82 1.82 1.88 1.88	55 56 57	40 9 38 8 39	0.48 .48 .50 .52 .52	° 45 44 43 42 41	54.5 53.6 52.6 51.6 50.6
50 51 52 53 54	33 34	48 20 52 23 54	1.88 1.88 1.94 1.94 2.00	57 58 59	16 49 23 58 33	•.55 •57 •58 •58 •62	32 33 34	28 0 32 3 33	1.88 1.88 1.94 2.00 2.00	58 59	43 16 50 24 59	• 55 • 57 • 57 • 58 • 62	32 33 34	9 40 11 42 12	1.94 1.94 1.94 2.00 2.07	58 59 60	10 43 16 50 25	• 55 • 55 • 57 • 58 • 60	39 38 37 36	49.6 48.6 47.6 46.6 45.5
55 50 57 58 59	353637	24 53 22 51 19	2.07 2.07 2.07 2.14 2.22	60 61 62	47 26 5 45	.65 .65 .67 .68	35 36	3 32 0 28 56	2.07 2.14 2.14 2.14 2.22	60 61 62 63	36 13 51 30 9	.63 .65 .65	35 36	41 10 38 6 33	2.07 2.14 2.14 2.22 2.31	61 62 63	38 15 54 33	.62 .65 .65	35 34 33 32 31	44.5 43.4 42.3 41.2 40.1
60 61 62 63 64	38 39	46 12 38 3 27	2.31 2.31 2.40 2.50 2.50	63 64 65 66	26 8 51 35 20	•.7° •72 •73 •75 •75	37 38 39	23 49 14 39 3	2.31 2.40 2.40 2.50 2.61	64 65 66	50 32 14 57 42	0.70 .70 .72 .75 .75	37 38	59 25 50 14 38	2.31 2.40 2.50 2.50 2.61	64 65 66 67	14 55 37 20 3	0.68 •70 •72 •72 •75	30 29 28 27 26	39.0 37.9 36.7 35.5 34.4
65 66 67 68 69	40 41	51 14 36 58 19	2.61 2.73 2.73 2.86 3.00	67 68 69 70	5 52 40 28 17	0.78 .80 .80 .82 .83	40	26 49 11 32 52	2.61 2.73 2.86 3.00 3.00	67 68 69 70	27 13 0 48 36	0.77 .78 .80 .80	39 40	1 23 45 6 26	2.73 2.73 2.86 3.00 3.16	68 69 70	48 33 20 7 55	0.75 .78 .78 .80	25 24 23 22 21	33.2 32.0 30.8 29.5 28.3
70 71 72 73 74	4.2	39 58 16 33 49	3.16 3.33 3.53 3.75 3.75	71 72 73 74	7 58 50 42 35	0.85 .87 .87 .88	41 42	12 30 48 5 21	3.33 3.33 3.53 3.75 3.75	71 72 73 74	25 15 6 58 51	0.83 .85 .87 .88	41	45 3 21 38 54	3·33 3·33 3·53 3·75 4·00	71 72 73 74 75	43 33 23 14 6	0.83 .83 .85 .87 .87	20 19 18 17 16	27.0 25.8 24.5 23.2 21.9
75 76 77 78 79	43	5 19 33 46 57	4.29 4.29 4.62 5.45 5.45	75 76 77 78 79	29 24 19 15 12	0.92 .92 .93 .95	43	37 51 5 17 29	4.29 4.29 5.00 5.00 6.00	75 76 77 78 79	44 38 32 27 23	0.90 .90 .92 .93	42	9 23 36 48 0	4.29 4.62 5.00 5.00 6.00	76 77 78 79	58 51 45 39 34	0.88 .90 .90 .92	15 14 13 12 11	20.6 19.3 17.9 16.6 15.2
80 81 82 83 84	44	8 18 27 34 41	6.00 6.67 8.57 8.57 10.0	80 81 82 83 84	9 7 5 3 2	•97 •97 •97 •98 •98	44	39 49 57 5 12	6.00 7.50 7.50 8.57 12.0	80 81 82 83 84	19 16 13 10 8	0.95 •95 •95 •97 •97		10 20 28 35 42	6.00 7.50 8.57 8.57 12.0	80 81 82 83 84	29 25 21 17 14	0.93 •93 •93 •95 •95	10 9 8 7 6	13.9 12.5 11.2 9.8 8.4
85 86 87 88 89		47 52 55 58 59	12.0 20.0 20.0 60.0 60.0		I 0 0 0	0.98 1.00 1.00 1.00		17 22 25 28 29	12.0 20.0 20.0 60.0 60.0		6 5 3 2 1	0.98 •97 •98 •98		47 52 55 58 59	12.0 20.0 20.0 60.0 60.0		9 6 4 2	0.97 .95 .97 .97	5 4 3 2 1	7.0 5.6 4.2 2.8 1.4
90	45	0	0 90 0				_	30		90	0		44	0		90	0		0	0.0
+	0	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $						a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	(a	$\frac{60'}{\Delta}$	l	b	$\frac{\Delta}{60'}$		а
$\mid t \mid$			d=4	.5°	0′			(d=4	5° 8	30′				d = 4	6° (0′			

			•949				733							1
b	C	a=40	6° 30′			a = 4	7° 0′			a = 4	7° 30′		c	a
B	h d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h d	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	h d	<u>6ο′</u> Δ	Z	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
o 0 1 2 3 4	0 0 4I I 23 2 4 45	1.46 1.43 1.46 1.46	46 30 30 31 32 34	0.00 .02 .02 .03	0 0 4I I 22 2 3 44	1.46 1.46 1.46 1.46 1.46		0.00	0 / 0 0 4I I 2I 2 2 42	1.46 1.50 1.46 1.50 1.46	47 30 30 31 32 34	.02	90 89 88 87 86	90.0 89.3 88.5 87.8 87.1
5 6789	3 26 4 8 49 5 30 6 11	1.43 1.46 1.46 1.46 1.46	36 39 43 47 51	0.05 .07 .07 .07	3 25 4 5 46 5 27 6 7	1.50 1.46 1.46 1.50 1.46	I I I I I I I I I I I I I I I I I I I	.07	3 23 4 3 43 5 24 6 4	1.50 1.50 1.46 1.50 1.50	36 39 43 47 51	.07 3 .07 7 .07	85 84 83 82 81	86.3 85.6 84.9 84.1 83.4
10 11 12 13 14	52 7 33 8 14 55 9 35	1.46 1.46 1.46 1.50 1.46	56 47 2 8 15 22	0.10 .10 .12 .12	48 7 29 8 9 49 9 30	1.46 1.50 1.50 1.46 1.50	33 34 4 55	.10	44 7 24 8 4 44 9 24	1.50 1.50 1.50 1.50 1.50	48 2 8 12 21	2 .10 3 .10 4 .12	80 79 78 77 76	82.7 81.9 81.2 80.4 79.7
15 16 17 18 19	10 16 56 11 37 12 17 57	1.50 1.46 1.50 1.50 1.50	30 38 47 56 48 6	0.13 .15 .15 .17	10 10 50 11 30 12 10 50	1.50 1.50 1.50 1.50 1.54	48 6	3 .15 7 .15 5 .17	10 4 44 11 24 12 3 43	1.50 1.50 1.54 1.50 1.54	37 46 56 49	7 .15 5 .17 5 .17	75 74 73 72 71	78.9 78.2 77.4 76.6 75.9
20 21 22 23 24	13 37 14 17 57 15 36 16 16	1.50 1.50 1.54 1.50 1.54	17 28 40 52 49 5	0.18 .20 .20 .22 .22	13 29 14 9 48 15 27 16 6	1.50 1.54 1.54 1.54 1.54	49 49 2 34	.20	13 22 14 1 40 15 19 57	1.54 1.54 1.58 1.58	39 50 50	.20 .20 .22	70 69 68 67 66	75.1 74.3 73.5 72.8 72.0
25 26 27 28 29	55 17 34 18 13 51 19 30	1.54 1.54 1.58 1.54 1.54	18 32 47 50 2 18	0.23 .25 .25 .27 .28	45 17 24 18 2 40 19 18	1.54 1.58 1.58 1.58 1.58	50 1 3 4	2 .25	16 35 17 13 51 18 29 19 7	1.58 1.58 1.58 1.58 1.58	18 34 46 51	2 .23 5 .25 1 .27	65 64 63 62 61	71.2 70.4 69.6 68.8 67.9
30 31 32 33 34	20 8 46 21 24 22 1 38	1.58 1.58 1.62 1.62 1.62	35 52 51 10 29 48	0.28 .30 .32 .32 .33	56 20 34 21 11 48 22 25	1.58 1.62 1.62 1.62 1.62	51 2: 40 52 52 1;	30 .30	45 20 22 59 21 36 22 12	1.62 1.62 1.62 1.67 1.67	52 51 52 28 42	.30 .32 .32	59 58 57 56	67.1 66.3 65.4 64.6 63.7
35 36 37 38 39	23 15 52 24 28 25 4 40	1.62 1.67 1.67 1.67 1.67	52 29 . 52 48 . 52 52 8 0. 67 29 . 67 51 . 67 53 13 .		23 2 38 24 14 50 25 25	1.67 1.67 1.67 1.71	53 53 54 54	35	48 23 24 24 0 35 25 10	1.67 1.67 1.71 1.71 1.76	53 2 27 48 54 10 31	7 ·35 8 ·37 0 ·38 3 ·38	55 54 53 52 51	62.9 62.0 61.1 60.3 59.4
40 41 42 43 44	26 16 51 27 26 28 0 34	1.71 59 0. 1.71 54 23 . 1.76 48 . 1.76 55 14 .		0.40 •42 •43 •45 •45	26 0 35 27 9 43 28 17	1.71 1.76 1.76 1.76 1.76	56	2 .42 7 .42 2 .45 9 .45	26 18 52 27 26 59	1.76 1.76 1.76 1.82 1.82	55 20 55 20 56 10	0 .42 5 .42 0 .43	47 46	58.5 57.6 56.6 55.7 54.8
45	29 8		56 8		50		3	5	28 32		57	3	45	53.8
	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	а	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$		a
t			6° 30′				7° 0′			d = 4	7° 30′	,		

b		a	ı = 46	3° 3	0′				a = 4	7° (D'			0	a=4	7° 3	30′		\ c	a
B	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	ŧβ
45 46 47 48 49	29 30 31	8 41 14 46 18	1.82 1.82 1.88 1.88	56 57 58	8 36 5 35	0.47 .48 .50 .52 .52	28 29 30	50 23 55 27 59	1.82 1.88 1.88 1.88	56 57 58	36 4 33 2 33	0.47 .48 .48 .52 .52	28 29 30	3 ² 5 37 8 39	1.82 1.88 1.94 1.94 1.94	57 58	3 31 0 29 59	0.47 .48 .48 .50 .52	° 45 44 43 42 41	53.8 52.9 51.9 50.9 49.9
50 51 52 53 54	32 33	49 20 51 21 50	1.94 1.94 2.00 2.07 2.07	59 60	37 9 42 16 51	•.53 •55 •57 •58 •58	31 32 33	30 0 30 0 29	2.00 2.00 2.00 2.07 2.07	59 60 61	36 8 42 16	•53 •53 •57 •57 •60	31 32 33	10 40 10 39 8	2.00 2.00 2.07 2.07 2.14	59 60 61	30 2 34 7 41	• 53 • 53 • 55 • 57 • 58	39 38 37 36	48.9 47.9 46.9 45.9 44.8
55 56 57 58 59	34 35 36	19 48 16 43 10	2.07 2.14 2.22 2.22 2.31	61 62 63	26 3 40 18 57	0.62 .62 .63 .65	34 35	58 26 53 20 46	2.14 2.22 2.22 2.31 2.31	62 63 64	52 28 4 42 21	0.60 .60 .63 .65	34 35	36 4 31 57 23	2.14 2.22 2.31 2.31 2.40	62 63 64	16 52 29 6 44	0.60 .62 .62 .63	35 34 33 32 31	43.8 42.7 41.6 40.5 39.4
60 01 62 63 64	<i>37</i> <i>38</i>	36 1 26 50 13	2.40 2.40 2.50 2.61 2.61	64 65 66 67	37 18 59 41 25	•.68 •.7° •.73 •.73	36 37	37 1 25 48	2.40 2.50 2.50 2.61 2.73	65 66 67	0 40 21 3 46	0.67 .68 .70 .72 .73	36 37	48 13 37 0 23	2.40 2.50 2.61 2.61 2.73	65 66 67 68	23 3 43 25 7	0.67 .67 .70 .70	30 29 28 27 26	38.3 37.2 36.0 34.9 33.7
65 60 67 68 69	39	36 58 19 39 59	2.73 2.86 3.00 3.00 3.16	68 69 70 71	9 54 39 26 13	•75 •75 •78 •78 •80	38 39	10 32 53 13 33	2.73 2.86 3.00 3.00 3.33	68 69 70 71	59	0.73 .75 .77 .77 .80	38 39	45 6 27 47 6	2.86 2.86 3.00 3.16 3.33	69 70 71	50 34 18 3 49	0.73 .73 .75 .77 .78	25 24 23 22 21	32.5 31.3 30.1 28.9 27.7
70 71 72 73 74	40 41	18 36 53 10 26	3.33 3.53 3.53 3.75 4.29	72 73 74 75	50 39 29 20	0.82 .82 .83 .85	40	51 9 26 42 58	3·33 3·53 3·75 3·75 4·29	72 73 74 75	7 56 45 35	0.80 .82 .82 .83	40	24 42 59 15 30	3.33 3.53 3.75 4.00 4.29	72 73 74 75	36 23 11 0 49	0.78 .80 .82 .82 .83	20 19 18 17 16	26.5 25.2 24.0 22.7 21.4
75 76 77 78 79	42	40 54 7 19 31	4.29 4.62 5.00 5.00 6.00	76 77 78 79	12 4 57 50 44	0.87 .88 .88 .90	41 42	12 26 39 51 2	4.29 4.62 5.00 5.45 6.00	76 77 78 79	26 17 9 2 55	0.85 .87 .88 .88	41	44 58 10 22 33	4.29 5.00 5.00 5.45 6.00	76 77 78 79 80	39 30 21 13 5	0.85 .85 .87 .87	15 14 13 12 11	20.1 18.8 17.5 16.2 14.9
80 81 82 83 84	43	41 50 58 6 12	6.67 7.50 7.50 10.0	80 81 82 83 84	38 33 29 24 20	•93 •93 •93 •93		12 21 29 36 42	6.67 7.5° 8.57 10.° 10.°	80 81 82 83 84	48 42 36 31 26	0.90 .90 .92 .92	42	43 52 0 7 13	6.67 7.50 8.75 10.0 12.0	81 82 83 84	58 51 44 38 32	0.88 .88 .90 .90	9 8 7 6	13.6 12.2 10.9 9.5 8.2
85 86 87 88 89		18 22 26 28 30	15.0 15.0 30.0 30.0	85 86 87 88 89	16 13 9 6 3	0.95 •93 •95 •95	43	48 52 56 58 0	15.0 15.0 30.0 30.0	85 86 87 88 89	21 17 12 8 4	c.93 .92 .93 .93		18 22 26 28 30	15.0 15.0 30.0 30.0	89	26 20 15 10 5	0.90 .92 .92 .92 .92	5 4 3 2 1	6.8 5.5 4.1 2.7 1.4
90		30		90 0 60' A A				0		90	0			30	10.1	90	0		0	0.0
		a			b	$\frac{\Delta}{60'}$	0	ı			b	$\frac{\Delta}{60'}$		a	60′ <u>∆</u>	1	b	$\frac{\Delta}{60'}$		a
t		ĺ	d=40	6° 3	0′			C	l = 4	.7° (O'			ä	l = 4	7° 8	30′			

1	Ī			4.00	<u> </u>		T	==					1	==					1/	Th.
1			a = a	48°	0′				a = 4	8°	30′				a = a	49°	0′		0	a
B	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	<u>Δ</u> 60'	C	β
0 I 2 3 4	11 22	40	1.50 1.50 1.50	1	0 0 1 2 4	.02		40	1.50 1.50 1.54 1.50 1.50	48	30 30 31 32 34	.02	C	39 19 58	1.54 1.50 1.54 1.54 1.50			4	89 88 87	90.0 89.3 88.5 87.8 87.0
5 6 7 8 9	56	40	1.50 1.50 1.50 1.50		6 9 13 17 21	0.05 .07 .07 .07	3 4 5	58 38 17 57	1.54 1.50 1.54 1.50 1.54		36 39 43 47 51	0.05 .07 .07 .07	3 4 5	56	1.54 1.54 1.54 1.54 1.54		6 9 13 17 21	0.05 .07 .07 .08	84 83 82	86.3 85.5 84.7 84.0 83.2
10 11 12 13 14	7 8 9	39 19	1.50 1.50 1.54 1.50 1.54		26 32 38 44 51	0.10 .10 .10 .12	6 7 8 9	36 16 55 34 13	1.50 1.54 1.54 1.54 1.54	49	56 8 14 21	0.10 .10 .10 .12	6 7 8 9	32 11 50 29 8	1.54 1.54 1.54 1.54 1.54		26 32 38 44 51	0.10 .10 .10 .12	80 79 78 77 76	82.5 81.7 81.0 80.2 79.4
15 16 17 18 19	10 11	58 38 17 56 35	1.50 1.54 1.54 1.54 1.54	49	59 7 16 25 35	0.13 .15 .15 .17	10 11	52 31 10 49 28	1.54 1.54 1.54 1.54 1.58	50	29 37 46 55 5	0.13 .15 .15 .17	10 11	47 25 4 42 20	1.58 1.54 1.58 1.58 1.58	50	59 7 16 25 35	0.13 .15 .15 .17	75 74 73 72 71	78.7 77.9 77.1 76.3 75.5
20 21 22 23 24	13 14 15	53 31 9 47	1.54 1.58 1.58 1.58 1.58	50	46 57 9 21 34	0.18 .20 .20 .22	13 14 15	6 44 22 0 38	1.58 1.58 1.58 1.58 1.58	51	16 27 38 50 3	0.18 .18 .20 .22	13 14 15	58 36 14 51 29	1.58 1.58 1.62 1.58 1.62	51	45 56 8 20 33	0.18 .20 .20 .22 .22	70 69 68 67 66	74.8 74.0 73.2 72.4 71.6
25 26 27 28 29	16 17 18	25 3 41 19 56	1.58 1.58 1.58 1.62 1.62	51	47 1 16 31 47	0.23 .25 .25 .27	16 17 18	16 53 30 7 44	1.62 1.62 1.62 1.62 1.62	52	17 31 45 0 16	0.23 .23 .25 .27	16 17 18	6 43 20 56 33	1.62 1.62 1.67 1.62 1.67	52	46 0 14 29 45	0.23 .23 .25 .27 .28	65 64 63 62 61	70.7 69.9 69.1 68.3 67.5
30 31 32 33 34	19 20 21	33 10 46 22 58	1.62 1.67 1.67 1.67 1.67	52 53	3 20 38 56 15	0.28 .30 .30 .32 .33	19 20 21	21 57 33 9 45	1.67 1.67 1.67 1.67 1.71	53	32 49 7 25 44	0.28 .30 .30 .32 .33	19 20 21	9 45 21 56 31	1.67 1.67 1.71 1.71	53 54	2 19 36 54 13	0.28 .28 .30 .32 .33	60 59 58 57 56	66.6 65.8 64.9 64.1 63.2
35 36 37 38 39	22 23 24	34 10 45 20 54	1.67 1.71 1.71 1.76 1.76	54 55	35 56 17 39	•35 •35 •37 •37 •38	22 23 24	20 55 30 5 39	1.71 1.71 1.71 1.76 1.76	54 55	4 24 45 7 29	• 33 • 35 • 37 • 37 • 38	22 23 24	6 41 15 49 23	1.71 1.76 1.76 1.76 1.76	55	33 53 14 35 57	•33 •35 •35 •37 •38	55 54 53 52 51	62.3 61.4 60.6 59.7 58.8
40 41 42 43 44	25 26 27	28 2 36 9 42	1.76 1.76 1.82 1.82 1.88	56 57	24 48 13 38 4	0.40 .42 .42 .43 .45	252627	13 46 19 52 24	1.82 1.82 1.82 1.88 1.88	56 57	52 16 41 6 32	0.40 .42 .42 .43 .43	25 26 27	35	1.82 1.82 1.88 1.88 1.94	56 57	20 44 8 33 59	0.40 .40 .42 .43 .43	50 49 48 47 46	57.9 56.9 56.0 55.1 54.1
45	28	14			31			56			58			38		58	25		45	53.2
+	0	ı	$\frac{60'}{\Delta}$	ľ		$\frac{\Delta}{60'}$	а		$\frac{60'}{\Delta}$	l		$\frac{\Delta}{60'}$	a		$\frac{60'}{\Delta}$	ĕ	,	$\frac{\Delta}{60'}$		a.
t		,	d = 4	8° 0)′			d	=48	° 3	0′			a	l=4	9° ()′			

6			a = 4	8° ()′			(a = 4	8° 8	30′				a = 4	9°	0′		c	a
B	h	d	$\frac{60'}{\Delta}$	z	·t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	·t	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	28 29 30	14 46 18 49 20	1.88 1.88 1.94 1.94 2.00	57 58 59	31 59 27 56 26	0.47 .47 .48 .50 .50	27 28 29 30	56 28 59 30 0	1.88 1.94 1.94 2.00 2.00	57 58 59	58 26 54 23 52	0.47 .47 .48 .48 .50	27 28 29	38 9 40 11 41	1.94 1.94 1.94 2.00 2.07	58 59 60	25 52 20 49 18	0.45 •47 •48 •48 •50	° 45 44 43 42 41	53.2 52.2 51.2 50.2 49.3
50 51 52 53 54	31 32	50 20 49 18 46	2.00 2.07 2.07 2.14 2.14	60 61 62	56 28 0 33 7	•53 •53 •55 •57 •57	31 32	30 0 29 57 25	2.00 2.07 2.14 2.14 2.22	60 61 62	22 53 25 58 32	0.52 •53 •55 •57 •57	30 31 32	39 8 36 3	2.07 2.07 2.14 2.22 2.22	61 62	48 19 51 23 56	•53 •53 •55 •55	40 39 38 37 36	48.2 47.2 46.2 45.2 44.1
55 56 57 58 59	33 34 35	14 41 8 34 0	2.22 2.22 2.31 2.31 2.40	63 64 65	41 17 53 30 7	0.60 .60 .62 .62	33 34	52 19 45 11 36	2.22 2.31 2.31 2.40 2.40	63 64 65	6 41 16 53 30	0.58 .58 .62 .62 .63	33 34	30 57 23 48 13	2.22 2.31 2.40 2.40 2.50	63 64 65	30 5 40 16 53	0.58 .58 .60 .62 .63	35 34 33 32 31	43.1 42.0 40.9 39.8 38.7
60 61 62 63 64	36	25 49 13 36 58	2.50 2.50 2.61 2.73 2.73		46 25 5 46 28	.65 .67 .68 .7°	35 36	1 25 48 11 33	2.50 2.61 2.61 2.73 2.86	66 67 68	8 47 27 7 48	0.65 .67 .67 .68	35 36	37 1 24 46 8	2.50 2.61 2.73 2.73 2.86	66 67 68 69	31 9 48 28 8	0.63 .65 .67 .67	30 29 28 27 26	37.6 36.5 35.4 34.2 33.1
65 66 67 68 69	37 38	20 41 1 21 40	2.86 3.00 3.00 3.16 3.33	69 70 71 72	10 53 37 22 7	•.72 •73 •75 •75 •77	37 38	54 15 35 54 13	2.86 3.00 3.16 3.16 3.33	69 70 71 72	30 13 56 40 25	0.72 •72 •73 •75 •75	37	29 49 9 28 46	3.00 3.00 3.16 3.33 3.53	70 71 72	50 32 14 58 42	•.7° •.7° •.73 •.73	25 24 23 22 21	31.9 30.7 29.5 28.3 27.1
70 71 72 73 74	39 40	58 15 31 47 2	3.53 3.75 3.75 4.00 4.29	73 74 75 76	53 40 27 15	0.78 .78 .80 .82 .82	39	31 48 4 19 34	3.53 3.75 4.00 4.00 4.29	73 74 75 76	10 56 43 30 18	•.77 •.78 •.78 •.80	38 39	3 20 36 51 6	3.53 3.75 4.00 4.00 4.62	73 74 75 76	27 12 58 44 31	•75 •77 •77 •78 •80	20 19 18 17 16	25.9 24.7 23.5 22.2 21.0
75 76 77 78 79	41	16 29 41 53 3	4.62 5.00 5.00 6.00 6.00	78 79	53 43 33 24 15	0.83 .83 .85 .85	40	48 I I3 24 34	4.62 5.00 5.45 6.00 6.00	77 78 79 80	6 55 45 35 25	0.82 .83 .83 .83	40	19 32 44 55 5	4.62 5.00 5.45 6.00 6.00	77 78 79 80	7 56 45 35	0.80 .82 .82 .83	15 14 13 12 11	19.7 18.4 17.1 15.8 14.6
80 81 82 83 84		13 22 30 37 43	6.67 7.50 8.57 10.0 12.0	81 82 83 84	7 59 52 45 38	0.87 .88 .88 .88	41	44 53 1 8 14	6.67 7.50 8.57 10.0 12.0	81 82 83 84	16 7 59 51 43	0.85 .87 .87 .87 .87		15 23 31 38 44	7.50 7.50 8.57 10.0	81 82 83 84	25 15 6 57 48	0.83 .85 .85 .85	10 9 8 7 6	13.2 11.9 10.6 9.3 8.0
85 86 87 88 89	42	48 52 56 58 0	15.0 15.0 30.0 30.0		31 24 18 12 6	0.88 .90 .90 .90	=	19 23 26 28 30	15.0 20.0 30.0 30.0	85 86 87 88 89	35 28 21 14 7	0.88 .88 .88 .88	41	49 53 56 58 0	15.0 20.0 30.0 30.0	85 86 87 88 89	40 32 24 16 8	0.87 .87 .87 .87 .87	5 4 3 2 1	6.7 5.3 4.0 2.7 1.3
90	_	0		90	0			30		90	0			0		90	0		0	0.0
$ _t$	0	ı	$\frac{60'}{\Delta}$	t	Ò	$\frac{\Delta}{60'}$	a	ı	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$	i	Ь	$\frac{\Delta}{60'}$		a
			d = 4	8° 0)′			C	l=48	8° 3	0′				d = 4	9° ()′			

6	a	i = 49	9° 3	0′				a = 5	0° ()′			C	a = 50)° 3	0′		\ c	a
B	h d	$\frac{60'}{\Delta}$	Z	t	<u>Δ</u> 60'	h	d	$\frac{60'}{\Delta}$	\overline{z}	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	\overline{z}	t	$\frac{\Delta}{60'}$	C	β
0 0 1 2 3 4	0 0 39 1 18 57 2 36	1.54 1.54 1.54 1.54 1.54	49	30 30 31 32 34	0.00 .02 .02 .03	0 I 2	39 17 56 34	1.54 1.58 1.54 1.58 1.54	50	0 0 1 2 4	0.00 .02 .02 .03	0 0 1 2	38 16 54 33	1.58 1.58 1.58 1.54 1.54	50	30 30 31 32 34	0.00	90 89 88 87 86	90.0 89.2 88.5 87.7 86.9
5 6 7 8 9	3 15 54 4 32 5 11 50	1.54 1.58 1.54 1.54 1.54		36 39 43 47 51	0.05 .07 .07 .07	3 4 5	13 51 30 8 46	1.58 1.54 1.58 1.58 1.54		6 9 13 17 21	0.05 .07 .07 .07	3 4 5	11 49 27 5 43	1.58 1.58 1.58 1.58 1.62		36 39 43 47 51	0.05 .07 .07 .07	85 84 83 82 81	86.2 85.4 84.6 83.9 83.1
10 11 12 13 14	6 29 7 7 46 8 24 9 2	1.58 1.54 1.58 1.58 1.58	50	56 1 7 14 21	0.08 .10 .12 .12	6 7 8	25 3 41 19 57	1.58 1.58 1.58 1.58 1.58		26 31 37 44 51	0.08 .10 .12 .12	6 7 8	20 58 36 14 51	1.58 1.58 1.58 1.62 1.58	51	56 1 7 14 21	0.08	80 79 78 77 76	82.3 81.5 80.8 80.0 79.2
15 16 17 18 19	10 18 56 11 34 12 12	1.58 1.58 1.58 1.58 1.58	51	29 37 46 55 5	0.13 .15 .15 .17	9 10 11 12	35 12 50 28 5	1.62 1.58 1.58 1.62 1.62	51	59 7 15 24 34	0.13 .13 .15 .17	9 10	29 6 43 20 57	1.62 1.62 1.62 1.62 1.62	52	28 36 45 54 4	0.13 .15 .15 .17	75 74 73 72 71	78.4 77.6 76.8 76 0 75.2
20 21 22 23 24	50 13 28 14 5 42 15 19	1.58 1.62 1.62 1.62 1.62	52	26 38 50 2	0.18 .20 .20 .20	13 14 15	42 19 56 33 9	1.62 1.62 1.62 1.67 1.67	52	45 56 7 19 32	0.18 .18 .20 .22	12 13	34 11 47 23 59	1.62 1.67 1.67 1.67 1.67	53	14 25 37 49	0.18 .20 .20 .20	70 69 68 67 66	74·4 73.6 72.8 72.0 71.2
25 20 27 28 29	56 16 33 17 9 45 18 21	1.62 1.67 1.67 1.67 1.67	53	15 29 44 59 15	0.23 .25 .25 .27 .27	16 17 18	46 22 58 34 10	1.67 1.67 1.67 1.67 1.71	53	45 59 13 28 44	0.23 .23 .25 .27	15 16 17	35 11 47 23 58	1.67 1.67 1.67 1.71	54	14 28 42 57 13	c.23 .23 .25 .27 .27	65 64 63 62 61	70.3 69.5 68.7 67.8 67.0
30 31 32 33 34	57 19 33 20 8 43 21 18	1.67 1.71 1.71 1.71 1.76	54	31 48 5 23 42	0.28 .28 .30 .32 .32	19 20 21	45 20 55 30 4	1.71 1.71 1.71 1.76 1.76	54 55	0 17 34 52 11	0.28 .28 .30 .32	18 19 20	33 8 42 16 50	1.71 1.76 1.76 1.76 1.76	55	29 46 3 21 39	0.28 .28 .30 .30 .32	59 58 57 56	66.1 65.3 64.4 63.6 62.7
35 36 37 38 39	52 22 26 23 0 34 24 7	1.76 1.76 1.76 1.82 1.82	5 5	1 21 42 3 25	0.33 .35 .35 .37 .38	22 23	38 12 46 19 52	1.76 1.76 1.82 1.82 1.88	56	30 50 10 32 54	0.33 .33 .37 .37	21 22 23	24 57 30 3 36	1.82 1.82 1.82 1.82 1.88	56 57	58 18 39 0 22	0.33 .35 .35 .37 .37	55 54 53 52 51	61.8 60.9 60.0 59.1 58.2
40 41 42 43 44	40 25 13 45 26 17 49		5 <i>7</i> 58	48 12 36 1 26	0.40 .40 .42 .42 .43	24 25 26		1.88 1.88 1.88 1.94 1.94	57 58	16 39 3 28 53	0.38 .40 .42 .42 .43	24 25 26	8 40 11 42 13	1.88 1.94 1.94 1.94 1.94	58 59	44 7 31 55 20	0.38 .40 .40 .42 .43	50 49 48 47 46	57·3 56·3 55·4 54·5 53·5
45	27 20		- 0 1-				2		59	19			44			46		45	52.5
t	a		b	$\frac{\Delta}{60'}$	0	ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	(a	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$		а	
	a	l = 49	9° 3	0′				d = 5	60° ()′			(d = 5	0° 3	30°			

1.,																				N I	l.
b			a =	= 49°	30)′			•	a = 50)° ()′			a	a = 50	0° 3	0′		$\setminus c$	a
B	7	'in a	l	<u>60′</u> <u>△</u>	Z	t	<u>Δ</u> 6ο'	h	d	60' ▲	Z	t	<u>∆</u> 60′	h	d	$\left \frac{60'}{\Delta} \right $	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
45 46 47 48 49	7 2	° 27 2 5 28 2 5 29 2	I I	1.94 2.00 2.00 2.00 2.07	58 59 60	52 19 47 15 44	0.45 .47 .47 .48	27 28 29	32 32 32 32 1	2.00 2.00 2.00 2.07 2.07	59 60 61	19 46 13 41	0.45 •45 •47 •48 •50	26 27 28	44 14 43 12 41	2.00 2.07 2.07 2.07 2.07	59 60 61	46 12 39 7 36	0.43 .45 .47 .48 .48	° 45 44 43 42 41	52.5 51.6 50.6 49.6 48.6
50 52 52 53 53	1 3 2 3 3	30 I 4 31 I	7	2.07 2.14 2.14 2.22 2.22	61 62 63	45	0.52 .52 .53 .55 .55	30 31	30 58 26 53 20	2.14 2.14 2.22 2.22 2.31	62 63	40 10 41 13 45	•52 •53 •53 •55	29 30	38 5 32 58	2.14 2.22 2.22 2.31 2.31	62 63 64	5 35 6 37 9	0.50 .52 .52 .53	40 39 38 37 36	47.6 46.6 45.6 44.5 43.5
55 57 58 58	7 3	3 33 2	5 0 5	2.31 2.40 2.40 2.40 2.50	64 65 66	54 28 3 39 15	0.57 .58 .60 .60	32 33	46 12 37 2 26	2.31 2.40 2.40 2.50 2.50	64 65 66	18 52 26 2 38	•57 •57 •60 •60	31 32 33	24 49 14 39 3	2.40 2.40 2.40 2.50 2.61	65 66 67	42 15 49 24 0	0.55 •57 •58 •60 •60	35 34 33 32 31	42.4 41.4 40.3 39.2 38.1
6: 6: 6: 6:	2 3	35 2	4 7 0 2 3	2.61 2.61 2.73 2.86 2.86	67 68 69	52 30 9 48 28	0.63 .65 .65 .67	34	50 13 35 56 17	2.61 2.73 2.86 2.86 2.86	67 68 69	14 52 30 9 48	0.63 .63 .65 .65	34	26 48 10 31 52	2.73 2.73 2.86 2.86 3.00	68 69 70	36 13 51 29 8	0.62 .63 .63 .65	30 29 28 27 26	37.0 35.9 34.8 33.6 32.5
65 66 66	5 7 3 3	2 4 37		3.00 3.16 3.16 3.33 3.53	70 71 72	9 51 33 16 59	0 70 .70 .72 .72 .73	36	38 58 17 35 53	3.00 3.16 3.33 3.33 3.53	70 71 72 73	28 9 51 33 16	0.68 •70 •70 •72 •72	35 36	12 31 50 8 26	3.16 3.16 3.33 3.33 3.75	71 72 73	48 28 9 50 32	0.67 .68 .68 .70 .72	25 24 23 22 21	31.3 30.2 29.0 27.8 26.6
70 7 7 7	1 2 3	38 2	7 3 9 4 8	3.75 3.75 4.00 4.29 4.62	73 74 75 76	43 28 13 59 45	0.75 .75 .77 .77	37 38	10 26 41 56 10	3.75 4.00 4.00 4.29 4.62	74 75 76	59 43 28 13 59	0.73 .75 .75 .77 .77	37	42 58 13 28 42	3.75 4.00 4.00 4.29 4.62	74 75 76 77	15 59 43 27 12	•.73 •.73 •.73 •.75 •.75	20 19 18 17 16	25.4 24.2 23.0 21.8 20.5
7: 7: 7: 7: 7: 7:	6 . 7 8	39 I 2	1 4 6 7	4.62 5.00 5.45 6.00 6.67	77 78 79 80	32 20 8 56 45	0.80 .80 .80 .82	39	23 35 47 57 7	5.00 5.00 6.00 6.00 6.67	77 78 79 80	45 32 19 6 54	0.78 .78 .78 .80 .80	38	55 7 18 28 38	5.00 5.45 6.00 6.00 6.67	78 79 80 81	57 43 30 17 4	0.77 .78 .78 .78 .78	15 14 13 12 11	19.3 18.0 16.8 15.5 14.2
86 8 8 8	1 2 3	40	6 4 2 8 4	7.50 7.50 10.0 10.0	81 82 83 84	34 23 13 3 54	0.82 .83 .83 .85		16 24 32 38 44	7.5° 7.5° 10.0 10.0	81 82 83 84	42 31 20 10 59	0.82 .82 .83 .82 .83	39	47 55 3 9	7.50 7.50 10.0 10.0	82 83 84 85	51 39 27 16 5	0.80 .80 .82 .82	9 8 7 6	13.0 11.7 10.4 9.1 7.8
8: 8: 8: 8: 8: 8:	7	2	9368	15.0 20.0 30.0 30.0	85 86 87 88 89	45 36 27 18 9	0.85 .85 .85 .85		49 53 56 58 0	15.0 20.0 30.0 30.0		49 39 29 19	0.83 .83 .83 .85 .83		19 23 26 28 30	15.0 20.0 30.0 30.0		54 43 32 21 10	0.82 .82 .82 .82	5 4 3 2 1	6.5 5.2 3.9 2.6 1.3
90		3	30		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				0		90	0			30		90	0		0	0.0
		a		$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	(ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		а	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
t			d	=49	9° 3	0′				d = 5	60°	0′	1		(d=5	0° 3	0′			
	1							1						1							E

b		a = 5	51° 0′			. 0	i=5	1° 3	0′				a = 5	2° (0′		\ c	
$B \setminus$	h d	60' Δ	Z	$\frac{\Delta}{60'}$	h	$\frac{d}{}$	$\frac{60'}{\Delta}$	z	t	<u>Δ</u> 6ο'	h	d	$\frac{6o'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	0 0 38 1 16 53 2 31	1.58 1.58 1.62 1.58 1.58	51 0 0 1 2 4	0.00 .02 .02 .03	0 I 2	37 15 52 29	1.62 1.58 1.62 1.62 1.58	51	30 30 31 32 34	0.00 .02 .02 .03	0 I 2	0 37 14 51 28	1.62 1.62 1.62 1.62 1.62	52	0 0 1 2 4	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.2 88.4 87.7 86.9
5 6 7 8 9	3 9 47 4 24 5 2 39	1.58 1.62 1.58 1.62 1.62	6 9 13 17 21	0.05 .07 .07 .07	3 4 5	7 44 21 58 35	1.62 1.62 1.62 1.62 1.62		36 39 42 46 51	0.05 .05 .07 .08	3 4 5	5 41 18 55 32	1.67 1.62 1.62 1.62 1.67		6 9 12 16 21	0.05 .05 .07 .08	85 84 83 82 81	86.1 85.3 84.5 83.7 82.9
10 11 12 13 14	6 16 54 7 31 8 8 45	1.58 1.62 1.62 1.62 1.62	26 31 37 44 51	0 08 10 .12 .12	6 7 8	12 49 26 3 40	1.62 1.62 1.62 1.62 1.67	52	56 1 7 13 20	0.08 .10 .10 .12	6 7 8	8 45 21 58 34	1.62 1.67 1.62 1.67 1.67		26 31 37 43 50	0.08 .10 .10 .12	80 79 78 77 76	82.1 81.4 80.6 79.8 79.0
15 16 17 18 19	9 22 59 10 36 11 13 49	1.62 1.62 1.62 1.67 1.62	58 52 6 15 24 34	0.13 .15 .15 .17	9 10 11	16 53 29 5 41	1.62 1.67 1.67 1.67 1.67	53	28 36 45 54 3	0.13 .15 .15 .15	9	10 46 22 58 34	1.67 1.67 1.67 1.67	53	58 6 14 23 33	0.13 .13 .15 .17	75 74 73 72 71	78.2 77.4 76.5 75.7 74.9
20 21 22 23 24	12 26 13 2 38 14 14 50	1.67 1.67 1.67 1.67 1.67	44 55 53 6 18 30	0.18 .18 .20 .20	12 13 14	17 53 29 5 40	1.67 1.67 1.67 1.71 1.71	54	13 24 35 47 0	0.18 .18 .20 .22	12 13 14	9 45 20 55 30	1.67 1.71 1.71 1.71 1.71	54	43 54 5 17 29	0.18 .18 .20 .20	70 69 68 67 66	74.1 73.3 72.5 71.6 70.8
25 26 27 28 29	15 26 16 1 36 17 11 46	1.71 1.71 1.71 1.71 1.71	43 57 54 11 26 42	0.23 .23 .25 .27	15 16 17	15 50 25 0 34	1.71 1.71 1.71 1.76 1.76	55	13 26 40 55 10	0.22 .23 .25 .25	15 16 17	5 40 14 48 22	1.71 1.76 1.76 1.76 1.76	55	42 55 9 24 39	0.22 .23 .25 .25	65 64 63 62 61	70.0 69.1 68.3 67.4 66.5
30 31 32 33 34	18 20 55 19 29 20 3 37	1.71 1.76 1.76 1.76 1.76	58 55 14 31 49 56 7	0.27 .28 .30 .30	19	8 42 16 49 22	1.76 1.76 1.82 1.82 1.82	56	26 43 0 18 36	0.28 .28 .30 .30	18 19 20	56 29 2 35 8	1.82 1.82 1.82 1.82 1.82	56 57	55 11 28 46 4	0.27 .28 .30 .30	59 58 57 56	65.7 64.8 63.9 63.1 62.2
35 36 37 38 39	21 10 43 22 16 48 23 20	1.82 1.82 1.88 1.88	26 46 57 7 28 49	0.33 .35 .35 .35 .37	2I 22 23	55 28 0 32 4	1.82 1.88 1.88 1.88	5 <i>7</i>	55 14 34 55 17	0.32 •33 •35 •37 •37		41 13 45 17 48	1.88 1.88 1.88 1.94 1.94	58	23 42 2 23 44	•33 •35 •35 •35	55 54 53 52 51	61.3 60.4 59.5 58.6 57.6
40 41 42 43 44	52 24 23 54 25 25 55	1.94 1.94 1.94 2.00 2.00	58 11 34 58 59 22 47	0.38 .40 .40 .42 .42	24 25	35 6 37 7 37	1.94 1.94 2.00 2.00 2.00	59 60	39 2 25 49 13	0.38 .38 .40 .40 .43	24	19 50 20 50 19	1.94 2.00 2.00 2.07 2.07	59 60	6 29 52 15 40	0.38 .38 .38 .42 .42	50 49 48 47 46	56.7 55.8 54.8 53.9 52.9
45	26 25		60 12		26	7			39			48		61	5		45	52.0
$ _t$	а	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	а	,	60' Δ		b	$\frac{\Delta}{60'}$	0	ı	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$		a
		d = 5	1° 0′			C	l=5	1° 3	0′				d=5	2° ()′	0		

ſ	<u> </u>					_		_						_						1	1
	\ b			a = 5	61° (0′				a = 5	1° 3	30′				a = 5	52°	0′		$\setminus c$	a
	$B \setminus$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	C	β
	o 45 46 47 48 49	26 27 28	25 55 24 53 21	2.00 2.07 2.07 2.14 2.14	60° 61 62	12 38 5 33 1	0.43 .45 .47 .47	26 27 28	7 36 5 33 1	2.07 2.07 2.14 2.14 2.14	60 61 62	39 5 31 58 26	0.43 .43 .45 .47 .48	25 26 27	48 17 46 14 41	2.07 2.07 2.14 2.22 2.22	6i 62	31 57	0.43 .43 .45 .47	° 45 44 43 42 41	52.0 51.0 50.0 49.0 48.0
	50 51 52 53 54	29 30	49 17 44 10 36	2.14 2.22 2.31 2.31 2.31	63 64	30 30 1 33	0.50 .50 .52 .53	29 30	29 56 23 49	2.22 2.22 2.31 2.31 2.40	63 64	55 24 54 25 56	0.48 .50 .52 .52 .53	28 29	8 35 1 27 52	2.22 2.31 2.31 2.40 2.40	63 64 65	20 49 19 49 20	0.48 .50 .50 .52 .53	40 39 38 37 36	47.0 46.0 45.0 43.9 42.9
	55 56 57 58 59	31	2 27 51 15 39	2.40 2.50 2.50 2.50 2.61	65 66 67	5 38 12 47 22	0.55 .57 .58 .58	31 32	40 4 28 52 15	2.50 2.50 2.50 2.61 2.73	65 66 67	28 I 35 9 43	• 55 • 57 • 57 • 57 • 60	30	17 41 5 28 51	2.50 2.50 2.61 2.61 2.73	66 67 68	52 24 57 31 5	0.53 •55 •57 •57 •58	35 34 33 32 31	41.8 40.8 39.7 38.6 37.5
	60 61 62 63 64	33 34	2 24 45 6 27	2.73 2.86 2.86 2.86 3.00	68 69 70	58 34 11 49 27	0.60 .62 .63 .63	33 34	37 59 20 41 1	2.73 2.86 2.86 3.00 3.00	68 69 70	19 55 31 9 47	0.60 .60 .63 .63	32	13 35 56 16 36	2.73 2.86 3.00 3.00 3.16	69 70 71	40 15 51 28 6	0.58 .60 .62 .63	30 29 28 27 26	36.4 35.3 34.2 33.1 31.9
	65 66 67 68 69	35	47 6 24 42 59	3.16 3.33 3.33 3.53 3.75	71 72 73	6 46 26 7 49	0.67 .67 .68 •7° •7°	35	21 40 58 15 32	3.16 3.33 3.53 3.53 3.75	71 72 73 74	25 4 44 24 5	0.65 .67 .67 .68	34 35	55 13 31 48 5	3.33 3.33 3.53 3.53 3.75	72 73 74	44 22 I 4I 2I	0.63 .65 .67 .67	25 24 23 22 21	30.8 29.6 28.5 27.3 26.1
	70 71 72 73 74	36 37	15 31 46 0	3.75 4.00 4.29 4.62 4.62	74 75 76 77	31 14 57 41 25	0.72 •72 •73 •73 •75	36	48 3 18 32 45	4.00 4.00 4.29 4.62 4.62	75 76 77	47 29 11 54 38	0.70 .70 .72 .73 .73	36	21 36 50 4 17	4.00 4.29 4.29 4.62 5.00	75 76 77	2 44 26 8 51	0.70 .70 .70 .72 .72	20 19 18 17 16	24.9 23.7 22.5 21.3 20.1
	75 76 77 78 79	38	26 38 49 59	5.00 5.45 6.00 6.00 6.67	78 79 80 81	10 55 41 27 13	0.75 .77 .77 .77 .78	37	58 10 21 31 40	5.00 5.45 6.00 6.67 6.67	78 79 80 81	22 6 51 36 22	0.73 .75 .75 .77 .77	37	29 41 52 2 11	5.00 5.45 6.00 6.67 7.50	78 79 80 81	34 18 2 46 31	0.73 .73 .73 .75 .75	15 14 13 12 11	18.9 17.7 16.5 15.2 13.9
	80 81 82 83 84		18 26 33 39 45	7.50 8.57 10.0 10.0	82 83 84 85	0 47 34 22 10	0.78 .78 .80 .80	38	49 57 4 10 15	7.50 8.57 10.0 12.0 15.0	82 83 84 85	8 54 41 28 15	0.77 .78 .78 .78 .78		19 27 34 40 45	7.50 8.57 10.0 12.0 12.0	82 83 84 85	16 2 48 34 20	0.77 .77 .77 .77 .77	9 8 7 6	12.7 11.4 10.2 8.9 7.6
	85 86 87 88 89	39	49 53 56 58 0	15.0 20.0 30.0 30.0	86 87 88 89	58 46 34 23	0.80 .80 .82 .80		19 23 26 28 30	15.0 20.0 30.0 30.0		2 49 37 24 12	0.78 .80 .78 .80 .80	38	50 53 56 58 0	20.0 20.0 30.0 30.0		53 39 26 13	0.78 .77 .78 .78 .78	5 4 3 2 1	6.4 5.1 3.8 2.6 1.3
-	90		0		90	0			30		90	0			0		90	0		0	0.0
		(ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	a	ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
	t			d = 5	1° (D'			(d = 5	1° 3	30′				d = 5	2°	0′			

b	a	a = 52	2° 30′			a = 5	63° ()′			а	= 53	3° 3	0′		c	a
$B \setminus$	h d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	$\frac{d}{\Delta}$	z	$\stackrel{t}{\checkmark}$	$\frac{\Delta}{60'}$	h	$\frac{d}{}$	<u>6ο'</u> Δ	Z	\downarrow^t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 1 2 3 4	0 0 37 1 13 50 2 26	1.62 1.67 1.62 1.67 1.62	5 ² 30 30 31 32 32	.02	3 1 1 4	0 1.67 6 1.67 2 1.67 8 1.67 24 1.67	53	, 0 0 1 2 4	0.00 .02 .02 .03	0 0 I 2	ó 36 11 47 23	1.67 1.71 1.67 1.67	53	30 30 31 32 34	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.2 88.4 87.6 86.8
5 6 7 8 9	3 3 39 4 15 52 5 28	1.67 1.62 1.67 1.67	30 30 42 40 50	.05	3 4 I 4	0 1.67 36 1.67 2 1.67 8 1.67		6 9 12 16 20	0.05 .05 .07 .07	3 4 5	58 34 9 45 20	1.67 1.71 1.67 1.71 1.67		36 39 42 46 50	0.05 .05 .07 .07	85 84 83 82 81	86.0 85.2 84.4 83.6 82.8
10 11 12 13 14	6 4 40 7 16 52 8 28	1.67 1.67 1.67 1.67 1.67	53	.10	7 I 4	0 1.67 36 1.71 1 1.67 17 1.71 122 1.67		25 30 36 43 50	0.08 .10 .12 .12	6 7 8	56 31 6 41 16	1.71 1.71 1.71 1.71 1.71	54	55 0 6 12 19	0.08	80 79 78 77 76	82.0 81.2 80.4 79.6 78.7
15 16 17 18 19	9 4 40 10 15 51 11 26	1.67 1.71 1.67 1.71	2; 3; 44 5; 54	.15	9 3 10 4	8 1.71 8 1.71 8 1.71 3 1.71 1.71	54	57 5 13 22 32	0.13 .13 .15 .17	9 10	51 26 1 36 10	1.71 1.71 1.71 1.76 1.76	55	27 35 43 52 I	0.13 .13 .15 .15	75 74 73 72 71	77.9 77.1 76.3 75.5 74.6
20 21 22 23 24	12 I 36 13 II 46 14 20	1.71 1.71 1.71 1.76 1.76	12 2; 34 46 58	.18	12 2	1.76 27 1.71 2 1.76 36 1.76 1.76	55	42 52 3 15 27	0.17 .18 .20 .20	12 13 14	44 18 52 26 0	1.76 1.76 1.76 1.76 1.76		11 22 33 44 56	0.18 .18 .18 .20	70 69 68 67 66	73.8 73.0 72.1 71.3 70.4
25 26 27 28 29	54 15 28 16 2 36 17 10	1.76 1.76 1.76 1.76 1.82	55 11 22 38 56	.23	15 I 16 2	1.76 8 1.82 1.76 25 1.82 1.82	56	40 53 7 22 37	0.22 .23 .25 .25	15 16	34 7 40 13 46	1.82 1.82 1.82 1.82 1.88	56 57	9 22 36 50 5	0.22 .23 .23 .25 .27	65 64 63 62 61	69.6 68.7 67.9 67.0 66.1
30 31 32 33 34	43 18 16 49 19 22 54	1.82 1.82 1.82 1.88 1.88	22 49 57 57 12 32	.28	18 19	3 1.88 3 1.82 36 1.88 8 1.88 40 1.88	57	52 8 25 42 0	0.27 .28 .28 .30 .32	17 18 19	18 50 22 54 26	1.88 1.88 1.88 1.88	58	21 37 54 11 29	0.27 .28 .28 .30	60 59 58 57 56	65.2 64.4 63.5 62.6 61.7
35 36 37 38 39	20 26 58 21 30 22 1 32	1.88 1.88 1.94 1.94 2.00	58 16 30 59 1	33 33 35 35	2I I	1.94 1.94 1.94 1.94 2.00 2.00	59	19 38 58 18	0.32 .33 .33 .35 .35	20 21	57 28 59 29 59	1.94 1 94 2.00 2.00 2.00	59 60	47 6 25 45 6	0.32 •32 •33 •35 •35	55 54 53 52 51	60.8 59.9 59.0 58.0 57.1
40 41 42 43 44	23 2 32 24 2	2.00 2.00 2.00 2.07 2.07	3. 60 13 61 6	38 .40	23 1 24 1	2.00 2.00 45 2.07 2.07 2.07 2.14	61	22 45	0.37 .38 .38 .40 .42	22 23 24	29 58 27 56 24	2.07 2.07 2.07 2.14 2.14	61	27 49 12 35 59	0.37 .38 .38 .40	50 49 48 47 46	56.2 55.2 54.3 53.3 52.4
45	30		3		25 1	11		57			52		62	23		45	51.4
	а	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
t	0	d = 5	2° 30′			d = 3	53°	0′			c	l = 5	3° 3	30′			

\ b		0	t = 52	2° 3	0′				a = 5	3° (0′				i = 5	3° 5	30′			\ a
	_	$\frac{d}{d}$	60'		$\frac{t}{t}$	Δ		\overline{d}	60'		$\frac{t}{t}$	Δ	_	$\frac{d}{d}$	60'		$\frac{1}{t}$	Δ		
$B \setminus$	h	1	Δ	z	/	60'	h	\ <u>a</u>	$\frac{\delta \delta}{\Delta}$	z	/	60'	h	\ <u>a</u>	$\frac{30}{\Delta}$	z	/	60'	$C \setminus$	$\beta \setminus$
45 40		30 58	2.14	61	31 57	0.43 •43	25 25	11 39	2.14	61 62	57 22	0.42	0 24 25	52 20	2.14	62	48	0.42	° 45 44	51.4 50.4
47 48 49		26 54 21	2.14 2.22 2.22	62 63	23 50 17	•45 •45 •47	26 27	7 34 I	2.22 2.22 2.31	63	48 15 42	•45 •45 •45	26	47 14 40	2.22 2.31 2.31	63 64	39 6	·43 ·45 ·47	43 42 41	49·4 48·4 47·4
50 51	28	48 14	2.31	64	45 14	0.48 .48	-0	27 53	2.31	64	9 38	0.48	27	6 32	2.31	65	34	°.47	40 39	46.4 45.4
52 53 54	29	40 5 30	2.40 2.40 2.40	65	43 13 44	.50 .52 .52	28 29	19 44 8	2.40 2.50 2.50	65 66	7 36 6	.48 .50	28	57 22 46	2.40 2.50 2.50	66	31 0 30	.48 .50	38 37 36	44·4 43·3 42·3
55 56	30	55	2.50	_	15 47	∘.53 •53		32 56	2.50 2.61	67	37 9	•53 •53	29	33	2.61 2.61	67	0 31	0.52 •53	35 34	41.2 40.2
57 58 59	31	42 5 27	2.61 2.73 2.73	67 68	52 26	•55 •57 •58	30	19 41 3	2.73 2.73 2.73	68	41 14 47	•55 •55 •57	30	56 18 39	2.73 2.86 2.86	68 69	3 3 8	•53 •55 •57	33 32 31	39.1 38.0 37.0
60 61	32	49 10	2.86 2.86	69	36	0.58		25 46	2.86 3.00	69	21 56	0.58	31	0 2I	2,.86 3.00	70	42 16	0.57 .58	30 29 28	35·9 34·8
62 63 64		31 51 10	3.00 3.16 3.16	70 71	47 24	.60 .62	32	6 26 45	3.00 3.16 3.33	70 71	31 7 43	.60 .60	32	4I 0 I9	3.16 3.16 3.33	7I 72	51 26 2	.58 .60	27 26	33·7 32·5 31·4
65		29 47	3·33 3·33	72	2 40	0.63	33	3 21	3·33 3·53	72	20 58	o.63		37 55	3·33 3·53	73	38 15	0.62	25 24	30.3
67 68 69		5 22 38	3.53 3.75 3.75	73	19 58 37	.65 .65	34	38 55 11	3.53 3.75 4.00	73 74	36 14 53	.63 .65	33	12 28 44	3.75 3.75 4.00	74 75	52 30 9	.63 .65	23 22 2 I	28.0 26.8 25.7
70 71	35	54	4.00	75	18 59	o.68 .68		26 41	4.00 4.29	75 76	33 13	0.67 .68	34	59 13	4.29	76	48 27	0.65	20 19 18	24.5 23.3
72 73 74		23 36 49	4.62 4.62 5.00	76 77 78	40 21 3	.68 .7° .72	35	55 8 21	4.62 4.62 5.00	77 78	54 35 16	.68 .68		27 40 52	4.62 5.00 5.00	77	47 28	.67 .68	17 16	22.1 20.9 19.7
75 76		12	5•45 5•45	79	46 29	0.72 •72		33 44	5.45 6.00	79	58 40	0.70 •72	35	4	5.45	79	9 51	•.7°	15 14	18.5 17.3 16.1
77 78 79		23 33 42	6.00 6.67 7.50	80	56 40	•73 •73 •75	36	54 4 13	6.00 6.67 7.50	80	23 6 49	•72 •72 •73		25 35 44	6.00 6.67 7.50	80	33 15 58	.7° .72	13 12 11	14.9
80 81		50 57	8.57 8.57	82 83	25 9	•73 •75		2I 28	8.57 8.57	82 83	33 17	•73 •73	26	52 59	8.57	82	41 24	0.72 •72	1 0 9 8	12.5 11.2 10.0
82 83 84	37	4 10 15	12.0	84 85	54 39 25	•75 •77 •75		35 41 46	10.0 12.0 15.0	84	45 30	•73 •75 •75	36	5 11 16	10.0	84	7 51 35	•73 •73 •73	7 6	8. ₇ 7. ₅
85 86 87		20 24	15.0	86	10 56	°-77		50 54	15.0	86 87	0	0.75 •75		20 24	15.0	86 87	19	○.73 ·73	5 4 3	6.3 5.0 3.8
88 89		27 29 30	30.0 60.0		42 28 14	•77 •77	37	57 59 0	30.0 60.0	88 89	45 30 15	•75 •75 •75		27 29 30	30.0 60.0	88 89	47 31 16	•73 •75 •73	2 I	2.5
90		30		90	0			0		90	0			30		90	0		0	0.0
	а		6ο' Δ		b	$\frac{\Delta}{60'}$	(a	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	(a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
t		(d=5	2°	30′				$d = \xi$	53°	0′			a	l=5	3° 3	0′			

N												1						1	1
b		a = 5	4° ()′			a	u = 54	4° 3	30′				a = 5	5° ()′		$\setminus c$	a
$B \setminus$	h d	$\frac{60'}{\Delta}$	\overline{z}	t	$\frac{\Delta}{60'}$	h	$\stackrel{d}{\searrow}$	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 1 2 3 4	0 0 35 1 11 46 2 21	1.71 1.67 1.71 1.71	54	0 0 1 2 4	0.00 .02 .02 .03	0 I 2	0 35 10 44 19	1.71 1.71 1.76 1.71	54	30 30 31 32 34	0.00 .02 .02 .03	0 I 2	0 34 9 43 18	1.76 1.71 1.76 1.71	55	0 0 1 2 4	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.2 88.4 87.6 86.7
5 6 7 8 9	56 3 31 4 6 41 5 16	1.71 1.71 1.71 1.71 1.71		6 9 12 16 20	0.05 .05 .07 .07	3 4 5	54 29 3 38 13	1.71 1.76 1.71 1.71 1.76		36 39 42 46 50	0.05 .05 .07 .07	3 4 5	52 26 0 35	1.76 1.76 1.71 1.76 1.76		6 9 12 16 20	0.05 .05 .07 .07	85 84 83 82 81	85.9 85.1 84.3 83.5 82.7
10 11 12 13 14	51 6 26 7 1 36 8 11	1.71 1.71 1.71 1.71 1.76		25 30 36 42 49	0.08 .10 .10 .12	6 7 8	47 22 56 30 4	1.71 1.76 1.76 1.76 1.76	55	55 0 6 12 19	0.08 .10 .10 .12	6 7	43 17 51 25 59	1.76 1.76 1.76 1.76 1.82		25 30 36 42 49	0.08 .10 .10 .12	80 79 78 77 76	81.8 81.0 80.2 79.4 78.5
15 16 17 18	45 9 19 54 10 28 11 2	1.76 1.71 1.76 1.76 1.76	55	56 4 12 21 31	0.13 .13 .15 .17	9	38 12 46 20 54	1.76 1.76 1.76 1.76 1.82	56	26 34 42 51 0	0.13 .13 .15 .15	8 9 10	32 6 39 13 46	1.76 1.82 1.76 1.82 1.82	56	56 3 11 20 29	0,12 .13 .15 .15	75 74 73 72 71	77.7 76.9 76.0 75.2 74.3
20 21 22 23 24	36 12 10 43 13 17 50	1.76 1.82 1.76 1.82 1.82	56	41 51 2 14 26	0.17 .18 .20 .20	11 12 13	27 I 34 7 40	1.76 1.82 1.82 1.82 1.82		10 20 31 43 55	0.17 .18 .20 .20	11 12 13	19 52 25 57 30	1.82 1.82 1.88 1.82 1.88	57	39 49 0 12 24	0.17 .18 .20 .20	70 69 68 67 66	73.5 72.6 71.8 70.9 70.1
25 26 27 28 29	14 23 56 15 29 16 1 33	1.82 1.82 1.88 1.88 1.88	57	38 51 5 19 34	0.22 .23 .23 .25 .25	14 15 16	13 45 17 49 21	1.88 1.88 1.88 1.88	57 58	7 20 34 48 3	0.22 .23 .23 .25	14 15 16	34 6 37 9	1.88 1.88 1.94 1.88 1.94	58	36 49 2 16 31	0.22 .22 .23 .25	65 64 63 62 61	69.2 68.3 67.5 66.6 65.7
30 31 32 33 34	17 5 37 18 9 40 19 11	1.88 1.88 1.94 1.94 1.94	58	49 5 22 39 56	0.27 .28 .28 .28 .30	17 18	53 24 55 26 57	1.94 1.94 1.94 1.94 2.00	59	18 34 50 7 24	0.27 .27 .28 .28 .30	1 <i>7</i> 18	40 11 42 12 42	I.94 I.94 2.00 2.00	59	46 2 18 35 52	0.27 .27 .28 .28	59 58 57 56	64.8 63.9 63.0 62.1 61.2
35 36 37 38 39	42 20 I3 43 21 I3 43	1.94 2.00 2.00 2.00 2.07	59 60	14 33 52 12 33	0.32 .32 .33 .35	19 20 21	27 57 27 57 26	2.00 2.00 2.00 2.07 2.07	60 61	42 I 20 40 O	0.32 .32 .33 .33	19 20 21	12 42 12 41 10	2.00 2.00 2.07 2.07 2.14	60	10 28 47 7 27	0.30 .32 .33 .33	55 54 53 52 51	60.3 59.4 58.5 57.5 56.6
40 41 42 43 44	22 12 41 23 10 38 24 6	2.07 2.07 2.14 2.14 2.14	61 62	54 16 38 1 25	0.37 .37 .38 .40 .40	22	55 24 52 20 48	2.07 2.14 2.14 2.14 2.22	62	21 42 4 27 50	0.35 •37 •38 •38 •40	22	38 6 34 2 29	2. I4 2. I4 2. I4 2. 22 2. 22	62 63	48 9 31 53 16	•35 •37 •37 •38 •40	40	55·7 54·7 53.8 52.8 51.8
45	34			49		24	15		63	14			56			40		45	50.9
	a	<u>6ο′</u> Δ	b		$\frac{\Delta}{60'}$	C	ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$		a	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$		a
		d = 5	4° ()′			á	l = 54	4° 3	30′				d = 5	5°	0′			

$\setminus b$		($\alpha = 5$	4° ()′			а	= 54	° 3	0′			(a = 5	5° ()′		\ c	a
B	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	\overline{z}	t	<u>Δ</u> 6ο'	C	β
9 45 46 47 48 49	25	34 1 28 54 20	2.22 2.22 2.31 2.31 2.31	62 63 64	49 13 38 4 31	0.40 .42 .43 .45	24 25 26	15 42 8 34 0	2.22 2.31 2.31 2.31 2.40	63 64	14 38 3 29 55	0.40 •42 •43 •43	23 24 25	56 22 48 14 39	2.31 2.31 2.31 2.40 2.40	63 64 65	40 4 29 54 20	0.40 .42 .42 .43 .43	° 45 44 43 42 41	50.9 49.9 48.9 47.9 46.9
50 51 52 53 54	27	16 11 36 0 24	2.40 2.40 2.50 2.50 2.61	65 66	58 26 54 23 52	•47 •48 •48 •5°	27 28	25 50 14 38 1	2.40 2.50 2.50 2.61 2.61	65 66 67	22 49 17 46 15	0.45 •47 •48 •48 •50	26 27	4 28 52 16 39	2.50 2.50 2.50 2.61 2.61	66 67	46 13 41 9 38	•47 •47 •48 •48	40 39 38 37 36	45.9 44.8 43.8 42.8 41.7
55 56 57 58 59	29	17 10 32 54	2.61 2.73 2.73 2.86 2.86	67 68 69	22 53 25 57 29	•52 •53 •53 •53 •55	29	24 47 9 30 51	2.61 2.73 2.86 2.86 3.00	68 69	45 15 46 18 50	0.50 •52 •53 •53 •53	28 29	2 24 45 6 27	2.73 2.86 2.86 2.86 3.00	68 69 70	7 37 8 39 10	0.50 .52 .52 .52 .53	35 34 33 32 31	40.7 39.6 38.6 37.5 36.4
60 61 62 63 64	31	36 56 16 35	3.00 3.00 3.16 3.33 3.33	70 71 72	2 36 10 45 20	•57 •57 •58 •58 •60	30	11 31 51 10 28	3.00 3.00 3.16 3.33 3.53	70 71 72	22 55 29 3 38	• 55 • 57 • 57 • 58 • 58	30 31	47 7 26 44 2	3.00 3.16 3.33 3.33 3.53	71 72	42 15 48 22 56	0.55 .55 .57 .57 .58	30 29 28 27 26	35·3 34·3 33·1 32·0 30·9
65 66 67 68 69	33	1 1 28 45 1	3.53 3.53 3.75 3.75 4.00	73 74 75	56 32 9 46 24	0.60 .62 .62 .63	32	45 2 19 35 50	3.53 3.53 3.75 4.00 4.29	73 74 75	13 49 25 2 39	0.60 .60 .62 .62	32	19 36 52 8 23	3.53 3.75 3.75 4.00 4.29	73 74 75	31 6 42 18 55	0.58 .60 .60 .62 .62	25 24 23 22 21	29.8 28.7 27.5 26.4 25.2
70 71 72 73 74	34	32 46 59 12	4.29 4.62 4.62 5.00 5.45	76 77 78	3 42 21 1 41	0.65 .65 .67 .67	33	4 18 31 44 56	4.29 4.62 4.62 5.00 5.45	76 77 78	17 55 34 13 53	0.63 .65 .65 .67	33	37 51 4 16 28	4.29 4.62 5.00 5.00 5.45	76 77 78 79	32 9 47 26 5	0.62 .63 .65 .65	20 19 18 17 16	24.1 22.9 21.8 20.6 19.4
75 76 77 78 79	35	35 46 56 6	5.45 6.00 6.00 7.50 7.50	79 80 81 82	21 2 43 25 7	0.68 .68 .70 .70	34	7 18 28 37 45	5.45 6.00 6.67 7.50 7.50	79 80 81 82	33 13 53 34 15	0.67 .67 .68 .68	34	39 49 59 8 16	6.00 6.00 8.57 7.50 7.50	80 81 82	44 23 3 43 23	0.65 .67 .67 .68	15 14 13 12 11	18.2 17.0 15.8 14.6 13.4
80 81 82 83 84		22 29 36 41 46	8.57 8.57 12.0 12.0 15.0	83 84 85	49 31 13 56 39	0.70 .70 .72 .72 .73	35	53 0 6 12 17	8.57 10.0 10.0 12.0 15.0	83 84 85	56 38 20 2 44	0.70 .70 .70 .70		24 31 37 42 47	8.57 10.0 12.0 12.0 15.0	83 84 85	4 45 26 7 49	0.68 .68 .68 .70 .68	10 9 8 7 6	12.2 11.0 9.8 8.6 7.4
85 86 87 88 89		50 54 57 59	15.0 20.0 30.0 60.0	86 87 88 89	23 6 49 33 16	0.72 .72 .73 .72 .73		21 24 27 29 30	20.0 20.0 30.0 60.0	86 87 88 89	26 9 52 34 17	0.72 .72 .70 .72 .72		51 54 57 59 0	20.0 20.0 30.0 60.0	86 87 88 89	30 12 54 36 18	0.70 •70 •70 •70	2	6.1 4.9 3.7 2.5 1.2
90		0		90	0			30		90	0			0		90	0		0	0.0
$ \cdot _{t}$	а		$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	-	а	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$		а	6ο' Δ		<i>b</i>	$\frac{\Delta}{60'}$		a
			d = 5	64°	0′			Ó	l=5	4° 8	30′				$d = \xi$	55°	0′			

N .								_								7	1.
b	а	u=58	5° 30′			<i>a</i> =	56°	0′			а	= 56	3° 3	0′		$\setminus c$	0
$B \setminus$	h d	60' Δ	z	$\frac{\Delta}{60'}$	h	$d \frac{60}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	$\frac{d}{\langle}$	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{\epsilon o'}$	$C \setminus$	β
0 1 2 3 4	0 0 34 1 8 42 2 16	1.76 1.76 1.76 1.76 1.76	55 3 3 3 3 3	0 .02 I .02 2 .03	I 4	0 1.70 34 1.83 7 1.70 41 1.83 14 1.70		0 0 0 0 1 2 4	0.00		33 6 39 12	1.82 1.82 1.82 1.82 1.82	56	30 30 31 32 34	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.2 88.3 87.5 86.7
5 6 7 8 9	50 3 24 57 4 31 5 5	1.76 1.82 1.76 1.76 1.76	3 3 4 4 5	9 .05	3 2	18 1.8: 21 1.8: 54 1.70 28 1.8: 1 1.8:	5	6 9 12 16 20	0.05 .05 .07 .07	3	45 18 51 24 57	1.82 1.82 1.82 1.82 1.82		36 39 42 46 50	0.05 .05 .07 .07	85 84 83 82 81	85.9 85.0 84.2 83.4 82.5
10 11 12 13 14	39 6 12 46 7 19 53	1.82 1.76 1.82 1.76 1.82		0 .08 5 .10 I .12	6 7 1	7 1.8: 40 1.8: 13 1.8: 16 1.8:		24 29 35 41 48	0.08 .10 .10 .12	6 7	30 35 35 40	1.82 1.88 1.82 1.88 1.82	57	54 59 5 11 18	0.08 .10 .10 .12	80 79 78 77 76	81.7 80.8 80.0 79.2 78.3
15 16 17 18 19	8 26 59 9 32 10 5 38	1.82 1.82 1.82 1.82 1.88	2 3 4 5 5	3 .13 I .15 O .15	9 2	19 1.8 52 1.8 25 1.8 57 1.8 29 1.8	57	55 3 11 19 28	0.13 .13 .13 .15	9	13 45 17 49 21	1.88 1.88 1.88 1.88		25 32 40 49 58	0.12 .13 .15 .15	75 74 73 7 ² 7 ¹	77.5 76.6 75.8 74.9 74.1
20 21 22 23 24	11 10 43 12 15 47 13 19	1.82 1.88 1.88 1.88 1.88	57 I 3 4 5	1 .20	12	1 1.83 33 1.83 5 1.83 7 1.83 9 1.93	5 58	38 48 59 10 22	0.17 .18 .18 .20	11	53 25 56 27 58	1.88 1.94 1.94 1.94 1.94	58	7 17 28 39 50	0.17 .18 .18 .18	70 69 68 67 66	73.2 72.3 71.5 70.6 69.7
25 26 27 28 29	51 14 23 54 15 25 56	1.88 1.94 1.94 1.94 1.94	58 I 3 4 5	1 .23 5 .23	14 1 2 15 1	10 1.9. 11 1.9. 12 1.9. 13 1.9. 14 2.0	59 1	34 47 0 14 28	0.22 .22 .23 .23	14	29 0 31 1 31	1.94 1.94 2.00 2.00 2.00	59	2 15 28 42 56	0.22 .22 .23 .23	65 64 63 62 61	68.9 68.0 67.1 66.2 65.3
30 31 32 33 34	16 27 58 17 28 58 18 28	1.94 2.00 2.00 2.00 2.00	59 I 3 4 60 2	0 .27 6 .28 3 .28	17 1	14 2.0 14 2.0 14 2.0 14 2.0 13 2.0	60	43 58 14 30 47	0.25 .27 .27 .28 .30	16 17	31 1 30 59	2.00 2.00 2.07 2.07 2.07	60	11 26 42 58 15	0.25 .27 .27 .28	59 58 57 56	64.4 63.5 62.6 61.7 60.8
35 36 37 38 39	58 19 27 56 20 25 53	2.07 2.07 2.07 2.14 2.14	61 1 3 5	5 ·32 4 ·33 4 ·33	19 1 20	12 2.0 1 1 2.0 40 2.1 8 2.1 36 2.1	62	23 41	0.30 .30 .32 .33	19	28 56 24 52 20	2. I4 2. I4 2. I4 2. I4 2. I4	62	32 50 8 27 47	0.30 .30 .32 .33	55 54 53 52 51	59.9 58.9 58.0 57.1 56.1
40 41 42 43 44	21 21 49 22 16 43 23 10	2.14 2.22 2.22 2.22 2.22	62 I 3 5 63 I 4	5 · 37 7 · 37 9 · 38	22 2	4 2.2 3 I 2.2 5 8 2.2 2.5 2 2.3 2.3	63	23 45	0.35 .37 .37 .38	21	47 14 41 7 33	2.22 2.22 2.31 2.31 2.40	63 64	7 27 48 10 32	0.33 .35 .37 .37 .38		55.2 54.2 53.3 52.3 51.3
45	37		64	5	23 1	7		30			58			55		45	50.3
	а	<u>6ο'</u> Δ	b	$\frac{\Delta}{60'}$	а	<u>60</u> Δ		b	$\frac{\Delta}{60'}$	а	,	60' Δ		b	$\frac{\Delta}{60'}$		a
t	a		5° 30				56°	0′			C	l=5	6° 3	ŋ'			

	_																			
\b		а	= 5	5° 3	0′			Ш.,	a = 5	6° ()′			a	<i>t</i> = 56	3° 3	0′		$\setminus c$	a
B	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	\overline{z}	t	$\frac{\Delta}{60'}$	$c \setminus$	β
45 40 47 48 49	23 24 25	37 38 28 53 18	2.31 2.40 2.40 2.40 2.40	64 65	5 29 53 18 44	0.40 .40 .42 .43	23 24	17 43 33 58	2.31 2.40 2.40 2.40 2.50	64 65 66	30 54 18 43 8	0.40 .40 .42 .42 .43	22 23 24	58 23 48 13 37	2.40 2.40 2.40 2.50 2.50	64 65 66	55 18 42 7 32	0.38 .40 .42 .42 .42	9 45 44 43 42 41	50.3 49.4 48.4 47.4 46.4
50 51 52 53 54	26 27	43 7 31 54 16	2.50 2.50 2.61 2.73 2.73	.66 67 68	37 4 32 0	0.45 •45 •47 •47 •48	25 26	22 46 9 32 54	2.50 2.61 2.61 2.73 2.73	67 68	34 0 27 54 22	•43 •45 •45 •47 •48	25 26	1 24 47 9 31	2.61 2.61 2.73 2.73 2.73	67 68	57 23 50 17 45	0.43 .45 .45 .47 .47	40 39 38 37 36	45·3 44·3 43·3 42·3 41·2
55 56 57 58 59	28 29	38 0 22 43 3	2.73 2.73 2.86 3.00 3.00	69 70	29 59 29 59 30	0.50 .50 .50 .52 .53	27	16 37 58 18 38	2.86 2.86 3.00 3.00 3.00	69 70	51 20 50 20 51	0.48 .50 .50 .52 .52	27 28	53 14 34 54 14	2.86 3.00 3.00 3.00 3.16	69 70 71	13 41 10 40 10	•.47 •.48 •.50 •.50 •.52	35 34 33 32 31	40.2 39.1 38.1 37.0 35.9
60 61 62 63 64	30	23 42 0 18 36	3.16 3.33 3.33 3.33 3.53	71 72 73	2 34 7 40 14	•53 •55 •55 •57 •57	29 30	58 17 35 53 10	3.16 3.33 3.33 3.53 3.53	71 72 73	22 54 26 59 32	•53 •53 •55 •55 •55	29	33 52 10 27 44	3.16 3.33 3.53 3.53 3.53	72 73	41 12 44 16 49	•53 •53 •55 •55	30 29 28 27 26	34.9 33.8 32.7 31.6 30.5
65 66 67 68 69	31	53 10 26 41 55	3.53 3.75 4.00 4.29 4.29	74 75 76	48 23 58 34 10	0.58 .58 .60 .60	31	27 43 59 14 28	3.75 3.75 4.00 4.29 4.29	74 75 76	5 39 14 49 25	0.57 .58 .58 .60	30	1 17 32 47 1	3.75 4.00 4.00 4.29 4.62	74 75 76	22 56 30 4 39	•57 •57 •58 •60	25 24 23 22 21	29. 4 28. 2 27. I 26. 0 24. 8
70 71 72 73 74	32	9 23 36 48 59	4.29 4.62 5.00 5.45 5.45	77 78 79	46 23 0 38 16	.62 .63 .63	32	42 55 8 20 31	4.62 4.62 5.00 5.45 5.45	77 78 79	37 14 51 28	0.60 .62 .62 .62	32	14 27 40 52 3	4.62 4.62 5.00 5.45 6.00	77 78 79	50 26 3 40	0.58 .60 .62 .62 .62	20 19 18 17 16	23.7 22.6 21.4 20.2 19.1
75 76 77 78 79	33	10 20 30 39 47	6.00 6.00 6.67 7.50 8.57	80 81 82	55 34 13 52 32	0.65 .65 .65 .67	33	42 52 1 10 18	6.00 6.67 6.67 7.50 8.57	80 81 82	6 44 22 1 40	0.63 .63 .65 .65		13 23 32 40 48	6.00 6.67 7.50 7.50 8.57	80 81 82	17 54 32 10 48	0.62 .63 .63 .63	15 14 13 12 11	17.9 16.7 15.6 14.4 13.2
80 81 82 83 84	34	54 7 12 17	8.57 10.0 12.0 12.0 15.0	83 84 85	52 32	0.67 .67 .68 .67		25 32 38 43 47	8.57 10.0 12.0 15.0 15.0	83 84 85	59 38 18 58	0.67 .65 .67 .67	33	55 8 13 17	8.57 10.0 12.0 15.0 15.0	83 84 85 86	26 5 44 23 3	0.65 .65 .67	9 8 7 6	12.0 10.8 9.6 8.4 7.2
85 86 87 88 89		21 24 27 29 30	20.0 20.0 30.0 60.0	89	56 38 19	.68				89	18 59 39	.68		21 24 27 29 30	-	11 -	42 21 1 41 20	1	I	6.0 4.8 3.6 2.4 1.2
90	_	30	1	90	0		_	0		90	0	1 .	_	30	1	90	0		0	0.0
t		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
			d = 5	5° 3	30′				d = 3	56°	0′				d = 5	6° 3	30′			

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1	1/1	a = 5	7° 0′			C	a=5	7° 3	80′				a = 5	68°	0′		c	\ a
B	h	<u>6ο'</u> Δ	Z^{t}	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	C	β
0 I 2 3 4	0 0 33 1 5 38 2 11	1.82 1.88 1.82 1.82 1.88	57 O	.02	O I 2	32 4 37 9	1.88 1.88 1.82 1.88 1.88	57	30 30 31 32 34	0.00 .02 .02 .03	0 I 2	32 4 35 7	1.88 1.88 1.94 1.88	58	0 0 1 2 4	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.2 88.3 87.5 86.6
• 5 6 7 8 9	43 3 16 48 4 21 53	1.82 1.38 1.82 1.88 1.82	6 9 12 15	.05	3 4	41 13 45 17 49	1.88 1.88 1.88 1.88		36 39 42 45 49	0.05 .05 .05 .07	3 4	39 11 42 14 45	1.88 1.94 1.88 1.94 1.88		6 8 11 15	0.03 .05 .07 .07	85 84 83 82 81	85.8 84.9 84.1 83.2 82.4
10 11 12 13 14	5 26 58 6 30 7 2 34	1.88 1.88 1.88 1.88	24 29 35 41 47	0.08 .10 .10	5 6 7	21 53 25 57 28	1.88 1.88 1.88 1.94 1.88	58	54 59 4 10	0.08 .08 .10 .12	5 6 7	17 48 20 51 22	1.94 1.88 1.94 1.94 1.94		24 29 34 40 46	0.08 .08 .10 .10	80 79 78 77 76	81.5 80.7 79.8 79.0 78.1
15 16 17 18	8 6 38 9 10 42 10 13	1.88 1.88 1.88 1.94 1.94	58 2 10 18 27	0.13 .13 .13 .15	8 9 10	0 31 2 33 4	1.94 1.94 1.94 1.94 1.94		24 31 39 47 56	0.12 .13 .13 .15	8	53 24 55 26 56	1.94 1.94 1.94 2.00	59	53 0 8 17 26	0.12 .13 .15 .15	75 74 73 72 71	77·3 76·4 75·5 74·7 73·8
20 21 22 23 24	44 11 15 46 12 17 48	1.94 1.94 1.94 1.94 1.94	36 46 57 59 8 19	0.17 .18 .18 .18	11 12	35 6 37 7 37	1.94 1.94 2.00 2.00 2.00	59	6 16 26 37 48	0.17 .17 .18 .18	10 11 12	27 57 27 57 27	2,00 2,00 2,00 2,00 2,00	60	35 45 55 6	0.17 .17 .18 .18	70 69 68 67 66	72.9 72.1 71.2 70.3 69.4
25 26 27 28 29	13 19 49 14 19 49 15 19	2.00 2.00 2.00 2.00 2.07	31 44 57 60 10 24	0.22 .22 .22 .23	13 14 15	7 37 7 37 6	2.00 2.00 2.00 2.07 2.07	60	0 12 25 38 52	0,20 .22 .22 .23 .25	13	57 26 55 24 53	2.07 2.07 2.07 2.07 2.07	61	29 41 54 7 21	0.20 .22 .22 .23 .23	65 64 63 62 61	68.5 67.6 66.7 65.8 64.9
30 31 32 33 34	48 16 17 46 17 15 44	2.07 2.07 2.07 2.07 2.14	39 54 61 10 26 42	0.25 .27 .27 .27 .28	16 17	35 4 33 1 29	2.07 2.07 2.14 2.14 2.14	61	7 22 37 53 10	0.25 .25 .27 .28	15 16 17	22 50 18 46 14	2.14 2.14 2.14 2.14 2.14	62	35 50 5 21 37	0.25 .25 .27 .27 .28	59 58 57 56	64.0 63.1 62.2 61.3 60.4
35 36 37 38 39	18 12 40 19 8 36 20 3	2.14 2.14 2.14 2.22 2.22	62 17 35 54 63 13	0.30 .30 .32 .32 .33	18 19	57 25 52 19 46	2.14 2.22 2.22 2.22 2.31	63	27 44 2 21 40	0.28 .30 .32 .32 .32	18	42 9 36 3 29	2.22 2.22 2.22 2.31 2.31	63 64	54 11 29 47 6	0.28 .30 .30 .32 .32	55 54 53 52 51	59·4 58·5 57·6 56·6 55·7
40 41 42 43 44	30 56 21 22 48 22 14	30 2.31 33 33 0.3 56 2.31 53 53 34 14 2.31 48 2.31 2.40 58 3				12 38 4 30 55	2.31 2.31 2.31 2.40 2.40	64 65	59 19 40 1 23	0.33 .35 .35 .37 .37	20 21	55 21 46 11 36	2.31 2.40 2.40 2.40 2.50	65	25 45 5 26 48	0.33 .33 .35 .37 .37	50 49 48 47 46	54.7 53.8 52.8 51.8 50.8
45	39		65 20		22	20			45		22	0		66	10		45	49.9
	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$		ь	$\frac{\Delta}{60'}$		a
t		d = 5	7° 0′			C	l=5	7° 3	0′				d = 5	8° (0′			

7	1				ī						1			==	===		1\	l
$\setminus b$	(a = 5	8° 30′				a = 5	9° (0′				a = 5	9° 3	30′		$\setminus c$	a
$B \setminus$	h	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	$\frac{d}{}$	<u>6ο'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	6ο' Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	0 0 31 1 3 34 2 5	1.94 1.88 1.94 1.94 1.88	58 30 30 31 32 34	.02	0 0 1 2	0 31 2 33 4	1.94 1.94 1.94 1.94 2.00	59	0 0 1 2 4	0.00 .02 .02 .03	0 0 I 2	0 30 1 31 2	2.00 I.94 2.00 I.94 2.00	59	30 30 31 32 34	0.00 .02 .02 .03	90 89 88 87 86	90.0 89.1 88.3 87.4 86.6
5 6 78 9	37 3 8 39 4 10 41	1.94 1.94 1.94 1.94 1.94	36 38 41 45 49	.05	3 4	34 5 36 7 37	1.94 1.94 1.94 2.00		6 8 11 15 19	0.03 .05 .07 .07	3 4	32 2 33 3 3	2.00 1.94 2.00 2.00 2.00		36 38 41 45 49	0.03 .05 .07 .07	85 84 83 82 81	85.7 84.9 84.0 83.1 82.3
10 11 12 13 14	5 12 43 6 14 45 7 16	1.94 1.94 1.94 1.94	53 58 59 4 10 16	01.	5 6 7	8 38 9 39 9	2.00 1.94 2.00 2.00 2.00		23 28 33 39 45	0.08 .08 .10 .10	5 6 7	3 33 33 33 3	2.00 2.00 2.00 2.00 2.00	60	53 58 3 9	0.08 .08 .10 .10	80 79 78 77 76	81.4 80.5 79.7 78.8 77.9
15 16 17 18 19	8 17 47 9 17 47	2.00 2.00 2.00 2.00 2.00	23 30 38 46 55	.13	8 9	39 39 39 39	2.00 2.00 2.00 2.00 2.00	60	52 59 7 15 24	0.12 .13 .13 .15	8	33 32 1 31	2.00 2.07 2.07 2.00 2.07		22 29 37 45 53	0.12 .13 .13 .13	75 74 73 72 71	77.1 76.2 75.3 74.4 73.6
20 21 22 23 24	10 17 •47 11 17 47 12 16	2.00 2.00 2.00 2.07 2.07	60 4 14 24 34 45	.17	10 11 12	38 7 36 5	2.07 2.07 2.07 2.07 2.07	61	33 43 53 3 14	0.17 .17 .17 .18	10	0 29 58 26 55	2.07 2.07 2.14 2.07 2.14	61	2 12 22 32 43	0.17 .17 .17 .18	70 69 68 67 66	72.7 71.8 70.9 70.0 69.1
25 26 27 28 29	45 13 14 43 14 12 41	2.07 2.07 2.07 2.07 2.07 2.14	61 9 22 35 49	.22	13	34 31 59 27	2.07 2.14 2.14 2.14 2.14	62	26 38 50 3 17	0.20 .20 .22 .23	12 13 14	23 51 19 47 15	2.14 2.14 2.14 2.14 2.14 2.22	62	54 6 18 31 44	0.20 .20 .22 .22 .23	65 64 63 62 61	68.2 67.3 66.4 65.5 64.6
30 31 32 33 34	15 9 37 16 5 32 59	2.14 2.14 2.22 2.22 2.22	62 3 17 32 48 63 4	.25	15 16	55 23 50 17 44	2.14 2.22 2.22 2.22 2.22	63	31 45 0 15 31	0.23 .25 .25 .27 .28	15 16	42 9 36 3 29	2,22 2,22 2,22 2,31 2,31	63	58 13 28 43 58	0.25 .25 .25 .25 .27	59 58 57 56	63.7 62.8 61.8 60.9 60.0
35 36 37 38 39	17 26 53 18 20 46 19 12	2.22 2.22 2.31 2.31 2.31	21 38 55 64 13	.28	17	37 3 29 55	2.31 2.31 2.31 2.31 2.40	64	48 5 22 40 58	0.28 .28 .30 .30	1 <i>7</i> 18	55 21 47 12 37	2.31 2.31 2.40 2.40 2.40	64 65	31 48 6 24	0.28 .28 .30 .30 .32	55 54 53 52 51	59.0 58.1 57.1 56.2 55.2
40 41 42 43 44	38 20 3 28 53 21 17	2.40 2.40 2.40 2.50 2.50	65 11 31 66 13	•33 •35 •35	20	20 45 10 34 58	2.40 2.40 2.50 2.50 2.50	65 66	17 36 56 17 38	0.32 ·33 ·35 ·35 ·35		2 27 51 15 39	2.40 2.50 2.50 2.50 2.61	66 67	43 2 22 42 2	•33 •33 •33 •35	50 49 48 47 46	54·3 53·3 52·3 51·4 50·4
45	41		34		21	22			59		21	2			23		45	49-4
	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	a	ι	6ο' Δ		b	$\frac{\Delta}{60'}$	(ı	6ο' Δ		Ь	$\frac{\Delta}{60'}$		a
t			8° 30′				d = 5	9° ()′			(d = 5	9° 8	30′			

\ b		C	<i>u</i> = 58	8° 3	0′				a = 5	9° (0′			a	ı = 5	9° 3	0′		\ c	\ a
$B \setminus$	h	d	<u>6ο'</u> Δ	z	*	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	6ο' Δ	z	*	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	21 22 23	41 5 28 51 14	2.50 2.61 2.61 2.61 2.73	66 67 68	34 56 19 42 6	0.37 .38 .38 .40	2I 22	22 45 8 30 52	2.61 2.61 2.73 2.73 2.73	66 67 68	59 21 43 6 29	0.37 .37 .38 .38 .40	2°1 22	2 25 47 9 31	2.61 2.73 2.73 2.73 2.73	67 68	23 45 7 29 52	0.37 .37 .37 .38	° 45 44 43 42 41	49.4 48.4 47.4 46.4 45.4
50 51 52 53 54	24 25	36 58 19 40 0	2.73 2.86 2.86 3.00 3.00	69 70	30 55 20 45 11	0.42 .42 .42 .43 .45	23 24	14 36 57 17 37	2.73 2.86 3.00 3.00 3.00	69 70	53 17 42 7 33	0.40 .42 .42 .43 .43	23 24	53 14 35 55 15	2.86 2.86 3.00 3.00 3.16	69 70	16 40 4 29 54	0.40 .40 .42 .42 .43	40 39 38 37 36	44·4 43·4 42·3 41·3 40·3
55 56 57 58 59	26	20 40 59 18 36	3.00 3.16 3.16 3.33 3.33	71 72	38 5 33 1 29	0.45 •47 •47 •47 •48	25 26	57 17 36 54 12	3.00 3.16 3.33 3.33 3.53	71 72	59 26 53 20 48	•45 •45 •45 •47 •48	25	34 53 12 30 47	3.16 3.16 3.33 3.53 3.53	71 72 73	20 46 13 40 7	0.43 •45 •45 •45 •47	35 34 33 32 31	39.2 38.2 37.1 36.1 35.0
60 61 62 63 64	27 28	54 12 29 45 1	3.33 3.53 3.75 3.75 4.00	73 74	58 27 57 27 58	0.48 .50 .50 .52	27	29 46 3 19 35	3.53 3.53 3.75 3.75 4.00	73 74 75	17 46 15 45 15	0.48 .48 .50 .50	26 27	4 21 37 53 8	3.53 3.75 3.75 4.00 4.00	74 75	35 4 33 2 31	0.48 .48 .48 .48	30 29 28 27 26	34.0 32.9 31.8 30.7 29.6
65 66 67 68 69	29	16 31 45 59 12	4.00 4.29 4.29 4.62 5.00	75 76 77	29 0 32 4 37	0.52 •53 •53 •55 •55	28	50 4 18 31 44	4.29 4.29 4.62 4.62 4.62	76 77	45 16 47 19 51	•52 •53 •53 •53	28	23 37 51 4 17	4.29 4.29 4.62 4.62 5.00	76 77 78	31 2 33 5	0.50 •52 •52 •53 •53	25 24 23 22 21	28.5 27.4 26.3 25.2 24.1
70 71 72 73 74	30	24 36 48 59	5.00 5.00 5.45 6.00 6.00	78 79 80	10 43 17 51 25	0.55 .57 .57 .57 .57	29	57 9 20 30 40	5.00 5.45 6.00 6.00 6.00	78 79 80	23 56 29 2 36	• 55 • 55 • 55 • 57 • 57	29	29 41 52 2 12	5.00 5.45 6.00 6.00 6.67	79 80	37 9 41 14 47	•53 •53 •55 •55 •55	20 19 18 17 16	23.0 21.9 20.8 19.6 18.5
75 76 77 78 79		19 28 36 44 51	6.67 7.50 7.50 8.57 8.57	81 82 83	59 34 9 44 20	0.58 .58 .58 .60	30	50 59 7 15 22	6.67 7.50 7.50 8.57 8.57	81 82 83	10 44 18 53 28	•57 •57 •58 •58 •58		30 38 46 53	6.67 7.50 7.50 8.57 10.0	81 82 83	20 53 27 1 35	• 57 • 57 • 57 • 57 • 57 • 58	15 14 13 12 11	17.4 16.2 15.1 13.9 12.8
80 81 82 83 84	31	58 4 9 14 18	10.0 12.0 12.0 15.0 15.0	84 85 86	56 32 8 44 20	0.60 .60 .60 .60		29 35 40 45 49	10.0 12.0 12.0 15.0 20.0	84 85 86	38 13 49 24	0.58 .58 .60 .58 .60	30	59 5 10 15 19	10.0 12.0 12.0 15.0 20.0	84 85 86	10 44 19 54 29	0.57 .58 .58 .58	10 9 8 7 6	11.6 10.5 9.3 8.2 7.0
85 86 87 88 89		22 25 27 29 30	20.0 30.0 30.0 60.0	87 88 89	56 33 10 46 23	0.62 .62 .60 .62		52 55 57 59 0	20.0 30.0 30.0 60.0	87 88 89	0 36 12 48 24	0.60 .60 .60 .60		22 25 27 29 30	20.0 30.0 30.0 60.0	87 88 89	4 39 14 49 25	0.58 .58 .58 .60 .58	5 4 3 2 1	5.8 4.7 3.5 2.3 1.2
90		30		90	0			0		90	0			30		90	0		0	0.0
,		a	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $					ı	$\frac{60'}{\Delta}$	1	ь	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a.
t		C	l=5	8° 3	0′			(d = 5	9° (0′			d	= 59	9° 3	0′			

	b			a = 0	60°	0′	***		(a = 6	0° 8	30′	(، شد	1	,	a = 0	31°	0′		\\ c	a
1	8	h	d	60' <u>A</u>	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	Δ 60'	h	d	. <u>60'</u> Δ	Z	t	Δ 60'	$C \setminus$	B
	o 1 2 3 4	0 0 1 2	30 0 30 0			0 0 1 2 4	0.00	00	30 59 29 58	2.00 2.07 2.00 2.07 2.00	60°	30 30 31 32 34	0.00 .02 .02 .03	I	0 29 58	2.07 2.07 2.07 2.07 2.07	61	0 0 1 2 4	0.00	90 89 88 87 86	90.0 89.1 88.3 87.4 86.5
	5 6 78 9	3 4	30 30 59 29	2.00 2.00 2.07 2.00 2.00		6 8 11 14 18	0.03 .05 .05 .07	3 4	28 57 26 56 25	2.07 2.07 2.00 2.07 2.07		36 38 41 44 48	0.03 .05 .05 .07		54 23 52	2.07 2.07 2.07 2.07 2.07		6 8 11 14 18	0.03	85 84 83 82 81	85.6 84.8 83.9 83.0 82.2
	10 11 12 13 14	5 6	59 29 58 28 57	2.00 2.07 2.00 2.07 2.07		23 28 33 38 44	0.08 .08 .08 .10	5 6	54 23 52 21 50	2.07 2.07 2.07 2.07 2.07	61	52 57 2 8 14	0.08 .08 .10 .10	5	50 19 47 16 44	2.07 2.14 2.07 2.14 2.07		22 27 32 38 44	0.08	80 79 78 77 76	81.3 80.4 79.5 78.6 77.8
	15 16 17 18 19	7 8 9	26 55 24 53 22	2.07 2.07 2.07 2.07 2.07	61	51 58 6 14 22	0.12 .13 .13 .13	7 8 9	19 48 17 45 14	2.07 2.07 2.14 2.07 2.14		21 28 35 43 51	0.12 .12 .13 .13	7 8 9	13 41 9 37 5	2.14 2.14 2.14 2.14 2.14	62	50 57 4 12 20	0.12 .12 .13 .13	75 74 73 72 71	76.9 76.0 75.1 74.2 73.3
2 2 2	20 21 22 23 24	10	51 19 48 16 44	2.14 2.07 2.14 2.14 2.14	62	31 40 50 1	0.15 .17 .18 .18	10	42 10 38 6 33	2. I4 2. I4 2. I4 2. 22 2. I4	62	0 9 19 29 40	0.15 .17 .17 .18	10	33 0 28 55 22	2.22 2.14 2.22 2.22 2.22	63	29 38 48 58	0.15 .17 .17 .18	70 69 68 67 66	72.4 71.5 70.6 69.7 68.8
2 2 2	25 26 27 28 29	12 13 14	12 40 7 34 1	2.14 2.22 2.22 2.22 2.22	63	23 35 47 59 12	0,20 .20 .20 .22 .23	13	28 55 22 49	2.22 2.22 2.22 2.22 2.31	63	51 3 15 27 40	0.20 .20 .20 .22 .23	12	49 16 43 9 36	2.22 2.22 2.31 2.31 2.31	64	20 31 43 55 8	0.18 .20 .20 .22 .22	65 64 63 62 61	67.9 67.0 66.1 65.2 64.2
3333	30 31 32 33 34	15 16	28 55 22 48 14	2.22 2.22 2.3I 2.3I 2.3I	64	26 40 55 10 25	0.23 .25 .25 .25 .25	14	15 41 7 33 59	2.31 2.31 2.31 2.31 2.40	64	54 22 37 52	0.23 .23 .25 .25 .27	14	28 53 19 44	2.31 2.40 2.31 2.40 2.40	65	21 35 49 4 19	0.23 .23 .25 .25	60 59 58 57 56	63.3 62.4 61.5 60.5 59.6
3000	35 36 37 38 39	17	40 6 31 56 21	2.31 2.40 2.40 2.40 2.50	65	41 58 15 32 50	0.28 .28 .28 .30	16 17 18	24 49 14 39 3	2.40 2.40 2.40 2.50 2.50	65 66	8 24 41 58 16	0.27 .28 .28 .30	16	9 34 58 22 46	2.40 2.50 2.50 2.50 2.50	66	35 51 7 24 42	0.27 .27 .28 .30 .30	55 54 53 52 51	58.6 57.7 56.7 55.8 54.8
4 4 4		19	45 9 33 56 19	2.50 2.50 2.61 2.61 2.61	66	8 27 47 7 27	•33 •33 •33 •35	-	27 51 14 37 0	2.50 2.61 2.61 2.61 2.61	67	34 53 12 31 51	0.32 .32 .32 .33	18	10 33 56 19 41	2.61 2.61 2.61 2.73 2.73	67 68		0.30 .32 .32 .33	50 49 48 47 46	53.9 52.9 51.9 50.9 50.0
4	5		42	60'	7	48	Δ		23	60'	68		Δ	20	3	60'		36	Δ	45	49.0
1	t			d = 6			60'	а		=60		0 ′	60′	a		d = 6)'	60'	O	a

											_						7
b		a = 6	80° 0′			C	a = 60	0° 3	0′				a = 6	1° 0′		c	a
$B \setminus$	h	$\frac{1}{\Delta}$	Z	$t \frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{6\phi'}$	h	d	<u>60'</u> Δ	Z	$\frac{\Delta}{60'}$	$C \setminus$	β
9 45 46 47 48 49	20 4 21 2 4 22 10	2.73 2.73 2.86	68	8 0.35 9 .37 1 .37 3 .37 5 .38	20 21	23 45 7 28 49	2.73 2.73 2.86 2.86 2.86	68 ⁶	33 54 16 38	0.35 .35 .37 .37 .38	20 21	3 25 46 7 28	2.73 2.86 2.86 2.86 3.00	69 I	6 35	45 44 43 42 41	49.0 48.0 47.0 46.0 45.0
50 51 52 53 54	23 I: 33 55	2 3.00 2 3.00 2 3.00	70 2	8 0.40 2 .40 6 .40 0 .42 5 .43	22	10 30 50 10 29	3.00 3.00 3.16 3.33	70 <u>.</u>	1 24 48 12 36	0.38 .40 .40 .40	22	48 8 28 47 6	3.00 3.00 3.16 3.16 3.33	71 3 5	6 .38 9 .40 3 .40	39 38 37 36	44.0 42.9 41.9 40.9 39.9
55 56 57 58 59	24 I 25 25 2	3·33 7 3·33 5 3·33	3	7 ·43 3 ·43 9 ·45	24	47 5 23 41 58	3·33 3·33 3·33 3·53 3·53	72	1 27 53 19 45	0.43 •43 •43 •43	24	24 42 0 17 33	3·33 3·33 3·53 3·75 3·75	72 2 4 73 I 3 74	7 .42	35 34 33 32 31	38.8 37.8 36.7 35.7 34.6
60 61 62 63 64	26 1: 26 1: 27	3.75 2 4.00 7 4.00	74 2	0 .48 9 .48	25 26	31 46 1 16	3.75 4.00 4.00 4.00 4.29	74 75 76	40 8 36 4	•47 •47 •47 •47 •48	25	49 5 21 36 50	3.75 3.75 4.00 4.29 4.29	75 2 76 2	7 .47 5 .47 3 .47 1 .47	30 29 28 27 26	33.6 32.5 31.4 30.3 29.3
65 66 67 68 69	27 1 22 32 50	4.62 4.62 4.62	76 I 4 77 I 4 78 I	7 ·5° 7 ·5² 8 ·5²	27	30 44 57 10 22	4.29 4.62 4.62 5.00 5.00	77 78	33 2 32 2 32	0.48 .50 .50 .50	26	4 17 30 43 55	4.62 4.62 4.62 5.00 5.45	77 I 4 78 I 4	8 .48 7 .48 6 .50	25 24 23 22 21	28.2 27.1 26.0 24.9 23.8
70 71 72 73 74	28 1 1 22 34	5.45 4 6.00 4 6.00	79 2 80 2	3 .53	28	34 45 56 6 15	5.45 5.45 6.00 6.67 6.67	79. 80. 81	3 34 5 36 8	0.52 .52 .52 .53	27	6 17 27 37 46	5.45 6.00 6.00 6.67 6.67	79 I 80 I 81 I	6 .52 7 .52 8 .52	20 19 18 17 16	22.7 21.6 20.5 19.4 18.2
75 76 77 78 79	_	7.50 7.50 8.57	82 83	3 ·55 6 ·55 9 ·57 13 ·55		24 32 40 47 54	7.50 7.50 8.57 8.57 10.0	82	40 12 45 17 50	• 53 • 55 • 53 • 55 • 55	28	55 3 11 18 25	7.50 7.50 8.57 8.57 10.0	82 2 5 83 2 5	2 ··53 4 ·53 6 ·53	15 14 13 12 11	17.1 16.0 14.0 13.', 12.6
80 81 82 83 84	30 4 4 4	12.0 1 15.0 5 15.0	85 2	6 0.57 0 .57 4 .57 8 .58 3 .57	29	0 6 11 15 19	10.0 12.0 15.0 15.0 20.0	84 85 86	23 56 30 3 37	0.55 .57 .55 .57 .57		31 37 42 46 50	10.0 12.0 15.0 15.0 20.0	84 3 85 3 86 4	3 ·53 5 ·55 8 ·55	10 9 8 7 6	11.5 10.3 9.2 8.0 6.9
85 86 87 88 89	5 5 5 5 30	30.0	88 I 89 2	7 0.58 .57 .6 .58 .1 .57 .58		22 25 27 29 30 30	20.0 30.0 30.0 60.0	87 88 89 90	11 44 18 52 26	0.55 .57 .57 .57 .57	29	53 55 57 59 0	30.0 30.0 30.0 60.0	87 I 4 88 2 5 89 2	7 -55 0 -55 3 -57 7 -55	5 4 3 2 1	5.7 4.6 3.4 2.3 1.1
=	a	$\frac{60'}{\Delta}$	$\frac{\parallel}{\parallel}$ b	$\frac{\Delta}{60'}$		a	60' \(\Delta \)	11	b	<u>Δ</u> 6ο'	-		<u>6ο'</u> Δ	b	Δ 6ο'		
t		-	∥ 60° 0′			d	l=60)° 3	0′	00	_			1° 0′	00'	:	

$\setminus b$	a	u = 6	l° 30′			a = 6	2° 0′		a	<i>i</i> = 62	2° 30′		c	a
$B \setminus$	h	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	h d	$\left \frac{6o'}{\Delta} \right $	Z	$\frac{\Delta}{60'}$	h d	6ο' Δ	Z t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	0 0 29 57 1 26 54	2.07 2.14 2.07 2.14 2.07	61 30 30 31 32 33	0.00 .02 .02 .02	0 0 28 56 1 25 53	2.14 2.14 2.07 2.14 2.14	62 0 0 1 2 3	.02	0 0 28 55 1 23 51	2.14 2.22 2.14 2.14 2.22	62 30 30 31 32 33	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.1 88.2 87.4 86.5
5 6 7 8 9	2 23 52 3 20 49 4 17	2.07 2.14 2.07 2.14 2.14	35 38 41 44 48	0.05 .05 .05 .07	2 21 49 3 17 45 4 13	2.14 2.14 2.14 2.14 2.14	5 8 11 14 18	0.05 .05 .05 .07	2 18 46 3 14 41 4 9	2.14 2.14 2.22 2.14 2.22	35 38 41 44 47	0.05 .05 .05 .05	85 84 83 82 81	85.6 84.7 83.8 82.9 82.0
10 11 12 13 14	45 5 13 41 6 9 37	2. I4 2. I4 2. I4 2. I4 2. I4	52 57 62 2 7 13	0.08 .08 .08	5 8 5 36 6 4 31	2.22 2.14 2.14 2.22 2.14	22 26 31 37 43	.10	36 5 3 31 58 6 25	2.22 2.14 2.22 2.22 2.22	51 56 63 1 6	0.08	80 79 78 77 76	81.2 80.3 79.4 78.5 77.6
15 16 17 18 19	7 5 33 8 1 29 56	2.14 2.14 2.14 2.22 2.14	19 26 33 41 49	0.12 .12 .13 .13	59 7 26 53 8 20 47	2.22 2.22 2.22 2.22 2.22	63 3 11	.12	52 7 19 46 8 12 39	2.22 2.22 2.31 2.22 2.31	18 25 32 40 48	0.12 .12 .13 .13	75 74 73 72 71	76.7 75.8 74.9 74.0 73.1
20 21 22 23 24	9 24 51 10 18 45 11 12	2.22 2.22 2.22 2.22 2.31	63 7 17 27 37	0.15 .17 .17 .17	9 14 41 10 8 34 11 0	2.22 2.22 2.31 2.31 2.31	27 36 45 55 64	.17	9 5 31 57 10 23 49	2.31 2.31 2.31 2.31 2.31	56 64 5 14 24 34	0.15 .15 .17 .17	70 69 68 67 66	72.2 71.3 70.4 69.5 68.5
25 26 27 28 29	38 12 4 30 56 13 22	2.31 2.31 2.31 2.31 2.31	48 59 64 11 23 36	0.18 .20 .20 .22 .22	26 52 12 18 44 13 9	2.31 2.31 2.31 2.40 2.40	16 27 39 51 65 4	.20	11 15 41 12 6 31 56	2.31 2.40 2.40 2.40 2.40	45 56 65 7 19 31	0.18 .18 .20 .20	65 64 63 62 61	67.6 66.7 65.8 64.9 63.9
30 31 32 33 34	48 14 14 39 15 4 29	2.31 2.40 2.40 2.40 2.50	65 3 17 31 46	0.23 .23 .23 .25	34 59 14 24 49 15 13	2.40 2.40 2.40 2.50 2.50	17 30 44 58 66 13	.23	13 21 46 14 10 34 58	2.40 2.50 2.50 2.50 2.50	44 57 66 11 25 39	0,22 .23 .23 .23 .25	60 59 58 57 56	63.0 62.1 61.1 60.2 59.2
35 36 37 38 39	53 16 17 41 17 5 29	2.50 2.50 2.50 2.50 2.61	66 I 17 33 50 67 7	0.27 .27 .28 .28	37 16 I 25 48 17 II	2.50 2.50 2.61 2.61 2.61	67 6 16 33	.27	15 22 45 16 8 31 54	2.61 2.61 2.61 2.61 2.73	67 10 26 42 59	0.27 .27 .27 .28 .28	55 54 53 52 51	58.3 57.3 56.4 55.4 54.4
40 41 42 43 44	52 18 15 37 59 19 21	2.61 2.73 2.73 2.73 2.73	25 43 68 2 21 40	0.30 .32 .32 .32 .33		2.73 2.73 2.73 2.73 2.73 2.86	68 8 26 45 69 4	.30		2.73 2.73 2.86 2.86 2.86	68 16 33 51 69 9 28	0.28 .30 .30 .32	50 49 48 47 46	53.5 52.5 51.5 50.5 49.5
45	43		69 0		23		24		19 3		47		45	48.6
	а	6ο' Δ	b	$\frac{\Delta}{60'}$	а	60' Δ	b	$\frac{\Delta}{60'}$	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$		a
t	0	l=6	1° 30′			$d = \epsilon$	32° 0′		(d=6	2° 30′			

b		a	=61	° 3	0′	`		C	a = 6	2° C)′			а	=62	2° 3	0′		$\setminus c$	a
$ B\rangle$	h	d	<u>6ο'</u> Δ	\overline{z}	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	\overline{z}	t	<u>Δ</u> 6ο'	h	d	<u>6ο′</u> Δ	\overline{z}	t	$\frac{\Delta}{60'}$	$C \setminus$	β
9 45 46 47 48 49	0 19 20 21	43 4 25 46 6	2.86 2.86 2.86 3.00 3.00	69°	0 20 41 2 24	0.33 .35 .35 .37 .37	20	23 44 5 25 45	2.86 2.86 3.00 3.00 3.00	69 70	24 44 4 25 46	0.33 .33 .35 .35	20	3 24 44 4 24	2.86 3.00 3.00 3.00 3.16	69 70 71	47 7 27 48 9	0.33 .33 .35 .35	° 45 44 43 42 41	48.6 47.6 46.6 45.6 44.6
50 51 52 53 54	22	26 46 5 24 43	3.00 3.16 3.16 3.16 3.33	71 72	46 8 31 54 18	•.37 •38 •38 •40 •40	2I 22	5 24 43 1 19	3.16 3.16 3.33 3.33 3.33	7 I 72	8 30 52 15 39	0.37 .37 .38 .40 .38	21	43 20 38 56	3.16 3.33 3.33 3.33 3.53	72	30 52 14 36 5 9	0.37 .37 .37 .38 .38	40 39 38 37 36	43.5 42.5 41.5 40.5 39.5
55 56 57 58 59	23 24	18 35 52 8	3.53 3.53 3.53 3.75 3.75	73 74	42 7 32 57 23	0.42 .42 .42 .43 .43	23	37 54 11 28 44	3.53 3.53 3.53 3.75 4.00	73 74	2 26 51 16 41	0.40 •42 •42 •42 •43	22	13 30 47 3 19	3.53 3.53 3.75 3.75 4.00	73 74 75	22 46 10 35 0	0.40 .40 .42 .42 .42	35 34 33 32 31	38.4 37.4 36.3 35.3 34.2
60 61 62 63 64	25	24 40 55 10 24	3.75 4.00 4.00 4.29 4.29	75 76	49 15 42 9 37	0.43 .45 .45 .47	24	59 14 29 44 58	4.00 4.00 4.00 4.29 4.62	75 76	7 33 59 26 53	•43 •45 •45 •45	24	34 49 4 18 31	4.00 4.00 4.29 4.62 4.62	76 77	25 50 16 42 9	0.42 •43 •43 •45 •45	30 29 28 27 26	33.2 32.1 31.0 30.0 28.9
65 66 67 68 69	26	38 51 3 15 27	4.62 5.00 5.00 5.00 5.45	77 78	5 33 1 30 59	0.47 •47 •48 •48 •50	25 26	11 24 36 48 0	4.62 5.00 5.00 5.00 5.45	77 78 79	20 48 16 44 13	0.47 .47 .47 .48 .48	25	44 57 9 21 32	4.62 5.00 5.00 5.45 5.45	78 79	36 30 58 26	0.45 .45 .47 .47	25 24 23 22 21	27.8 26.8 25.7 24.6 23.5
70 71 72 73 74	27	38 49 59 18	5.45 6.00 6.00 6.67 6.67	79 80 81	29 59 29 59 29	0.50 .50 .50 .50		11 21 31 41 50	6.00 6.00 6.00 6.67 7.50	80 81	42 11 40 10 40	0.48 .48 .50 .50	26	43 53 3 12 21	6.00 6.00 6.67 6.67 7.50	80 81	54 23 52 21 50	0.48 .48 .48 .48	20 19 18 17 16	22.4 21.3 20.2 19.1 18.0
75 76 77 78 79		27 35 42 49 56	7.5° 8.57 8.57 8.57 10.0	82 83 84	31 2 33	0.52 .52 .52 .53	27	58 6 13 20 26	7.50 8.57 8.57 10.0	82 83 84	10 40 11 41 12	0.50 .52 .50 .52		29 37 44 51 57	7.50 8.57 8.57 10.0	82 83 84	49 19 49	0.48 .50 .50 .52	15 14 13 12 11	16.9 15.8 14.7 13.5 12.4
80 81 82 83 84	28	2 7 12 16 20	12.0 12.0 15.0 15.0 20.0	85 86	37 9 41 13 45	• 53 • 53 • 53 • 53		32 37 42 46 50	12.0 12.0 15.0 15.0 20.0	85 86	43 15 46 18 49	0.53 .52 .53 .52 .53	27	3 8 13 17 20	12.0 12.0 15.0 20.0 20.0	85 86	51	0.52 .50 .52 .52	10 9 8 7 6	11.3 10.2 9.0 7.9 6.8
85 86 87 88 89		23 25 27 29 30	30.0 60.0	87 88 89	50	.53		53 56 58 59	20.0 30.0 60.0 60.0	87 88 89	21 52 24 56 28	0.52 •53 •53 •53		23 26 28 29 30		87 88 89	55	0.52 .52 .53 .52 .52	3 2	5·7 4·5 3·4 2·3 1·1
90	_	30	-	90	0	1 .	_	0		90	0		_	30	<u> </u>	90	0	1	0	0.0
$ _t$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a °	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
			d = 6	1° a	30′				$d = \mathbf{c}$	32°	0′				d = 6	2°	30′			

b	1		a = 6	33°	0			_	a = 6	3° :	30′	-,			a = 0	34°	0′		\ c	\ a
B	h	d	60' Δ	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	\downarrow^t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 1 2 3 4	O	27 54	2.22	63°	0 0 1 2 3	0.00	, O	0 27 54	2.22 2.22 2.31 2.22 2.22	63	30 30 31 32 33	0.00 .02 .02 .02	O		2.31 2.22 2.31 2.31 2.31	64	0 0 1 2 3	0.00		90.0 89.1 88.2 87.3 86.4
56789	3 4	16 43 10 37 4	2,22 2,22 2,22 2,22 2,22		5 7 10 13 17	0.63 .05 .05 .07	3 4	14 40 7 34 0	2.31 2.22 2.22 2.31 2.22		35 37 40 43 47	0.03 .05 .05 .07	3	38	2.22 2.31 2.31 2.31 2.31		5 7 10 13 17	0.03 .05 .05 .07	85 84 83 82 81	85.5 84.6 83.7 82.8 81.9
10 11 12 13 14	5	31 58 25 52 18	2.22 2.22 2.22 2.31 2.22		21 26 31 36 42	0.08 .08 .08	5 6	27 53 20 46 12	2.31 2.22 2.31 2.31 2.31	64	51 55 0 .5	0.07 .08 .08 .10	4 5 6	22 48 14 40 5	2.31 2.31 2.31 2.40 2.31		21 25 30 35 40	0.07 .08 .08 .08	80 79 78 77 76	81.0 80.1 79.2 78.3 77.4
15 16 17 18 19	7 8	45 11 38 4 30	2.31 2.22 2.31 2.31 2.31	64	48 54 1 9	0.10 .12 .13 .13	<i>7</i> 8	38 4 30 56 21	2.31 2.31 2.31 2.40 2.31		17 24 31 38 46	0.12 .12 .12 .13	<i>7</i> 8	31 56 22 47 12	2.40 2.31 2.40 2.40 2.40	65	46 53 0 7 15	0.12 .12 .12 .13	75 74 73 72 71	76.5 75.6 74.7 73.8 72.9
20 21 22 23 24	01	56 22 48 13 39	2.31 2.31 2.40 2.31 2.40	65	25 34 43 52 2	0.15 .15 .15 .17	9	47 12 37 2 27	2.40 2.40 2.40 2.40 2.40	65	54 2 11 21 31	0.13 .15 .17 .17	9	37 2 27 52 16	2.40 2.40 2.40 2.50 2.40		23 31 40 49 59	0.13 .15 .15 .17	70 69 68 67 66	72.0 71.0 70.1 69.2 68.3
25 26 27 28 29	11	4 29 54 19 43	2.40 2.40 2.40 2.50 2.50		13 24 35 47 59	0.18 .18 .20 .20	11	52 17 41 5 29	2.40 2.50 2.50 2.50 2.50	66	41 52 3 14 26	0.18 .18 .18 .20	11	41 5 29 53 16	2.50 2.50 2.50 2.61 2.50	66	9 20 31 42 54	0.18 .18 .18 .20	65 64 63 62 61	67.3 66.4 65.5 64.6 63.6
30 31 32 33 34	13	7 31 55 19 43	2.50 2.50 2.50 2.50 2.61	66 67	11 24 38 52 6	0.22 .23 .23 .23 .25	13	53 17 41 4 27	2.50 2.50 2.61 2.61 2.61	67	39 52 5 19 33	0,22 .22 .23 .23 .23	13	40 3 26 49 12	2.61 2.61 2.61 2.61 2.73	67	6 19 32 45 59	0.22 .22 .22 .23 .23	59 58 57 56	62.7 61.7 60.8 59.8 58.9
35 36 37 38 39	15	6 29 52 14 36	2.61 2.61 2.73 2.73 2.73	68	21 36 51 7 24	0.25 .25 .27 .28	15	50 12 34 56 18	2.73 2.73 2.73 2.73 2.73	68	47 2 17 33 49	0.25 .25 .27 .27 .28	15 16	34 56 18 40	2.73 2.73 2.73 2.86 2.86	68 69	13 28 43 59 15	0.25 .25 .27 .27 .27	55 54 53 52 51	57.9 57.0 56.0 55.0 54.1
40 41 42 43 44	17	58 20 41 2 23	2.73 2.86 2.86 2.86 2.86	69	41 58 16 34 52	0.28 .30 .30 .30	17 18	40 I 22 43 3	2.86 2.86 2.86 3.00 3.00	69 70	6 23 40 58 16	0.28 .28 .30 .30	17	22 43 4 24 44	2.86 2.86 3.00 3.00 3.00	70	31 48 5 22 40	0.28 .28 .28 -30	50 49 48 47 46	53.1 52.1 51.1 50.2 49.2
45		44		70	11	'		23		1	35		18	4			58		45	48.2
t	a		.6ο' Δ	t)	$\frac{\Delta}{60'}$	а	,	<u>6ο'</u> Δ	1	b	<u>Δ</u> 6ο'	a	ı	60' ∆	ĕ		$\frac{\Delta}{60'}$		a
			d = 6	3° ()′			d	=68	3° 3	0′				d = 6	4° ()′			1

b		a = 6	3° 0′			(a = 6	3° 3	30′			1	a = 6	4° (0′		c	a
$B \setminus$	h	<u>60'</u> Δ	Z	t <u>∆</u> 60'	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
o 45 46 47 48 49	0 18 44 19 4 24 43 20 2	3.00 3.16 3.16	71	0.32 30 .33 50 .33 10 .35 31 .35	18	23 43 3 22 41	3.00 3.00 3.16 3.16 3.33	70°	35 54 13 33 53	0.32 •32 •33 •33 •35	18	4 23 42 1 19	3.16 3.16 3.16 3.33 3.33	70 71 72	58 17 36 55 15	0.32 •32 •32 •33 •35	°45 44 43 42 41	48.2 47.2 46.2 45.2 44.2
50 51 52 53 54	21 40 58 21 16 33	3.33	72 1	32 0.35 33 ·37 35 ·37 57 ·38 20 ·38	20	59 17 35 52 9	3.33 3.33 3.53 3.53 3.53	72 73	14 35 56 18 40	0.35 .35 .37 .37 .37	20	37 55 12 29 46	3·33 3·53 3·53 3·53 3·53	73 74	36 56 17 38 0	0-33 -35 -35 -37 -37	39 38 37 36	43.2 42.1 41.1 40.1 39.1
55 56 57 58 59	22 7 23 39 54	3.75 3.75 4.00	74	0.38 6 .40 30 .40 4 .40 8 .40	22	26 42 58 14 29	3.75 3.75 3.75 4.00 4.00	74 75	2 25 48 12 36	0.38 .38 .40 .40	21	3 19 34 49 4	3.75 4.00 4.00 4.00 4.00	75	22 45 7 30 54	0.38 •37 •38 •40 •40	35 34 33 32 31	38.0 37.0 36.0 34.9 33.9
60 61 62 63 64	23 9 24 38 52 24 5	4.00 4.29 4.29 4.62 4.62	76 3 5	7 ·43 3 ·43 9 ·43 5 ·43	23	44 58 12 26 39	4.29 4.29 4.29 4.62 5.00	76 77	0 25 50 15 40	0.42 .42 .42 .42 .43	23	19 33 46 59 12	4.29 4.62 4.62 4.62 5.00	76 77	18 42 6 31 56	0.40 .40 .42 .42 .42	30 29 28 27 26	32.8 31.8 30.7 29.7 28.6
65 66 67 68 69	18 30 42 54 25 5	5.00 5.00 5.00 5.45 6.00	78 I 4 79 I	8 .45 .45 .45 .2 .45 .9 .47	24	51 3 15 26 37	5.00 5.00 5.45 5.45 6.00	78 79	6 32 58 25 52	•43 •45 •45 •45	24	24 36 48 59	5.00 5.00 5.45 5.45 6.00	78 79 80	21 47 13 39 5	0.43 .43 .43 .43	25 24 23 22 21	27.5 26.5 25.4 24.3 23.2
70 71 72 73 74	25 25 35 44 53	6.00 6.00 6.67 6.67 7.50	81	7 0.47 35 .47 3 .48 32 .47 0 .48	25	47 57 7 16 24	6.00 6.00 6.67 7.50 7.50	80 31 82	19 47 15 43	•47 •47 •47 •47 •47		20 29 38 47 55	6.67 6.67 6.67 7.50 7.50	81 82	32 59 26 53 20	0.45 •45 •45 •45 •47	20 19 18 17 16	22.1 21.0 20.0 18.9 17.8
75 76 77 78 79	26 I 8 I 5 22 28	8.57 8.57 8.57 10.0 12.0	83 2	29 0.48 58 .50 28 .48 57 .50 27 .50		32 39 46 53 59	8.57 8.57 8.57 10.0 12.0	83 84	39 7 36 5 34	0.47 .48 .48 .48	25	3 10 17 23 29	8.57 8.57 10.0 10.0	83 84	48 16 44 13 41	•47 •48 •47 •47	15 14 13 12 11	16.7 15.6 14.5 13.4 12.3
80 81 82 83 84	33 38 43 47 50	15.0	85 2 86 2	7 0.50 27 .50 57 .50 57 .50	26	4 9 13 17 21	12.0 15.0 15.0 15.0 20.0	85 86 87	32 2 31 1	0.48 .50 .48 .50	-	34 39 43 47 51	12.0 15.0 15.0 15.0 20.0	85 86 87	9 38 7 36 5	0.48 .48 .48 .48	9 8 7 6	11.1 10.0 8.9 7.8 6.7
85 86 87 88 89	53 56 58 59 27	60.0	88 2	27 0.52 58 .50 28 .52 59 .50		24 26 28 29 30	30.0 30.0 60.0 60.0	88 89	31 30 0 30	0.48 .50 .50 .50	26	54 56 58 59 0	30.0 30.0 60.0 60.0	88 89	34 32 1 31	0.48 .48 .48 .50	5 4 3 2 1	5.6 4.5 3.4 2.2 1.1
90	0		90	0		30		90	0			0		90	0		0	0.0
t	а 	<u>δο'</u> Δ	b	$\frac{\Delta}{60'}$	0	t	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	- 0	ı	$\frac{60'}{\Delta}$	- 1	b	Δ 60'		a
		d = 6	3° 0′	. 1			d = 6	3° 3	80′				d = 6	4° (0′			1)

b		C	a = 6	4° 8	30′				a = 6	5°	0′				a=6	5° 3	30′		\ c	a
B	h	d	<u>60'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	6ο' Δ	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 I 2 3 4	O	26 52	2.31 2.31 2.31 2.40 2.31	64	30 30 31 32 33	0.00	0	0 25 51 16 41	2.40 2.31 2.40 2.40 2.31	65	0 0 1 2 3	0.00	O	0 25 50	2.40 2.40 2.40 2.50 2.40	65	30 30 31 32 33	0.00	90 89 88 87 86	90.0 89.1 88.2 87.3 86.4
5 6 7 8 9	3	9 35 0 26 52	2.31 2.40 2.31 2.31 2.40		35 37 40 43 46	0.03 .05 .05 .05	3	7 32 57 22 47	2.40 2.40 2.40 2.40 2.40		5 7 10 13 16	0.03 .05 .05 .05	3	4 29 54 19 43	2.40 2.40 2.40 2.50 2.40		35 37 40 43 46	0.03 .05 .05 .05	85 84 83 82 81	85.5 84.6 83.7 82.7 81.8
10 11 12 13 14	5	17 43 8 3 3 59	2.31 2.40 2.40 2.31 2.40	65	50 54 59 4	0.07 .08 .08 .10	4 5	12 37 2 27 52	2.40 2.40 2.40 2.40 2.40		20 24 29 34 39	0.07 .08 .08 .08	5	8 32 57 21 45	2,50 2,40 2,50 2,50 2,40	66	50 54 58 3 9	0.07 .07 .08 .10	80 79 78 77 76	80.9 80.0 79.1 78.2 77.3
15 16 17 18 19	6 7 8	24 49 14 39 4	2.40 2.40 2.40 2.40 2.50		16 0.10 22 29 36 .13 44 .13 66 0 52 0.15 9 18 .15		6 7	17 41 6 30 54	2.50 2.40 2.50 2.50 2.50	66	45 51 58 5	0.10 .12 .12 .12	6 7	10 34 58 22 46	2.50 2.50 2.50 2.50 2.61		15 21 27 34 41	0.10 .10 .12 .12	75 74 73 72 71	76.4 75.4 74.5 73.6 72.7
20 21 22 23 24	9	28 53 17 41 5	2.40 2.50 2.50 2.50 2.50	66	9	.15	9	18 42 6 30 54	2.50 2.50 2.50 2.50 2.61		20 28 37 46 56	0.13 .15 .15 .17	8 9	9 33 56 19 42	2.50 2.61 2.61 2.61 2.61	67	49 57 6 15 24	0.13 .15 .15 .15	70 69 68 67 66	71.7 70.8 69.9 69.0 68.0
25 26 27 28 29	11 12	29 53 17 40 3	2.50 2.50 2.61 2.61 2.61	67	37 48 59 10 21	0.18 .18 .18 .18	10	17 41 4 27 50	2.50 2.61 2.61 2.61 2.73	67	6 16 26 37 49	0.17 .17 .18 .20	11	5 28 51 14 36	2.61 2.61 2.61 2.73 2.73	68	34 44 54 5 16	0.17 .17 .18 .18	65 64 63 62 61	67.1 66.2 65.2 64.3 63.3
30 31 32 33 34	13	26 49 11 34 56	2.61 2.73 2.61 2.73 2.73	68	33 46 59 12 26	0.22 .22 .22 .23 .23	12	34 56 18 40	2.73 2.73 2.73 2.73 2.73 2.73	68	1 13 25 38 52	0.20 .20 .22 .23	12	58 20 42 3 24	2.73 2.73 2.86 2.86 2.86	69	28 40 52 5 18	0,20 .20 .22 .22 .23	60 59 58 57 56	62.4 61.4 60.5 59.5 58.6
35 36 37 38 39	14	18 40 1 22 43	2.73 2.86 2.86 2.86 2.86	69	40 54 9 24 40	0.23 .25 .25 .27 .27	14	2 23 44 5 26	2.86 2.86 2.86 2.86 3.00	69 70	6 20 34 49 5	0.23 .23 .25 .27 .27	14	45 6 27 48 8	2.86 2.86 2.86 3.00 3.00	70	32 46 0 15 30	0.23 .23 .25 .25	55 54 53 52 51	57.6 56.6 55.7 54.7 53.7
40 41 42 43 44	16 17	4 24 44 4 24	3.00 3.00 3.00 3.00 3.16		56 12 29 46 4	0.27 .28 .28 .30	16 17	46 6 26 45 4	3.00 3.00 3.16 3.16 3.16	71	21 37 53 10 27	0.27 .27 .28 .28	16	28 47 6 25 44	3.16 3.16 3.16 3.16 3.16	71	45 1 17 34 51	0.27 .27 .28 .28 .28	50 49 48 47 46	52.7 51.8 50.8 49.8 48.8
45		43			22			23			45		17	3		72	8		45	47.8
	0	ı	<u>6ο'</u> Δ	l	6	<u>Δ</u> 60'	a	ı	<u>6ο'</u> Δ	i	ь	<u>Δ</u> 60'	d	ı	$\frac{60'}{\Delta}$	l	5	$\frac{\Delta}{60'}$		a
t		d	=64	۱° 3	0′			(d = 6	5° ()′				d = 6	5° 3	30′			

8		(a = 6	4° 3	30′				a = 6	5° (0′			C	a = 6	5° 8	30′		c	\ a
$B \setminus$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	17 18	43 2 21 40 58	3.16 3.16 3.33 3.33	7º 72	22 40 59 18 37	0.30 .32 .32 .32 .33	17 18	23 42 0 18 36	3.16 3.33 3.33 3.33 3.53	7 I 72	45 3 21 40 59	0.30 .30 .32 .32 .33	18	3 21 39 57 14	3.33 3.33 3.33 3.53 3.53	72	8 26 44 2 21	0.30 .30 .30 .32	° 45 44 43 42 41	47.8 46.8 45.8 44.8 43.8
50 51 52 53 54	19 20	16 33 50 7 23	3.53 3.53 3.53 3.75 3.75	73 74	57 17 38 59 20	0.33 .35 .35 .35 .37	19	53 10 27 43 59	3.53 3.53 3.75 3.75 3.75	73 74	19 39 59 19 40	0.33 .33 .33 .35	19	31 48 4 20 36	3.53 3.75 3.75 3.75 3.75	74 75	40 0 20 40 0	• 33 • 33 • 33 • 33 • 35	39 38 37 36	42.8 41.8 40.8 39.7 38.7
55 56 57 58 59	21	39 55 10 25 39	3.75 4.00 4.00 4.29 4.29	75 76	42 4 26 49 12	0.37 .37 .38 .38 .38	20 21	15 30 45 0	4.00 4.00 4.00 4.29 4.29	75 76	1 23 45 7 30	0.37 .37 .37 .38 .38	20	52 7 21 35 49	4.00 4.29 4.29 4.29 4.29	76	21 42 4 26 48	0.35 .37 .37 .37 .37	35 34 33 32 31	37.7 36.7 35.6 34.6 33.5
60 61 62 63 64	22	53 7 20 33 46	53 4-29 35 0. 7 4-62 59 20 4-62 77 23 33 4-62 78 11 58 5.00 36 0. 10 5-45 79 1 26 32 6.00 52 2 3			0.40 .40 .40 .40	22	28 42 55 7 19	4.29 4.62 5.00 5.00 5.00	77 78	53 16 39 3 27	0.38 .38 .40 .40	21	3 16 29 41 53	4.62 4.62 5.00 5.00 5.00	77 78	10 32 55 19 42	0.37 .38 .40 .38 .40	30 29 28 27 26	32.5 31.5 30.4 29.3 28.3
65 66 67 68 69	23	21	33 4.62 47 46 5.00 78 11 58 5.00 36 0 10 5.45 79 1 26 32 6.00 80 18 52 6.67 44 0 52 6.67 44 0			0.42 .42 .43 .43	23	31 43 54 4 14	5.00 5.45 6.00 6.00 6.00	79 80	51 16 41 6 31	0.42 .42 .42 .42 .42	22	5 16 27 37 47	5.45 5.45 6.00 6.00 6.67	79 80	6 30 54 19 44	0.40 .40 .42 .42 .42	25 24 23 22 21	27.2 26.2 25.1 24.0 23.0
70 71 72 73 74	24	52 I IO I9 27		81 82		0.43 •45 •45 •45 •45		24 33 42 50 58	6.67 6.67 7.50 7.50 7.50	81	56 22 48 14 40	0.43 .43 .43 .43	23	56 5 14 22 30	6.67 6.67 7.50 7.50 8.57	81	9 34 59 25 51	0.42 .42 .43 .43	20 19 18 17 16	21.9 20.8 19.7 18.6 17.6
75 76 77 78 79	25	34 41 48 54 0	8.57 8.57 10.0 10.0 12.0	83 84	58 25 52 20 48	0.45 •45 •47 •47	24	6 13 19 25 31	8.57 10.0 10.0 10.0	83 84	7 34 1 28 55	0.45 •45 •45 •45 •45	24	37 44 50 56 1	8.57 10.0 10.0 12.0 12.0	83 84 85	17 43 9 35 2	0.43 .43 .43 .45 .45	15 14 13 12 11	16.5 15.4 14.3 13.2 12.1
80 81 82 83 84		5 10 14 18 21	12.0 15.0 15.0 20.0 20.0	85 86 87	16 44 12 40 9	0.47 .47 .47 .48 .47		36 40 44 48 51	15.0 15.0 15.0 20.0 20.0	85 86 87	22 50 17 45 12	• 47 • 45 • 47 • 45 • 47		6 11 15 18 21	12.0 15.0 20.0 20.0 20.0	86 87	29 55 22 49 16	0.43 •45 •45 •45 •47	9 8 7 6	9.9 8.8 7.7 6.6
85 86 87 38 89		21 20.0 87 9 24 30.0 37 0 26 30.0 88 6 28 60.0 34 29 60.0 89 3 30 — 89 3				0.48 •47 •48 •47 •48	25	54 56 58 59	30.0 30.0 60.0 60.0	88 89	40 8 36 4 32	0.47 .47 .47 .47 .47		24 26 28 29 30	30.0 30.0 60.0 60.0	88 89	44 11 38 5 33	•45 •45 •47 •45	5 4 3 2 1	5.5 4.4 3.3 2.2 1.1
90		30		90	0			0		90	0			30		90	0		0	0.0
t		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	(a	$\frac{60'}{\Delta}$	1	b	$\frac{\Delta}{60'}$	(ı	$\frac{60'}{\Delta}$	i	b	$\frac{\Delta}{60'}$		a
ı		C	l=64	4° 3	0′				d = 6	5° (0′			á	= 68	5° 3	0′			

\ b		a = 6	36° 0′			(a = 6	6° 3	30′				a = 0	37°	0′		\ c	a
B	h	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 1 2 3 4	0 0 24 49 1 13 38	2.50 2.40 2.50 2.40	66 0 0 1 2 3	0.00 .02 .02 .02	0	6 24 48 12 36	2.50 2.50 2.50 2.50 2.50	66	30 30 31 32 33	0.00	O	0 23 47	2.61 2.50 2.61 2.50 2.61	67°	0 0 1 2 3	0.00	90 89 88 87 86	90.0 89.1 88.2 87.2 86.3
5 6 7 8 9	2 2 26 50 3 15 39	2.50 2.50 2.40 2.50 2.50	5 7 9 12 16	0.03 .03 .05 .07	3	0 23 47 11 35	2.61 2.50 2.50 2.50 2.61		35 37 39 42 45	0.03 .03 .05 .05	3	57 20 44 7 30	2.61 2.50 2.61 2.61 2.61		5 7 9 12 15	.03 .03 .05 .05	85 84 83 82 81	85.4 84.5 83.6 82.7 81.7
10 11 12 13 14	4 3 27 51 5 15 39	2.50 2.50 2.50 2.50 2.50	20 24 28 33 38	0.07 .07 .08 .08	4 5	58 22 45 9 32	2.50 2.61 2.50 2.61 2.61	67	49 53 57 2 7	0.07 .07 .08 .08	4 5	53 16 39 2 25	2.61 2.61 2.61 2.61 2.61		19 23 27 32 37	0.07 .07 .08 .08	80 79 78 77 76	80.8 79.9 79.0 78.0 77.1
15 16 17 18 19	6 3 26 50 7 13 37	2.61 2.50 2.61 2.50 2.61	44 50 56 67 3	0.10 .10 .12 .12	6 7	55 18 41 4 27	2.61 2.61 2.61 2.61 2.61		13 19 25 32 39	0.10 .10 .12 .12	6 7	48 11 34 56 19	2.61 2.61 2.73 2.61 2.73	68	42 48 54 1 8	0.10 .10 .12 .12	75 74 73 72 71	76.2 75.3 74.3 73.4 72.5
20 21 22 23 24	8 0 23 46 9 9 31	2.61 2.61 2.61 2.73 2.61	18 26 34 43 52	0.13 .13 .15 .15	8	50 13 36 58 20	2.61 2.61 2.73 2.73 2.73	68	46 54 2 11 20	0.13 .13 .15 .15	8	41 3 25 47 9	2.73 2.73 2.73 2.73 2.73 2.86		15 23 31 39 48	0.13 .13 .13 .15	70 69 68 67 66	71.5 70.6 69.7 68.7 67.8
25 26 27 28 29	54 10 16 38 11 0 22	2.73 2.73 2.73 2.73 2.73 2.73	68 2 12 22 32 43	0.17 .17 .17 .18	10	42 4 26 48 9	2.73 2.73 2.73 2.86 2.86	69	29 39 49 0	0.17 .17 .18 .18	10	30 52 13 34 55	2.73 2.86 2.86 2.86 2.86	69	57 7 17 27 38	0.17 .17 .17 .18	65 64 63 62 61	66.8 65.9 65.0 64.0 63.1
30 31 32 33 34	12 6 27 48 13 9	2.73 2.86 2.86 2.86 2.86 2.86	55 69 7 19 31 44	0.20 .20 .20 .22	12	30 51 12 33 53	2.86 2.86 2.86 3.00 3.00	<i>7</i> 0	22 34 46 58 11	0.20 .20 .20 .22	11	16 37 57 17 37	2.86 3.00 3.00 3.00 3.00	70	49 0 12 24 37	0.18 .20 .20 .22 .22	60 59 58 57 56	62.1 61.1 60.2 59.2 58.3
35 36 37 38 39	30 50 14 10 30 50	3.00 3.00 3.00 3.00 3.16	58 70 12 26 40 55	0.23 .23 .23 .25	13	13 33 53 13 32	3.00 3.00 3.00 3.16 3.16	71	24 37 51 5 20	0.22 .23 .23 .25	13	57 17 36 55 14	3.00 3.16 3.16 3.16 3.16	71	50 30 30 44	0.22 .22 .23 .23	55 54 53 52 51	57·3 56·3 55·4 54·4 53·4
40 41 42 43 44	15 9 28 47 16 6 25	3.16 3.16 3.16 3.16 3.33	71 10 26 42 58 72 14	0.27 .27 .27 .27 .28	15	51 10 29 47 5	3.16 3.16 3.33 3.33 3.33	72	35 50 6 22 38	0.25 .27 .27 .27 .28	15	33 51 9 27 45	3·33 3·33 3·33 3·33 3·53	72	59 14 29 45	0.25 .25 .27 .27 .28	50 49 48 47 46	52.4 51.4 50.5 49.5 48.5
45	43		31			23			55		16	2			18		45	47.5
	а	<u>6ο'</u> Δ	b	<u>Δ</u> 6ο'	а		<u>60'</u> Δ	l	ь	<u>Δ</u> 6ο'	a		<u>6ο'</u> Δ	l	5	$\frac{\Delta}{60'}$		a
t		d = 6	6° 0′		_	d	=66	3° 3	0′				d = 6	7° ()′	1		

b			a = 6	6° ()′			а	=66	3° 3	0′				a=6	7° ()′		c	a
$ B\rangle$	h	d	60' Δ	Z	t	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	Z	t	<u>∆</u> 60′	h	d	6ο' Δ	\overline{z}	t	<u>Δ</u> 60'	$C \setminus$	$\beta \setminus$
45 46 47 48 49	16	43 1 18 35 52	3-33 3-53 3-53 3-53 3-53	7 ^o 73	31 49 7 25 43	0.30 .30 .30 .30	16	23 40 57 14 31	3.53 3.53 3.53 3.53 3.75	72 73 74	55 12 29 47 5	0.28 .28 .30 .30	16	19 36 53 9	3.53 3.53 3.53 3.75 3.75	73	18 34 51 8 26	0.27 .28 .28 .30	° 45 44 43 42 41	47.5 46.5 45.5 44.5 43.5
50 51 52 53 54	18	9 25 41 57 13	3.75 3.75 3.75 3.75 4.00	74 75	2 21 40 0 20	0.32 .32 .33 .33	18	47 3 19 34 49	3.75 3.75 4.00 4.00 4.00	75	23 42 1 20 40	0.32 .32 .32 .33	18	25 41 56 11 26	3.75 4.00 4.00 4.00 4.29	75	44 3 21 40 59	0.32 .30 .32 .32 .33	39 38 37 36	42.5 41.4 40.4 39.4 38.4
55 56 57 58 59	20	28 43 57 11 24	4.00 4.29 4.29 4.62 4.62	76 77	40 I 22 43 5	0.35 .35 .35 .37 .37	19	4 18 32 46 59	4.29 4.29 4.29 4.62 4.62	76 77	0 20 41 2 23	•35 •35 •35 •35 •35	19	40 54 8 21 34	4.29 4.29 4.62 4.62 4.62	76 77	19 39 59 19 40	0.33 •33 •33 •35 •35	35 34 33 32 31	37·4 36·3 35·3 34·3 33·2
60 61 62 63 64	21	37 50 3 15 27	4.62 4.62 5.00 5.00 5.45	78	27 49 11 34 57	0.37 .37 .38 .38	20	12 25 37 49 0	4.62 5.00 5.00 5.45 5.45	78 79	44 6 28 50 12	• 37 • 37 • 37 • 37 • 38	20	47 59 11 23 34	5.00 5.00 5.00 5.45 5.45	78 79	1 22 44 6 28	0.35 •37 •37 •37 •37	30 29 28 27 26	32.2 31.2 30.1 29.1 28.0
65 66 67 68 69	22	38 49 59 9	5.45 6.00 6.00 6.00 6.67	79 80	20 44 8 32 56	0.40 .40 .40 .40		11 22 32 42 51	5.45 6.00 6.00 6.67 6.67	80 81	35 58 21 45 9	0.38 .38 .40 .40	21	45 55 5 15 24	6.00 6.00 6.67 6.67	80 81	50 12 35 58 21	0.37 .38 .38 .38	25 24 23 22 21	27.0 25.9 24.8 23.8 22.7
70 71 72 73 74	23	28 37 45 53	6.67 7.50 7.50 7.50 8.57	81 82 83	20 45 10 35 0	0.42 .42 .42 .42 .43	22	0 9 17 25 32	6.67 7.50 7.50 8.57 8.57	82	33 57 21 45 10	0.40 .40 .40 .42 .42	22	33 41 49 57 4	7.5° 7.5° 7.5° 8.57 8.57	82	44 8 32 56 20	0.40 .40 .40 .40	20 19 18 17 16	21.6 20.6 19.5 18.4 17.4
75 76 77 78 79		8 15 21 27 32	8.57 10.0 10.0 12.0 12.0	84 85	26 51 17 43 9	0.42 •43 •43 •43 •43	23	39 46 52 58 3	8.57 10.0 10.0 12.0 12.0	84	35 O 25 50 I 5	0.42 •42 •42 •42 •43		11 17 23 28 33	10.0 10.0 12.0 12.0 12.0	8 ₄	44 8 33 57 22	0.40 .42 .40 .42 .42	15 14 13 12 11	16.3 15.2 14.1 13.1 12.0
80 81 82 83 84		37 41 45 49 52	15.0 15.0 15.0 20.0 30.0	86 87	35 1 27 54 20	0.43 .43 .45 .43 .45		8 12 16 19 22	15.0 15.0 20.0 20.0 30.0	86 87	41 6 32 58 24	0.42 •43 •43 •43 •43		38 42 46 49 52	15.0 15.0 20.0 20.0 30.0	86 87	47 12 37 2 28	0.42 .42 .42 .43 .42	10 9 8 7 6	9.8 8.7 7.6 6.5
85 86 87 88 89	24	54 56 58 59	30.0 30.0 60.0 60.0	88 89	47 13 40 7 33	0.43 .45 .45 .43 .45		24 26 28 29 30	30.0 30.0 60.0 60.0	88 89	50 16 42 8 34	0.43 .43 .43 .43 .43	23	54 56 58 59	30.0 30.0 60.0 60.0	88 89	53 18 44 9 34	0.42 •43 •42 •42 •43	5 4 3 2 1	5.5 4.4 3.3 2.2 1.1
90	_	0	90 0				_	30	6-1	90	0		_	0	601	90			0	0.0
t		a	60' Δ		b	$\frac{\Delta}{60'}$		a	60' <u>∆</u>		<i>b</i>	<u>Δ</u> 6ο'		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
			d = 6	6°	0′				d=6	6° 3	30′				$d = \mathbf{c}$	37°	0′			

Ĭ\ _	1				1			_							_	===	(7.
$\setminus b$		a = 6	7° 30′				$a = \epsilon$	38°	0′			(a = 6	8° 3	30′		c	x /
$B \setminus$	h d	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	\overline{z}	t	$\frac{\Delta}{60'}$	$C \setminus$	3
0 1 2 3 4	0 0 23 46 1 9 32	2.61	67 30 30 31 32 33	.02	0	0 22 45 7 30	2.73 2.61 2.73 2.61 2.73	68	0 0 1 2 3	0.00	O		2.73 2.73 2.73 2.73 2.73	68	30 30 31 32 33	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.1 88.1 87.2 86.3
5 6 78 9	55 2 18 40 3 3 26	2.61 2.73 2.61 2.61 2.61	35 37 39 42 45	.03	3	52 15 37 59 22	2.61 2.73 2.73 2.61 2.73		5 7 9 12 15	0.03 .03 .05 .05	3	50 12 34 55 17	2.73 2.73 2.86 2.73 2.73		35 37 39 41 44	0.03 .03 .03 .05	85 84 83 82 81	85.4 84.4 83.5 82.6 81.6
10 11 12 13 14	49 4 11 34 56 5 19	2.73 2.61 2.73 2.61 2.73	48 52 56 68 1	.08	4 5	44 6 28 50 12	2.73 2.73 2.73 2.73 2.73 2.73		18 22 26 31 36	.07 .08 .08	4 5	39 1 22 44 5	2.73 2.86 2.73 2.86 2.73	69	48 52 56 0 5	0.07 .07 .07 .08	80 79 78 77 76	80.7 79.8 78.9 77.9 77.0
15 16 17 18 19	6 3 25 47 7 9	2.73 2.73 2.73 2.73 2.73 2.73	12 18 24 30 37	.10	6 7	34 56 17 39 0	2.73 2.86 2.73 2.86 2.73	69	41 47 53 59 6	0,10 .10 .10 .12	6	27 48 9 30 51	2.86 2.86 2.86 2.86 2.86		10 16 22 28 34	0.10 .10 .10 .10	75 74 73 72 71	76.0 75.1 74.2 73.2 72.3
20 21 22 23 24	31 53 8 15 36 57	2.73 2.73 2.86 2.86 2.86	69 0 8	.13	8	22 43 4 25 46	2.86 2.86 2.86 2.86 2.86		13 20 28 36 44	0.12 .13 .13 .13	8	12 33 54 14 34	2.86 2.86 3.00 3.00 3.00	70	41 48 56 4 12	0.12 .13 .13 .13	70 69 68 67 66	71.4 70.4 69.5 68.5 67.6
25 26 27 28 29	9 18 39 10 0 21 42	2.86 2.86 2.86 2.86 3.00	25 35 45 55 70 5	.17	9	7 27 48 8 28	3.00 2.86 3.00 3.00 3.00	70	53 2 12 22 32	0.15 .17 .17 .17	9	54 14 34 54 14	3.00 3.00 3.00 3.00 3.00		21 30 39 49 59	0.15 .15 .17 .17	65 64 63 62 61	66.6 65.7 64.7 63.8 62.8
30 31 32 33 34	11 2 22 42 12 2 22	3.00 3.00 3.00 3.16	16 27 39 51 71 3	.20	11	48 27 46 5	3.00 3.16 3.16 3.16 3.16	71	43 54 5 17 29	0.18 .18 .20 .20	ΙΊ	34 53 12 31 50	3.16 3.16 3.16 3.16 3.33	71	10 21 32 43 55	0.18 .18 .18 .20	59 58 57 56	61.8 60.9 59.9 58.9 58.0
35 36 37 38 39	41 13 0 19 38 56	3.16 3.16 3.16 3.33 3.33	15 28 41 55 72 9	.22	13	24 43 2 20 38	3.16 3.16 3.33 3.33 3.33	72	41 54 7 20 34	0.22 .22 .22 .23 .23	12	8 26 44 2 20	3.33 3.33 3.33 3.33 3.33	72	7 19 32 45 59	0.20 .22 .22 .23 .23	55 54 53 52 51	57.0 56.0 55.1 54.1 53.1
40 41 42 43 44	14 14 32 50 15 8 25	3·33 3·33 3·33 3·53 3·53	24 39 54 73 9 25	.25	14	56 14 31 48 5	3.33 3.53 3.53 3.53 3.53	73	48 2 17 32 48	0.23 .25 .25 .27 .25	14	38 55 12 29 45	3.53 3.53 3.53 3.75 3.75	73 74	13 27 41 56 11	0.23 .23 .25 .25 .25	50 49 48 47 46	52.1 51.1 50.1 49.2 48.2
45	42		41			22		74	3		15	I			26		45	47.2
+	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	a	ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$. (a	<u>6ο'</u> Δ	b		$\frac{\Delta}{60'}$		a
$\mid t \mid$	(l = 67	7° 30′				d = 6	8° (0′			à	= 68	3° 3	0′			

6		a	a = 67	7° 3	0′				a = 6	8° ()′			a	=68	3° 3	0′		c	a
B	h	d	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 60'	h	d	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 60'	h	d	$\frac{60'}{\Delta}$	Z	t	<u>Δ</u> 6ο′	$C \setminus$	β
9 45 46 47 48 49	16	42 59 15 31 47	3.53 3.75 3.75 3.75 3.75 3.75	73 74	41 57 14 31 48	0.27 .28 .28 .28	16	22 38 54 10 26	3.75 3.75 3.75 3.75 4.00	74 75	3 19 36 52 9	0.27 .28 .27 .28 .28	16	1 17 33 48 3	3.75 3.75 4.00 4.00 4.00	74 75	26 42 58 14 31	0.27 .27 .27 .28 .28	\$45 44 43 42 41	47.2 46.2 45.2 44.2 43.2
50 51 52 53 54	17	3 18 33 48 2	4.00 4.00 4.00 4.29 4.29	75 76	6 24 42 0 19	0.30 .30 .30 .32 .32	17	41 56 10 24 38	4.00 4.29 4.29 4.29 4.29	76	26 44 2 20 38	0.30 .30 .30 .30	17	18 33 47 1	4.00 4.29 4.29 4.29 4.62	76	48 5 22 40 58	0.28 .28 .30 .30	40 39 38 37 36	42.1 41.1 40.1 39.1 38.1
5 5 56 57 58 59	19	16 30 43 56 9	4.29 4.62 4.62 4.62 5.00	77	38 57 17 37 57	•33 •33 •33 •35	18	52 6 19 32 44	4.29 4.62 4.62 5.00 5.00	77 78	57 16 35 55 15	•32 •33 •33 •33	18	28 41 54 6 18	4.62 4.62 5.00 5.00 5.00	77 78	16 35 54 13 32	0.32 .32 .32 .32 .32	35 34 33 32 31	37.1 36.0 35.0 34.0 32.9
60 61 62 63 64	20	21 33 45 56 7	5.00 5.45 5.45 5.45	78 79	18 39 0 21 42	0.35 .35 .35 .35 .37	19	56 8 19 30 41	5.00 5.45 5.45 5.45 6.00	<i>7</i> 9	35 55 16 37 58	•33 •35 •35 •35 •35	19	30 42 53 4 14	5.00 5.45 5.45 6.00 6.00	79 80	51 11 31 51 12	0.33 .33 .33 .35 .35	30 29 28 27 26	31.9 30.9 29.8 28.8 27.7
65 66 67 68 69		18 28 38 47 56	6.00 6.00 6.67 6.67 6.67	80	48 48 11 33	• 37 • 37 • 38 • 37 • 38	20	51 10 10 19 28	6.00 6.67 6.67 6.67 6.67	80	19 40 2 24 46	• 35 • 37 • 37 • 37 • 37	20	24 34 43 52 I	6.00 6.67 6.67 6.67 7.50	81	33 54 15 36 58	0.35 .35 .35 .37 .37	25 24 23 22 21	26.7 25.7 24.6 23.5 22.5
70 71 72 73 74	21	5 13 21 28 35	7.5° 7.5° 8.57 8.57 8.57	82	56 19 42 6 29	0.38 .38 .40 .38 .40	21	37 45 52 59 6	7.5° 8.57 8.57 8.57 8.57	82	8 30 53 16 39	0.37 .38 .38 .38 .38		9 17 24 31 38	7.50 8.57 8.57 8.57 10.0	82 83	20 42 4 26 48	0.37 .37 .37 .37 .38	20 19 18 17 16	21.4 20.4 19.3 18.3 17.2
75 76 77 78 79	22	42 48 54 59 4	10.0 10.0 12.0 12.0	84 85	53 17 41 5 29	0.40 .40 .40 .40		13 19 25 30 35	10.0 10.0 12.0 12.0 15.0	84 85	2 25 48 12 36	0.38 .38 .40 .40 .38	21	44 50 55 0	10.0 12.0 12.0 12.0 15.0	84 85	33 56 19 42	0.37 .38 .38 .38 .38	15 14 13 12 11	16.1 15.1 14.0 12.9 11.8
80 81 82 83 84	-	8 12 16 19 22	15.0 15.0 20.0 20.0 20.0	86 87	53 17 42 7 31	0.40 •42 •42 •40 •42		39 43 47 50 53	15.0 15.0 20.0 20.0 30.0	86 87	59 23 47 11 35	0.40 .40 .40 .40		9 13 17 20 23	15.0 15.0 20.0 20.0 30.0	86 87	28 52 15 39	0.38 .40 .38 .40 .38	9 8 7 6	9.7 8.6 7.5 6.5
85 86 87 88 89		25 27 28 29 30	30.0 60.0 60.0 60.0	88 89	56 21 45 10 35	0.42 .40 .42 .42 .42	22	55 57 58 59 0	30.0 60.0 60.0 —	88 89	59 23 47 12 36	0.40 .40 .42 .40		25 27 28 29 30	30.0 60.0 60.0 -	88	2 26 49 13 36	0.40 .38 .40 .38	5 4 3 2 1	5.4 4.3 3.2 2.2 1.1
90	_	30	604	90			_	0	601	90		Δ		30	600	90		 	0	0.0
t	_	a					-	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	0	ı	$\frac{60'}{\Delta}$		b	<u>Δ</u> 6ο'		a
		C	d=6	7° 3	0′				d = 6	8°	0′			(<i>l</i> = 6	8° 3	30′		A	

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1	,6			a=6	9° (D'				a = 6	9° 8	30′				a = 7	70°	0′	4	\ c	\ a
1	B	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
	0 1 2 3 4	2 4 I	0 2 3 5 6	2.73 2.86 2.73 2.86 2.86	69°	0 0 1 2 3	0.00 .02 .02 .02	°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°	0 21 42 3 24	2.86 2.86 2.86 2.86 2.86	69°	30 30 31 32 33	0.00 .02 .02 .02	0	0 2I 4I 2 22	2.86 3.00 2.86 3.00 2.86	7°	0 0 1 2 3	0.00	90 89 88 87 86	90.0 89.1 88.1 87.2 86.3
	56789	2 3	7 9 0 2 3	2.73 2.86 2.73 2.86 2.86		4 6 8 11 14	0.03 .03 .05 .05	2	45 6 27 48 9	2.86 2.86 2.86 2.86 3.00		34 36 38 41 44	.03 .05 .05	3	43 3 23 44 4	3.00 3.00 2.86 3.00 3.00		4 6 8 11 14	0.03 .03 .05 .05	85 84 83 82 81	85.3 84.4 83.4 82.5 81.6
	10 11 12 13 14	4 1	5 6 7 8	2.86 2.86 2.86 2.86 2.86		17 21 25 29 34	0.07 .07 .07 .08	4	29 50 11 31 52	2.86 2.86 3.00 2.86 3.00	70	47 51 55 59 4	0.07 .07 .07 .08	4	24 45 5 25 45	2.86 3.00 3.00 3.00 3.00		17 20 24 28 33	0.05 .07 .07 .08	80 79 78 77 76	80.6 79.7 78.7 77.8 76.8
	15 16 17 18 19	6 2	9 0 1 2	2.86 2.86 2.86 3.00 2.86	70	39 45 51 57 3	0.10 .10 .10 .10	6	33 53 13 33	2.86 3.00 3.00 3.00 3.00		9 14 20 26 32	0.08 .10 .10 .10	5 6	5 25 44 4 24	3.00 3.16 3.00 3.00 3.16	71	38 43 49 55 1	0.08	75 74 73 72 71	75.9 75.0 74.0 73.1 72.1
	20 21 22 23 24	· 8 4	33333	3.00 3.00 3.00 3.00 3.00		10 17 24 32 40	0.12 .12 .13 .13	7 8	53 13 32 52 12	3.00 3.16 3.00 3.00 3.16	71	39 46 53 1	0.12 .12 .13 .13	7 8	43 3 22 41 0	3.00 3.16 3.16 3.16 3.16		7 14 21 29 37	0.12 .12 .13 .13	70 69 68 67 66	71.2 70.2 69.3 68.3 67.4
	25 26 27 28 29	9 2	3 2 2 1 0	3.16 3.00 3.16 3.16 3.16	71	49 58 7 17 27	0.15 .15 .17 .17	9	31 50 9 28 47	3.16 3.16 3.16 3.16 3.33		17 26 35 44 54	0.15 .15 .15 .17	9	19 38 56 15 33	3.16 3.33 3.16 3.33 3.33	72	45 53 2 11 20	0.13 .15 .15 .15	65 64 63 62 61	66.4 65.4 64.5 63.5 62.6
	30 31 32 33 34	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 8 7 5 3	3.16 3.16 3.33 3.33 3.33	72	37 47 58 9 21	0.17 .18 .18 .20	11	5 23 41 59 17	3-33 3-33 3-33 3-33	72	4 14 25 36 47	0.17 .18 .18 .18	10	51 9 27 44 2	3·33 3·33 3·53 3·33 3·53	73	30 40 51 2 13	0.17 .18 .18 .18	59 58 57 56	61.6 60.6 59.7 58.7 57.7
	35 36 37 38 39	12	9752	3·33 3·33 3·33 3·53 3·53	73	33 45 57 10 23	0.20 .20 .22 .22 .23	12	35 53 10 27 44	3.33 3.53 3.53 3.53 3.53	73	58 10 22 35 48	0.20 .20 .22 .22	12	19 36 53 9 26	3.53 3.53 3.75 3.53 3.75	74	24 36 48 0	0.20 .20 .20 .20	55 54 53 52 51	56.7 55.8 54.8 53.8 52.8
	40 41 42 43 44	3 5 14	13 2 3.53 19 3.53 36 3.53 53 3.75 14 9 3.75 25 3.75		37 51 5 19 34	0.23 .23 .23 .25	13	1 17 33 49 5	3.75 3.75 3.75 3.75 4.00	74	1 14 28 42 57	0.22 .23 .23 .25 .23	13	42 58 14 29 44	3.75 3.75 4.00 4.00 4.00	75	25 38 52 6 20	0.22 .23 .23 .23 .23	50 49 48 47 46	51.8 50.8 49.9 48.9 47.9	
_	45	4	I	6.1		49			20		75	11			59	6.1		34		45	46.9
	t	a		<u>6ο'</u> Δ	l	b	$\frac{\Delta}{60'}$	_ a	ı	60' Δ	l	6	$\frac{\Delta}{60'}$	0	ı	<u>6ο'</u> Δ	l	,	<u>Δ</u> 60'		a
			(d = 6	9° ()′			C	l=69	9° 3	80′				d = 7	′0° ()′			į,

\ b	1		a = 6	9°	0′	÷		a	ı = 69	9° 3	0′				a = 7	70°	0′		\ c	a
B	h	d	<u>60'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
45 46 47 48 49	14	41 56 11 26 41	4.00 4.00 4.00 4.00 4.00	74 75	49 4 20 36 52	0.25 .27 .27 .27 .27	14	20 35 50 5 19	4.00 4.00 4.00 4.29 4.29	75°	11 26 42 57 13	0.25 .27 .25 .27 .27	13 14	59 14 29 43 57	4.00 4.00 4.29 4.29 4.29	75°	34 49 4 19 34	0.25 .25 .25 .25	° 45 44 43 42 41	46.9 45.9 44.9 43.9 42.9
50 51 52 53 54	16	56 10 24 38 51	4.29 4.29 4.29 4.62 4.62	76 77	8 25 42 59 17	.28 .28 .30 .30	16	33 47 1 14 27	4.29 4.29 4.62 4.62 4.62	77	29 45 2 19 36	0.27 .28 .28 .28 .30	15	11 25 38 51 4	4.29 4.62 4.62 4.62 5.00	77	50 6 22 39 55	0.27 .27 .28 .27 .28	40 39 38 37 36	41.9 40.8 39.8 38.8 37.8
55 56 57 58 59	17	4 17 29 41 53	4.62 5.00 5.00 5.00 5.00	78	35 53 11 30 49	0.30 .30 .32 .32	17	40 53 5 17 28	4.62 5.00 5.00 5.45 5.45	78 79	54 12 30 48 6	0.30 .30 .30 .30	17	16 28 40 52 3	5.00 5.00 5.45 5.45	78 79	12 30 47 5 23	0.30 .28 .30 .30	35 34 33 32 31	36.8 35.8 34.7 33.7 32.7
60 61 62 63 64	18	5 16 27 37 47	5.45 5.45 6.00 6.00 6.00	79 80	8 27 47 7 27	0.32 •33 •33 •33 •33	18	39 50 I II 21	5.45 5.45 6.00 6.00 6.67	80	25 44 3 22 42	0.32 .32 .32 .33 .33		14 24 34 44 54	6.00 6.00 6.00 6.00 6.67	80	41 0 18 37 56	0.32 .30 .32 .32 .32	30 29 28 27 26	31.6 30.6 29.6 28.5 27.5
65 66 67 68 69	19	57 7 16 25 33	6.00 6.67 6.67 7.50 7.50	81	47 8 28 49 10	•35 •35 •35 •35	19	30 39 48 57 5	6.67 6.67 6.67 7.50 7.50	81	I 2I 4I I 22	•33 •33 •35 •35	18	3 12 21 29 37	6.67 6.67 7.50 7.50 7.50	81	15 35 54 14 34	•33 •33 •33 •33	25 24 23 22 21	26.5 25.4 24.4 23.3 22.3
70 71 72 73 74	20	41 49 56 3	7.50 8.57 8.57 10.0 10.0	83	31 53 14 36 58	• 37 • 35 • 37 • 37 • 37		13 20 27 34 40	8.57 8.57 8.57 10.0	8 ₃	43 4 25 46 7	0.35 •35 •35 •35 •35	19	45 52 59 6	8.57 8.57 8.57 10.0	8 ₃	54 15 35 56 16	•35 •35 •35 •35	20 19 18 17 16	21.2 20.2 19.1 18.1 17.0
75 76 77 78 79		15 21 26 31 36	10.0 12.0 12.0 12.0 15.0	84 85	20 42 4 26 49	• 37 • 37 • 38 • 37	20	46 52 57 2 6	10.0 12.0 12.0 15.0 15.0	85	28 50 11 33 55	•37 •35 •37 •37 •37		18 23 28 33 37	12.0 12.0 12.0 15.0	8 ₅	37 58 19 40 2	•35 •35 •35 •37 •35	15 14 13 12 11	16.0 14.9 13.8 12.8 11.7
80 81 82 83 84		40 44 47 50 53	15.0 20.0 20.0 20.0 30.0	86 87	11 34 57 19 42	0.38 .38 .37 .38 .38		10 14 17 20 23	15.0 20.0 20.0 20.0 30.0	86 87	17 39 1 23 46	• 37 • 37 • 37 • 38 • 37		41 45 48 51 53	15.0 20.0 20.0 30.0 30.0	87	23 44 6 28 49	0.35 .37 .37 .35 .37	10 98 7 6	10.7 9.6 8.5 7.5 6.4
85 86 87 88 89	21	55 57 58 59 0	30.0 60.0 60.0 -	88	5 28 51 14 37	0.38 .38 .38 .38		25 27 28 29 30	30.0 60.0 60.0 	88	8 30 53 15 37	• 37 • 38 • 37 • 37 • 38	20	55 57 58 59 0	30.0 60.0 60.0 60.0	88 89	33 55 16 38	• 37 • 35 • 37 • 37	5 4 3 2 1	5.3 4.3 3.2 2.1 1.1
90		ο 90 ο <u>Δ</u>					_	30	601	90	0	Δ	_	0	600	90		Δ.	0	0.0
t		$a \mid \overline{\Delta} \mid b \mid \overline{60}$						1	$\frac{60'}{\Delta}$		b	<u>Δ</u> 6ο'	-	ı	$\frac{60'}{\Delta}$		<i>b</i>	<u>Δ</u> 6ο′		a
	d = 69° 0′							a	l = 69	9° 3	0′				d = 7	0°	0′			

b		(a = 7	0° 8	30′				a = 7	1°	0′			-	<i>a</i> = 7	1° 8	30′		\ c	a
B	h	d	<u>6ο'</u> Δ	Z	t	<u>∆</u> 60′	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	$\beta \setminus$
0 I 2 3 4	O	20 40 0 20	3.00 3.00 3.00 3.00 3.00	70	30 30 31 32 33	0.00 .02 .02 .02	00	0 20 39 59 18	3.00 3.16 3.00 3.16 3.00	71	0 0 1 2 3	0.00 .02 .02 .02	O	0 19 38 57 16	3.16 3.16 3.16 3.16 3.16	7 I	30 30 31 32 33	0.00 .02 .02 .02	90 89 88 87 86	90.0 89.1 88.1 87.2 86.2
5 6 7 8 9	3	40 0 20 40 0	3.00 3.00 3.00 3.00 3.00		34 36 38 40 43	0.03 .03 .03 .05	2	38 57 17 36 55	3.16 3.00 3.16 3.16 3.00		4 6 8 10 13	0.03 .03 .03 .05	2	35 54 13 32 51	3.16 3.16 3.16 3.16 3.16		34 36 38 40 43	0.03 .03 .03 .05	85 84 83 82 81	85.3 84.3 83.4 82.4 81.5
10 11 12 13 14	4	20 39 59 18 38	3.16 3.00 3.16 3.00 3.16	71	46 50 54 58 2	0.07 .07 .07 .07	3	15 34 53 12 31	3.16 3.16 3.16 3.16 3.16		16 19 23 27 31	0.05 .07 .07 .07	3	10 28 47 6 24	3.33 3.16 3.16 3.33 3.16	72	46 49 53 57	0.05 .07 .07 .07	80 79 78 77 76	80.5 79.6 78.6 77.7 76.7
15 16 17 18 19	5	57 17 36 55 14	3.00 3.16 3.16 3.16 3.16		7 12 17 23 29	0.08	5 6	50 9 28 46 5	3.16 3.16 3.33 3.16 3.16		36 41 46 52 58	0.08	5	43 1 19 38 56	3.33 3.33 3.16 3.33 3.33		5 10 15 21 27	0.08	75 74 73 72 71	75.8 74.8 73.9 72.9 72.0
20 21 22 23 24	7	33 52 11 30 48	3.16 3.16 3.16 3.33 3.16	72	35 42 49 57 5	0.12 .12 .13 .13	7	24 42 0 18 36	3.33 3.33 3.33 3.33 3.33	72	4 11 18 25 32	0.12 .12 .12 .12	6 7	14 32 50 7 25	3·33 3·33 3·53 3·33 3·53	73	33 39 46 53 0	0.10 .12 .12 .12	70 69 68 67 66	71.0 70.1 69.1 68.1 67.2
25 26 27 28 29	9	7 25 43 1	3·33 3·33 3·33 3·33 3·33		13 21 29 38 47	0.13 .13 .15 .15	8	54 12 30 48 5	3·33 3·33 3·33 3·53 3·53	73	40 48 56 5	0.13 .13 .15 .15	8	42 0 17 34 51	3·33 3·53 3·53 3·53 3·53		8 16 24 32 41	0.13 .13 .13 .15	65 64 63 62 61	66.2 65.2 64.3 63.3 62.3
30 31 32 33 34	10	37 54 11 28 45	3.53 3.53 3.53 3.53 3.53	73	57 7 17 27 38	0.17 .17 .17 .18 .18	10	39 56 13 30	3.53 3.53 3.53 3.53 3.75	74	24 34 44 54 4	0.17 .17 .17 .17	9	8 24 41 57 13	3.75 3.53 3.75 3.75 3.75	74	50 0 10 20 30	0.17 .17 .17 .17	60 59 58 57 56	61.4 60.4 59.4 58.4 57.5
35 36 37 38 39	11	2 19 35 51 7	3.53 3.75 3.75 3.75 3.75 3.75	74	49 1 13 25 37	0.20 .20 .20 .20	11	46 18 34 50	3.75 3.75 3.75 3.75 4.00	75	15 26 37 49 1	0.18 .18 .20 .20	11	29 45 1 16 31	3.75 3.75 4.00 4.00 4.00	75	40 51 2 14 26	0.18 .18 .20 .20	55 54 53 52 51	56.5 55.5 54.5 53.5 52.6
40 41 42 43 44	13	23 39 54 9 24	3.75 4.00 4.00 4.00 4.00	75	49 15 29 43	0.22 .22 .23 .23 .23	12	- 1	4.00 4.00 4.00 4.29 4.29	76	13 26 39 52 5	0.22 .22 .22 .22 .23	12	46 1 16 30 44	4.00 4.00 4.29 4.29 4.29	76	38 50 2 15 28	0,20 ,20 ,22 ,22	50 49 48 47 46	51.6 50.6 49.6 48.6 47.6
45		39	60'	,	57	Δ		18	60'		19	Δ		58	60'	7	41	Δ	45	46.6
t	a		Δ		9	$\frac{\Delta}{60'}$	a		Δ		b	<u>Δ</u> 6ο'			Δ			60′		α
		d	=70)° 3	0′			(d=7	1° ()′ 			d	=71	° 3	0′			

\ b		C	<i>u</i> = 70)° 3	0′				a = 7	71° (0′			(a = 7	1° 3	0′		c	a
$ B\rangle$	h	d	<u>60'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
9 45 46 47 48 49	13	39 54 8 22 36	4.00 4.29 4.29 4.29 4.62	75 76	57 11 25 40 55	0.23 .23 .25 .25	13	18 32 46 0	4.29 4.29 4.29 4.62 4.62	76 77	19 33 47 1 16	0.23 .23 .23 .25	12 13	58 12 25 38 51	4.29 4.62 4.62 4.62 4.62	78 77	41 55 9 23 37	0.23 .23 .23 .23 .25	° 45 44 43 42 41	46.6 45.6 44.6 43.6 42.6
50 51 52 53 54	15	49 2 15 28 40	4.62 4.62 4.62 5.00 5.00	77 78	10 26 42 58 15	0.27 .27 .27 .28 .27	15	26 39 52 4 16	4.62 4.62 5.00 5.00 5.00	78	31 46 2 18 34	0.25 .27 .27 .27 .27	14	4 17 29 41 53	4.62 5.00 5.00 5.00 5.45	78	52 7 22 37 52	0.25 .25 .25 .25 .27	40 39 38 37 36	41.6 40.6 39.6 38.6 37.5
55 56 57 58 59	16	52 4 16 27 38	5.00 5.00 5.45 5.45 6.00	79	31 48 5 22 40	0.28 .28 .28 .30	16	28 40 51 2 12	5.00 5.45 5.45 6.00 6.00	79	50 6 23 40 57	0.27 .28 .28 .28	15	4 15 26 37 47	5.45 5.45 5.45 6.00 6.00	79 80	8 24 40 57 13	0.27 .27 .28 .27 .28	35 34 33 32 31	36.5 35.5 34.5 33.5 32.4
60 61 62 63 64	17	48 58 8 18 27	6.00 6.00 6.00 6.67 6.67	80	58 16 34 52 10	0.30 .30 .30 .30	17	22 32 42 52 1	6.00 6.00 6.00 6.67 6.67	80	14 31 49 7 25	0.28 .30 .30 .30	16	57 7 16 25 34	6.00 6.67 6.67 6.67 6.67	81	30 47 4 22 39	0.28 .28 .30 .28	30 29 28 27 26	31.4 30.4 29.4 28.3 27.3
65 66 67 68 69	18	36 45 54 2	6.67 6.67 7.50 7.50 8.57	82	29 48 7 27 46	0.32 .32 .33 .32 .33		10 18 26 34 42	7.5° 7.5° 7.5° 7.5° 8.57	82	43 2 20 39 58	0.32 .30 .32 .32 .32	17	43 51 59 7 14	7.50 7.50 7.50 8.57 8.57	82	57 15 33 51 10	0.30 .30 .30 .32 .30	25 24 23 22 21	26.3 25.2 24.2 23.1 22.1
70 71 72 73 74		17 24 31 37 43	8.57 8.57 10.0 10.0	83 84	6 25 45 5 26	0.32 .33 .33 .35 .33	18	49 56 2 8 14	8.57 10.0 10.0 10.0	83 84	17 36 56 15 35	0.32 •33 •32 •33 •32		21 28 34 40 46	8.57 10.0 10.0 10.0	84	28 47 6 25 44	0.32 .32 .32 .32 .32	20 19 18 17 16	21.1 20.0 19.0 17.9 16.9
75 76 77 78 79	19	49 54 59 4 8	12.0 12.0 12.0 15.0 15.0	8 ₅	46 6 27 47 8	0.33 .35 .33 .35 .35		20 25 30 34 38	12.0 12.0 15.0 15.0 15.0	8 ₅	54 14 34 54 14	0.33 .33 .33 .33	18	51 56 1 5	12.0 12.0 15.0 15.0	85 86	3 22 42 1 21	0.32 .33 .32 .33 .32	15 14 13 12 11	15.8 14.8 13.7 12.7 11.6
80 81 82 83 84		12 15 18 21 23	20.0 20.0 20.0 30.0 30.0	87	29 50 11 32 53	0.35 .35 .35 .35		42 45 48 51 53	20.0 20.0 20.0 30.0 30.0	87	35 55 15 36 56	0.33 .33 .35 .33		13 16 19 22 24	20.0 20.0 20.0 30.0 30.0	87 88	40 0 20 40 0	0.33 .33 .33 .33	9 8 7 6	10.6 9.5 8.5 7.4 6.3
85 86 87 88 89		25 27 28 29 30	30.0 60.0 60.0	88	14 35 56 18 39	0.35 .35 .37 .35 .35	19	55 57 58 59 0	30.0 60.0 60.0 60.0	88	17 37 58 19 39	0.33 •35 •35 •33 •35		26 27 28 29 30	60.0 60.0 60.0 -	89	20 40 0 20 40	0.33 .33 .33 .33	5 4 3 2 1	5·3 4·2 3·2 2·1 1·1
90	_	30 90 0 a 60' b 4				_	0		90	0		_	30		90	0		0	2.0 ——	
t	_					$\frac{\Delta}{60'}$	0	ı	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$		a	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$		a
			d=7	0° 3	0′				d = 7	71°	0′			(d=7	1° 3	80′			

\ b	/	a = 7	2° 0′	\ \ 1		a	s = 72	2º 3	0′				a = 7	3° ()′	y	c	\ a
B	h d	$\frac{60'}{\Delta}$	Z	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	6ο' Δ	Z	t	$\frac{\Delta}{60'}$	C	β
0 0 1 2 3 4	0 0 19 37 56 1 14	3.16 3.33 3.16 3.33 3.16	72 ° 0 ° 0 ° 1 ° 1 ° 2	0.00 .02 .00 .02		0 18 36 54 12	3·33 3·33 3·33 3·33	72	30 30 31 31 32	0.00 .02 .00 .02	0	0 18 35 53 10	3·33 3·53 3·33 3·53 3·33	73	0 0 1 1 2	0.00 .02 .00 .02	90 89 88 87 86	90.0 89.0 88.1 87.1 86.2
5 6 78 9	33 51 2 9 28 46	3.33 3.33 3.16 3.33 3.16	4 6 8 10 13	0.03 .03 .03 .05	2	30 48 6 24 42	3.33 3.33 3.33 3.33 3.33		34 35 37 39 42	0.02 .03 .03 .05	2	28 45 3 20 37	3.53 3.33 3.53 3.53 3.33		4 5 7 9 12	0.02 .03 .03 .05	85 84 83 82 81	85.2 84.3 83.3 82.4 81.4
10 11 12 13 14	3 5 23 41 59 4 17	3.33 3.33 3.33 3.33 3.33	16 19 22 26 30	0.05 .05 .07 .07		0 17 35 53 10	3.53 3.33 3.33 3.53 3.53		45 48 51 55 59	0.05 .05 .07 .07	3	55 12 29 46 3	3.53 3.53 3.53 3.53 3.53		15 18 21 25 29	0.05 .05 .07 .07	80 79 78 77 76	80.5 79.5 78.5 77.6 76.6
15 16 17 18 19	35 53 5 11 29 46	3.33 3.33 3.33 3.53 3.33	34 39 44 49 55	0.08 .08 .08		28 45 3 20 37	3.53 3.33 3.53 3.53 3.53	73	3 8 13 18 24	80.0 80. 80. 10	5	20 37 54 11 28	3.53 3.53 3.53 3.53 3.75		33 37 42 47 52	0.07 .08 .08 .08	75 74 73 72 71	75·7 74·7 73·7 72·8 71.8
20 21 22 23 24	6 4 21 39 56 7 13	3.53 3.53 3.53 3.53 3.53	73 I 7 14 21 28	0.10 .12 .12 .12		54 11 28 45 2	3.53 3.53 3.53 3.53 3.75		30 36 42 49 56	0.10 .10 .12 .12	6	44 1 17 34 50	3.53 3.75 3.53 3.75 3.75	74	58 4 10 17 24	0,10 .10 .12 .12	70 69 68 67 66	70.9 69.9 68.9 68.0 67.0
25 26 27 28 29	30 47 8 4 21 37	3.53 3.53 3.53 3.75 3.75	35 43 51 59 74	0.13 .13 .13 .15	8	18 35 51 7 23	3.53 3.75 3.75 3.75 3.75	74	3 11 19 27 35	0.13 .13 .13 .13	<i>7</i> 8	6 22 38 54 9	3.75 3.75 3.75 4.00 3.75	75	31 38 46 54 2	0.12 .13 .13 .13	65 64 63 62 61	66.0 65.1 64.1 63.1 62.1
30 31 32 33 34	53 9 9 25 41 57	3.75 3.75 3.75 3.75 3.75	17 26 36 46 56	0.15 .17 .17 .17	9	39 55 10 26 41	3.75 4.00 3.75 4.00 4.00	75	44 53 2 11 21	0.15 .15 .15 .17	9	25 40 55 10 25	4.00 4.00 4.00 4.00 4.29		10 19 28 37 46	0.15 .15 .15 .15	59 58 57 56	61.2 60.2 59.2 58.2 57.2
35 36 37 38 39	10 13 28 43 58 11 13	4.00 4.00 4.00 4.00	75 6 16 27 38 50	0.17 .18 .18 .20	10	56 11 26 40 54	4.00 4.00 4.29 4.29 4.29	76	31 41 52 3 14	0.17 .18 .18 .18	10	39 54 8 22 36	4.00 4.29 4.29 4.29 4.29	76	56 6 17 27 38	0.17 .18 .17 .18	55 54 53 52 51	56.3 55.3 54.3 53.3 52.3
40 41 42 43 44	28 42 56 12 10 24	4.29 4.29 4.29 4.29 4.29		0.20		8 22 36 50 3	4.29 4.29 4.29 4.62 4.62	77	25 37 49 1	0.20 .20 .20 .20	11	50 4 17 30 43	4.29 4.62 4.62 4.62 4.62	77	49 0 12 24 36	0.18 .20 .20 .20	50 49 48 47 46	51.3 50.3 49.3 48.4 47.4
45	38		77 4	1		16	6-1		26			56	601		48	1 1	45	46.4
t	а	6ο' Δ	b	$\frac{\Delta}{60'}$	0	ı	<u>δο'</u> Δ		b	$\frac{\Delta}{60'}$	- 0	a	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$		a
		d = 7	2° 0′	,		(d = 7	2° 3	0′				d = 7	'3° (0′			

8			a = 7	2°	0′			a	a = 72	2° 3	0′	1		:	a=7	3° ()′∶	.)	\ c	
B	h	<i>d</i>	<u>6ο′</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	d	<u>60</u> ⁴ Δ	z	t	<u>Δ</u> 6ο'	h	d	6ο'. Δ	Z	t	<u>A</u> ,	$C \setminus$	β
45 46 47 48 49	13	38 51 4 17	4.62 4.62 4.62 5.00 5.00	77	4 17 30 44 58	0,22 ,22 ,23 ,23 ,23	12	16 29 42 55 7	4.62 4.62 4.62 5.00 5.00	77 78	26 39 52 5	0.22	0 II I2	56 9 21 33 45	4.62 5.00 5.00 5.00 5.00	77 78	48 1 13 26 39	0.22	45 44 43 42 41	46.4 45.4 44.4 43.4 42.3
50 51 52 53 54	14	41 53 5 17 29	5.00 5.00 5.00 5.00 5.45	78 79	12 26 41 56 11	0.23 .25 .25 .25 .25	14	19 31 43 54 5	5.00 5.00 5.45 5.45 5.45	79	33 47 1 15 30	0.23 .23 .23 .25	13	57 8 19 30 41	5.45 5.45 5.45 5.45 5.45	79	53 7 21 35 49	0.23 .23 .23 .23 .23	40 39 38 37 36	41.3 40.3 39.3 38.3 37.3
55 56 57 58 59	15	40 51 1 11 21	5.45 6.00 6.00 6.00 6.00	80	26 42 58 14 30	0.27 .27 .27 .27 .27	Ļ	16 26 36 46 56	6.00 6.00 6.00 6.00	80	45 0 15 31 47	0.25 .25 .27 .27 .27	14	52 12 22 31	6.00 6.00 6.67 6.67	80	3 3 3 48 3	25 25 25 25 25	35 34 33 32 31	36.3 35.3 34.3 33.2 32.2
60 61 62 63 64	2	31 50 59 8	6.00 6.67 6.67 6.67 7.50	81	46 3 20 37 54	.28 .28 .28 .28	15	6 15 24 33 41	6.67 6.67 6.67 7.50 7.50	81	3 19 35 51 8	0.27 .27 .27 .28 .28	15	40 49 58 6	6.67 6.67 7.50 7.50 7.50	82	18 34 50 22	0.27 .27 .27 .27 .27	30 29 28 27 26	31.2 30.2 29.1 28.1 27.1
65 66 67 68 69	(A critical	16 24 32 39 46	7.50 7.50 8.57 8.57 8.57	82	11 28 46 4 22	.30 .30 .30	16	49 57 4 11 18	7.5° 8.57 8.57 8.57 8.57	83	25 42 59 16 33	.28 .28 .28 .28		22 30 37 44 51	7.50 8.57 8.57 8.57 10.0	83	38 55 11 28 45	0.28 .27 .28 .28	25 24 23 22 21	26.1 25.0 24.0 23.0 21.9
70 71 72 73 74	17	53 59 51 17	10.0 10.0 10.0 10.0	84	40 58 16 34 53	0.30 .30 .30 .32 .32		25 31 37 43 48	10.0 10.0 10.0 12.0 12.0	84	51 8 26 44 2	.30 .30 .30 .30	16	57 3 9 14 19	10.0 10.0 12.0 12.0	84	19 36 53 11	0.28 .28 .28 .30 .28	20 19 18 17 16	20.9 19.9 18.8 17.8 16.7
75 76 77 78 79	2	22 27 31 35	12.0 15.0 15.0 15.0	85	30 49 8 27	0.30 .32 .32 .32 .32	17	53 58 2 6	12.0 15.0 15.0 15.0	86	20 38 56 15 33	0.30 .30 .32 .30		24 29 33 37 41	12.0 15.0 15.0 15.0 20.0	86	28 46 4 22 40	.30 .30 .30 .30	15 14 13 12 11	15.7 14.7 13.6 12.6 11.5
80 81 82 83 84	4	13 16 19 52	20.0 20.0 20.0 30.0 30.0	87 88	46 5 25 44 3	•33 •32 •32 •33		14 17 20 22 24	20.0 20.0 30.0 30.0 30.0	87 88	52 10 29 48 7	0.30 .32 .32 .32 .30		44 47 50 52 54	20.0 20.0 30.0 30.0 30.0	87 88	58 16 34 52 10	.30 .30 .30 .30	9 8 7 6	10.5 9.4 8.4 7.3 6.3
85 86 87 88 89		56 57 58 59 0	60.0 60.0 60.0	89	23 42 1 21 40	0.32 •32 •33 •32 •33		26 27 28 29 30	60.0 60.0 60.0	89	25 44 3 22 41	0.32 •32 •32 •32 •32	17	56 57 58 59 0	60.0 60.0 60.0	89	28 47 5 23 42	.30 .30 .32 .30	5 4 3 2 1	5.2 4.2 3.1 2.1 1.0
90	a	0	60'	90	о b	Δ	-	30	60'	90	b	Δ	-	о а	60′	90	o b:	Δ	0	0.0 a
t			d = 7			60'	_		d = 7	1		60'			d = 7			60'		, , , ,

1	,			a=7	'3° :	30′				a = 7	74°	0′			1	a = 7	4° 8	80′		c	\ a
B		h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	6ο' Δ	z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
3 4		o	34 51 8	3.53 3.53 3.53				0		3.53 3.75 3.53 3.75 3.53	74		0,00 ,02 ,00 ,02	O		3.75 3.75 3.75 3.75 3.75 3.75	74		0.00 .02 .00 .02	90 89 88 87 86	90.0 89.0 88.1 87.1 86.2
5 6 7 8 9		2	25 42 59 16 33	3.53 3.53 3.53 3.53 3.53		33 35 37 39 41	.03 .03 .03 .03	2	23 39 56 12 28	3.75 3.53 3.75 3.75 3.53		3 5 7 9	0.03 .03 .03 .03	2	20 36 52 8 24	3.75 3.75 3.75 3.75 3.75		33 35 37 39 41	0.03 .03 .03 .03	85 84 83 82 81	85.2 84.2 83.3 82.3 81.3
10 11 12 13 14		3	50 6 23 40 56	3.75 3.53 3.53 3.75 3.53		44 47 50 54 58	0.05 .05 .07 .07	3	45 1 17 33 49	3.75 3.75 3.75 3.75 3.75		14 17 20 23 27	0.05 .05 .05 .07	3	40 55 11 27 42	4.00 3.75 3.75 4.00 3.75		43 46 49 53 56	0.05 .05 .07 .05	80 79 78 77 76	80.4 79.4 78.5 77.5 76.5
15 16 17 18 19		5	13 29 46 2 18	3.75 3.53 3.75 3.75 3.75	74	2 6 11 16 21	0.07 .08 .08 .08	5	5 21 37 53 9	3.75 3.75 3.75 3.75 3.75		31 35 40 45 50	0.07 .08 .c8 .08	4	58 14 29 44 59	3.75 4.00 4.00 4.00 4.00	75	0 4 9 13 18	0.07 .08 .07 .08	75 74 73 72 71	75.6 74.6 73.6 72.7 71.7
20 21 22 23 24		6	34 50 6 22 38	3.75 3.75 3.75 3.75 3.75		27 33 39 45 51	0.10 .10 .10 .10	6	25 40 56 11 26	4.00 3.75 4.00 4.00 4.00	75	55 1 7 13 19	0.10 .10 .10 .10	5 6	14 29 44 59 14	4.00 4.00 4.00 4.00 4.00		23 29 35 41 47	0.10	70 69 68 67 66	70.7 69.7 68.8 67.8 66.8
25 26 27 28 29		7	54 9 25 40 55	4.00 3.75 4.00 4.00 4.00	75	58 5 13 21 29	0.12 .13 .13 .13	7	41 56 11 26 41	4.00 4.00 4.00 4.00 4.29		26 33 40 48 55	0.12 .12 .13 .12 ,13	7	29 44 58 12 26	4.00 4.29 4.29 4.29 4.29	76	53 0 7 14 22	0,12 .12 .12 .13	65 64 63 62 61	65.9 64.9 63.9 62.9 62.0
30 31 32 33 34		9	10 25 40 54 8	4.00 4.29 4.29 4.29	76	37 45 54 3	0.13 .15 .15 .15	8	55 10 24 38 52	4.00 4.29 4.29 4.29 4.29	76	3 11 20 29 38	0.13 .15 .15 .15	8	40 54 8 22 36	4.29 4.29 4.29 4.29 4.62	77	30 38 46 54 3	0.13 .13 .13 .15	59 58 57 56	61.0 60.0 59.0 58.0 57.0
35 36 37 38 39	1	0	22 36 50 4 18	4.29 4.29 4.29 4.29 4.62	77	22 32 42 52 2	0.17 .17 .17 .17	9	6 19 33 46 5 9	4.62 4.29 4.62 4.62 4.62	77	47 56 6 16 26	0.15 .17 .17 .17	9	49 2 15 28 41	4.62 4.62 4.62 4.62 4.62		12 21 31 40 50	0.15 .17 .15 .17	55 54 53 52 51	56.1 55.1 54.1 53.1 52.1
40 41 42 43 44	I	I	31 44 57 10 23	4.62 4.62 4.62 4.62 5.00		13 24 35 46 58	0.18 .18 .18 .20	10	12 25 38 50 2	4.62 4.62 5.00 5.00 5.00	78	37 47 58 9 21	0.17 .18 .18 .20	10	54 6 18 30 42	5.00 5.00 5.00 5.00 5.00	78	0 11 21 32 43	0.18 .17 .18 .18	50 49 48 47 46	51.1 50.1 49.1 48.1 47.1
45	_	_	35		78	10			14			32			54			54		45	46.1
t		a		6ο' Δ	b	,	<u>Δ</u> 6ο'	(ı	<u>6ο'</u> Δ	i	b	$\frac{\Delta}{60'}$	C	ı	6ο' Δ		b	$\frac{\Delta}{60'}$		α
			d	=78	0′				d = 7	4° ()′			d	l=74	1° 3	0′				

\ b		a =	73°	30′				a = 7	4°	0′			C	a=74	4° 3	0′		c	a
B	h	d 60 Δ	1 2	* *	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	11 3 4 5 12 1 2	7 5.0 9 5.0 I 5.0		22 34 47	0.20 .20 .22 .22	12	14 26 38 49 0	5.00 5.00 5.45 5.45 5.45	78 79	3 ² 44 56 8 21	0.20 .20 .20 .22 .20	10 11	54 5 16 27 38	5.45 5.45 5.45 5.45 5.45	78 79	54 6 17 29 41	0.20 .18 .20 .20	\$\frac{9}{45}\$ 44 43 42 41	46.1 45.1 44.1 43.1 42.1
50 51 52 53 54	3 4 5 13	5 5.4 6 5.4 7 6.0	5	13 26 40 54 7	0.22 .23 .23 .22 .23		11 22 33 43 53	5.45 5.45 6.00 6.00 6.00	80	33 46 59 13 26	0.22 .22 .23 .22 .23	12	49 59 9 19 29	6.00 6.00 6.00 6.00 6.00	80	53 6 19 32 45	0.22 .22 .22 .22 .22	40 39 38 37 36	41.1 40.1 39.1 38.1 37.1
55 56 57 58 59	2 3 4 5	7 6.0 7 6.6	7 8:	21 36 50 1 5 20	0.25 .23 .25 .25	13	3 13 22 31 40	6.00 6.67 6.67 6.67 6.67	81	40 54 8 22 36	0.23 .23 .23 .23	13	39 48 57 6	6.67 6.67 6.67 6.67 7.5°	81	58 11 25 38 52	0.22 .23 .22 .23 .23	35 34 33 32 31	36.1 35.1 34.0 33.0 32.0
61 62 63 64	1 2 3 3 4	3 7.59 1 7.59 9 7.59	82	35 50 2 5 20 36	0.25 .25 .25 .27 .27	14	49 57 5 13 21	7.5° 7.5° 7.5° 7.5° 8.57	82	50 5 20 35 50	0.25 .25 .25 .25		23 31 39 47 54	7.5° 7.5° 7.5° 8.57 8.57	82	6 20 35 49 4	0.23 .25 .23 .25 .25	30 29 28 27 26	31.0 30.0 29.0 27.9 26.9
65 66 67 68 69		2 8.5 9 8.5 5 8.5	7 8	52 8 24 40 56	0.27 .27 .27 .27 .28		28 35 42 49 55	8.57 8.57 8.57 10.0	83 84	5 21 36 52 8	0.27 .25 .27 .27 .27	14	1 8 15 21 27	8.57 8.57 10.0 10.0	84	19 34 49 4 19	0.25 .25 .25 .25 .27	25 24 23 22 21	25.9 24.9 23.8 22.8 21.8
70 71 72 73 74	2 3 4 4 5	5 12. 5 12.	8	29 46	0.27 .28 .28 .28	15	1 7 12 17 22	10.0 12.0 12.0 12.0 12.0	85	24 40 56 12 29	0.27 .27 .27 .28 .27		33 38 43 48 53	12.0 12.0 12.0 12.0	85	35 50 6 22 38	0.25 .27 .27 .27 .27	20 19 18 17 16	20.7 19.7 18.7 17.6 16.6
75 76 77 78 79		15.0	86	37 54 5 11 28 46	0.28 .28 .28 .30 .28		27 31 35 39 42	15.0 15.0 15.0 20.0 20.0	86	45 2 19 35 52	0.28 .28 .27 .28 .28	15	58 2 6 9	15.0 15.0 20.0 20.0 20.0	86	54 10 26 42 58	0.27 .27 .27 .27 .27	15 14 13 12 11	15.6 14.5 13.5 12.5 11.4
80 81 82 83 84	I I 2 2 2	7 20.0 30.0 2 30.0		21 38 56	0.30 .28 .30 .28		45 48 51 53 55	20.0 20.0 30.0 30.0 60.0	87 88	9 26 43 0	0.28 .28 .28 .28		15 18 21 23 25	20.0 20.0 30.0 30.0 30.0	87 88	14 31 47 4 20	0.28 .27 .28 .27 .28	10 9 8 7 6	10.4 9.4 8.3 7.3 6.2
85 86 87 88 89	2 2 2 2 3	7 60.6 8 60.6 9 60.6	89	31 49 7 24 42	0.30 .30 .28 .30	16	56 57 58 59 0	60.0 60.0 60.0 -	89	34 51 8 26 43	0.28 .28 .30 .28 .28		27 28 29 30 30	60.0 60.0 60.0	89	37 53 10 27 43	0.27 .28 .28 .27 .28	5 4 3 2 1	5.2 4.2 3.1 2.1 1.0
90	3		90	0			0		90	0			30		90	0		0	0.0
t	а	<u>6ον</u>		b	$\frac{\Delta}{60'}$	a	ı	<u>6ο'</u> Δ	l	5	$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$	l)	$\frac{\Delta}{60'}$		α
ı		d='	73°	30′				d=7	4° ()′			à	l=74	۱° 3	0′			

b	1	,	a = 7	5°	0′,	¥ .,†		(a = 7	5° 3	80′	۸.			a = 7	6°	0′)	c	a
$B \setminus$	h	d	<u>6ο'</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	z	t	$\frac{\Delta}{60'}$	h,	d	<u>60′</u> Δ	Z	t	<u>Δ</u> 60'	$C \setminus$	β
0 1 2 3 4	0	0 16 31 47 2	3.75 4.00 3.75 4.00 3.75	75	0 0 1 1 2	0.00 .02 .00 .02	O	0 15 30 45 0	4.00 4.00 4.00 4.00 4.00	75	30 30 31 31 32	0.00	°O	0 15 29 44 58	4.00 4.29 4.00 4.29 4.00	76	0 0 0 1 2	0.00 .00 .02 .02	90 89 88 87 86	90.0 89.0 88.1 87.1 86.1
5 6 78 9	2	18 33 49 4 19	4.00 3.75 4.00 4.00 3.75		3 5 6 8 10	0.03 .02 .03 .03	2	15 30 45 0	4.00 4.00 4.00 4.00 4.00		33 34 36 38 40	0.02 .03 .03 .03	2	13 27 41 56 10	4.29 4.29 4.00 4.29 4.00		3 4 6 8 10	0.02 .03 .03 .03	85 84 83 82 81	85.2 84.2 83.2 82.3 81.3
10 11 12 13 14	3	35 50 5 20 35	4.00 4.00 4.00 4.00 4.00		13 16 19 22 25	0.05 .05 .05 .05	3	30 44 59 14 28	4.29 4.00 4.00 4.29 4.00		43 45 48 51 55	0.03 .05 .05 .07	3	25 39 53 7 21	4.29 4.29 4.29 4.29 4.29		12 15 18 21 24	0,05	80 79 78 77 76	80.3 79.3 78.4 77.4 76.4
15 16 17 18 19	4	50 5 20 35 50	4.00 4.00 4.00 4.00 4.00		29 33 38 42 47	0.07 .08 .07 .08	4	43 57 12 26 41	4.29 4.00 4.29 4.00 4.29	76	58 2 7 11 16	0.07 .08 .07 .08	.4	35 49 3 17 31	4.29 4.29 4.29 4.29 4.29		27 31 35 40 44	0.07 .07 .08 .07	75 74 73 72 71	75.5 74.5 73.5 72.5 71.6
20 21 22 23 24	6	5 19 34 48 3	4.29 4.00 4.29 4.00 4.29	76	52 57 3 9	0.08	5	55 9 23 37 51	4.29 4.29 4.29 4.29 4.62		20 25 31 37 43	0.08	5	45 59 12 26 39	4.29 4.62 4.29 4.62 4.62	77	49 54 59 4	0.08	70 69 68 67 66	70.6 69.6 68.6 67.7 66.7
25 26 27 28 29	7	17 31 45 59 13	4.29 4.29 4.29 4.29 4.62		21 27 34 41 48	0.10 .12 .12 .12	6	4 18 32 45 58	4.29 4.29 4.62 4.62 4.62	77	49 55 1 8 15	0.10 .10 .12 .12	6	52 5 18 31 44	4.62 4.62 4.62 4.62 4.62		16 22 28 35 42	0.10 .10 .12 .12	65 64 63 62 61	65.7 64.7 63.7 62.8 61.8
30 31 32 33 34	8	26 40 53 6 19	4.29 4.62 4.62 4.62 4.62	77	56 4 12 20 28	0.13 .13 .13 .13	<i>7</i> 8	11 24 37 50 3	4.62 4.62 4.62 4.62 4.62		22 30 38 46 54	0.13 .13 .13 .13	7	57 10 22 34 46	4.62 5.00 5.00 5.00 5.00	78	49 56 4 11	0,12 .13 .12 .13	60 59 58 57 56	60.8 59.8 58.8 57.8 56.9
35 36 37 38 39	9	32 45 58 10 22	4.62 4.62 5.00 5.00 5.00	78	37 46 55 4 14	0.15 .15 .15 .17	9	16 28 40 52 4	5.00 5.00 5.00 5.00 5.00	78	2 11 20 29 38	0.15 .15 .15 .15	8	58 10 22 34 46	5.00 5.00 5.00 5.00 5.45	79	27 36 44 53 2	0.15 .13 .15 .15	55 54 53 52 51	55.9 54.9 53.9 52.9 51.9
40 41 42 43 44	10	34 5.00 24 0.17 46 5.00 34 .17 58 5.00 44 .18 10 5.00 55 .17 22 5.45 79 5 .18 33 16					10	16 27 39 50 1	5.45 5.00 5.45 5.45 5.45	79	47 57 7 17 28	0.17 .17 .17 .18	9	57 8 19 30 41	5.45 5.45 5.45 5.45 6.00		11 21 30 40 50	0.17 .15 .17 .17	50 49 48 47 46	50.9 49.9 48.9 47.9 46.9
45		33			16			12			38		_	51	,	80	0	11	45 ===	45-9
t	0	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$	C	ı	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$. (a ·	60' <u>Δ</u>	1	b	$\frac{\Delta}{60'}$	0	a
L			d = 7	5° ()′				d = 7	5°	30′				d = 7	6° ()′ ,			

8	,	Ĭ	a = 7	5° (0′.			а	= 75	5° 3	0′ -				a = 7	6°	0′.	, ,	c	\ a
$B \setminus$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	Z	t	$\frac{\Delta}{60^{s}}$	$C \setminus$	β
45 46 47 48 49	11		5.45 5.45 5.45 6.00 6.00	7.9 80	16 27 39 50 2	0.18 .20 .18 .20	10	12 23 33 43 53	5.45 6.00 6.00 6.00 6.00	7.9 80	38 49 0 11 ,22	0.18 .18 .18 .18	9	51 1 11 21 31	6.00 6.00 6.00 6.00 6.00	80	0 10 21 32 43	0.17 .18 .18 .18	° 45 44 43 42 41	45.9 44.9 43.9 42.9 41.9
50 51 52 53 54	12	26 36 46 56	6.00 6.00 6.00 6.67 6.67	81	14 26 38 50 3	.20 .20 .20 .22 .22	11	3 13 23 32 41	6.00 6.67 6.67 6.67	81	34 45 57 9 21	0.18 .20 .20 .20 .22	11	41 50 59 8 17	6.67 6.67 6.67 6.67 6.67	81	54 5 16 28 40	0.18 .18 .20 .20	39 38 37 36	40.9 39.9 38.9 37.9 36.9
55 56 57 58 59		14 23 32 41 49	6.67 6.67 6.67 7.50 7.50	82	16 29 42 55 9	0.22 .22 .22 .23 .22	12	50 59 7 15 23	6.67 7.50 7.50 7.50 7.50	82	34 46 59 12 25	0.20 .22 .22 .22 .22		26 34 42 50 58	7.50 7.50 7.50 7.50 7.50	82	52 4 16 28 41	0.20 .20 .20 .22	35 34 33 32 31	35.9 34.9 33.9 32.8 31.8
60 61 62 63 64	13	57 5 13 20 27	7.5° 7.5° 8.57 8.57 8.57	83	22 36 50 4 18	0.23 .23 .23 .23 .23	13	31 39 46 53 0	7.5° 8.57 8.57 8.57 8.57 8.57	83	38 51 5 18 32	0.22 .23 .22 .23 .23	12	6 13 20 27 34	8.57 8.57 8.57 8.57 10.0.	83	54 7 20 33 46	0.22 .22 .22 .22 .22	30 29 28 27 26	30.8 29.8 28.8 27.8 26.7
65 66 67 68 69		34 41 47 53 59	8.57 10.0 10.0 10.0	84	32 47 1 16 31	0.25 .23 .25 .25 .25		7 13 19 25 31	10.0 10.0 10.0 10.0	84	46 0 14 28 42	0,23 .23 .23 .23 .25	13	40 46 52 58 3	10.0 10.0 10.0 12.0 12.0	84	59 12 26 40 54	0.22 .23 .23 .23	25 24 23 22 21	25.7 24.7 23.7 22.7 21.6
70 71 72 73 74	14	5 10 15 20 25	12.0 12.0 12.0 12.0 15.0	85	46 1 16 31 47	0.25 .25 .25 .27 .25		36 41 46 51 56	12.0 12.0 12.0 12.0 15.0	85	57 11 26 40 55	0.23 .25 .23 .25 .25	,	8 13 18 23 27	12.0 12.0 12.0 15.0	8 ₅	8 22 36 50 4	0.23 .23 .23 .23	20 19 18 17 16	20.6 19.6 18.6 17.5 16.5
75 76 77 78 79		29 33 37 40 43	15.0 15.0 20.0 20.0 20.0	86 87	2 17 33 49 4	0.25 .27 .27 .25 .27	14	0 4 7 10 13	15.0 20.0 20.0 20.0 20.0	86	10 25 40 55 10	0.25 .25 .25 .25		31 35 38 41 44	15.0 20.0 20.0 20.0 20.0	87	18 33 47 2 17	0.25 .23 .25 .25	15 14 13 12 11	15.5 14.4 13.4 12.4 11.4
80 81 82 83 84		46 49 51 53 55	20.0 30.0 30.0 30.0 30.0	88	20 36 52 8 24	0.27 .27 .27 .27 .27		16 19 21 23 25	20.0 30.0 30.0 30.0 30.0	88	26 41 56 12 27	0.25 .25 .27 .25 .25		47 50 52 54 56	20.0 30.0 30.0 30.0 60.0	88	31 46 1 15 30	0.25 .25 .23 .25 .25	10 9 8 7 6	10.3 9.3 8.3 7.2 6.2
85 86 87 88 89	15	57 60.0 40 0.27 58 60.0 56 .27 59 60.0 89 12 .27 0 — 28 .27 0 — 44 .27			27 28 29 30 30	60.0 60.0 60.0	89	42 58 13 29 44	0.27 .25 .27 .25 .27	14	57 58 59 0	60.0 60.0 	89	45 0 15 30 45	0.25 .25 .25 .25	5 4 3 2 1	5.2 4.1 3.1 2.1 1.0			
90		0		90	0			30		90	0			0		90	0		0	0.0
t	. ($a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $						ı	$\frac{60'}{\Delta}$	ŀ		$\frac{\Delta}{60'}$	a	ı	$\frac{60'}{\Delta}$	ľ)	$\frac{\Delta}{60'}$		a
0.	d=75° 0′							à	= 78	5° 3	0′			(d = 7	6° C)′ ,			-

\b		a	ı = 76	3° 3	0′				a = 7	7° (0′			C	i = 7	7° 3	0′		$\setminus c$	a
$B \setminus$	h	d	$\frac{60'}{\Delta}$	z	*	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	z	*	<u>Δ</u> 6ο'	h	$\frac{d}{}$	$\frac{60'}{\Delta}$	Z	*	<u>3</u>	$C \setminus$	3
0 I 2 3 4	0	0 14 28 42 56	4.29 4.29 4.29 4.29 4.29	76	30 30 30 31 32	0.00 .00 .02 .02	0	ó 14 27 41 54	4.29 4.62 4.29 4.62 4.62	77 [°]	, 0 0 0 1 2	0.00 .00 .02 .02	00	0 13 26 39 52	4.62 4.62 4.62 4.62 4.62 4.62	77 [°]	30 30 30 31 32	0.00 .00 .02 .02	90 89 88 87 86	90.0 89.0 88.1 87.1 86.1
5 6 78 9	2	10 24 38 52 6	4.29 4.29 4.29 4.29 4.62		33 34 36 38 40	0.02 .03 .03 .03	2	7 21 34 48 1	4.29 4.62 4.29 4.62 4.62		3 4 6 7 9	0.02 .03 .02 .03	I	5 31 44 56	4.62 4.62 4.62 5.00 4.62		33 34 35 37 39	0.02 .02 .03 .03	85 84 83 82 81	85.1 84.2 83.2 82.2 81.2
10 11 12 13 14	3	19 33 47 1	4.29 4.29 4.29 4.62 4.29		42 44 47 50 53	0.03 .05 .05 .05	3	14 28 41 54 7	4.29 4.62 4.62 4.62 4.62		11 14 16 19 22	0.05 .03 .05 .05	3	9 22 35 47 0	4.62 4.62 5.00 4.62 4.62		41 43 46 49 52	0.03 .05 .05 .05	80 79 78 77 76	80.3 79.3 78.3 77.3 76.3
15 16 17 18 19	4	28 42 55 8 22	4.29 4.62 4.62 4.29 4.62	77	57 0 4 8 13	0.05 .07 .07 .08	4	20 33 46 59 12	4.62 4.62 4.62 4.62 4.62		26 29 33 37 41	0.05 .07 .07 .07	4	13 25 38 50 2	5.00 4.62 5.00 5.00 4.62	78	55 58 2 6	0.05 .07 .07 .07	75 74 73 72 71	75·4 74·4 73·4 72·4 71·5
20 21 22 23 24	5	35 48 1 14 27	4.62 4.62 4.62 4.62 4.62		17 22 27 32 38	0.08	5	25 37 50 3 15	5.00 4.62 4.62 5.00 5.00	78	45 50 55 0 5	0.08 .08 .08	5	15 27 39 51 3	5.00 5.00 5.00 5.00 5.00		14 18 23 28 33	0.07 .08 .08 .08	70 69 68 67 66	70.5 69.5 68.5 67.5 66.5
25 26 27 28 29	6	40 53 5 18 30	4.62 5.00 4.62 5.00 5.00	78	44 50 56 2 8	0.10 .10 .10 .10	6	27 39 51 3 15	5.00 5.00 5.00 5.00 5.00		11 17 23 29 35	01,0	6	15 27 38 50 2	5.00 5.45 5.00 5.00 5.45	79	38 44 50 56 2	01.0	65 64 63 62 61	65.6 64.6 63.6 62.6 61.6
30 31 32 33 34	7	42 54 6 18 30	5.00 5.00 5.00 5.00 5.00		15 22 30 37 45	0.12 .13 .12 .13 .12	7	27 39 51 2 14	5.00 5.00 5.45 5.00 5.45	79	41 48 55 3	0.12 .12 .13 .12		13 24 35 46 57	5.45 5.45 5.45 5.45 5.45		8 14 21 28 35	0,10 .12 .12 .12	59 58 57 56	60.6 59.7 58.7 57.7 56.7
35 36 37 38 39	8	42 53 5 16 27	5.45 5.00 5.45 5.45 5.45	79	52 0 9 17 26	0.13 .15 .13 .15	8	25 36 47 58 8	5.45 5.45 5.45 6.00 5.45		17 25 33 41 50	0.13 .13 .13 .15	7	8 19 29 40 50	5.45 6.00 5.45 6.00 6.00	80	42 50 58 5	0.13 .13 .12 .13	55 54 53 52 51	55.7 54.7 53.7 52.7 51.7
40 41 42 43 44	9		5.45 6.00 5.45 6.00 6.00	80	35 44 53 2 12	0.15 .15 .15 .17		19 29 39 49 5 9	6.00 6.00 6.00 6.00	80	58 7 16 25 34	0.15 .15 .15		0 10 20 29 39	6.00 6.00 6.67 6.00 6.67		30 39 47 56	0.13 .15 .13 .15	50 49 48 47 46	50.7 49.7 48.7 47.7 46.7
45		30			22		9	9			43		_	48		81	5		45	45.7
$ _t$	a	ι	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		а	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a	$\frac{60'}{\Delta}$	1	b	$\frac{\Delta}{60'}$		a
		(l=70	6° 3	0′				d = 7	7 7 °	0′			(l = 7'	7° 3	0′			

\ b		a	ı = 76	3° 3	0′				a = 7	7° () [′]			a	a = 77	7° 3	0′		\ c	a
$B \setminus$	h	d	<u>6ο'</u> Δ	\overline{z}	*	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	Z	*	<u>Δ</u> 6ο'	h	d	6ο' Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
45 46 47 48 49	9 10	30 40 50	6.00 6.00 6.00 6.67 6.67	80°	22 32 42 52 3	0.17 .17 .17 .18	9	9 19 28 37 46	6.00 6.67 6.67 6.67 6.67	80 81	43 53 3 13 23	0.17 .17 .17 .17	8 9	48 57 6 15 24	6.67 6.67 6.67 6.67 6.67	81	5 15 24 34 43	0.17 .15 .17 .15	° 45 44 43 42 41	45.7 44.7 43.7 42.7 41.7
50 51 52 53 54		18 27 36 45 53	6.67 6.67 6.67 7.50 7.50		14 25 36 47 58	0.18 .18 .18	10	55 4 13 21 29	6.67 6.67 7.50 7.50 7.50	82	33 44 55 6	0.18 .18 .18 .18	10	33 41 49 57 5	7.50 7.50 7.50 7.50 7.50 7.50	82	53 3 14 24 35	0.17 .18 .17 .18	40 39 38 37 3 6	40.7 39.7 38.7 37.7 36.7
55 56 57 58 59	II	9 17 25 33	7.50 7.50 7.50 7.50 8.57	82	9 21 33 45 57	0.20 .20 .20 .20	11	37 45 53 0 7	7.5° 7.5° 8.57 8.57 8.57	83	28 39 50 1	0.18 .18 .18 .20		13 20 27 34 41	8.57 8.57 8.57 8.57 8.57	83	45 56 7 18 29	0.18 .18 .18	35 34 33 32 31	35·7 34·7 33·7 32·7 31·7
60 61 62 63 64	12	40 47 54 I 7	8.57 8.57 8.57 10.0	83	9 22 34 47 59	0.22 .20 .22 .20		14 21 28 34 40	8.57 8.57 10.0 10.0	84	25 37 49 1	0.20 .20 .20 .20	11	48 55 1 7 13	8.57 10.0 10.0 10.0	84	40 52 3 15 27	0.20 .18 .20 .20	30 29 28 27 26	30.6 29.6 28.6 27.6 26.6
65 66 67 68 69		13 19 25 30 35	10.0 10.0 12.0 12.0 12.0	84 85	12 25 38 52 5	0.22 .22 .23 .22	12	46 52 57 2 7	10.0 12.0 12.0 12.0 12.0	85	25 38 51 3	0.22 .22 .20 .22 .22		19 24 29 34 39	12.0 12.0 12.0 12.0 12.0	85	39 51 3 15 27	0.20 .20 .20 .20	25 24 23 22 21	25.6 24.6 23.5 22.5 21.5
70 71 72 73 74		40 45 50 54 58	12.0 12.0 15.0 15.0	86	18 32 45 59 13	0.23 .22 .23 .23 .23		12 17 21 25 29	12.0 15.0 15.0 15.0	86	29 42 55 8 22	0.22 .22 .22 .23 .22	12	44 49 53 57	12.0 15.0 15.0 15.0 20.0	86	40 52 5 17 30	0.20 .22 .20 .22 .22	20 19 18 17 16	20.5 19.5 18.4 17.4 16.4
75 76 77 78 79	13	2 6 9 12 15	15.0 20.0 20.0 20.0 20.0	87	27 41 55 9 23	0.23 .23 .23 .23 .23		33 37 40 43 46	15.0 20.0 20.0 20.0 30.0	87	35 48 2 15 29	0.22 .23 .22 .23 .22		4 7 10 13 16	20.0 20.0 20.0 20.0 30.0	87	43 56 9 22 35	0.22 .22 .22 .22 .22	15 14 13 12 11	15.4 14.4 13.3 12.3 11.3
80 81 82 83 84		18 20 22 24 26	30.0 30.0 30.0 30.0 60.0	88	37 51 5 19 34	0.23 .23 .23 .25 .23		48 50 52 54 56	30.0 30.0 30.0 60.0	88	42 56 10 23 37	0.23 .23 .22 .23 .23		18 20 22 24 26	30.0 30.0 30.0 60.0	88	48 I 14 27 40	0.22 .22 .22 .22 .23	9 8 7 6	10.3 9.2 8.2 7.2 6.2
85 86 87 88 89		27 60.0 48 0.23 28 60.0 29 12 .25 29 60.0 17 .23 30 — 31 .23 30 90 0		13	57 58 59 0	60.0 60.0 60.0	89	51 5 18 32 46	0.23 .22 .23 .23 .23		27 28 29 30 30	60.0 60.0 60.0	89	54 7 20 33 47	0.22 .22 .22 .23 .22	5 4 3 2 1	5.I 4.I 3.I 2.I 1.0			
90	_	30	60'	90		Δ	_	0	60'	90	0	Δ	_	30	60′	90	0	Δ	0	0.0
t	_ '	Δ 60						ι	Δ		b	60'		а —	Δ	1		60'		a
	d=76° 30′								d = 7	7° (0′			(l=7	7° 3	0′			

b		а	=7	8° 0)′			a	a = 78	3° 3	0′				a = 7	/9° ()′		c	a
$B \setminus$	h	d	60' Δ	\overline{z}	t	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	60' Δ	z	t	$\frac{\Delta}{60'}$	$C \setminus$	β
0 1 2 3 4	1 2 3	2 4 5 5 7 4	5.00 4.62 5.00 4.62 5.00	78	0 0 0 1 2	0.00 .00 .02 .02	0	0 12 24 36 48	5.00 5.00 5.00 5.00 5.00	78	30 30 30 31 32	0.00	0	0 11 23 34 46	5.45 5.00 5.45 5.00 5.45	79°	0 0 0 1 2	0.00 .00 .02 .02	90 89 88 87 86	90.0 89.0 88.0 87.1 86.1
5 6 78 9	3	5 5 7 5 9 4	4.62 5.00 5.00 4.62 5.00		3 4 5 7 9	.02 .03 .03 .03	I	0 12 24 35 47	5.00 5.00 5.45 5.00 5.00		33 34 35 37 38	0.02 .02 .03 .02	I	57 9 20 31 43	5.00 5.45 5.45 5.00 5.45		3 4 5 6 8	.02 .02 .02 .03	85 84 83 82 81	85.1 84.1 83.1 82.2 81.2
10 11 12 13 14	1 2 4	7 5 9 5 I 5	4.62 5.00 5.00 5.00		11 13 15 18 21	0.03 .03 .05 .05	2	59 11 23 34 46	5.00 5.00 5.45 5.00 5.00		40 42 45 47 50	0.03 .05 .03 .05	2	54 5 16 28 39	5.45 5.45 5.00 5.45 5.45		10 12 14 16 19	0.03 .03 .03 .05	80 79 78 77 76	80.2 79.2 78.2 77.3 76.3
15 16 17 18 19	2 4	17 5.00 27 .05 29 5.00 30 .07 41 5.00 34 .07 53 5.00 38 .07 4 5 5.00 42 0.07		3	58 9 21 32 43	5.45 5.00 5.45 5.45 5.00	79	53 56 59 3	0.05 .05 .07 .07	3	50 I I 2 23 34	5.45 5.45 5.45 5.45 5.45		22 25 28 31 35	0.05 .05 .05 .07	75 74 73 72 71	75-3 74-3 73-3 72-3 71-4			
20 21 22 23 24	4 1 2 4 5	7 5 8 5 0 5	5.00 5.45 5.00 5.45		42 46 51 56 1	0.07 .08 .08 .08	4	55 6 17 28 39	5.45 5.45 5.45 5.45 5.45		11 15 19 24 28	.07 .08 .07 .08	4	45 55 6 17 27	6.00 5.45 5.45 6.00 5.45		39 43 47 51 56	0.07 .07 .07 .08	70 69 68 67 66	70.4 69.4 68.4 67.4 66.4
25 26 27 28 29	5 1 2 3 4	4 5 5 5 5 5 5 5 5 5	5.45 5.45 5.45 5.45		6 11 16 22 28	0.08 .08 .10	5	50 I I2 22 33	5.45 5.45 6.00 5.45 6.00		33 38 43 49 54	0.08 .08 .10 .08	5	38 48 58 8 18	6.00 6.00 6.00 6.00	80	1 6 11 16 21	0.08 .08 .08 .08	65 64 63 62 61	65.4 64.5 63.5 62.5 61.5
30 31 32 33 34	6 2	9 5			34 40 47 54	0.10 .12 .12 .12	6	43 54 4 14 24	5.45 6.00 6.00 6.00 6.00	80	0 6 12 19 25	0.10 .10 .12 .10	6	28 38 48 58	6.00 6.00 6.00 6.00 6.67		27 33 39 45 51	01.0 01. 01. 01.	59 58 57 56	60.5 59.5 58.5 57.5 56.5
35 36 37 38 39	41 6.00 80 1 .12 51 6.00 8 0.12		.13	7	34 44 54 3	6.00 6.67 6.00 6.67	81	32 39 46 53 1	0,12 .12 .12 .13		17 27 36 45 54	6.00 6.67 6.67 6.67 6.67	81	57 4 11 18 25	0.12 .12 .12 .12	55 54 53 52 51	55.5 54.6 53.6 52.6 51.6			
40 41 42 43 44	41 6.00 45 0.13 51 6.67 53 .13 8 0 6.67 81 1 .15 9 6.67 10 .13 18 6.67 18 .15			22 31 40 49 58	6.67 6.67 6.67 6.67 7.50		8 16 24 32 40	0.13 .13 .13 .13	7	3 12 20 29 37	6.67 7.50 6.67 7.50 7.50	82	32 39 47 55 2	0.12 .13 .13 .12	50 49 48 47 46	50.6 49.6 48.6 47.6 46.6				
45	2	27 27 27 A						6			49		A	45).		10	1	45	45.6
t	а	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60'} \right $					a		<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	a	,	6ο' Δ	1	5	<u>Δ</u> 60'		a
		d=78° 0′						d	=78	3° 3	0′-				d = 7	9° (0′	-		

0.203

0.194

8			a=7	8° (oʻ			a	-78	3° 3	0′				a = 7	9°	0′		\ c	\ .
B	h	d	6ο' Δ	Z	t	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	z	*	<u>Δ</u> 60'	$C \setminus$	β
45 46 47 48 49	8	27 36 45 53 2	6.67 6.67 7.5° 6.67 7.5°	81	27 36 45 54 4	0.15 .15 .15 .17	8	6 15 23 31 39	6.67 7.5° 7.5° 7.5° 7.5°	81° 82	49 57 6 15 24	0,13 .15 .15 .15	°7 8	45 53 1 9	7.5° 7.5° 7.5° 7.5° 8.57	82	10 19 27 35 44	0.15 .13 .13 .15	45 44 43 42 41	45.6 44.6 43.6 42.6 41.6
50 51 52 53 54		10 18 26 34 41	7.5° 7.5° 7.5° 8.57 8.57		13 23 33 43 53	0.17 .17 .17 .17	9	47 55 3 10 17	7.50 7.50 8.57 8.57 8.57	83	33 42 51 1	0.15 .15 .17 .17	,	24 32 39 46 53	7.50 8.57 8.57 8.57 8.57	83	53 2 11 20 29	0.15 .15 .15 .15	40 39 38 37 36	40.6 39.6 38.6 37.6 36.6
55 56 57 58 59	10	48 55 2 9 16	8.57 8.57 8.57 8.57 8.57	83	3 13 24 34 45	0.17 .18 .17 .18		24 31 38 44 50	8.57 8.57 10.0 10.0	84	21 31 41 51	0.17 .17 .17 .17	9	0 6 13 19 25	10.0 8.57 10.0 10.0	84	38 48 57 7 17	0.17 .15 .17 .17	35 34 33 32 31	35·5 34·5 33·5 32·5 31·5
60 61 62 63 64		23 29 35 41 46	10.0 10.0 10.0 12.0 10.0	84	56 7 18 29 41	0.18 .18 .18 .20	10	56 2 8 14 19	10.0 10.0 10.0 12.0 12.0		11 22 33 43 54	0.18 .18 .17 .18		31 37 42 47 52	10.0 12.0 12.0 12.0 12.0	85	27 37 47 57 8	0.17 .17 .17 .18	30 29 28 27 26	30.5 29.5 28.5 27.5 26.5
65 66 67 68 69	11	52 57 2 7 12	12.0 12.0 12.0 12.0 15.0	85	52 4 15 27 39	0.20 .18 .20 .20		24 29 34 39 44	12.0 12.0 12.0 12.0 15.0	85	5 16 27 38 50	0.18 .18 .18 .20	10	57 2 7 11 15	12.0 12.0 15.0 15.0	86	18 29 39 50 1	0.18 .17 .18 .18	25 24 23 22 21	25.4 24.4 23.4 22.4 21.4
70 71 72 73 74		16 20 24 28 32	15.0 15.0 15.0 15.0 20.0	86	51 3 15 27 39	0.20 .20 .20 .20	11	48 52 56 0 3	15.0 15.0 15.0 20.0 20.0	86	1 13 24 36 47	0.20 .18 .20 .18		19 23 27 31 34	15.0 15.0 15.0 20.0 20.0		12 23 34 45 56	0.18 .18 .18 .18	20 19 18 17 16	20.4 19.4 18.3 17.3 16.3
75 76 77 78 79		35 38 41 44 47	20.0 20.0 20.0 20.0 30.0	87	51 3 16 28 41	0.20 .22 .20 .22 .20		6 9 12 15	20.0 20.0 20.0 30.0 30.0	87	59 11 23 35 47	0.20 .20 .20 .20		37 40 43 46 48	20.0 20.0 20.0 30.0 30.0	87	7 18 30 41 53	0.18 .20 .18 .20	15 14 13 12 11	15.3 14.3 13.3 12.2 11.2
80 81 82 83 84		49 51 53 55 56	30.0 30.0 30.0 60.0 60.0	88	53 6 18 31 44	0.22 .20 .22 .22 .20		19 21 23 25 26	30.0 30.0 30.0 60.0 60.0	88	59 11 23 35 47	0.20 .20 .20 .20		50 52 54 55 56	30.0 30.0 60.0 60.0 60.0	88	4 15 27 39 50	0.18 .20 .20 .18	10 9 8 7 6	10.2 9.2 8.2 7.1 6.1
85 86 87 88 89	12	57 58 59 0	60.0 60.0 60.0	89	56 9 22 34 47	0.22		27 28 29 30 30	60.0 60.0 60.0	89	59 11 23 35 48	0.20 .20 .20 .22 .22	11	57 58 59 0	60.0 60.0 60.0	89	2 13 25 37 48	0.18 .20 .20 .18	5 4 3 2 1	5.1 4.1 3.1 2.0 1.0
90	_	0		90	0		_	30		90	0			0		90	0		0	0.0
t	(ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	0	a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		а	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$		a
			d = 7	78°	0′				d = 7	8° 3	30′			,	d = 7	/9° (0′			

1			00.65		Ī	-					ī	-		_			i\	Ţ
\"		a=7	9° 30′				a = 8	0°	0′				a = 8	0° 3	30′		$\setminus c$	C
$B \setminus$	h d	<u>6ο'</u> Δ	Z	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	z	t	$\frac{\Delta}{60'}$	h	d	<u>60'</u> Δ	Z	t	$\frac{\Delta}{60'}$	$C \setminus$	3
0 I 2 3 4	0 0 11 22 33 44	5.45 5.45 5.45 5.45 5.45	79 30 30 30 31 31	0,00	0	0 10 21 31 42	6.00 5.45 6.00 5.45 6.00	8ô	0 0 0 1 1	0.00	0	0 10 20 30 40	6.00 6.00 6.00 6.00 6.00	80	30 30 30 31 31	0.00 .00 .02 .00	90 89 88 87 86	90.0 89.0 88.0 87.0 86.1
56 78 9	55 1 6 17 27 38	5.45 5.45 6.00 5.45 5.45	32 33 34 36 38	.02	I	52 13 23 33	6.00 5.45 6.00 6.00 5.45		3 4 6 7	0.02 .02 .03 .02 .03	I	50 59 9 19 29	6.67 6.00 6.00 6.00 6.00		32 33 34 35 37	0.02 .02 .02 .03 .02	85 84 83 82 81	85.1 84.1 83.1 82.1 81.1
10 11 12 13 14	49 2 0 10 21 32	5.45 6.00 5.45 5.45 6.00	39 41 43 46 48	0.03 .03 .05 .03	2	44 54 4 14 24	6.00 6.00 6.00 6.00		9 11 13 15	0.03 .03 .03 .03	2	39 48 58 8	6.67 6.00 6.00 6.67 6.00		38 40 42 44 46	0.03 .03 .03 .03	80 79 78 77 76	80.1 79.2 78.2 77.2 76.2
15 16 17 18 19	42 53 3 3 14 24	5.45 6.00 5.45 6.00 6.00	51 54 57 80 0	0.05 .05 .05 .05	3	34 44 54 4 14	6.00 6.00 6.00 6.00		20 23 26 29 32	0.05 .05 .05 .05	3	27 36 46 55 5	6.67 6.00 6.67 6.00 6.67	81	49 52 54 57 0	0.05 .03 .05 .05	75 74 73 72 71	75.2 74.2 73.2 72.3 71.3
20 21 22 23 24	34 45 55 4 5 15	5.45 6.00 6.00 6.00 6.00	7 11 15 19 23	0.07 .07 .07 .07	4	24 34 44 53 3	6.00 6.67 6.00 6.00		35 39 43 47 51	0.07 .07 .07 .07 .07		14 24 33 42 51	6.00 6.67 6.67 6.67 6.67		4 7 11 15	0.05 .07 .07 .07	70 69 68 67 66	70.3 69.3 68.3 67.3 66.3
25 26 27 28 29	25 35 45 55 5 4	6.00 6.00 6.00 6.67 6.00	28 33 37 42 47	0.08 .07 .08 .08		13 22 31 41 50	6.67 6.67 6.00 6.67 6.67	81	55 0 4 9 14	0.08 .07 .08 .08	4	0 9 18 27 36	6.67 6.67 6.67 6.67 7.50		23 27 31 36 40	0.07 .07 .08 .07	65 64 63 62 61	65.3 64.3 63.4 62.4 61.4
30 31 32 33 34	14 23 33 42 51	6.67 6.67 6.67 6.67	53 58 81 4 10 16	0.08	5	59 8 17 26 34	6.67 6.67 6.67 7.50 6.67		19 24 30 35 41	0.08	5	44 53 1 9 18	6.67 7.50 7.50 6.67 7.50	82	45 50 55 1 6	0.08 .08 .10 .08	60 59 58 57 56	60.4 59.4 58.4 57.4 56.4
35 36 37 38 39	6 0 9 18 27 35	6.67 6.67 6.67 7.50 6.67	22 28 35 41 48	0.10 .12 .10 .12	6	43 52 0 8 16	6.67 7.50 7.50 7.50 7.50 7.50	82	47 53 59 5	0.10 .10 .10 .12		26 34 42 50 58	7.5° 7.5° 7.5° 7.5° 8.57		12 17 23 29 35	0.08 .10 .10 .10	55 54 53 52 51	55-4 54-4 53-4 52-4 51-4
40 41 42 43 44	44 52 7 0 8 16	7.5° 7.5° 7.5° 7.5° 7.5°	82 ⁵⁵ 9 17 24	0.12 .12 .13 .12		24 32 40 48 56	7.5° 7.5° 7.5° 7.5° 8.57		18 25 32 39 46	0.12 .12 .12 .12	6	5 13 20 28 35	7.5° 8.57 7.5° 8.57 8.57	83	42 48 55 1 8	0.10 .12 .10 .12		50.4 49.4 48.4 47.4 46.4
45	24		32		7	3			54			42			15		45	45-4
	a	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	a		60' <u>∆</u>		b	Δ 60'	a	ı	<u>6ο'</u> Δ	ŀ		<u>Δ</u> 60'		a.
t	(d = 79	9° 30′			(d = 8	0° (0′			á	2=80)° 3	0′			

				.105									_							
b		a	-79	9° 3	0′				a=8	0° (0′			ı	a = 8	0° 3	0′		$\setminus c$	a
$B \setminus$	h	d	<u>6ο'</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	Z	*	<u>Δ</u> 60'	h	d	$\frac{60'}{\Delta}$	Z	*	$\frac{\Delta}{60'}$	$c \setminus$	β
45 46 47 48 49	7	24 32 40 47 54	7.5° 7.5° 8.57 8.57 8.57	82 83	32 40 48 56 4	0.13 .13 .13 .13	7	3 11 18 25 32	7.5° 8.57 8.57 8.57 8.57	82 83	54 1 9 16 24	0.12 .13 .12 .13	6 7	42 49 56 3 9	8.57 8.57 8.57 10.0 8.57	83°	1 5 22 29 37 44	0.12 .12 .13 .12	45 44 43 42 41	0 45.4 44.4 43.4 42.4 41.4
50 51 52 53 54	8	1 8 15 22 29	8.57 8.57 8.57 8.57 10.0		12 21 29 38 47	0.15 .13 .15 .15	8	39 45 52 58 4	10.0 8.57 10.0 10.0	84	32 40 48 5 7 5	0.13 .13 .15 .13		16 22 28 34 40	10.0 10.0 10.0 10.0	84	52 59 7 15 23	0.12 .13 .13 .13	40 39 38 37 36	40.4 39.4 38.4 37.4 36.4
55 56 57 58 59		35 41 47 53 59	10.0 10.0 10.0	84	56 5 14 23 33	0.15 .15 .15 .17		16 22 28 34	10.0 10.0 10.0 10.0		13 22 31 40 49	0.15 .15 .15 .15	8	46 52 58 3	IO.0 IO.0 I2.0 I2.0 I2.0	85	31 39 47 56 4	0.13 .13 .15 .13	35 34 33 32 31	35·4 34·4 33·4 32·4 31·4
60 61 62 63 64	9	5 11 16 21 26	10.0 12.0 12.0 12.0 12.0	85	42 52 I II 2I	0.17 .15 .17 .17		39 44 49 54 59	12.0 12.0 12.0 12.0 12.0	85	58 7 16 25 35	0.15 .15 .15 .17		13 18 23 28 32	12.0 12.0 12.0 15.0		13 22 30 39 48	0.15 .13 .15 .15	30 29 28 27 26	30.4 29.4 28.4 27.4 26.3
65 66 67 68 69		31 15.0 31 0.17 35 15.0 41 .17 39 15.0 86 2 .17 47 15.0 12 .17 51 15.0 22 0.18 55 15.0 33 1.7 59 20.0 43 .18		9	4 8 12 16 20	15.0 15.0 15.0 15.0	86	44 54 4 13 23	0.17 .17 .15 .17		36 40 44 48 52	15.0 15.0 15.0 15.0	86	57 6 15 25 34	0.15 .15 .17 .15	25 24 23 22 21	25.3 24.3 23.3 22.3 21.3			
70 71 72 73 74	10	51 55 59 2 5	15.0	87		.17		24 27 30 33 36	20.0 20.0 20.0 20.0 20.0	87	33 43 53 3 13	0.17 •17 •17 •17	9	56 59 2 5	20,0 20,0 20,0 20,0 20,0	87	43 53 2 12 22	0.17 .15 .17 .17	20 19 18 17 16	20.3 19.3 18.3 17.2 16.2
75 76 77 78 79		8 11 14 16 18	20.0 20.0 30.0 30.0 30.0		26 37 47 58	0.18 .18 .17 .18		39 42 45 47 49	20.0 20.0 30.0 30.0 30.0	88	23 33 44 54 4	0.17 .18 .17 .17		11 13 15 17	30.0 30.0 30.0 30.0	88	31 41 51 0	0.17 .17 .15 .17	15 14 13 12 11	15.2 14.2 13.2 12.2 11.2
80 81 82 83 84		18 30.0 58 .1 20 30.0 88 9 0.1 22 30.0 20 .1 24 60.0 31 .1 25 60.0 42 .1 26 60.0 53 .1		0.18 .18 .18 .18		51 53 54 55 56	30.0 60.0 60.0 60.0		25 36 46 57	0.17 .18 .17 .18		21 23 25 26 27	30.0 30.0 60.0 60.0 60.0	89	20 30 40 50	0.17 .17 .17 .17	9 8 7 6	9.1 8.1 7.1 6.1		
85 86 87 88 89		28 60.0 15 .2 29 60.0 27 .1 30 — 38 .1				0.18 .20 .18 .18	10	57 58 59 0	60.0 60.0 -	89	7 18 28 39 49	0.18 .17 .18 .17 .18		28 29 29 30 30	60.0 60.0		10 20 30 40 50	0.17 .17 .17 .17	5 4 3 2 1	5.1 4.1 3.0 2.0 1.0
90	_	30		90		<u> </u>	_	0	601	90		1 4		30	60'	90			0	0.0
$ _t$		a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a 	<u>60'</u> <u>∆</u>		b	$\frac{\Delta}{60'}$	Ĺ	a 	$\frac{60'}{\Delta}$	111	b	$\frac{\Delta}{60'}$		a
		(d = 7	9° 8	30′				d = 8	80°	0′			(d = 8	0° 3	80′			

\ b			a = 8	1° ()′			C	ı = 81	° 3	0′			(<i>a</i> = 8	2° ()′		\ c	\ a
$B \setminus$	h	d	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 60'	h	$\frac{d}{}$	60' ∆	Z	t	<u>∆</u> 60′	h	d	<u>6ο'</u> Δ	\overline{z}	*	<u>Δ</u> 60'	$C \setminus$	β
0 1 2 3 4	2	0 9 9 8 8	6.67 6.00 6.67 6.00 6.67	81	0 0 0 I I	0.00 .00 .02 .00	00	0 9 18 27 35	6.67 6.67 6.67 7.50 6.67	81	30 30 30 31 31	0.00 .00 .02 .00	00	0 8 17 25 33	7.50 6.67 7.50 7.50 6.67	82	0 0 0 1	0.00 .00 .02 .00	90 89 88 87 86	90.0 89.0 88.0 87.0 86.0
5 6 7 8 9	1 1	7 6 6 5 4	6.67 6.00 6.67 6.67 6.67		2 3 4 5 6	0.02 .02 .02 .02	I	44 53 2 11 20	6.67 6.67 6.67 6.67 7.50		32 33 34 35 36	0.02 .02 .02 .02	I	42 50 58 7 15	7.5° 7.5° 6.67 7.5° 7.5°		2 3 4 5 6	0.02 .02 .02 .02	85 84 83 82 81	85.1 84.1 83.1 82.1 81.1
10 11 12 13 14	2	3 3 2 1	6.00 6.67 6.67 6.67 6.67		8 10 12 14 16	0.03 .03 .03 .03	2	28 37 46 54 3	6.67 6.67 7.50 6.67 6.67		38 39 41 43 45	.03 .03 .03 .03		23 31 40 48 56	7.50 6.67 7.50 7.50 7.50		7 9 10 12 14	0.03 .02 .03 .03	80 79 78 77 76	80.1 79.1 78.1 77.1 76.1
15 16 17 18 19	3	9876	6.67 6.67 6.67 6.67 6.67		18 20 23 26 29	0.03 .05 .05 .05		12 20 29 37 46	7.50 6.67 7.50 6.67 7.50		47 49 52 55 57	0.03 .05 .05 .03	2	4 12 20 28 36	7.50 7.50 7.50 7.50 7.50 7.50		16 18 21 23 26	0.03 .05 .03 .05	75 74 73 72 71	75.2 74.2 73.2 72.2 71.2
20 21 22 23 24	3	4 3 2 2 3 0 9 9	6.67 6.67 7.50 6.67 7.50		32 35 39 42 46	0.05 .07 .05 .07	3	54 2 10 19 27	7.50 7.50 6.67 7.50 7.50	82	0 3 7 10 13	0.05 .07 .05 .05	3	44 52 59 7 15	7.5° 8.57 7.5° 7.5° 8.57		29 32 35 38 41	0.05 .05 .05 .05	70 69 68 67 66	70.2 69.2 68.2 67.2 66.2
25 26 27 28 29	4	5 3 21	6.67 6.67 7.50 7.50 7.50	82	50 54 58 2 7	.07 .07 .08 .08	4	35 43 51 59 7	7.5° 7.5° 7.5° 7.5° 8.57		17 21 25 29 33	0.07 .07 .07 .07		22 30 37 45 52	7.5° 8.57 7.5° 8.57 8.57	83	44 48 52 56 0	0.07 .07 .07 .07	65 64 63 62 61	65.2 64.2 63.3 62.3 61.3
30 31 32 33 34	3	29 15 15 1	7.5° 7.5° 7.5° 7.5° 7.5°		11 16 21 26 31	0.08 .08 .08 .08		14 22 30 37 45	7.5° 7.5° 8.57 7.5° 8.57		37 42 47 51 56	0.08 .08 .07 .08	4	59 7 14 21 28	7.5° 8.57 8.57 8.57 8.57		4 8 12 17 21	.07 .08 .07 .08	59 58 57 56	60.3 59.3 58.3 57.3 56.3
35 36 37 38 39	3	9 7 24 32	7.50 8.57 7.50 8.57 8.57		36 42 47 53 59	01.0	5	52 59 6 13 20	8.57 8.57 8.57 8.57 8.57	83	1 6 12 17 22	0.08 .10 .08 .08	5	35 42 48 55 2	8.57 10.0 8.57 8.57 10.0		26 31 36 41 46	0.08 .08 .08 .08	55 54 53 52 51	55·3 54·3 53·3 52·3 51·3
40 41 42 43 44	6	46 8.57 83 5 0.10 53 8.57 11 .10 6 0 8.57 17 .10 7 8.57 23 .12 14 8.57 30 .12			27 34 41 47 54	8.57 8.57 10.0 8.57 10.0		28 34 40 46 52	01.0		8 14 21 27 33	10.0 8.57 10.0 10.0	84	51 57 2 8 14	0.10	50 49 48 47 46	50.3 49.3 48.3 47.3 46.3			
45	-	21 37					6	0			58			39			20		45	45-3
	a	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60} \right $					0	ı	<u>6ο'</u> Δ		b	$\frac{\Delta}{60'}$	(a	$\frac{60'}{\Delta}$		b	$\frac{\Delta}{60'}$		a
t		d=81° 0′						(l = 8	1° 8	0'				d = 8	2° (0′			

\ b		a = 8	31° 0′			C	u = 81	l° 3	0′				a = 8	2° ()′		\ c	a
B	h	$\frac{60'}{\Delta}$	Z	$\frac{\Delta}{60'}$	h	d	<u>6ο′</u> Δ	Z	t	$\frac{\Delta}{60'}$	h	d	$\frac{60'}{\Delta}$	Z	t	$\frac{\Delta}{60'}$	cackslash	β
9 45 46 47 48 49	6 21 28 34 41 47	8.57 10.0	83 37 43 50 57 84 4	.12	6	0 6 12 18 24	10.0 10.0 10.0	83 84	58 4 11 17 24	0.10 .12 .10 .12	6	39 45 51 56 2	10.0 10.0 12.0 10.0	84	20 26 32 38 44	0.10	° 45 44 43 42 41	0 45·3 44·3 43·3 42·3 41·3
50 51 52 53 54	53 59 7 5 11 16	10.0 10.0 12.0	11 18 26 33 41	0.12 .13 .12 .13		30 36 41 47 52	10.0 12.0 10.0 12.0 12.0		31 38 45 52 59	0.12 .12 .12 .12		7 13 18 23 28	10.0 12.0 12.0 12.0 12.0	85	50 57 3 10 17	0.12 .10 .12 .12	40 39 38 37 36	40.3 39.3 38.3 37.3 36.3
55 56 57 58 59	22 27 32 · 37 42	12.0 12.0 12.0	49 56 85 4 12 20	0.12 .13 .13 .13	7	57 7 12 17	12.0 12.0 12.0 12.0 12.0	85	6 13 21 28 36	0.12 .13 .12 .13		33 38 42 47 51	12.0 15.0 12.0 15.0		23 30 37 44 52	0.12 .12 .12 .13	35 34 33 32 31	35·3 34·3 33·3 32·3 31·3
60 61 62 63 64	47 52 57 8 I	12.0 15.0 15.0	28 37 45 53 86 2	0.15 .13 .13 .15		22 26 30 34 38	15.0 15.0 15.0 15.0	86	44 51 59 7 15	0.12 .13 .13 .13	7	55 59 3 7	15.0 15.0 15.0 15.0	86	59 6 13 21 28	0.12 .12 .13 .12	30 29 28 27 26	30.3 29.3 28.3 27.3 26.3
65 66 67 68 69	9 13 17 21 24	15.0 15.0 20.0	10 19 28 36 45	0.15 .15 .13 .15		42 46 49 53 56	15.0 20.0 15.0 20.0 20.0		23 31 39 48 56	0.13 .13 .15 .13		15 19 22 25 28	15.0 20.0 20.0 20.0 20.0	87	36 44 51 59 7	0.13 .12 .13 .13	25 24 23 22 21	25.2 24.2 23.2 22.2 21.2
70 71 72 73 74	27 30 33 36 39	20.0	87 3 12 21 30	.15	8	59 5 8 10	20.0 20.0 20.0 30.0 20.0	87	4 13 21 30 38	0.15 .13 .15 .13		31 34 37 39 41	20.0 20.0 30.0 30.0 30.0		15 23 31 39 47	0.13 .13 .13 .13	20 19 18 17 16	20.2 19.2 18.2 17.2 16.2
75 76 77 78 79	42 44 46 48 50	30.0	39 48 58 7 16	1.15		13 15 17 19 21	30.0 30.0 30.0 60.0	88	47 56 4 13 22	0.15 .13 .15 .15	-	43 45 47 49 51	30.0 30.0 30.0 30.0 30.0	88	55 3 11 20 28	0.13 .13 .15 .13	15 14 13 12 11	15.2 14.2 13.1 12.1 11.1
80 81 82 83 84	54 55 56				22 24 25 26 27	30.0 60.0 60.0 60.0 60.0	89	31 40 48 57 6	0.15 .13 .15 .15		53 54 55 56 57	60.0 60.0 60.0 60.0	89	36 44 53 1	0.13 .15 .13 .15	10 9 8 7 6	10.1 9.1 8.1 7.1 6.1	
85 86 87 88 89	59 59	0 - 50 .17			28 29 29 30 30	60,0 60,0		15 24 33 42 51	0.15 .15 .15 .15	8	58 59 59 0	60.0 60.0 		18 26 35 43 52	0.13 .15 .13 .15	5 4 3 2 1	5.1 4.0 3.0 2.0 1.0	
90		 	90 0			30		90	0			0		90	0		0	0.0
t	а	$\frac{60'}{\Delta}$	b	$\frac{\Delta}{60'}$	0	ı	<u>60'</u> Δ		b	$\frac{\Delta}{60'}$	(ı	60' ▲		b	∆ 60′		a
L		d = 8	31° 0′			C	l = 8	1°3	0′				d=8	2° ()′			

b		C	a = 8	2° 3	30′				a = 8	3°	0′			(a = 83	3° 3	0′		c	•
$B \setminus$	h	d	$\frac{60'}{\Delta}$	Z	t	<u>Δ</u> 6ο'	h	d	<u>6ο'</u> Δ	z	*	$\frac{\Delta}{60'}$	h	$\frac{d}{d}$	$\frac{60'}{\Delta}$	Z	t	<u>Δ</u> 6ο'	$C \setminus$	β
0 1 2 3 4	0	0 8 16 24 31	7.50 7.50 7.50 8.57 7.50	82	30 30 30 31 31	0.00	°	0 7 15 22 29	8.57 7.50 8.57 8.57 7.50	83	0 0 0 1 1	0.00	°O	0 7 14 20 27	8.57 8.57 10.0 8.57 8.57	83	30 30 30 31 31	0.00 .00 .02 .00	90 89 88 87 86	90.0 89.0 88.0 87.0 86.0
5 6 78 9	I	39 47 55 3	7.5° 7.5° 7.5° 8.57 7.5°		32 32 33 34 35	0.00 .02 .02 .02	I	37 44 51 58 6	8.57 8.57 8.57 7.50 8.57		2 2 3 4 5	0.00 .02 .02 .02	I	34 41 47 54	8.57 10.0 8.57 8.57 8.57		31 32 33 34 35	0.02 .02 .02 .02	85 84 83 82 81	85.0 84.0 83.1 82.1 81.1
10 11 12 13 14		18 26 33 41 49	7.5° 8.57 7.5° 7.5° 8.57		37 38 40 41 43	.03 .02 .03 .03		13 20 27 34 41	8.57 8.57 8.57 8.57 8.57		6 8 9 11 12	0.03 .02 .03 .02		8 14 21 28 34	10.0 8.57 8.57 10.0 8.57		36 37 38 40 41	0.02 .02 .03 .02 .03	80 79 78 77 76	80.1 79.1 78.1 77.1 76.1
15 16 17 18 19	2	56 4 11 19 26	7.5° 8.57 7.5° 8.57 7.5°		45 47 49 52 54	0.03 .03 .05 .03	2	48 55 2 9 16	8.57 8.57 8.57 8.57 8.57 8.57		14 16 18 20 23	0.03 .03 .03 .05	2	41 47 54 0 7	10.0 8.57 10.0 8.57 10.0		43 45 47 49 51	0.03 .03 .03 .03	75 74 73 72 71	75.1 74.1 73.1 72.1 71.1
20 21 22 23 24	3	34 41 48 55	8.57 8.57 8.57 7.5° 8.57	83	5 .05 8 .07 12 0.05 15 .05 18 .07			23 30 37 44 50	8.57 8.57 8.57 10.0 8.57		25 28 30 33 36	0.05 .03 .05 .05		13 20 26 32 38	8.57 10.0 10.0 10.0 8.57	84	53 56 58 1	0.05 .03 .05 .03	70 69 68 67 66	70.1 69.1 68.1 67.2 66.2
25 26 27 28 29		10 17 24 31 38	8.57 8.57 8.57 8.57 8.57			.05	3	57 4 10 17 23	8.57 10.0 8.57 10.0 8.57		39 42 45 49 52	0.05 .05 .07 .05	3	45 51 57 3 9	10.0 10.0 10.0 10.0		6 9 12 15	0.05 .05 .05 .05	65 64 63 62 61	65.2 64.2 63.2 62.2 61.2
30 31 32 33 34	4	45 51 58 5	8.57 8.57 10.0 8.57		30 34 38 42 46	0.07 .07 .07 .07		30 36 42 48 54	10.0 10.0 10.0 10.0	84	56 0 3 7	0.07 .05 .07 .07		15 21 26 32 38	10.0 12.0 10.0 10.0		22 25 29 32 36	0.05 .07 .05 .07	60 59 58 57 56	60,2 59.2 58.2 57.2 56.2
35 36 37 38 39		18 24 30 37 43	10.0 10.0 8.57 10.0 10.0	46 .08 51 0.07 55 .08 84 0 .08 5 .07 9 .08		4	0 6 12 18 24	10.0 10.0 10.0 10.0		15 20 24 28 33	0.08 .07 .07 .08	4	43 49 54 0 5	10.0 12.0 10.0 12.0 12.0		40 44 48 52 56	0.07 .07 .07 .07	55 54 53 52 51	55.2 54.2 53.2 52.2 51.2	
40 41 42 43 44	5	49 55 1 6	5 10.0 19 .10 1 12.0 25 .08 6 10.0 30 .08 2 10.0 35 .10					30 35 41 46 52	12.0 10.0 12.0 10.0 12.0		38 42 47 52 57	0.07 .08 .08 .08		10 16 21 26 31		85	1 5 10 14 19	0.07 .08 .07 .08	50 49 48 47 46	50.2 49.2 48.2 47.2 46.2
45		18			41			57		85	2		_	36			24		45	45.2
+	a	$a \left \frac{60'}{\Delta} \right b \left \frac{\Delta}{60'} \right $						1	60' ▲		b	$\frac{\Delta}{60'}$	(ı	60' <u>∆</u>		b	$\frac{\Delta}{60'}$		a
t		d = 82° 30'							d = 8	3°	0′			C	<i>l</i> = 8	3° 3	0′			

c

a

B

0

45.2

44.2

43.2

42.2

41.2

40.2

39.2 38.2

37.2 36.2

35.2

34.2

33.2

32.2

31.2

30.2

29.2

28.2

27.2

26.2

25.2

24.2

23.2

22.2

2I.I

20. I

19.1

18.1

17.1

16.1

15.1

14.1

13.1

12.1

II.I

10. I

9.I 8.I

7.1

6.0

5.0

4.0

3.0

2.0

I.O

0.0

a.

5

4

Δ

60

b

601

Δ

 $d = 83^{\circ} 30'$

a

 $d = 83^{\circ} 0'$

601

Δ

 α

60

b

60'

604

Δ

 $d = 82^{\circ} 30'$

 α

t

h

	b			a = 8	4° (0′				a = 8	5° (0′				a = 8	6° (0′		\ c	\ a
E	3/	h	d	$\frac{60'}{\Delta}$	z	t	$\frac{\Delta}{60'}$	h	d	<u>6ο'</u> Δ	Z	*	$\frac{\Delta}{60'}$	h	$\frac{d}{d}$	<u>6ο′</u> Δ	Z	*	<u>∆</u> 60′	C	β
	o 0 1 2 3 4		ó 6 13 19 25	10.0 8.57 10.0 10.0	84	0 0 0 0	0.00	0	6 5 10 16 21	12.0 12.0 10.0 12.0 12.0	85	0 0 0 0	0.00	0	0 4 8 13	15.0 15.0 12.0 15.0	86	0 0 0 0	0.00	90 89 88 87 86	90.0 89.0 88.0 87.0 86.0
	56 78 9		31 38 44 50 56	8.57 10.0 10.0 10.0		1 2 3 3 4	.02 .02 .00 .02 .02		26 31 37 42 47	12.0 10.0 12.0 12.0 12.0		1 2 2 3 4	0.02 .00 .02 .02		21 25 29 33 38	15.0 15.0 15.0 12.0 15.0		I I 2 2 3	0.00 .02 .00 .02 .02	85 84 83 82 81	85.0 84.0 83.0 82.0 81.0
1	10 11 12 13 14		2 9 15 21 27	8.57 10.0 10.0 10.0		5 7 8 9	.02 .02 .03 .02	I	52 57 2 7	12.0 12.0 12.0 12.0 10.0		5 6 7 8 9	.02 .02 .02 .02		42 46 50 54 58	15.0 15.0 15.0 15.0		4 4 5 6 7	0.00 .02 .02 .02	80 79 78 77 76	80.0 79.0 78.0 77.0 76.1
1	15 16 17 18		33 39 45 51 57	10.0 10.0 10.0 10.0		12 14 16 18 20	0.03 .03 .03 .03		18 23 28 33 38	12.0 12.0 12.0 12.0 12.0		10 12 13 15	0.03 .02 .03 .02	1	2 6 10 14 18	15.0 15.0 15.0 15.0		8 9 10 12 13	0.02 .02 .03 .02	75 74 73 72 71	75.1 74.1 73.1 72.1 71.1
2 2 2	21 22 23 24		3 9 1 5 20 26	10.0 10.0 12.0 10.0		22 24 26 28 31	0.03 .03 .03 .05	2	43 48 52 57 2	12.0 15.0 12.0 12.0 12.0		18 20 22 24 26	0.03 .03 .03 .03		22 26 30 34 38	15.0 15.0 15.0 15.0 20.0		14 16 17 19 21	0.03 .02 .03 .03	70 69 68 67 66	70.1 69.1 68.1 67.1 66.1
2 2 2	25 26 27 28 29		32 38 43 49 54	10.0 12.0 10.0 12.0 10.0		34 36 39 42 45	0.03 .05 .05 .05		7 11 16 21 25	15.0 12.0 12.0 15.0 12.0		28 30 33 35 37	0.03 .05 .03 .03		41 45 49 53 56	15.0 15.0 15.0 20.0 15.0		22 24 26 28 30	0.03 .03 .03 .03	65 64 63 62 61	65.1 64.1 63.1 62.1 61.1
63,63,63	30 31 32 33 34		0 5 11 16 21	12.0 10.0 12.0 12.0 12.0	85	48 51 54 58 1	0.05 .05 .07 .05		30 35 39 43 48	12.0 15.0 15.0 12.0 15.0		40 43 45 48 51	0.05 .03 .05 .05	2	0 4 7 11	15.0 20.0 15.0 20.0 15.0		32 34 3 6 39 41	0.03 .03 .05 .03	60 59 58 57 56	60.1 59.1 58.1 57.1 56.1
30303	35 36 37 38 39		26 31 36 41 46	12.0 12.0 12.0 12.0 12.0		5 8 12 16 20	0.05 .07 .07 .07	3	52 56 0 5	15.0 15.0 12.0 15.0 15.0	86	54 57 0 3 7	.05 .05 .05 .07		18 21 24 28 31	20.0 20.0 15.0 20.0 20.0		43 46 48 51 53	0.05 .03 .05 .03	55 54 53 52 51	55.1 54.1 53.1 52.1 51.1
4 4	40 11 12 13 14	4	51 56 1 5	12.0 12.0 15.0 12.0		24 28 32 36 41	0.07 .07 .07 .08		13 17 21 25 28	15.0 15.0 15.0 20.0 15.0		10 13 17 20 24	0.05 .07 .05 .07		34 37 41 44 47	20.0 15.0 20.0 20.0 20.0	87	56 59 2 4 7	0.05 .05 .03 .05	50 49 48 47 46	50.1 49.1 48.1 47.1 46.1
4	45 —		14			45			32			28			50			10	•	45	45.1
	t	а		6ο' Δ	t)	<u>Δ</u> 6ο'	(ı	<u>60'</u> Δ	t	,	<u>Δ</u> 6ο'	a	ı	<u>60'</u> Δ		b	<u>∆</u> 60′		a
				d = 8	4° (0′				d = 8	5° ()′				d = 8	6° ()′			

1	ь			a=8	4° ()′				a = 8	5°	0′				a = 8	6°	0′		c	a
B	/	h	$\frac{d}{}$	<u>6ο'</u> Δ	Z	t	<u>Δ</u> 6ο'	h	d	60' <u>A</u>	\overline{z}	*	<u>Δ</u> 6ο'	h	d	<u>6ο′</u> Δ	Z	t	∆/60'	$C \setminus$	β
4 4 4 4 4	5 6 78 9	4		12.0 15.0 15.0 15.0	85 86	45 49 54 59 3	0.07 .08 .08 .07	3	32 36 39 43 46	15.0 20.0 15.0 20.0 15.0	86	28 31 35 39 43	0.05 .07 .07 .07	3	50 53 55 58 I	20.0 30.0 20.0 20.0 20.0	87	10 13 16 19 22	0.05 .05 .05 .05	° 45 44 43 42 41	45.1 44.1 43.1 42.1 41.1
5 5 5 5 5 5	I 2 3		35 39 43 47 51	15.0 15.0 15.0 15.0		8 13 18 23 28	0.08 .08 .08 .08	4	50 53 56 59 2	20.0 20.0 20.0 20.0 20.0	87	47 51 55 59 3	0.07 .07 .07 .07 .08		4 7 9 12 14	20.0 30.0 20.0 30.0 20.0		26 29 32 35 39	0.05 .05 .05 .07	40 39 38 37 36	40.1 39.1 38.1 37.1 36.1
5 5 5 5 5 5	6 7 8	5	55 58 2 58	20.0 15.0 20.0 20.0 20.0		33 38 43 49 54	0.08		5 8 11 14 17	20.0 20.0 20.0 20.0 20.0		8 12 16 21 25	0.07 .07 .08 .07 .08		17 19 21 24 26	30.0 30.0 20.0 30.0 30.0		42 46 49 53 56	0.07 .05 .07 .05	35 34 33 32 31	35.1 34.1 33.1 32.1 31.1
6 6 6 6 6	I 2 3		11 14 17 20 23	20.0 20.0 20.0 20.0 20.0	87	0 5 11 16 22	0.08 .10 .08 .10		20 22 25 27 30	30.0 20.0 30.0 20.0 30.0		30 34 39 44 48	0.07 .08 .08 .07		28 30 32 34 36	30.0 30.0 30.0 30.0 30.0	88	0 3 7 11 15	0.05 .07 .07 .07	30 29 28 27 26	30.1 29.1 28.1 27.1 26.1
6 6 6 6 6	6 7 8		26 29 31 34 36	20.0 30.0 20.0 30.0 30.0		27 33 39 45 51	0.10		32 34 36 38 40	30.0 30.0 30.0 30.0 30.0	88	53 58 3 7	0.08 .08 .07 .08		38 39 41 42 44	60.0 30.0 60.0 30.0 30.0		18 22 26 30 34	0.07 .07 .07 .07	25 24 23 22 21	25.1 24.1 23.1 22.1 21.1
777	2		38 40 42 44 46	30.0 30.0 30.0 30.0 30.0	88	56 2 8 14 20	0.10 .10 .10 .10		42 44 45 47 49	30.0 60.0 30.0 30.0 60.0		17 22 27 32 37	0.08 .08 .08 .08		46 47 48 50 51	60.0 60.0 30.0 60.0 60.0		38 42 46 50 54	0.07 .07 .07 .07	20 19 18 17 16	20.1 19.1 18.1 17.1 16.1
77	5 6 78 9		48 49 51 52 53	60.0 30.0 60.0 60.0 6 0.0		27 33 39 45 51	0.10		50 51 52 53 54	60.0 60.0 60.0 60.0	89	42 47 52 57 3	0.08 .08 .08		52 53 54 55 56	60.0 60.0 60.0 60.0	89	58 2 6 10 14	0.07 •07 •07 •07	15 14 13 12 11	15.1 14.1 13.0 12.0 11.0
8 8 8	1 2 3 4		54 55 56 57 58	60.0 60.0 60.0 60.0	89	57 3 10 16 22	0,10 .12 .10 .10		55 56 57 58 58	60.0 60.0 60.0		8 13 18 23 29	0.08 .08 .08		56 57 58 58 59	60.0 60.0 — 60.0		18 22 27 31 35	0.07 .08 .07 .07	10 9 8 7 6	10.0 9.0 8.0 7.0 6.0
8 8	56789	6	59 59 0 0	60.0		29 35 41 47 54	0,10 .10 .10 .12	5	59 59 0 0	60.0 —		34 39 44 50 55	0.08 .08 .10 .08	4	59 59 0 0	 60.0 		39 43 47 52 56	0.07 .07 .08 .07	5 4 3 2 1	5.0 4.0 3.0 2.0 1.0
9	0	_	0		90	0		_	0		90	0			0		90	0		0	0.0
	t		а	60' <u>A</u>	1	b	<u>Δ</u> 6ο'	,	a	<u>6ο′</u> Δ		b	$\frac{\Delta}{60'}$	а	ı	$\frac{60'}{\Delta}$	1	b	<u>Δ</u> 6ο'		a
'				d = 8	4° (0′				d = 8	5°	0′				d = 8	86°	0′			

a=89° 0' h Z 0 '89 0 1 2 0 3 0 4 0 5 0 7 0 10 11 13 14 15 2 16 2 17 2 18 3 19 20 4 4 22 4 23 55		90 888 887 886 885 884 883 881 80 778 777 70 698 686 667 666
89 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Z	90 889 887 86 85 884 882 881 80 79 77 77 77 77 77 77 77 77 77 77 77 77
1 2 0 0 0 3 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		85 84 83 81 80 79 78 77 76 75 74 73 77 70 69 68
2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		85 84 83 81 80 79 78 77 76 75 74 73 77 70 69 68
5 0 6 0 7 8 1 9 1 10 1 11 1 13 1 14 2 15 2 16 2 17 18 3 19 3		85 84 83 81 80 79 78 77 76 75 74 73 77 70 69 68
9 I 10 I 11 I 13 I 14 2 15 2 16 2 17 2 18 3 19 3 20 4		81 80 79 78 77 76 75 74 73 72 71 70 69 68
9 I 10 I 11 I 13 I 14 2 15 2 16 2 17 2 18 3 19 3 20 4		81 80 79 78 77 76 75 74 73 72 71 70 69 68
11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		79 78 77 76 75 74 73 72 71 70 69 68
15 2 16 2 17 2 18 3 19 3 20 4		75 74 73 72 71 70 69 68
17 2 18 3 19 3 20 4		74 73 72 71 70 69 68
19 20 4		71 70 69 68
21 4 22 4 22 4	0 0 0 0 0 0	70 69 68
22 4	0 0	68
23 5 24 5	0 0	66
25 6 26 6	0 0	65
27 7 28 7	0 0	63
30 8	0 0	61 60
31 9 32 9 33 10	0 0 0 0	59 58
34 10	0 0	57 56
35 II 36 I2	0 0	55 54 53
37 38 14	0 0	53 52 51
39 14 39 15	0 0	50 49 48
41 16 42 17	0 0	40 47 46
43 18	0 0	45
	a b	
a b		
	39 14 39 15 40 15 41 16 42 17 43 18	39

Change of Altitude per Minute of Arc of Hour Angle.

$$d \text{ and } L \text{ same name} \begin{cases} L < b : \frac{\Delta h}{\Delta t} = -; \frac{\Delta_1 Z}{\Delta t} = -\\ L > b : ,, = -; ,, = + \end{cases} \qquad \frac{\Delta h}{\Delta t} = \mp \cos L \sin Z'$$

$$d \text{ and } L \text{ contrary names} \ldots \ldots ,, = +; ,, = +$$

$$d \text{ and } L \text{ contrary names} \ldots \ldots ,, = -; ,, = +$$

L	$\frac{\mathbf{o}^{\circ}}{\sin Z'}$	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60 °	65°	70°	L/Z'
0° 2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	00.00	0.00	0° 2
4 6 8	.07	.07	.07	.07	.07	.06	.06	.06	.05	.05	.04	.04	.03	.03	.02	4 6 8
10 12 14	0.17	0.17	0.17	0.17 .20	0.16	0.16	0.15	0.14 .17	0.13 .16	0.12	0.11	0.10 .12	0.09	0.07 .09	0.06 .07 .08	10 12 14
14 16 18	.28	.27 .31	.30	.30	.26 .29	.25	.24	.23	.21	.19	.18	.16	.14	.12	.09	16 18
20 22 24 26 28	0.34 .37 .41 .44 .47	0.34 .37 .41 .44 .47	•.34 •37 •40 •43 •46	0.33 .36 .39 .42 .45	0.32 ·35 ·38 ·41 ·44	•34 •37 •40 •43	0.30 .32 .35 .38 .41	0.28 .31 .33 .36 .38	0.26 .29 .31 .34 .36	.27 .29 .31	0.22 .24 .26 .28	0.20 .21 .23 .25	0.17 .19 .20 .22	0.14 .16 .17 .19	0.12 .13 .14 .15	20 22 24 26 28
30 32 34 36 38	0.50 •53 •56 •59 •62	•.50 •53 •56 •59 •61	0.49 .52 .55 .58 .61	0.48 .51 .54 .57	0.47 .50 .53 .55 .58	0.45 .48 .51 .53	0.43 .46 .48 .51	0.41 •43 •46 •48	0.38 .41 .43 .45	0.35 .37 .40 .42 .44	0.32 •34 •36 •38 •40	0.29 .30 .32 .34	0.25 .27 .28 .29	0.21 .22 .24 .25 .26	0.17 .18 .19 .20	30 32 34 36 38
40 42 44 46 48	0.64 .67 .69 .72 .74	0.64 .67 .69 .72 .74	0.63 .66 .68 .71 .73	0.62 .65 .67 .69	0.60 .63 .65 .68	0.58 .61 .63 .65	0.56 .58 .60 .62 .64	• 53 • 55 • 57 • 59 • 61	0.49 .51 .53 .55	0.45 •47 •49 •51 •53	0.41 •43 •45 •46 •48	0.37 .38 .40 .41	0.32 •33 •35 •36 •37	0.27 .28 .29 .30	0.22 .23 .24 .25	40 42 44 46 48
50 52 54 56 58	°-77 •79 •81 •83 •85	0.76 .78 .81 .83	0.75 .78 .80 .82 .83	0.74 .76 .78 .80	0.72 •74 •76 •78 •80	0.69 •71 •73 •75 •77	0.66 .68 .70 .72 .73	0.63 .65 .66 .68	0.59 .60 .62 .64 .65	0.54 .56 .57 .59 .60	0.49 .51 .52 .53	•.44 •45 •46 •48 •49	0.38 .39 .40 .41	0.32 •33 •34 •35 •36	0.26 .27 .28 .28	50 52 54 56 58
60 62 64 66 68	0.87 .88 .90 .91 .93	0.86 .88 .90 .91	0.85 .87 .89 .90	0.84 .85 .87 .88	0.81 .83 .84 .86 .87	0.78 .80 .81 .83 .84	••75 •76 •78 •79 •80	0.71 .72 .74 .75 .76	0.66 .68 .69 .70	0.61 .62 .64 .65	0.56 •57 •58 •59 •60	0.50 .51 .52 .52 .53	•.43 •44 •45 •46	••37 •37 •38 •39 •39	0.30 .30 .31 .31	60 62 64 66 68
70 72 74 76 78	.94 .95 .96 .97	••94 •95 •96 •97 •97	0.93 •94 •95 •96	0.91 .92 .93 .94 .94	0.88 .89 .90 .91	0.85 .86 .87 .88	0.81 .82 .83 .84 .85	°.77 •78 •79 •79 •8°	0.72 •73 •74 •74 •75	0.66 .67 .68 .69	0.60 .61 .62 .62 .63	•.54 •55 •55 •56 •56	0.47 .48 .48 .49 .49	0.40 .40 .41 .41	•33 •33 •33 •33	70 72 74 76 78
80 82 84 86 88	0.98 •99 •99 1.00	0.98 •99 •99 •99	0.97 .98 .98 .98	0.95 .96 .96 .96	0.93 •93 •94 •94	0.89 .90 .90 .90	0.85 .86 .86 .86	0.81 .81 .81 .82 .82	0.75 .76 .76 .76 .77	0.70 .70 .70 .71	0.63 .64 .64 .64	0.56 •57 •57 •57 •57	0.49 .50 .50 .50	0.42 .42 .42 .42 .42	0.34 .34 .34 .34 .34	80 82 84 86 88
90	1.00	1.00	0.98	0.97	0.94	0.91	0.87	0.82	o. 7 7	0.71	0.64	0.57	0.50	0.42	0.34	90

To find $\frac{\Delta_1 Z}{\Delta t}$ or sin L, enter column $L = 0^\circ$ with L instead of Z'.

Change of Hour Angle per Minute of Arc of Altitude

 $\frac{\Delta t}{\Delta h} = \sec L \csc Z$

L	60°	62°	64°	66°	68°	70°	72°	74°	76°	78°	80°	82°	84°	87°	90°	Z_L
0 2 4 6 8	1.16	I.I3 I.I4 I.I4	I.II I.I2 I.I2	1.09 1.09 1.10 1.10	1.08 1.08	1.06	1.05 1.05 1.06	1.04 1.04 1.05	1.03 1.03 1.04	I.02 I.02 I.03	I.02 I.02 I.02	1.01 1.01 1.01	1.01 1.01 1.01	1.00	1.00	4 6
10 11 12 13 14	1.18	1.15	I.14 I.14	1.11 1.12 1.12	I.10 I.10 I.11	1.09	1.07	1.06	1.05 1.05 1.06	1.04 1.04 1.05	1.04 1.04	1.03 1.03 1.04	1.03	1.02	1.02 1.02 1.03	12
15 16 17 18 19	I.20 I.21 I.21 I.22	1.18	1.16	1.14	1.12	I.II I.II I.I2	I.10 I.11	1.08	1.07 1.08 1.08	1.06 1.07 1.07	1.06	1.05 1.06 1.06	1.05 1.05 1.06	1.04 1.05 1.05	1.05	18
20 21 22 23 24	1.23 1.24 1.24 1.25 1.26	1.21 1.22 1.23 1.24	I.2I I.22	1.17 1.18 1.19 1.20	1.16 1.17 1.18	1.14 1.15 1.16 1.17	1.13 1.13 1.14 1.15	1.11 1.12 1.13 1.14	I.IO I.II I.I2 I.I3	1.09 1.09 1.10 1.11 1.12	1.09	1.08	1.08	1.07 1.08 1.09	1.08	21 22 23 24
25 26 27 28 29	1.27 1.28 1.30 1.31 1.32	1.28	1.25 1.26 1.27	1.24	I.22 I.23	1.18	1.17 1.18 1.19 1.20	1.16	1.15 1.16 1.17	· 1	1.14	I.11 I.12 I.13 I.14 I.15	1.12 1.13 1.14		1.13	25 26 27 28 29
30 31 32 33 34	1.33 1.35 1.36 1.38 1.39	1.34 1.35 1.37	1.31 1.33 1.34	1.31	1.24 1.26 1.27 1.29 1.30	1.23 1.24 1.26 1.27 1.28	I.24 I.25 I.27	1.23 1.24 1.26	I.22 I.23 I.24	1.19 1.21 1.22 1.23	I.20 I.21 I.22	I.19 I.20 I.22	I.17 I.19 I.20 I.21		1.18	30 31 32 33 34
35 36 37 38 39	1.41 1.43 1.45 1.47 1.49	1.40 1.42 1.44 1.46	1.38 1.39 1.41	1.35 1.37 1.39	1.35 1.37 1.39	1.31 1.33 1.35 1.37	1.30 1.32 1.33 1.35	1.29 1.30 1.32 1.34	1.27 1.29 1.31 1.33	I.25 I.26 I.28 I.30 I.32	1.25 1.27 1.29	1.25	1.24 1.26 1.28	1.25	1.24 1.25 1.27	35 36 37 38 39
40 41 42 43 44	1.51 1.53 1.55 1.58 1.60	1.50 1.52 1.55 1.57	1.50 1.52	I.45 I.47 I.50	I.43 I.45	1.39 1.41 1.43 1.46 1.48	1.39 1.41 1.44	1.40	1.37 1.39 1.41	1.36 1.38 1.40	1.35 1.37 1.39	1.34 1.36 1.38		1.33 1.35 1.37	I.31 I.32 I.35 I.37 I.39	40 41 42 43 44
45 46 47 48 49	1.69 1.73 1.76	1.66 1.69 1.73	1.63 1.66 1.70	1.58 1.61 1.64 1.67	1.55 1.58 1.61 1.64	1.59	I.51 I.54 I.57 I.60	1.50 1.53 1.56 1.59	1.51 1.54 1.57	1.56	1.49 1.52 1.55	1.48 1.51 1.54	1.47 1.50 1.53	I.44 I.47 I.50 I.53	1.47 1.49 1.52	45 46 47 48 49
50 51 52 53 54	1.84 1.88 1.92 1.96	1.80 1.84 1.88 1.93	1.77 1.81 1.85 1.89		1.71 1.75 1.79 1.83	1.69 1.73 1.77 1.81	1.67 1.71 1.75 1.79	1.65 1.69 1.73 1.77	1.64 1.67 1.71 1.75	1.63 1.66 1.70 1.74	1.61 1.65 1.69 1.73	1.60 1.64 1.68 1.72	1.60 1.63 1.67 1.71	1.59 1.63 1.66	1.59 1.62 1.66 1.70	50 51 52 53 54
55 56 57 58 59 60	2.06 2.12 2.18 2.24	2.03 2.08 2.14 2.20	1.99 2.04 2.10 2.16	1.91 1.96 2.01 2.07 2.13	1.93 1.98 2.04 2.10	2.01	1.88 1.93 1.98 2.04	1.86 1.91 1.96 2.02	1.84 1.89 1.94 2.00	1.83 1.88 1.93 1.99	1.82 1.86 1.92 1.97	1.81 1.85 1.91 1.96	1.90	1.79 1.84 1.89 1.94	1.79 1.84 1.89 1.94	55 56 57 58 59 60
	2.31	2.2/	2.23	2.19		2.13	2.10	2.00	2.00	2.05	2.03	2.02	2.01	2.00	2.50	

Change of Azimuth per Minute of Arc of Altitude.

 $\frac{\Delta_2 Z}{\Delta h} = -\tan h' \cot Z'$ (-always with Z' less than 90°).

Z'	o°	5°									1					
$h' \setminus$		5	10°	15°	20°	25°	30°	35°	40°	45°	50°	60°	70°	80°	90°	Z'
0° 2	ind.	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	90°
4 6	∞	.80	•40	.26	.19	.15	.12	.10	.08	.07	.06	.04	.03	.01	.00	86
8	8 8	1.20	.80	•39 •52	• 3 9	.30	.18	.15	.13	.11	.09	.08	.04	.02	.00	84 82
10 12	8 8	2.02	1.00	o.66	0.48 .58	0.38 .46	0.31 •37	0.25 .30	0.21	0.18	0.15	0.10	o.o6 .o8	0.03 .04	0.00	80 78
14 16	∞	2.85	1.41	•93 1.07	.69	.61	•43	.36	.30	.25	.21	.14	.09	.04	.00	76
18	8 8	3.20	1.63 1.84	1.21	•79 •89	.70	.50 .56	.41 .46	•34	.32	.27	.19	.12	.06	.00	74 72
20 22	∞	4.16	2.06	1.36	1.00	°.78 .87	0.63	0.52 .58	0.43 .48	0.36	0.31	0.2I .23	0.13	0.06	0.00	70 68
24	8 8	5.09	2.29	1.51	1.22	.95	•7°	.64	•53	•45	•34 •37	.26	.16	.08	.00	66
26 28	8	5.57 6.08	2.77 3.02	1.82	1.34 1.46	1.05	.84	.7° .76	.58 .63	•49 •53	.41 .45	.28	.18	.09	.00	64 62
30	8	6.60	3.27	2.15	1.59	1.24	1.00	0.82	0.69	0.58	0.48	0.33	0.21	0.10	0,00	60
32 34	8 8	7.14	3.54 3.83	2.33	1.72	1.34 1.45	1.08	.89 .96	•74 .80	.67	•52 •57	.36	.23	.11	.00	58 56
36 38	8 8	8.30 8.93	4.12 4.43	2.71	2.00	1.56	1.26	1.04	.87	•73 •78	.61 .66	.42 .45	.26	.13	.co	54 52
40	8	9.59	4.76	3.13	2.31	1.80	1.45	1.20	1.00	0.84	0.70	0.48	0.31	0.15	0.00	50
42	8 8	10.29	5.11 5.48	3.36 3.60	2.47	1.93	1.56	1.29	1.07	.90	.76 .81	•52 •56	•33 •35	.16	.00	48
44 46	8	11.84	5.87	3.86	2.85	2.22	1.79	1.48	1.23	1.04	.87	.60	.38	.18	.co	44
48	8	12.69	6.30	4.14	3.05	2.38	1.92	1.59	1.32	1.11	•93	.64 0.69	.40	.20	.00	42
50 52	8 8	13.62	6.76 7.26	4.45 4.78	3.27 3.52	2.56 2.74	2.06 2.22	1.70	1.42	1.19	1.00	•74	•43 •47	.23	0.00	40 38
54 56	∞	15.73	7.81	5.14	3.78	2.95	2.38	1.97	1.64	1.38	I.15 I.24	.86	.50	.24	.00	36
50 58	8 8	16.95	8.41 9.08	5·53 5·97	4.4°	3.18 3.43	2.57 2.77	2.12	1.77	1.60	1.34	.92	•54 •58	.28	.00	34 32
60	00	19.80	9.82	6.46 7.02	4.76	3.71 4.03	3.00 3.26	2.47	2.06 2.24	1.73 1.88	1.45 1.58	1.00	0.63 .68	0.31 •33	0.00	30 28
62 64	8	21.50	11.63	7.65	5.63	4.40	3.55	2.93	2.44	2.05	1.72	1.19	-75	.36	.co	26
66 68	8 8	25.67	12.74	8.38 9.24	6.17	4.82 5.31	3.89 4.29	3.21 3.53	2.68 2.95	2.25	1.88	1.30	.82	.40	.00	24
70	8	31.40	14.04	10.25	7.55	5.89	4.76	3.92	3.27	2.75	2.31	1.59	1.00	0.48	0.00	20
72	00	35.18	17.45	11.49	8.46	6.60	5-33	4.40	3.67	3.08	2.58	1.78	1.12	•54	.00	18
74 76	8	39.86 45.84	19.78	13.01	9.58	7.48 8.60	6.04	4.98 5.73	4.16 4.78	3.49 4.01	2.93 3.37	2.01	1.27	.61	.00	16
78	00	53.77	26.68		12.93	10.09	8.15	6.72	5.61	4.70	3.95	2.72	1.71	.83	.00	12
80 82	% %	64.82 86.68	32.16 40.35		15.58	12.16 15.26	9.82	8.10	6.76 8.48	5.67 7.12	4.76 5.97	3.27 4.11	2.06	1.00	0.00	10
84	∞	_	53.96	35.51	26.14	20.40	16.48	13.59	11.34	9.51	7.98	5.49	3.46	1.68	.co	6
86 88	8	_	81.10	53.37	39.29 78.68	30.67 61.41	24.77 49.60	20.42 40.90	17.04 34.13	14.30 28.64	12.00 24.03	8.26 16.53	5.21	2.52	.00	4 2
90	∞	∞	8	8	8	8	8	∞	∞	∞	∞	∞	∞	∞	ind.	0
h'	90°	85°	80°	75°	70°	65°	60°	55°	50°	45°	40°	30°	20 °	100	o°	Z'

Table for Controlling the Coincidence of Lines of Position.

Giving D ($\frac{1}{2}$ of the useful length of the line of position) in minutes of the Equator.

d					Tru	e Alt	itude	of C	elesti	ial B	ody.					,
or t	o°	10°	20 °	30°	40°	50°	55°	60°	65°	70°	75°	80°	83°	86°	89°	t
o °	83	82	80	77	73	67	63	59	54	49	42	35	29	22	11	180°
10 20 30	84 86 89	83 85 88	81 83 86	78 80 83	73 75 78	67 69 71	63 65 67	59 61 63	54 56 58	49 50 52	43 44 45	35 36 37	29 30 31	22 23 24	11 11 12	170 160 150
40 50 60	95 103 117	94 103 116	92 100 114	96 109	83 91 103	76 83 94	72 78 89	67 73 83	62 67 76	55 60 6 ₇	48 53 60	39 43 49	33 36 41	25 27 31	13 14 15	140 130 120
70 80 90	142 199 ∞	141 198 ∞	137 193 ∞	132 185 ∞	124 174 ∞	114 159 ∞	107 151 ∞	100 141 ∞	92 129 ∞	83 116 ∞	72 101 ∞	59 83 ∞	49 69 ∞	° 37 53 ∞	19 26 ∞	100 100

To find D ($\frac{1}{2}$ of the useful length of the line of position on Mercator's chart: BB_3 in Fig. 3) enter the table with the declination in column d and corresponding to the altitude h will be found D_0 ($\frac{1}{2}$ of the useful length if t was 0°). Entering the table again with D_0 in the first horizontal line corresponding to $d=0^\circ$ and with t in column t we will find crossing the value of D, expressed in minutes of longitude.

Ex. $d=50^{\circ}$, $h=60^{\circ}$ and $t=40^{\circ}$. First we would find $D_0=73'$ and afterwards D=83'.

				F	Azim	uth	s of	Po	lari	s.				
Local Sidereal	Name.					L	atitud	ie.					Nome	Local
Time	Tvame,	o°	10°	20°	30°	40°	45°	50°	55°	60 °	65°	70°	Name.	Sidereal Time.
0 ^h 1 2	E E W	0.4	0.4 .1	0.5 .I .2	0.5	0.6	0.6	0.7 .2 .3	o.8 .2 .3	•.9 •3 •3	·3 ·4	.3 .6	W W E	12 ^h 13
3 4 5	W W W	•5 •7 •9	•5 •7 •9	.5 .8	.5 .8 1.1	.6 .9	.6 1.0 1.3	•7 1.1 1.5	.8 1.3 1.7	.9 1.4 1.9	I.I I.7 2.2	1.5 2.1 2.7	E E E	15 16 17
6 7 8	W W W	I.I I.2 I.2	I.I I.2 I.2	I.2 I.2 I.2	I.3 I.3 I.3	1.4 1.5 1.5	1.5 1.6 1.6	1.7 1.8 1.8	1.9 2.0 2.0	2.2 2.3 2.3	2.6 2.7 2.7	3.2 3.4 3.4	E E E	18 19 20
10 11	W W	·9 ·7	•9 •7	1.1 1.0 •7	1.2 1.1 .8	1.4 1.2 .9	I.5 I.3 I.0	1.7 1.4 1.1	1.9 1.6 1.2	2. I 1.8 1.4	2.5 2.2 1.7	3.2 2.7 2.1	E E E	21 22 23

This table will be very useful for finding the deviation of the compass in the northern hemisphere. It was computed assuming the Star's Right Ascension $1^h 27^m$ and its Declination 88° 50′ N. by the following formula: $Z \cos L = p \sin t$, where p represents the Star's Polar Distance=70′, the other terms being negligible within the limits of the table.

			C	ha	nge	e of	A	ltitı	ıde	per	Mi	nute	e of	Tin	ıe.			
LAT.										Azim	uth.							
DA1.	o°	5°	100	15°	20 °	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	75°	80°	90°
° 0	0	1.3	2.6	3. 9	5. I	6.3	7·5	8.6	9.6	10.6	11.5	12.3	13.0	13.6	14.1	14.5	14.8	15.0
4 8	0 0	1.3	2.6	3.9 3.8	5.1 5.1	6.3	7·5 7·4	8.6	9.6 9.5	10.6	11.5	12.3	13.0	13.6	14.1	14.5	14.7 14.6	15.0
12 16	0 0	1.3	2.5	3.8 3.7	5.0 4.9 4.8	6.2 6.1	7·3 7·2 7·0	8.4 8.3 8.1	9.4	10.4	11.2	11.8	12.7	13.3	13.8	13.9	14.4	14.7
20 24 26 28	0000	I.2 I.2 I.2	2.4 2.4 2.3 2.3	3.6 3.5 3.5 3.4	4.6 4.5	5.8 5.7 5.6	6.9 6.7 6.6	7.9 7.7 7.6	9.1 8.8 8.7 8.5	9.7 9.5 9.4	10.5	11.0	11.9	12.4 12.2 12.0	12.9 12.7 12.4	13.2 13.0 12.8	13.9 13.5 13.3 13.1	14.1 13.7 13.5 13.2
30 32 34 36	0 0 0 0	I.I I.I I.I I.I	2.3 2.2 2.2 2.1	3.4 3.3 3.2 3.1	4·4 4·4 4·3 4·2	5.5 5.4 5.3 5.1	6.5 6.4 6.2 6.1	7·4 7·3 7·1 7·0	8.3 8.2 8.0 7.8	9.2 9.0 8.8 8.6	9·9 9·7 9·5 9·3	10.6 10.4 10.2 9.9	11.2 11.0 10.8 10.5	11.8	12.2 12.0 11.7 11.4	12.5 12.3 12.0 11.7	12.8 12.5 12.3 12.0	13.0 12.7 12.4 12.1
38 40 42 44 46 48	0 0 0 0 0	1.0 1.0 .9	2.1 2.0 1.9 1.9 1.8	3.0 2.9 2.8 2.7 2.6	3.9 3.8 3.7 3.6 3.4	5.0 4.9 4.7 4.6 4.4 4.3	5.9 5.7 5.6 5.4 5.2 5.0	6.8 6.6 6.4 6.2 6.0 5.8	7.6 7.4 7.2 6.9 6.7 6.5	8.4 8.1 7.9 7.6 7.4 7.1	9.1 8.8 8.5 8.3 8.0 7.7	9.7 9.4 9.1 8.8 8.5 8.2	10.2 10.0 9.7 9.3 9.0 8.7	10.7 10.4 10.1 9.8 9.4 9.1	11.1 10.8 10.5 10.1 9.8 9.4	11.4 11.1 10.8 10.4 10.1 9.7	11.6 11.3 11.0 10.6 10.3	11.8 11.5 11.1 10.8 10.4
50 52 54 56 58	00000	.8 .8 .7	1.7 1.6 1.5 1.5	2.5 2.4 2.3 2.2 2.1	3·3 3·2 3·0 2·9 2·7	4. I 3. 9 3. 7 3. 5 3. 4	4.8 4.6 4.4 4.2 4.0	5.5 5.3 5.1 4.8 4.6	6.2 5.9 5.7 5.4 5.1	6.8 6.5 6.2 5.9 5.6	7.4 7.1 6.8 6.4 6.1	7.9 7.6 7.2 6.9 6.5	8.3 8.0 7.6 7.3 6.9	8.7 8.4 8.0 7.6 7.2	9.1 8.7 8.3 7.9 7.5	9.3 8.9 8.5 8.1 7.7	9.5 9.1 8.7 8.3 7.8	9.6 9.2 8.8 8.4 7.9
60 62 64 66 68	00000	.6 .6 .5	I.3 I.2 I.I I.I	1.9 1.8 1.7 1.6	2.6 2.4 2.2 2.1 1.9	3.2 3.0 2.8 2.6 2.4	3.8 3.5 3.3 3.1 2.8	4.3 4.0 3.8 3.5 3.2	4.8 4.5 4.2 3.9 3.6	5.3 5.0 4.6 4.3 4.0	5.7 5.4 5.0 4.7 4.3	6.1 5.8 5.4 5.0 4.6	6.5 6.1 5.7 5.3 4.9	6.8 6.4 6.0 5.5 5.1	7.0 6.6 6.2 5.7 5.3	7.2 6.8 6.4 5.9 5.4	7.4 6.9 6.5 6.0 5.6	7.5 7.0 6.6 6.1 5.6
70	0	•4	.9	1.3	1.8	2.2	2.6	2.9	3.3	3.6	3.9	4.2	4.4	4.6	4.8	5.0	5.1	5.1

	•	Tabl	e fo	or R	ecti	fyin	g L	ines	of	Pos	itior	1.	
h	D=	=30′	D	= 36′	D:	=42′	D:	=48′	D:	=54′	D:	=60′	h
	Δh	Z_1	Δh	Z_1	Δh	Z_1	Δh	Z_1	Δh	Z_1	Δh	Z_1	
20 30 40 45 50 55 60 61 62 63 64 65 66 67 68 69 70	0.0 .II .II .2 .2 .2 .2 .2 .2 .3 .3 .3 .3 .3 .3 .3 .3 .3 .3 .3 .3 .4 .4 .4	89.8 89.7 89.6 89.5 89.1 89.1 89.1 89.0 89.0 88.9 88.8 88.8 88.7 88.6 88.5	0.1 .1 .2 .2 .2 .3 .3 .3 .4 .4 .4 .4 .5 .5 .5 .5	89.8 89.7 89.5 89.4 89.1 88.9 88.9 88.8 88.7 88.6 88.5 88.4 88.4 88.3	0.1 .2 0.3 .3 .4 0.4 .5 .5 .5 .6 .6 .6 .6 .7	89.7 89.4 89.3 89.2 89.0 88.8 88.7 88.6 88.6 88.4 88.4 88.4 88.3 88.2 88.1 88.0 87.8	0.1 1 2 3 3 0.3 3 4 4 5 5 0.6 6 6 6 7 7 7 8 8 8 8 9 9 9 9 1.0	89.7 89.5 89.3 89.0 88.9 88.6 88.6 88.5 88.4 88.4 88.3 88.2 88.1 88.0 87.9 87.8	0.2 .2 .4 0.4 .5 .6 0.7 .8 .8 .8 .9 0.9 1.0 1.0 1.1	89.7 89.5 89.1 88.9 88.7 88.4 88.3 88.2 88.1 88.0 87.9 87.7 87.5 87.4	0.2 3 4 0.5 6 6 7 0.9 9 1.0 1.1 1.1 1.2 1.2 1.3 1.4 1.5 1.6	89.6 89.4 89.2 89.0 88.8 88.6 88.3 88.0 88.0 87.9 87.6 87.5 87.4 87.3 87.1 86.9	30 40 45 50 55 60 61 62 63 64 65 66 67
72 73 74 75	·4 ·4 ·5	88.5 88.4 88.3 88.1	.6 .7	88.0 87.9 87.8	.8	87.7 87.6 87.4	I.0 I.I I.2 I.3	87.5 87.4 87.2 87.0	1.3 1.4 1.5	87.1 86.9 86.6	1.7	86.7 86.5 86.3	72 73 74 75

			Tal	ble f	for 1	Rect	ifyir	ıg L	ines	s of	Pos	sitio	1		
h	D:	=6′	D=	=10′	D=	14'	D=	: 18′	D=	22′	D=	26′	D=	= 30′	h
12	Δh	Z_1	Δh	Z_1	Δh	Z_1	Δh	Z_1	Δh	Z_1	Δh	Z_1	Δh	Z_1	,,,
75 0 76 0 77 0 78 0 79 0	, o. o. o. o. o. o	89.6 89.6 89.5 89.5	, o. i . i . i . i	89.4 89.3 89.3 89.2 89.1	1,0 I .I .I .I .I .I .I	89.1 89.1 89.0 88.9 88.8	, 0, 2 , 2 , 2 , 2 , 2	88.9 88.8 88.7 88.6 88.5	·3 ·3 ·3 ·4	88.6 88.5 88.4 88.3 88.1	0.4 .4 .4 .5	88.4 88.3 88.1 88.0 87.8	0.5 .5 .6 .6	88.1 88.0 87.8 87.6 87.4	°5 0 75 0 76 0 77 0 78 0 79 0
80 0 81 0 82 0 83 0 84 0 30	0.0	89.5 89.4 89.3 89.2 89.0 89.0	1.0 1. 1. 1. 1.	89.0 88.9 88.8 88.6 83.4 88.3	.2 .2 .2 .3 .3	88.7 88.5 88.3 88.1 87.8 87.6	0.3 .3 .3 .4 .5	88.3 88.1 87.9 87.5 87.1 86.9	0.4 .4 .5 .6 .7	87.9 87.7 87.4 87.0 86.5 86.2	0.6 .6 .7 .8 .9	87.5 87.2 86.9 86.5 85.9	0.7 .8 .9 I.I I.2 I.4	87.1 86.8 86.4 85.9 85.2 84.8	80 0 81 0 82 0 83 0 84 0
85 0 20 40 86 0 20 40	1.0 1. 1. 1. 1.	88.9 88.8 88.7 88.6 88.4 88.3	0.2 .2 .2 .2 .2	88.1 83.0 87.8 87.6 87.4 87.1	0.3 .3 .4 .4 .4	87.3 87.1 86.9 86.7 86.4 86.0	0.5 .6 .6 .7 .7	86.6 86.3 86.0 85.7 85.3 84.9	0.8 .9 .9 I.0 I.I	85.8 85.5 85.2 84.8 84.3 83.7	1.1 1.2 1.3 1.4 1.5	85.0 84.7 84.3 83.8 83.3 82.6	I.5 I.6 I.7 I.9 2.0 2.2	84.3 83.9 83.4 82.9 82.2 81.5	85 0 20 40 86 0 20 40
87 0 10 20 30 40 50	1.0 1. 1. 1. 1.	88.1 88.0 87.9 87.7 87.5 87.4	0.3 .3 .3 .4 .4	86.8 86.7 86.4 86.2 85.9 85.6	0.5 .6 .6 .7 .7	85.6 85.3 85.0 84.7 84.3 83.9	0.9 1.0 1.1 1.1	84.3 84.0 83.6 83.2 82.7 82.1	1.3 1.4 1.5 1.6 1.7	83.0 82.6 82.2 81.7 81.1 80.4	1.9 2.0 2.1 2.2 2.4 2.6	81.8 81.3 80.8 80.2 79.5 78.7	2.5 2.6 2.8 3.0 3.2 3.4	80.5 80.0 79.4 78.7 77.9 77.0	87 0 10 20 30 40 50
88 0 5 10 15 20 25	0.I .2 .2 .2 .2 .2	87.1 87.0 86.9 86.7 86.6 86.4	0.4 •4 •5 •5 •5	85.2 85.0 84.8 84.6 84.3 84.0	0.8 .8 .9 .9 I.0	83.3 83.1 82.7 82.4 82.0 81.6	1.3 1.4 1.5 1.5 1.6	81.5 81.1 80.7 80.3 79.8 79.3	2.0 2.1 2.2 2.3 2.4 2.5	79.6 79.2 78.7 78.2 77.6 77.0	2.8 2.9 3.0 3.2 3.3 3.5	77.8 77.3 76.7 76.1 75.4 74.7	3.7 3.8 4.0 4.2 4.4 4.6	76.0 75.4 74.7 74.1 73.3 72.5	88 0 5 10 15 20 25
30 35 40 45 50 55	0.2 .2 .2 .2 .3 .3	86.2 86.0 85.7 85.4 85.1 84.7	0.6 .6 .6 .7 .7	83.7 83.3 82.9 82.4 81.9 81.3	I.I I.I I.2 I.3 I.4 I.5	81.2 80.6 80.1 79.4 78.7 77.8	1.8 1.9 2.0 2.1 2.3 2.4	78.7 78.0 77.3 76.5 75.6 74.5	2.7 2.8 3.0 3.2 3.4 3.6	76.3 75.5 74.6 73.7 72.6 71.3	3.7 3.9 4.1 4.4 4.7 5.0	73.9 73.0 72.0 70.9 69.6 68.2	4.9 5.1 5.4 5.8 6.2 6.6	71.6 70.6 69.4 68.2 66.8 65.2	30 35 40 45 50 55
89 0 3 6 9	•·3 •·3 •·4	84.3 84.0 83.7 83.3	0,8 •9 •9 1.0	80.5 80.0 79.5 78.9	1.6 1.7 1.8 1.9	76.9 76.2 75.5 74.6	2.6 2.8 2.9 3.1	73·3 72·5 71·6 70·6	3.9 4.1 4.3 4.5	69.9 68.9 67.8 66.7	5.4 5.7 5.9 6.3	66.6 65.5 64.3 63.0	7.0 7.4 7.8 8.2	63.4 62.2 60.9 59.5	89 0 3 6 9
12 15 18 21	0.4 •4 •4	82.9 82.4 81.9 81.3	I.0 I.I I.2 I.3	78.2 77.5 76.6 75.6	2.0 2.1 2.3 2.4	73.7 72.7 71.6 70.3	3·3 3·5 3·7 3·9	69.4 68.2 66.8 65.2	4.8 5.1 5.4 5.8	65.4 63.9 62.4 60.6	6.6 7.0 7.4 7.9	61.6 60.0 58.3 56.3		58.0 56.3 54.5 52.4	12 15 18 21
24 26 28 30	0.5 .5 .6 .6	80.5 80.0 79.4 7 8.7	I.4 I.5 I.5 I.6	74.5 73.6 72.6 71.6	2.6 2.8 2.9 3.1	68.7 67.6 66.6 65.0	4.2 4.5 4.7 5.0	63.4 62.1 60.6 59.0	6.2 6.5 6.8 7.2	58.6 57.1 55.5 53.7	8.4 8.8 9.2 9.7	54.2 52.6 50.9 49.1	11.3	50.2 48.6 46.8 45.0	24 26 28 30

	Con	versio	n	of I	Hours	ar	ıd	Minu	tes	int	o De	cim	ıal	Parts	of	a	Day.
h	ı m	D.P.	h	m	D.P.	h	m	D.P.	h	m	D.P.	h	m	D.P.	h	m	D.P.
C	0 10 20 30 40 50	0.00C .007 .014 .021 .028	4	0 10 20 30 40 50	0.167 .174 .181 .188 .194	8	0 10 20 30 40 50	0.333 .340 .347 .354 .361 .368	12	0 10 20 30 40 50	0.500 ·507 ·514 ·521 ·528 ·535	16	0 10 20 30 40 50	0.667 .674 .681 .688 .694	20	0 10 20 30 40 50	0.833 .840 .847 .854 .861 .868
I	0 10 20 30 40 50	0.042 .049 .056 .063 .069	5	0 10 20 30 40 50	0.208 .215 .222 .229 .236 .243	9	0 10 20 30 40 50	0.375 .382 .389 .396 .403 .410	13	0 10 20 30 40 50	 542 549 556 563 569 576 	17	0 10 20 30 40 50	0.708 .715 .722 .729 .736 .743	21	0 10 20 30 40 50	0.875 .882 .889 .896 .903
2	0 10 20 30 40 50	0.083 .090 .097 .104 .111	6	0 10 20 30 40 50	0.250 .257 .264 .271 .278 .285		0 10 20 30 40 50	0.417 .424 .431 .438 .444 .451	14	0 10 20 30 40 50	0.583 •590 •597 •604 •611 •618	18	0 10 20 30 40 50	0.750 .757 .764 .771 .778 .785	22	0 10 20 30 40 50	0.917 •924 •931 •938 •944 •951
3	0 10 20 30 40 50	0.125 .132 .139 .146 .153 .160	7	0 10 20 30 40 50	0.292 .299 .306 .313 .319		0 10 20 30 40 50	0.458 .465 .472 .479 .486 .493	15	0 10 20 30 40 50	0.625 .632 .639 .646 .653 .660	19	0 10 20 30 40 50	0.792 .799 .806 .813 .819	23	0 10 20 30 40 50	0.958 .965 .972 .979 .986 .993
4	0	0.167	8	0	0.333	12	0	0.500	16	0	0.667	20	0	0.833	24	0	1.000

Coı	nversion	of Interv			Time intar Time.	-	alent
1	7/	Cidonal	7//	Cidomost	7//	Cidamal	36-

	ereal erval.		Mea			ereal erval.		Mea			ereal rval.		Mea			real rval.	Mean Interval		
h 23	m 30 31 32 33 34	h 23	m 26 27 28 29 3°	s 9.0 8.8 8.7 8.5 8.4	h 23	m 45 46 47 48 49	h 23	m 41 42 43 44 45	s 6.6 6.4 6.2 6.1 5.9	h 24	m 0 1 2 3 4	h 23	m 56 57 58 59	s 4.1 3.9 3.8 3.6 3.4	h 24	m 15 16 17 18	h 24	m 11 12 13 14	s 1.6 1.5 1.3 1.1
23	35 36 37 38 39	23	31 32 33 34 35	8.2 8.0 7.8 7.7 7.5	23	50 51 52 53 54	23	46 47 48 49 50	5.7 5.6 5.4 5.2 5.1	24	56 78 9	24	1 2 3 4 5	3.3 3.1 2.9 2.8 2.6	24	20 21 22 23 24	24	16 17 18 19 20	0.8 0.7 0.5 0.3 0.2
23	40 41 42 43 44	23	36 37 38 39 40	7.4 7.2 7.0 6.9 6.7	23	55 56 57 58 59	23	51 52 53 54 55	4.9 4.7 4.6 4.4 4.3	24	10 11 12 13 14	24	6 7 8 9	2.5 2.3 2.1 1.9 1.8	24	25 26 27 28 29	24	21 21 22 23 24	59.8 59.7 59.5 59.3

This table is used in connection with the daily comparison of mean and sidereal time chronometers.

NEW ALTITUDE TABLES

A description of these Tables in Portuguese will be found in the *Revista Maritima Brazileira* for February, 1912, page 1335.

NEW ALTITUDE TABLES

HOW TO COMPUTE THE ALTITUDE OF A CELESTIAL BODY BY MEANS OF THE FOLLOWING TABLES

When the Hour Angle (t) and the Declination (d) of a celestial body are given and also the Latitude (L) of the observer we may calculate very easily, very rapidly and with as great accuracy as necessary the Altitude (h) of a celestial body as follows: In the fundamental equation

(1)
$$\cos (90^{\circ} - h) \text{ or } \sin h = \sin L \sin d + \cos L \cos d \cos t$$

we make

$$\cos t = I - 2 \sin^2 \frac{t}{2}$$

and we have

(2)
$$\cos (90^{\circ} - h) = \cos (L - d) - 2 \cos L \cos d \sin^2 \frac{t}{2}$$

or $I - \cos (90^{\circ} - h) = I - \cos (L - d) + 2 \cos L \cos d \sin^2 \frac{t}{2}$

If we make

(3)
$$2 \cos L \cos d \sin^2 \frac{t}{2} = \text{versine } \theta = 2 \sin^2 \frac{\theta}{2}$$

we will have finally

(4)
$$\operatorname{versine} (90^{\circ} - h) = \operatorname{versine} (L - d) + \operatorname{versine} \theta$$

Inverting equation (3), viz.:

$$2\cos L\cos d\sin^2\frac{t}{2} = 2\sin^2\frac{\theta}{2}$$

and multiplying both members by 2 we have

$$\sec L \sec d \csc^2 \frac{t}{2} = \csc^2 \frac{\theta}{2}$$

Applying logarithms to both members and dividing by 2 we have

(5)
$$1/2 \log \sec L + 1/2 \log \sec d + \log \csc \frac{t}{2} = \log \csc \frac{\theta}{2}$$

Therefore by means of formulæ (4) and (5) we can determine the Altitude with the aid of the following Tables.

The Tables on pages 2* to 9* give us 1/2 log sec L or 1/2 log sec d.

The Tables on pages 10* to 27* give us in columns marked "Hour Angle" the log cosec $\frac{t}{2}$ or log cosec $\frac{\theta}{2}$ when we enter with t or θ as arguments.

In columns marked "Sum or Diff." we find versine (L-d) and also in the same columns versine θ corresponding to the log cosec $\frac{\theta}{2}$ given in columns marked "Hour Angle."

The Tables on pages 28* to 36* give us log cosec $\frac{t}{2}$ when t is comprised between 90° and 270°.

The Altitude corresponding to versine $(90^{\circ} - h)$ will be found from below in columns marked "Alt.," the minutes of which are to be found on the right hand side of the pages.

Each versine and logarithm has been multiplied by 106 in order to reduce it to a whole number. On this account no characteristics appear and no periods also.

The numbers given correspond to six decimal places. When only five decimal place accuracy is desired drop the figure after the space or round up the fifth figure.

EXAMPLE I

GREENWICH HOUR ANGLE WEST.

The following expressions give us the value of to.—the Greenwich Hour Angle West:

$$t_a = G$$
. M. T. – Eq. of T. for the \odot
 $t_a = G$. M. T. +R. A. M. S – R. A. for *, \emptyset , and planets.

LOCAL HOUR ANGLE WEST.

Once known t_{a_n} the *local hour angle west* (t) is given by the expression

$$t = t_a \mp G$$

(- when G is West and + when G is East) G standing for Longitude.

When t_{a} is smaller than G add 360° to t_{a} . If $t_{a}+G$ is larger than 360° drop 360° from it.

EXAMPLE I.

On February 21, 1910, about 8^h A.M. in Lat. by D. R. = 36° 52′ N and Long. by D.R. = 8° 6′ W the Sun's true altitude was 21° 7′ at 21^h 6^m 11^s of the chronometer, 6^m 59^s slow of G. M. T. Required the D. R. altitude.

C.=21^h 6^m 11^s
C. C.= + 6 59
G. M. T.=21^h 13^m 10^s
Eq. of T.= - 13 46
G. A. T.=20^h 59^m 24^s or
$$t_a$$
=314° 51^q
 G_{W} = 8 6
 t =306° 45^r

EXPLANATION.

After applying the correction to the chronometer time and the equation of time to the G. M. T. we find the G. A. T. or t_a —the Sun's Greenwich Hour Angle West— t_a being G. A. T. converted into arc. The longitude by D. R. is combined with this t_a giving us t: the local hour angle west. Thus we have $t=306^{\circ}$ 45'.

¹ This procedure, not usually followed in the text books, has the *triple* advantage of simplifying the determination of *t*, abolishing the argument in time in the tables and the necessity of dealing with data expressed in time and in arc after G. A. T. is converted.

NEW ALTITUDE TABLES

The declination of the Sun, found in the Nautical Almanac at the same time as the Eq. of T., is taken to the nearest minute of arc. It is combined with the latitude, as shown.

When L and d are of the same name, both N or both S, subtract the smaller of the two from the larger. If they are of contrary names, as in our Examples, one N and the other S, add them together. We find $L+d=47^{\circ}$ 19'.

Entering the "Latitude or Declination" Tables with $L=36^{\circ}$ 52' we find on

page 5*: 4845, and with $d=10^{\circ}$ 27' we find on page 3*: 363.

Entering the tables on page 20* from below with $t=306^{\circ}$ 45' in the "Hour Angle" column we find 34858, which, added to the numbers corresponding to L and d, gives us 40066.

We look for this number 40066 on page 19* in the same "Hour Angle" column, and opposite it in column "Sum or Diff." we find 31609. Adding to this number 31609 the number 32205 found on page 19* corresponding to 47° 19' in "Sum or Diff." column we have 63814. This number corresponds to 21° 13' in the "Alt." column on page 23*.

Therefore the altitude from D. R. is 21° 13'.

EXAMPLE II.

On August 21, 1908, about 11^h A.M. in Lat. by D. R.=16° 34' S. and Long. by D. R.=38° 11' W. the Sun's true altitude was 59° 10' at 1^h 19^m 40^s of the chronometer 26^m 50^s slow of G. M. T. Required the D. R. altitude.

C.=1^h 19^m 40^s
C. C.=+ 26 59
G. M. T.=1^h 46^m 39^s
Eq. of T.=- 3 3
G. A. T.=1^h 43^m 36^s or
$$t_0$$
= 25° 54'
$$360^{\circ} + t_0 = 38^{\circ} 54'$$

$$G_{W} = 38 11$$

$$t = 347^{\circ} 43' 97067 t = 347^{\circ} 43'$$

$$L = 16 34 S 921$$

$$d = 12 10 N 493$$

$$98481 2143$$

$$L+d = 28^{\circ} 44' 12313$$

$$14456$$

$$h = 58^{\circ} 49'$$

How to FIND THE AZIMUTH.

The Azimuth can be readily and easily found by methods explained on pages xxxvii and xxxviii of the "Altitude and Azimuth Tables."

For the sake of further exercise we will find the Azimuth in one of the two examples above.

Example. Given $t=53^{\circ}$ 15' E, $d=10^{\circ}$ 27' S and $L=36^{\circ}$ 52' N. Find the Azimuth.

¹ When t is smaller than 180° we enter the tables at the top and the body is West of the meridian; when t is greater than 180° we enter the tables from below and the body is East of the meridian.

HOW TO FIND THE AZIMUTH

Entering the tables with $d=10^{\circ}$ 30' and $t=53^{\circ}$ we find on page 69: $a=52^{\circ}$ 0' and $b=17^{\circ}$. Combining b with L we have $C=54^{\circ}$ and entering the tables again with $a=52^{\circ}$ 0' and $C=54^{\circ}$ we find $Z=57^{\circ}$ 42'.

Generally (when $Z<70^\circ$) it will not be necessary to combine b and L. It is only necessary to run down column h corresponding to $a=52^\circ$ o' until we find $h=21^\circ$ 13 and alongside the value of the altitude we would find $Z=57^\circ$ 42'.

In the same way we would find $Z=23^{\circ}$ 41' in the second example.

Note.—It is evident that the Hour Angle t can be found given L, d and h by using backwards the process for finding h given L, d and t.

The author takes this opportunity to thank his good friend Lieutenant Renato Bayardino, Brazilian Navy, for his kindness in organising the "Latitude or Declination" Tables and for carefully revising with him these new Altitude Tables.

				Latitu		Declir	nation				
	o°	ı°	2 °	3°	4°	_5°	6°	7°	8°	9°	
0 I 2 3 4	0 0 0 0 0 0 0 0	3 3 3 4 3 5 3 6 3 8	13 3 13 5 13 7 13 9 14 1	29 8 30 I 30 4 30 8 31 I	53 ° 53 4 53 9 54 3 54 7	82 8 83 3 83 9 84 5 85 0	119 3 120 0 120 6 121 3 122 0	162 5 163 2 164 0 164 8 165 6	212 4 213 3 214 1 215 0 215 9	269 0 270 0 271 0 272 0 273 0	0 1 2 3 4
5 6 7 8 9	000000000000000000000000000000000000000	3 9 4 0 4 1 4 3 4 4 4 5	14 4 14 6 14 8 15 1 15 3	31 5 31 8 32 2 32 5 32 8 33 2	55 2 55 7 56 1 56 6 57 °	85 6 86 2 86 7 87 3 87 8 88 4	122 6 123 3 124 0 124 7 125 3 126 0	166 4 167 2 167 9 168 7 169 5	216 8 217 7 218 6 219 5 220 4	274 0 275 0 276 I 277 I 278 I 279 I	56 78 9
11 12 13 14 15	0 I 0 I 0 2 0 2	4 5 4 6 4 8 4 9 5 0 5 2	15 7 16 0 16 3 16 5	33 5 33 9 34 2 34 6 35 0	57 5 57 9 58 4 58 9 59 3 59 8	89 6 90 2 90 7 91 3	126 7 127 4 128 1 128 8	171 1 171 9 172 7 173 5	222 2 223 2 224 I 225 0 225 9	280 I 281 I 282 2 283 2 284 2	11 12 13 14 15 16
17 18 19 20	0 2 0 3 0 3 0 3	5 3 5 4 5 6 5 7 5 9	17 0 17 3 17 5 17 8	35 3 35 7 36 0 36 4 36 8	60 3 60 7 61 2 61 7 62 2	91 9 92 5 93 0 93 6 94 2	130 I 130 8 131 5 132 2	175 1 175 9 176 7 177 5	226 8 227 7 228 6 229 6 230 5	285 3 286 3 287 3 288 4 289 4	16 17 18 19 20 21
21 22 23 24 25 26	0 4 0 4 0 5 0 5 0 6	6 o 6 2 6 3 6 5 6 6 6 8	18 3 18 5 18 8 19 1 19 3 19 6	37 2 37 5 37 9 38 3 38 6 39 0	62 7 63 1 63 6 64 1 64 6 65 1	94 8 95 4 96 0 96 6 97 2 97 8	133 6 134 3 135 0 135 8 136 5 137 2	179 2 180 0 180 8 181 6 182 5 183 3	231 4 232 3 233 3 234 2 235 I 236 I	290 4 291 5 292 5 293 6 294 6 295 7	22 23 24 25 26
27 28 29 30 31	0 7 0 7 0 8 0 8	7 ° 7 1 7 3 7 4 7 6	19 9 20 1 20 4 20 7 21 0	39 4 39 8 40 2 40 5 40 9	65 6 66 1 66 5 67 0	98 4 99 0 99 6 100 2 100 8	137 9 138 6 139 3 140 0 140 8	184 1 184 9 185 7 186 6 187 4	237 0 238 0 238 9 239 8 240 8	296 7 297 8 298 8 299 9 300 9	27 28 29 30 31 32
32 33 34 35 36	0 9 1 0 1 1 1 1 1 2	7 8 7 9 8 1 8 3 8 5 8 6	21 2 21 5 21 8 22 1 22 4 22 7	41 3 41 7 42 1 42 5 42 9	68 0 68 5 69 0 69 6 70 1 70 6	101 4 102 0 102 7 103 3 103 9 104 5	141 5 142.2 142 9 143 7 144 4 145 1	188 2 189 1 189 9 190 8 191 6	241 7 242 7 243 6 244 6 245 5 246 5	302 0 303 0 304 I 305 2 306 2 307 3	33 34 35 36
37 38 39 40 41 42	1 3 1 4 1 4 1 5 1 5 1 6	8 8 9 0 9 2 9 4 9 6	22 7 22 9 23 2 23 5 23 8 24 I	43 3 43 7 44 1 44 5 44 9 45 3	71 1 71 6 72 1 72 6 73 1	105 I 105 8 106 4 107 0 107 6	145 9 146 6 147 3 148 1 148 8	193 3 194 1 195 0 195 8 196 7	247 5 248 4 249 4 250 3 251 3	308 4 309 5 310 5 311 6 312 7	38 39 40 41 42
43 44 45 46 47 48	17 18 19 19 20 21	9 8 9 9 10 1 10 3 10 5 10 7	24 4 24 7 25 0 25 3 25 6 25 9	45 7 46 1 46 5 47 0 47 4 47 8	73 7 74 2 74 7 75 3 76 3 76 8	108 3 108 9 109 5 110 2 110 8	149 6 150 3 151 0 151 8 152 5 153 3	197 5 198 4 199 3 200 1 201 0 201 8	252 3 253 2 254 2 255 2 256 2 257 1	313 8 314 9 315 9 317 0 318 1 319 2	40 47 48
50 51 52 53 54	2 2 2 3 2 4 2 5 2 6 2 7	10 9 11 1 11 3 11 5 11 7 11 9	26 2 26 6 26 9 27 2 27 5 27 8	48 2 48 6 49 1 49 5 49 9 50 3	77 4 77 9 78 4 79 0 79 5	112 1 112 7 113 4 114 0 114 7 115 4	154 0 154 8 155 6 156 3 157 1 157 8	202 7 203 6 204 4 205 3 206 2 207 I	258 I 259 I 260 I 261 I 262 0 263 0	320 3 321 4 322 5 323 6 324 7 325 8	50 51 52 53 54
55 56 57 58 59 60	28 29 30 31 32 33	12 2 12 4 12 6 12 8 13 0	28 2 28 5 28 8 29 1 29 5 29 8	50 8 51 2 51 7 52 1 52 5 53 0	80 I 80 6 81 2 81 7 82 2 82 8	116 0 116 6 117 3 118 0 118 6 119 3	158 6 159 4 160 1 160 9 161 7 162 5	208 0 208 8 209 7 210 6 211 5 212 4	264 0 265 0 266 0 267 0 268 0 269 0	326 9 328 0 329 I 330 2 331 3 332 4	56 57 58 59
	o°	ı°	2 °	3°	4°	5°	6°	7 °	8°	9°	
				Latitu	ide or	Decli	nation				

			I	Latitu	de or	Declin	ation				
	10°	IIº	12°	13°	14°	15°	16°	17°	18°	19°	
0 1 2 3 4	332 4 333 5 334 7 335 8 336 9	402 7 403 9 405 1 406 4 407 6	479 8 481 1 482 5 483 8 485 2	563 8 565 3 566 7 568 2 569 7	654 8 656 4 658 0 659 5 661 1	752 8 754 5 756 2 757 9 759 6	857 9 859 7 861 5 863 4 865 2	970 2 972 1 974 1 976 0 977 9	1089 7 1091 7 1093 8 1095 9 1097 9	1216 5 1218 7 1220 9 1223 0 1225 2	3 4
5 6 7 8 9	338 0 339 1 340 3 341 4 342 5 343 7	408 8 410 1 411 3 412 6 413 8 415 0	486 5 487 9 489 2 490 6 491 9 493 3	571 1 572 6 574 1 575 5 577 ° 578 5	662 7 664 3 665 9 667 5 669 0	761 3 763 0 764 7 766 4 768 1 769 8	867 0 868 8 870 6 872 5 874 3	979 9 981 8 983 8 985 7 987 6 989 6	1100 0 1102 0 1104 1 1106 2 1108 2	1227 4 1229 6 1231 8 1234 0 1236 2	5 6 7 8 9
11 12 13 14 15	344 8 345 9 347 1 348 2 349 3	416 3 417 5 418 8 420 1 421 3 422 6	494 7 496 0 497 4 498 8 500 1 501 5	580 0 581 4 582 9 584 4 585 9 587 4	672 2 673 8 675 4 677 0 678 6 680 2	771 6 773 3 775 0 776 7 778 4 780 1	878 0 879 8 881 6 883 5 885 3 887 2	991 6 993 5 995 5 997 4 999 4	1112 4 1114 5 1116 5 1118 6 1120 7 1122 8	1240 6 1242 8 1245 0 1247 2 1249 4 1251 6	11 12 13 14 15 16
17 18 19 20 21	35° 5 351 7 352 8 353 9 355 1 356 2	422 0 423 8 425 1 426 3 427 6 428 9	502 9 504 3 505 6 507 0 508 4	588 9 59° 4 591 9 593 4 594 9	681 9 683 5 685 1 686 7 688 3	781 9 783 6 785 3 787 1 788 8	889 0 890 8 892 7 894 5 896 4	1003 3 1005 3 1007 2 1009 2 1011 2	1124 9 1127 0 1129 0 1131 1 1133 2	1253 8 1256 0 1258 2 1260 4 1262 6	17 18 19 20 21
22 23 24 25 26 27	357 4 358 5 359 7 360 9 362 0 363 2	430 I 431 4 432 7 434 0 435 2 436 5	509 8 511 2 512 6 513 9 515 3 516 7	596 4 597 9 599 4 600 9 602 4 603 9	689 9 691 5 693 2 694 8 696 4 698 0	79° 5 792 3 794 ° 795 7 797 5 799 2	898 2 900 I 902 0 903 8 905 7 907 6	1013 2 1015 2 1017 1 1019 1 1021 1 1023 1	1135 3 1137 4 1139 5 1141 6 1143 7 1145 8	1264 8 1267 1 1269 3 1271 5 1273 7 1276 0	22 23 24 25 26 27
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34 35 36 37 38 39	37 ¹ 4 37 ² 6 37 ³ 8 37 ⁴ 9 37 ⁶ 1 377 3	445 5 446 8 448 1 449 4 450 7 452 0	526 5 528 0 529 4 530 8 532 2 533 6	614 5 616 0 617 6 619 1 620 6 622 2	709 5 711 1 712 8 714 4 716 1 717 7	811 5 813 3 815 0 816 8 818 6 820 3	920 7 922 5 924 4 926 3 928 2 930 I	1037 0 1039 0 1041 0 1043 0 1045 0 1047 0	1160 6 1162 8 1164 9 1167 0 1169 1	1291 6 1293 9 1296 1 1298 4 1300 6 1302 9	34 35 36 37 38 39
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	10°	II°	12°	I 3°	14°	15° Declin	16°	17°	18°	19°	
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	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	
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	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	
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1	3127 1	3350 5	3582 9	3824 5	4075 6	4336 2	4606 7		5 ¹ 78 3	5480 0	1
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14	3174 8	3400 I	3634 5	3878 1	4131 2	4394 0	4666 6	4949 5	5242 8	5546 8	14
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22	3204 3	3430 8	3666 4	3911 3	4165 7	4429 7	4703 8	4988 0	5282 7	5588 1	22
23	3208 0	3434 7	3670 4	3915 5	4170 0	4434 2	4708 4	4992 8	5287 7	5593 3	23
24	3211 7	3438 5	3674 4	3919 6	4174 3	4438 7	4713 1	4997 6	5292 7	5598 5	24
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	30°	31°	32°	33°	34°	35°	36°	37°	38°	39°	
				Latit	ude or	Decli	nation				

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	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	
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47 48 49 50 51 52	97 102 106 110	215606 6 214711 1 213833 8 212973 8 212130 5	49 3 50 3 51 2 52 1 53 1	180389 8 179989 6 179593 0 179200 0 178810 5	119 4 120 8 122 2 123 7 125 1	161203 8 160946 1 160689 9 160435 2 160182 1	219 8 221 8 223 7 225 7 227 6	147944 9 147754 9 147565 7 147377 4 147189 8	350 7 353 1 355 6 358 0 360 5	137803 8 137653 4 137503 5 137354 1 137205 2	12 11 10 9 8
53 54 55 56 57 58 59 60	11 9 12 3 12 8 13 3 13 7 14 2	211303 2 210491 5 209694 6 208912 1 208143 4 207388 1	54 ° 55 ° 55 9 56 9 57 9 58 9	178424 5 178041 9 177662 6 177286 6 176913 9 176544 3	126 6 128 1 129 5 131 0 132 5 134 0	159930 4 159680 1 159431 3 159183 9 158937 9 158693 2	229 6 231 6 233 5 235 5 237 5 239 5	147003 I 146817 2 146632 I 146447 7 146264 2 146081 4	363 0 365 5 368 0 370 5 373 0 375 5	137056 8 136908 9 136761 5 136614 6 136468 3 136322 4	5 4 3
59	14 7 15 2 Alt.	206645 7 205915 8 Hour Angle	50 9 59 9 60 9 Alt.	Hour Angle	134 0 135 5 137 0 Alt.	158450 0 158208 1 Hour Angle	241 6 243 6 Alt.	145899 3 145718 1 Hour Angle	378 o 380 5 Alt.	136177 0 136032 0 Hour Angle	0 ,
	89°	359°	88°	358°	87°	357°	86°	356°	85°	355°	

		5°		6°		7°		8°		9°	
′	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4		135887 6 135743 7 135600 2	553 9 557 °	128120 0 127999 6 127879 6 127759 9 127640 5	756 I	121432 5 121329 3 121226 4 121123 8 121021 3	9854	115641 5 115551 3 115461 3 115371 4 115281 7	1235 7 1240 3 1244 9	110455 5 110375 4 110295 6	60 59 58 57 56
56 78 9			566 2 569 3 572 4 575 5	127521 5 127402 8 127284 4 127166 3 127048 6		120919 2 120817 2 120715 5 120614 1 120512 8	1001 7 1005 8 1010 0	115192 2 115102 9 115013 8 114924 9 114836 1	1258 6 1263 2 1267 8 1272 5	110056 8 109977 5 109898 3 109819 3	55 54 53 52 51
10 11 12 13 14	411 6 414 2 416 8	134608 9 134469 2 134329 8 134191 0 134052 5	581 8 584 9 588 0 591 2	126931 2 126814 1 126697 3 126580 8 126464 6	788 5 792 2 795 8	120010 3	1018 2 1022 4 1026 5 1030 7	114482 9	1281 7 1286 4 1291 0 1295 7	109661 7 109583 1 109504 7 109426 4	50 49 48 47 46
15 16 17 18 19	422 2 424 8 427 5 430 2	133914 5 133777 0 133639 8 133503 2 133366 9	594 4 597 5 600 7 603 9 607 1	126348 8 126233 3 126118 0 126003 1 125888 5	803 2 806 9 810 6 814 3	119910 4 119810 8 119711 5 119612 4 119513 4 119414 8	1039 0 1043 2 1047 4 1051 6	114219 9 114132 6 114045 4	1305 0 1309 7 1314 4 1319 1	109270 3 109192 4 109114 7 109037 1	45 44 43 42 41 40
21 22 23 24 25	435 6 438 3 441 1 443 8	133095 7 132960 7 132826 1 132692 0	613 5 616 7 620 0 623 2	125660 I 125546 4 125433 0 125319 8	821 7 825 4 829 1 832 9 836 6	119316 3 119218 1 119120 1 119022 3 118924 7	1060 1 1064 3 1068 5 1072 8	113785 1 113698 6 113612 3 113526 2	1328 6 1333 3 1338 0 1342 8	108882 3 108805 1 108728 1 108651 2	39 38 37 36 35
26 27 28 29 30	452 0 454 8 457 6 460 4	132424 9 132292 0 132159 5 132027 4 131895 7	629 7 633 0 636 2 639 5 642 8	125094 5 124982 2 124870 3 124758 6 124647 2	840 4 844 2 847 9 851 7 855 5	118827 4 118730 2 118633 3 118536 6 118440 1	1081 3 1085 5 1089 8 1094 1 1098 4	113354 5 113269 0 113183 5 113098 3	1352 3 1357 1 1361 8 1366 6 1371 4	108421 3 108345 0 108268 7 108192 7	34 33 32 31 30
31 32 33 34 35	466 0 468 8 471 6 474 4	131764 4 131633 5 131502 9 131372 8	649 4 652 7 656 0 659 4	124536 1 124425 3 124314 8 124204 5 124094 6	863 1 866 9 870 8 874 6	118343 9 118247 8 118152 0 118056 4	1107 0 1111 3 1115 7 1120 0	112843 5 112759 0 112674 5 112590 3	1381 1 1385 9 1390 7 1395 5	108040 9 107965 2 107889 7 107814 2	28 27 26 25
36 37 38 39 40 41	480 1 482 9 485 8 488 7	131113 7 130984 8 130856 2 130728 0 130600 2 130472 8	669 4 672 8 676 2	123984 9 123875 5 123766 3 123657 5 123548 9 123440 6	882 3 886 2 890 0 893 9	1176760	1128 7 1133 1 1137 4 1141 8	112422 3 112338 5 112254 9 112171 5	1405 2 1410 1 1415 0 1419 9	107663 8 107588 8 107513 9 107439 1	24 23 22 21 20 10
42 43 44 45 46	494 4 497 3 500 2 503 I	130345 7	682 9 686 3 689 7	123332 5 123224 8 123117 2 123010 0 122903 0	901 7 905 6 909 5 913 4 917 3	117298 9 117205 1 117111 6 117018 2 116925 1	1150 6 1155 0 1159 4 1163 8 1168 3	112005 1 111922 1 111839 3 111756 7 111674 2	1429 6 1434 6 1439 5 1444 4 1449 3	107290 0 107215 6 107141 3 107067 2 106993 2	18 17 16
47 48 49 50 51	511 9 514 9 517 8 520 8	129466 5 129342 3 129218 5	700 0 703 4 706 9 710 3 713 8	122796 3 122689 9 122583 7 122477 7 122372 1	921 3 925 2 929 2 933 1 937 1	116832 1 116739 3 116646 8 116554 4 116462 3	1172 7 1177 2 1181 6 1186 1 1190 5	111591 9 111509 7 111427 7 111345 8 111264 1	1454 3 1459 2 1464 2 1469 1 1474 1	106919 4 106845 6 106772 0 106698 5 106625 1	13 12 11 10
52 53 54 55 56 57	523 7 526 7 529 7 532 7 535 7	128972 0 128849 3 128726 8		122161 5	945 I 949 0 953 I 957 I	116370 3 116278 5 116187 0 116095 6 116004 4 115913 4	1199 5 1204 0 1208 5 1213 0	111182 6 111101 2 111019 9 110938 8 110857 9	1484 I 1489 I 1494 I 1499 I	106478 8 106405 8 106332 9 106260 2	98 76 5432 I
55 56 57 58 59 60	541 7 544 8 547 8	128361 7 128240 6 128120 0	738 3	121639 5 121535 9 121432 5	965 I	115822 6 115732 0 115641 5	1222 I 1226 6	110696 5	1509 I 1514 2	106115 0	0
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	84°	354°	83°	353°	82°	352°	81°	351°	80°	350°	

	1	o°	I	ı°	12	2°	13	3°	14	°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	1519 2 1524 3 1529 3 1534 4	105970 4 105898 3 105826 2 105754 3 105682 6			2191 3 2197 3 2203 4	98076 5 98016 5 97956 5 97896 6 97836 8		94614 I 94558 7 94503 4 94448 I 94392 9	297° 4 2977 5 2984 5 2991 6	91410 6 91359 1 91307 8 91256 5	60 59 58 57 56
5 6 7 8	1539 5 1544 6 1549 7 1554 8 1559 9	105610 9 105539 4 105467 9 105396 6	1865 1 1870 7 1876 3 1881 9	101516 0 101450 9 101385 9 101321 1	2215 6 2221 7 2227 8 2233 9	97777 1 97717 5 97 ⁶ 57 9 9759 ⁸ 4	2595 8 2602 4 2609 0 2615 6	94337 8 94282 8 94227 8 94172 9	2998 6 3005 7 3012 8 3019 9 3027 0	91205 3 91154 1 91103 0 91052 0 91001 0	55 54 53 52
9 10 11 12 13	1565 0 1570 1 1575 3 1580 4 1585 6		1887 6 1893 2 1898 8 1904 5 1910 1	101256 3 101191 7 101127 1 101062 6 100998 3	2246 I 2252 3 2258 4	97539 ° 97479 7 9742° 5 97361 4 973°2 3	2622 2 2628 8 2635 5 2642 1 2648 8	94118 0 94063 3 94008 6 93954 0 93899 4	3034 I 304I 2 3048 3 3055 5 3062 6	90950 0 90899 2 90848 4 90797 6 90747 0	51 50 49 48 47
14 15 16 17 18	1590 8 1595 9 1601 1 1606 3 1611 5	104971 3	1915 8 1921 5 1927 1 1932 8	100934 0 100869 8 100805 7 100741 7 100677 8	2270 7 2276 9 2283 I	97243 3 97184 4 97125 6 97066 8 97008 2	2655 4 2662 1 2668 7 2675 4 2685 1	93844 9 9379° 5 93736 1 93681 9 93627 6	3069 7 3076 9 3084 1 3091 2 3098 4	90696 3 90645 8 90595 3 90544 8 90494 4	46 45 44 43 42
19 20 21 22	1616 7 1621 9 1627 1 1632 4	104620 0 104550 1 104480 3 104410 6	1944 2 1949 9 1955 7 1961 4	100614 0 100550 3 100486 7 100423 2	2301 6 2307 8 2314 1 2320 3	96949 6 96891 1 96832 7 96774 3	2688 8 2695 5 2702 2 2708 9	93573 5 93519 4 93465 4 93411 5	3105 6 3112 8 3120 0 3127 2	90444 I 90393 8 90343 6 90293 5	41 40 39 38
23 24 25 26 27	1637 6 1642 8 1648 1 1653 4 1658 6	104341 0 104271 6 104202 2 104133 0 104063 8	1972 9 1978 6 1984 4 1990 2	100359 8 100296 4 100233 2 100170 1 100107 0	2326 5 2332 8 2339 0 2345 3 2351 5	96716 1 96657 9 96599 8 96541 8 96483 8	2715 7 2722 4 2729 2 2735 9 2742 7	93357 6 93303 8 93250 1 93196 4 93142 8	3134 4 3141 7 3148 9 3156 2 3163 4	90243 4 90193 4 90143 4 90093 5 90043 6	37 36 35 34 33
28 29 30 31 32	1663 9 1669 2 1674 5 1679 8 1685 1	103994 8 103925 9 103857 1 103788 4 103719 9	1995 9 2001 7 2007 5 2013 3 2019 1	100044 0 99981 2 99918 4 99855 7 99793 1	2357 8 2364 1 2370 4 2376 7 2383 0	96425 9 96368 1 96310 4 96252 8 96195 2	2749 4 2756 2 2763 0 2769 8 2776 6	93089 3 93035 8 92982 4 92929 1 92875 8	3170 7 3178 0 3185 2 3192 5 3199 8	89993 8 89944 1 89894 4 89844 8 89795 2	32 31 30 29 28
33 34 35 36	1690 4 1695 8 1701 1 1706 5	103651 4	2025 0 2030 8 2036 6 2042 5	99730 6 99668 2 99605 9 99543 7	2389 3 2395 6 2402 0 2408 3	96137 7 96080 3 96023 0 95965 8	2783 4 2790 2 2797 I 2803 9 2810 7	92822 6 92769 4 92716 4 92663 4 92610 4	3207 I 3214 4 3221 7 3229 I	89745 7 89696 3 89646 9 89597 5 89548 3	27 26 25 24
37 38 39 40 41	1711 8 1717 2 1722 6 1727 9 1733 3	103310 7 103242 8 103175 1 103107 5	2054 2 2060 I 2065 9 2071 8	99481 5 99419 5 99357 5 99295 6 99233 9	2421 0 2427 4 2433 8 2440 I	95908 6 95851 5 95794 5 95737 5 95680 6	2817 6 2824 5 2831 3 2838 2	92557 6 92504 7 92452 0 92399 3	3236 4 3243 8 3251 1 3258 5 3265 8	89499 0 89449 9 89400 8 89351 7	23 22 21 20 19
42 43 44 45 46	1738 7 1744 1 1749 5 1755 0 1760 4	103040 0 102972 6 102905 3 102838 1 102771 1	2083 6 2089 5	99172 2 99110 6 99049 0 98987 6 98926 3	2452 9 2459 3	95623 8 95567 1 95510 5 95453 9 95397 4	2845 I 2852 0 2858 9 2865 8 2872 7	92346 7 92294 2 92241 7 92189 3 92136 9	3273 2 3280 6 3288 0 3295 4 3302 8	89302 7 89253 8 89204 9 89156 1 89107 3	18 17 16 15
47 48 49 50	1765 8 1771 3 1776 7 1782 2	102704 1 102637 2 102570 4 102503 8	2107 3 2113 3 2119 2 2125 2	98865 0 98803 8 98742 8 98681 8	2478 6 2485 I 249I 5 2498 0	95341 0 95284 6 95228 3 95172 1	2879 6 2886 6 2893 5 2900 5	92084 6 92032 4 91980 2 91928 1	3310 2 3317 7 3325 1 3332 5	89058 6 89009 9 88961 3 88912 7	13 12 11 10
51 52 53 54 55	1787 7 1793 1 1798 6 1804 1 1809 6	102370 7 102304 4 102238 1	2143 I 2149 I	98620 9 98560 0 98499 3 98438 7 98378 1	25109	94892 2	2907 4 2914 4 2921 4 2928 3 2935 3	91824 I 91772 2 91720 3 91668 5	334°° 3347 4 3354 9 3362 4 3369 9	88815 8 88767 4 88719 1 88670 8	9 8 7 6 5
55 56 57 58 59 60	1815 1 1820 7 1826 2 1831 7 1837 3	102105 9 102040 0 101974 1 101908 4	2161 1 2167 1 2173 2 2179 2	98317 6 98257 2 98196 9 98136 7	2536 9 2543 4 2549 9 2556 4	94836 5 94780 8 94725 I 94669 6	2942 3 2949 3 2956 4	916168 915652 915136 914620	3377 4 3384 9 3392 4 3399 9 3407 4	88574 4 88526 3 88478 2	5 4 3 2 1 0
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	79°	349°	78°	348°	77°	347°	76°	346°	75°	345°	

	15°	16°	17°	18°	19°	
,	Sum or Hour Angle	Sum or Diff. Hour Angle	Sum or Hour Angle	Sum or Diff. Hour Angle	Sum or Diff. Hour Angle	
0 I 2 3 4	3407 4 88430 2 3414 9 88382 3 3422 5 88334 4 3430 0 88286 5 3437 6 88238 7	3881 8 85599 5 3889 9 85554 7 3897 9 85509 8	4378 0 82987 5 4386 5 82945 3 4395 1 82903 2	4903 3 80526 9 4912 3 80487 1	5448 I 78239 I 5457 6 7820I 3 5467 I 78163 7 5476 6 78126 0 5486 I 78088 4	60 59 58 57 56
5 6 7 8 9	3445 2 88191 0 3452 7 88143 3 3460 3 88095 7 3467 9 88048 1 3475 5 88000 6	3922 1 85375 7 3930 2 85331 0 3938 2 85286 4	4420 7 82777 0 4429 3 82735 0 4437 8 82693 0	4948 4 80328 1 4957 5 80288 5	5495 6 78050 8 5505 1 78013 2 5514 6 77975 7 5524 2 77938 2 5533 7 77900 7	55 54 53 52 51
10 11 12 13 14	3483 I 87953 I 3490 7 87905 7 3498 3 87858 3 3506 0 87811 0 3513 6 87763 8	3962 5 85152 9 3970 6 85108 5 3978 7 85064 2	4463 6 82567 4 4472 2 82525 6 4480 8 82483 9	4984 6 80169 8 4993 7 80130 3 5002 8 80090 9 5011 9 80051 4 5021 0 80012 1	5543 2 77863 3 5552 8 77825 9 5562 4 77788 5 5571 9 77751 2 5581 5 77713 9	50 49 48 47 46
15 16 17 18 19	3521 3 87716 5 3528 9 87669 4 3536 6 87622 3 3544 3 87575 2 3551 9 87528 2	4003 2 84931 4 4011 3 84887 2 4019 5 84843 1 4027 6 84799 0	4506 6 82358 9 4515 3 82317 3 4523 9 82275 8 4532 6 82234 3	5030 I 79972 7 5039 2 79933 4 5048 3 79894 I 5057 4 79854 9 5066 6 79815 7	5591 1 77676 6 5600 7 77639 4 5610 3 77602 2 5619 9 77565 1 5629 5 77527 9	45 44 43 42 41
20 21 22 23 24	3559 6 87481 3 3567 3 87434 4 3575 0 87387 5 3582 7 87340 7 3590 5 87294 0	4044 0 84710 9 4052 2 84667 0 4060 4 84623 1 4068 6 84579 2	4549 9 82151 4 4558 6 82110 0 4567 3 82068 7 4576 0 82027 4	5075 7 79776 6 5084 9 79737 4 5094 0 79698 3 5103 2 79659 3 5112 4 79620 3	5639 1 77490 8 5648 8 77453 8 5658 4 77416 7 5668 1 77379 7 5677 7 77342 7	40 39 38 37 36
25 26 27 28 29	3598 2 87247 3 3605 9 87200 7 3613 7 87154 1 3621 4 87107 5 3629 2 87061 0	4085 0 84491 7 4093 3 84447 9 4101 5 84404 3 4109 8 84360 6	4584 7 81986 1 4593 4 81944 9 4602 1 81903 7 4610 8 81862 6 4619 6 81821 5	5140 0 79503 4 5149 2 79464 6 5158 4 79425 7	5687 4 77305 8 5697 1 77268 9 5706 8 77232 0 5716 4 77195 2 5726 1 77158 4	35 34 33 32 31
30 31 32 33 34	3636 9 87014 6 3644 7 86968 2 3652 5 86921 9 3660 3 86875 6 3668 1 86829 4	4126 3 84273 5 4134 6 84230 0 4142 8 84186 5 4151 1 84143 1	4628 3 81780 4 4637 1 81739 4 4645 8 81698 4 4654 6 81657 5 4663 4 81616 6	5167 6 79386 9 5176 9 79348 1 5186 1 79309 4 5195 4 79270 7 5204 6 79232 1	5735 8 77121 6 5745 6 77084 9 5755 3 77048 2 5765 0 77011 5 5774 7 76974 8	30 29 28 27 26
35 36 37 38 39	3675 9 86783 2 3683 7 86737 0 3691 6 86690 9 3699 4 86644 9 3707 2 86598 9	4167 7 84056 5 4176 1 84013 2 4184 4 83969 9 4192 7 83926 8	4689 7 81494 1 4698 5 81453 4 4707 4 81412 6	5213 9 79193 4 5223 2 79154 8 5232 4 79116 3 5241 7 79077 8 5251 0 79039 3	5784 5 76938 2 5794 2 76901 6 5804 0 76865 1 5813 8 76828 5 5823 6 76792 1	25 24 23 22 21
40 41 42 43 44	3715 1 86553 0 3723 0 86507 1 3730 8 86461 3 3738 7 86415 5 3746 6 86369 7	4209 4 83840 5 4217 7 83797 5 4226 1 83754 4 4234 5 83711 5	4725 0 81331 4 4733 8 81290 8 4742 7 81250 2 4751 6 81209 7	5260 3 79000 8 5269 6 78962 4 5279 0 78924 0 5288 3 78885 7 5297 6 78847 4	5833 3 76755 6 5843 1 76719 2 5852 9 76682 8 5862 8 76646 4 5872 6 76610 1	20 19 18 17 16
45 46 47 48 49	3754 5 86324 0 3762 4 86278 4 3770 3 86232 8 3778 2 86187 2 3786 1 86141 8	4251 2 83625 7 4259 6 83582 8 4268 0 83540 0 4276 5 83497 3	4769 3 81128 8 4778 2 81088 4 4787 1 81048 1 4796 0 81007 7	5307 0 78809 I 5316 3 78770 9 5325 7 78732 6 5335 I 78694 5 5344 4 78656 3	5911 9 76465 1 5921 8 76428 9	15 14 13 12 11
50 51 52 53 54	3794 I 86096 3 3802 0 8605 0 9 3809 9 86005 6 3817 9 85960 2 3825 9 85915 0 3833 8 85869 8	4293 3 83411 9 4301 7 83369 3 4310 2 83326 7 4318 6 83284 1	4822 7 80887 0 4831 6 80846 8 4840 6 80806 7	5353 8 78618 2 5363 2 78580 2 5372 6 78542 1 5382 0 78504 1 5391 5 78466 2	5931 6 76392 7 5941 5 76356 6 5951 4 76320 5 5961 3 76284 5 5971 2 76248 5	10 8 7 6
55 56 57 58 59 60	3833 8 85809 8 3841 8 85824 6 3849 8 85779 5 3857 8 85734 5 3865 8 85689 4 3873 8 85644 5	4344 0 83156 8 4352 5 83114 4	4849 5 80766 6 4858 5 80726 6 4867 4 80686 6 4876 4 80646 6 4885 4 80606 7 4894 3 80566 8	5400 9 78428 2 5410 3 78390 3 5419 8 78352 5 5429 2 78314 6 5438 7 78276 8 5448 1 78239 1	5981 1 76212 5 5991 0 76176 5 6000 9 76140 6 6010 9 76104 7 6020 8 76068 8 6030 7 76033 0	5 4 3 2 1
	Alt. Hour Angle	Alt. Hour Angle	Alt. Hour Angle	Alt. Hour Angle	Alt. Hour Angle	
	74° 344°	73° 343°	72° 342°	71° 341°	70° 340°	

	20	0	21	r°	2:	2°	2;	3°	2	4°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	6040 7 6050 6 6060 6	76033 0 75997 2 75961 4 75925 6 75889 9	6652 4 6662 8 6673 3	73936 7 73902 6 73868 6 73834 6 73800 6	7281 6 7292 5 73°3 4 7314 3 7325 3	71940 1 71907 6 71875 2 71842 7 71810 3		7°°34 5 7°°°3 4 69972 4 69941 4 69910 5	8645 4 8657 3 8669 1 8681 0 8692 8	68212 1 68182 4 68152 7 68123 1 68093 4	60 59 58 57 56
56 78 9	6080 6 6090 6 6100 6 6110 6	75854 2 75818 6 75783 0 75747 4 75711 8	6694 2 6704 6 6715 1 6725 6	73766 6 73732 7 73698 8 73664 9 73631 1	7336 2 7347 1 7358 1 7369 0 7380 0	71778 0 71745 6 71713 3 71681 0 71648 7	8006 4 8017 8 8029 3 8040 7 8052 1	69879 5 69848 6 69817 7 69786 8 69756 0	8704 7 8716 6 8728 5 8740 3 8752 2	68063 8	55 54 53 52 51
10 11 12 13 14	6130 6 6140 7 6150 7 6160 7	75676 3 75640 8 75605 3 75569 8	6746 6 6757 I 6767 6 6778 I	73597 3 73563 5 73529 7 73496 0	7391 0 7401 9 7412 9 7423 9 7434 9	71616 4 71584 2 71552 0 71519 8 71487 6	8063 6 8075 0 8086 5 8097 9 8109 4	69725 2	8764 2 8776 1	679160	50 49 48 47
15 16 17 18	6180 9 6190 9 6201 0 6211 1	75534 4 75499 0 75463 7 75428 3 75393 1 75357 8	6799 2 6809 8 6820 3 6830 9	734 ⁶ 2 3 734 ² 8 6 73394 9 733 ⁶ 1 3 733 ² 7 7 73 ² 94 1	7445 9 7445 9 7457 0 7468 0 7479 0 7490 1	71455 5 71423 4 71391 3 71359 2 71327 2	8120 9 8132 4 8143 9	69571 3 69540 7 69510 0 69479 3	8823 8 8835 7 8847 7 8859 7	67768 7 67739 3 67710 0 67680 6 67651 3	46 45 44 43 42 41
20 21 22 23 24	6231 3 7 6241 4 7 6251 5 7 6261 7	75322 5 75322 5 75287 3 75252 2 75217 0 75181 9	6852 0 6862 6 6873 2 6883 8	73260 5 73227 0 73193 5 73160 1 73126 6	7501 1 7512 2 7523 2	71295 2 71263 2 71231 2 71199 3	8178 4	69418 1 69387 5 69357 0	8883 6 8895 6	67622 0 67592 7 67563 4 67534 2	40 39 38 37 36
25 26 27 28 29	6281 9 6292 I 6302 3 6312 4	75146 8 75111 7 75076 7 75041 7 75006 7	6905 0	73093 2 73059 8 73026 4 72993 1 72959 8	7556 5 7567 6 7578 7 7589 8 7600 9	71135 5 71103 6 71071 8 71040 0	8236 I 8247 7 8259 2 8270 8 8282 4	69265 4	8943 6 8955 7 89 ⁶ 7 7	67475 7 67446 6	35 34 33 32 31
30 31 32 33 34	6332 8 6343 0 6353 2 6363 4	74971 8 74936 9 74902 0 74867 1 74832 3	6958 2 6968 9 6979 6 6990 3	72926 5 72893 3 72860 0 72826 8 72793 6	76120 76232 76343 76455 76566	70976 4 70944 7 70913 0 70881 3 70849 6	8294 0 8305 6 8317 2 8328 8 8340 4	69113 3	90159	67330 0 67300 9 67271 9 67242 8	30 29 28 27 26
35 36 37 38 39	6383 8 6394 0 6404 3 6414 5	74797 5 74762 7 74728 0 74693 3 74658 6	70116	72760 5 72727 4 72694 3 72661 2	7667 8 7679 0 7690 2 7701 3 7712 5	70818 0 70786 3 70754 7 70723 2 70691 6	8352 1 8363 7 8375 4 8387 0 8398 7	68901 3	9064 3 9076 4 9088 5 9100 6	67155 8 67126 9 67097 9	22
40 41 42 43 44	6435 0 6445 3 6455 6 6465 9	74623 9 74589 3 74554 7 74520 1 74485 6		72595 I 72562 I 72529 2 72496 2	7723 8 7735 0 7746 2 7757 4 7768 7	70597 I	8410 4 8422 0 8433 7 8445 4 8457 1	68780 6 68750 5 68720 4	9137 c 9149 2 9161 3	66982 4 66953 5	19 18
45 46 47 48 49	6486 5 6496 8 6507 1 6517 4	74451 0 74416 6 74382 1 74347 7 74313 3	71190 71298 71406 71514	7243° 4 72397 5		70408 7	8468 8 8480 6 8492 3 8504 0 8515 8	68630 2 68600 2 68570 3	9197 9 9210 0 9222 2	66780 9	14 13 12 11
50 51 52 53 54	6538 1 6548 5 6558 8 6569 2	74278 9 74244 6 74210 2 74175 9 74141 7	7173 ° 7183 9 7194 7 72°5 5 7216 4	72233 6 72200 9 72168 2	7847 5 7858 8 7870 1 7881 5	70283 6 70252 4 70221 2	8562 8 8574 6	68480 4 68450 5 68420 7 68390 8	9258 9 9271 1 9283 3 9295 6	66723 6 66694 9 66666 3 66637 6	9 8 7 6
55 56 57 58 59 60	6600 3 6610 7 6621 1 6631 5	74107 4 74073 2 74039 I 74004 9 73970 8	7259 8 7270 7	72070 3 72037 7 72005 2 71972 6	7892 8 7904 1 7915 4 7926 8 7938 1 7949 5	70158 8 70127 7 70096 6 70065 5	8610 0 8621 8	68331 1 68301 4 68271 6 68241 8	9320 I 9332 4 9344 6 9356 9	66580 5 66551 9 66523 3 66494 8	4 3 2
00	6642 0 Alt.	73936 7 Hour	7281 6 Alt.	Hour	Alt.	Hour	Alt.	Hour Angle	Alt.	Hour Angle	
	69°	Angle 339°	68°	Angle 338°	67°	Angle 337°	66°	336°	65°	335°	′

	2	5°	20	5°	2	7°	2	8°	20	o° l	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 I 2	9369 2 9381 5 9393 8	66466 3 66437 8 66409 4	10133 3	64763 8 64736 5	10912 6	63181 5 63155 2 63128 9	11718 9 11732 6	61607 2 61581 8	12552 I 12566 2	60140 0 60115 6 60091 2	60 59 58
3 4 5 6	9406 1 9418 5 9430 8 9443 1	66380 9 66352 5 66324 1 66295 7	10171 7 10184 4 10197 2	64681 9 64654 6 64627 4	10952 2 10965 5 10978 7	63102 6 63076 4 63050 1 63023 9	11759 9 11773 6 11787 3	61556 5 61531 3 61506 0 61480 8	12594 5 12608 6	60066 8 60042 5 60018 1 59993 8	57 56 55 54
7 8 9	9455 5 9467 8 9480 2	66267 4 66239 0 66210 7 66182 4	10210 0 10222 8 10235 7 10248 5	64572 9 64545 7	11005 2	62997 7 62971 5 62945 4	11814 7 11828 4	61430 3 61405 1	12636 9 12651 1 12665 2 12679 4	59969 4 59945 1 59920 8 59896 5	55 54 53 52 51
10 11 12 13 14	9492 5 9504 9 9517 3 9529 7 9542 1	66154 1 66125 8 66097 6 66069 3	10261 3 10274 2 10287 0	64491 3 64464 2	11045 1 11058 4 11071 7	62919 2 62893 1 62867 0 62840 9 62814 8	11855 9 11869 6 11883 4		12693 6 12707 8 12722 0	59872 3 59848 0 59823 8	50 49 48 47 46
15 16 17 18	9554 5 9566 9 9579 3 9591 7	66041 1 66012 9 65984 8 65956 6	10312 7 10325 6 10338 5 10351 4	64382 8 64355 7 64328 7 64301 6	11098 3 11111 6 11124 9 11138 3	62788 7 62762 7 62736 6 62710 6	11910 9 11924 7 11938 5 11952 3	61254 2 61229 1 61204 1 61179 0	12750 4 12764 6 12778 8	59775 3 59751 1 59726 9 59702 8	45 44 43 42
19 20 21 22	9604 2 9616 6 9629 1 9641 5	65928 5 65900 4 65872 3 65844 2	10364 2 10377 1 10390 1 10403 0	64274 6 64247 6 64220 6 64193 6	11151 6 11165 0 11178 3 11191 7	62684 6 62658 6 62632 6 62606 7	11966 1 11979 9 11993 7 12007 5	61078 9	12821 6 12835 8 12850 1	59678 6 59654 5 59630 3 59606 2	41 40 39 38
23 24 25 26	9654 0 9666 5 9678 9 9691 4	65816 1 65788 1 65760 1 65732 1	10428 8 10441 8 10454 7	64166 7 64139 7 64112 8 64085 9	11218 5 11231 8 11245 2	62580 8 62554 8 62528 9 62503 0	12035 1 12049 0 12062 8	61053 9 61028 9 61004 0 60979 0	12878 6 12892 9 12907 2	59509 9	37 36 35 34
27 28 29 30	9703 9 9716 4 9728 9 9741 5	65704 I 65676 I 65648 2 65620 3		64059 0 64032 2 64005 3 63978 5	11272 1 11285 5	62477 2 62451 3 62425 5 62399 7	12090 5 12104 4	60954 1 60929 2 60904 3 60879 4	12935 8 12950 1 12964 4	59485 9 59461 8 59437 8 59413 8	33 32 31 30
31 32 33 34		65592 4 65564 5 65536 6 65508 8	10532 5 10545 5 10558 5	63898 1 63871 3	11325 8 11339 2 11352 7		12146 1 12160 0 12173 9	60829 7 60804 9 60780 1	12993 1 13007 4 13021 8	59389 8 59365 9 59341 9 59318 0	29 28 27 26
35 36 37 38 39	9816 7 9829 3 9841 9	65480 9 65453 1 65425 3 65397 6 65369 8	10571 6 10584 6 10597 6 10610 6 10623 7	638178	11379 6 11393 1 11406 6	62270 8 62245 1 62219 4 62193 7 62168 0	12201 7 12215 6 12229 6	60730 5	13050 5 13064 9 13079 3	59246 2	
40 41 42 43	9867 1 9879 7 9892 3 9904 9	65342 1 65314 3 65286 6 65259 0	10636 7 10649 8 10662 9 10675 9	63711 1 63684 4 63657 8 63631 2	11433 6 11447 1 11460 6 11474 2	62142 3 62116 7 62091 1 62065 4	12257 5 12271 4 12285 4 12299 4	60631 5 60606 8 60582 1 60557 4	13108 0 13122 4 13136 8 13151 3	59174 6 59150 8 59126 9 59103 1	20 19 18 17
44 45 46 47 48	9930 2 9942 8 9955 5	65231 3 65203 7 65176 0 65148 4 65120 8	10702 1 10715 2 10728 3	63578 0	11501 2 11514 8 11528 3	62039 9 62014 3 61988 7 61963 2 61937 6	12327 3 12341 3 12355 3	60508 I	13180 1 13194 6 13209 0	59055 5 59031 8 59008 0	16 15 14 13
50 51 52	9980 8 9993 5 10006 1	65093 3 65065 7	10754 5 10767 7 10780 8	63471 9 63445 4 63419 0	11555 5 11569 0 11582 6	61912 1 61886 6	12383 3 12397 4 12411 4	60409 6 60385 0 60360 5	13237 9 13252 4 13266 9	58960 5 58936 8 58913 1	10
53 54	10031 5 10044 2 10056 9		10807 1 10820 2 10833 4	63366 I 63339 6 63313 2	11609 8 11623 4 11637 0	61810 2 61784 8 61759 4 61733 9	12439 5 12453 5 12467 6	60311 4 60286 8 60262 3 60237 9	13295 8 13310 3 13324 8	58865 7 58842 1 58818 4 58794 8	9 8 7 6 5 4
55 56 57 58 59 60		64873 4 64846 0 64818 6	10859 8 10872 9 10886 1	63260 5	11664 3 11677 9 11691 6	61708 6 61683 2 61657 8 61632 5	12495 8 12509 8 12523 9	602134	13353 9 13368 4 13382 9	58771 2	3 2 1
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	64°	334°	63°	333°	62°	332°	61°	331°	60°	330°	

	3	o°	3	ı°	3	2°	3	3°	3	4°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	13397 5 13412 0 13426 6 13441 1 13455 7	58700 4 58676 8 58653 3 58629 7 58606 2	14298 3 14313 2 14328 2	57287 3 57264 6 57241 8	15195 2 15210 6 15226 0 15241 5 15256 9	55944 I 55922 2 55900 2	16148 8	54623 2 54601 9	17096 2 17112 5 17128 8 17145 1 17161 4	53406 5 5338 5 8 53365 2 53344 5 53323 9	60 59 58 57 56
56 78 9	13470 3 13484 9 13499 4 13514 0 13528 7	585827 585592 585357	14358 3 14373 3 14388 3 14403 4	57196 4 57173 7	152 72 3 15287 8 15303 3	55856 2 55834 2 55812 3 55790 4	16212 2 16228 1 16244 0	54559 3 54538 1 54516 8 54495 6	17177 7 17194 0 17210 3 17226 6	533°3 3 53282 7 53262 1 53241 5	55 54 53 52
10 11 12 13	13543 3 13557 9 13572 5 13587 2	58465 3 58441 9 58418 5 58395 1	14433 4 14448 5 14463 6 14478 6	57083 0 57060 3 57037 7 57015 1	15349 7 15365 2 15380 7 15396 2	55746 5 55724 6 55702 7 55680 8	16291 7 16307 6 16323 6 16339 5	54410 7 54389 6	17259 3 17275 6 17291 9 17308 3	53221 0 53200 4 53179 8 53159 3 53138 8	51 50 49 48 47
14 15 16 17 18	13601 8 13616 4 13631 1 13645 8 13660 4	58278 3	14508 8 14523 9 14539 0 14554_1	56902 2	15411 7 15427 2 15442 7 15458 3 15473 8	55593 4 55571 6	16387 3 16403 3 16419 3	543°4 9 54283 8		53118 3 53097 8 53077 3 53056 8 53036 3	46 45 44 43 42
20 21 22 23	13675 1 13689 8 13704 5 13719 2 13733 9	58208 3 58185 0 58161 8	14599 5 14614 6 14629 8	567896	15536 o 15551 6	55528 0 55506 2 55484 5 55462 7	16467 2 16483 2 16499 2	54220 5 54199 4 54178 3	17406 6 17423 0 17439 4 17455 8 17472 2	53015 8 52995 4 52974 9 52954 5 52934 1	40 39 38 37 36
24 25 26 27 28	13807 6	58045 6	14705 6	56677 4		55375 8 55354 I		54157 3 54136 2 54115 2 54094 2 54073 2	17538 0 17554 4	52913 7 52893 3 52872 9 52852 5 52832 1	35 34 33 32
30 31 32 33	13881 4	58022 4 57999 3 57976 1 57953 0 57929 8	14751 2 14766 4 14781 6	56610 2 56587 8 56565 4	15692 1 15707 8	55289 1 55267 4 55245 8	16643 5 16659 6	54052 2 54031 2 54010 2 53989 2 53968 3	17603 9 17620 3 17636 8	52811 8 52791 4 52771 1 52750 8 52730 5	31 30 29 28 27 26
34 35 36 37 38	13925 8 13940 6 13955 4	57860 5 57837 4 57814 3	14827 3 14842 5 14857 8	56476 1 56453 8	15770 4 15786 1	551377	16724 0 16740 1	53947 3 53926 4 539°5 4 53884 5 53863 6	177194	52710 2 52689 9 52669 6 52649 3 52629 0	25 24 23 22
39 40 41 42 43	14029 6	57745 2 57722 2 57699 2	14888 3 14903 6 14918 9 14934 2	56409 2 56386 9 56364 7 56342 4	15817 5 15833 2 15848 9 15864 6		16772 3 16788 5 16804 6 16820 7	53842 7 53821 8 53801 0 53780 1 53759 3	17735 9 17752 5 17769 0 17785 6 17802 2	52527 9	21 20 19 18 17
44 45 46 47 48	14059 4 14074 2 14089 1 14104 0	57653 2 57630 3 57607 3 57584 4	14964 8 14980 1 14995 4 15010 7	56298 0 56275 8 56253 6 56231 4	15911 8 15927 6 15943 3	54987 ° 54965 5 54944 ° 54922 5	16869 2 16885 4 16901 6	53717 6 53696 8 53676 0 53655 2	17835 3 17851 9 17868 5 17885 1	52467 3 52447 I 52427 0	16 15 14 13 12
50 51 52 53 54	14133 8 14148 7 14163 6 14178 6	57538 5 57515 6 57492 7 57469 9	15041 4 15056 7 15072 1 15087 5	561428 561207	15974 9 15990 6 16006 4 16022 2	548154	16950 1 16966 3 16982 6	53613 6 53592 8 53572 1 53551 4	17901 7 17918 3 17934 9 17951 5 17968 2	52406 8 52386 7 52366 5 52346 4 52326 3	11 10 9 8 7 6
54 55 56 57 58 59 60	14208 4 14223 4 14238 4 14253 3	5737 ⁸ 5 57355 7	15118 2 15133 6 15149 0 15164 4	56032 3	160538 160696 160854 161013	54794 ° 54772 6 54751 2 54729 8 54708 5 54687 1	17031 2 17047 5 17063 7	53509 9 53489 2 53468 5 53447 8	18001 5 18018 1 18034 8	52306 2 52286 1 52266 0 52246 0 52225 9 52205 9	5 4 3 2 1
60	14283 3	57332 9 57310 1 Hour	15195 2	55988 2 55966 2 Hour	16132 9	54687 1 54665 8 Hour	17096 2		180848	Hour	0
	Alt.	Angle	Alt.	Angle	Alt.	Angle	Alt.	Angle	Alt.	Angle	1
	59°	329°	58°	328°	57°	327°	56°	326°	55°	325°	

	3	5°	3	6°	3	7°	3	8°	3	9°	
′	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	18101 5 18118 2 18134 9	52185 8 52165 8 52145 8 52125 8 52105 8	19132 5	50982 3 50962 9 50943 5	20154 0 20171 5 20189 0	49795 8	21 21 6 8 21234 8	48717 5 48699 1 48680 8	22303 7 22322 0	47650 5 47632 6 47614 8 47597 0 47579 2	60 59 58 57 56
5 6 7 8	18168 3 18185 0 18201 8 18218 5	52085 8 52065 8 52045 8 52025 9	19183 9 19201 0 19218 1 19235 3	50904 7 50885 3 50865 9 50846 5	20224 1 20241 6 20259 2 20276 7	49758 1 49739 3 49720 4 49701 6	21288 6 21306 5 21324 4 21342 4	48644 2 48625 9 48607 6 48589 3	22377 0 22395 4 22413 7 22432 I	47561 4 47543 6 47525 8 47508 0	55 54 53 52
9 10 11 12 13	18252 0 18268 7 18285 5 18302 3	51926 2	19269 6. 19286 8. 19304 0. 19321 1	50788 5	20311 8 20329 4 20347 0 20364 6	49664 0 49645 2 49626 5 49607 7	21378 3 21396 3 21414 3 21432 3	48498 1	22468 8		51 50 49 48 47
14 15 16 17 18	18369 4		19372 7	50730 5 50711 2 50691 9 50672 7 50653 4	20399 8 20417 4 20435 0	49570 2 49551 5 49532 7	21486 3 21504 3 21522 4	48461 6 48443 4 48425 2 48407 0	22597 6 22616 0	47401 6 47383 8 47366 1 47348 4 47330 7	46 45 44 43 42
20 21 22 23	18419 9 18436 7 18453 5		19441 6 19458 9 19476 1	50595 6 50576 4	20487 9 20505 6 20523 2	49457 9 49439 2	21558 4 21576 5 21594 5	48388 8 48370 6 48352 5 48334 3 48316 2	22689 7	47313 0 47295 4 47277 7 47260 0 47242 4	40 39 38 37
24 25 26 27 28	18520 9 18537 8	51707 9 51688 1 51668 4 51648 6 51628 8	19527 9 19545 2 19562 4	50499 5 50480 4	20576 2 20593 9 20611 6	49383 2 49364 6 49345 9	21666 8 21684 9	48279 9 48261 8 48243 6	22726 6 22745 1 22763 6 22782 1 22800 5	47224 7 47207 1 47189 5 47171 8 47154 2	36 35 34 33 32
30 31 32 33	18588 4 18605 3 18622 2	51609 1 51589 3 51569 6 51549 9 51530 2	19614 3	50442 0 50422 8 50403 7	20647 0 20664 7 20682 4 20700 I	493 ⁰⁸ 7 49 ² 90 1 49 ² 71 5 49 ² 52 9	21721 1 21739 2 21757 3 21775 4		228190 228375 228560 228746	47136 6 47119 0 47101 4 47083 9 47066 3	31 30 29 28 27
34 35 36 37 38	18673 0 18689 9	51510 5 51490 8 51471 1 51451 5 51431 8	19700 9 19718 2 19735 6	50346 3 50327 2 50308 1 50289 0 50269 9	20753 3 20771 0 20788 8	49178 6 49160 0	21829 8 21848 0 21866 1	48117 1 48099 0 48081 0 48062 9 48044 9	22930 I 22948 7 22967 2	47048 7 47031 2 47013 6 46996 1 46978 5	26 25 24 23 22
39 40 41 42 43	18740 8 18757 7 18774 7 18791 6 18808 6	51392 5	19822 4		20842 I 20859 9 20877 6	49104 4 49085 9 49067 4	21920 6 21938 8 21957 0	48026 9 48008 9 47990 9 47972 9 47954 9	23022 9 23041 5 23060 0	46961 0 46943 5 46926 0 46908 5 46891 0	21 20 19 18 17
44 45 46 47 48	18842 6 18859 6 18876 6 18893 6	51255 3	19874 6 19892 0 19909 4 19926 9	50117 5 50098 5 50079 6	20931 0 20948 8 20966 7 20984 5	49012 0 48993 5 48975 0 48956 6	22011 6 22029 8 22048 0 22066 2	47901 0 47883 1 47865 1	23115 8 23134 4 23153 0 23171 6	46821 1 46803 7	16 15 14 13 12
50 51 52 53	18910 6 1892 7 7 18944 7 18961 7 18978 8	51216 2 51196 6 51177 1 51157 6 51138 1	19944 3 19961 7 19979 2 19996 6 20014 1	50060 6 50041 6 50022 6 50003 7 49984 7	21002 3 21020 2 21038 0 21055 9 21073 7	48938 I 48919 7 48901 3 48882 8 48864 4	22084 4 22102 7 22120 9 22139 2 22157 4	47847 2 47829 3 47811 3 47793 4 47775 5	23190 3 23208 9 23227 5 23246 2 23264 8	46786 2 46768 8 46751 3 46733 9 46716 5	11 10 9 8 7 6
54 55 56 57 58 59 60	18995 8 19012 9 19030 0 19047 0 19064 1	51118 6 51099 1 51079 6 51060 1 51040 7	20031 5 20049 0 20066 5 20084 0 20101 5	49965 8 49946 9 49927 9 49909 0 49890 1	211091 6 21109 5 21127 3 21145 2 21163 1	48846 0 48827 6 48809 3 48790 9 48772 5	22175 7 22194 0 22212 2 22230 5 22248 8	47757 6 47739 8 47721 9 47704 0 47686 2	23283 5 23302 1 23320 8 23339 5 23358 2	46699 1 46681 7 46664 3 46646 9 46629 6	5 4 3 2
59 60		51021 2 51001 8	20118 9 20136 4	49852 4	211810	48735 8	22267 I 22285 4	47668 3 47650 5	23376 9 23395 6	46612 2 46594 8	0 —
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	54°	324°	53°	323°	52°	322°	51°	321°	50°	320°	

	4	o°	4	ı°	4	2 °	4.	3°	4	4°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 I 2 3	23433 0	46594 8 46577 5 46560 1 46542 8	24567 2	455 ⁶ 7 5 45550 6 45533 7 45516 8	25705 0 25724 5	44534 2	26864 6 26884 5 26904 3 26924 2	43560 4	28086 2 28106 4	426112	60 59 58 57
4 5 6 7 8	23489 I 23507 9 23526 6	46490 8 46473 5	24624 5 24643 7 24662 8		25782 9 25802 4 25821 9	44484 9 44468 5 44452 I	26983 8 27003 7	43512 4 43496 4 43480 4	28167 1 28187 4 28207 6	42564 4 42548 8 42533 2	56 55 54 53
9 10 11 12	23564 I 23582 9 23601 6	46439 0 46421 7 46404 4	24681 9 24701 1 24720 2 24739 4 24758 5	454 ¹ 5 7 4539 ⁸ 9 453 ⁸ 2 1	25860 9 25880 5 25900 0	44419 3 44402 9 44386 5	27043 4 27063 3 27083 2	43448 4 43432 4 43416 5	28268 4 28288 7	42502 0 42486 4 42470 9	52 51 50 49 48
13 14 15 16	23639 2 23658 0 23676 8 23695 6	46369 9 46352 6 46335 4 46318 2	24777 7 24796 8 24816 0 24835 2	45348 5 45331 7 45314 9 45298 1	25939 1 25958 6 25978 2 25997 7	44353 8 44337 4 44321 1	27123 0 27143 0 27162 9	43384 6 43368 6 43352 7	28329 2 28349 5 28369 8	424398	47 46 45 44
17 18 19 20	23714 4 23733 2 23752 0 23770 8	46300 9 46283 7 46266 5 46249 3	24854 4 24873 6 24892 8 24912 0	45281 3 45264 6 45247 8 45231 1	26017 3 26036 9 26056 5 26076 1	44288 4 44272 0 44255 7 44239 4	27202 8 27222 7 27242 7 27262 6	43320 8 43304 9 43289 0 43273 I	28410 4 28430 7 28451 0 28471 4	42377 6 42362 1 42346 6 42331 1	43 42 41 40
21 22 23 24 25	23808 5 23827 3 23846 2	46214 9 46197 7	24988 9	45197 6 45180 9	26115 2 26134 9 26154 5	44206 8 44190 5	27322 5 27342 5	43241 3 43225 4	28512 0 28532 4	42300 I 42284 6	39 38 37 36 35
26 27 28 29	23883 9 23902 8 23921 6 23940 5	46146 2 46129 1 46112 0 46094 8	25027 4 25046 6 25065 9	45130 7 45114 0	26193 7 26213 3 26233 0 26252 6	44141 7 44125 4 44109 1 44092 9	27382 5 27402 5 27422 5 27442 5	43177 8	28593 4 28613 8 28634 2 28654 6	42238 2 42222 7 42207 3 42191 8	34 33 32 31
30 31 32 33 34	23959 4 23978 3 23997 2 24016 1 24035 0	46043 5 46026 4	25123 7 25143 0	45064 0 45047 3 45030 7 45014 0 44997 4	26291 9 26311 6 26331 3	44044 2 44027 9	27462 6 27482 6 27502 6 27522 7 27542 7	43082 8 43067 0	287157 287361	42160 9 42145 5	30 29 28 27 26
35 36 37 38 39	24053 9 24072 9 24091 8 24110 7 24129 7	45958 o 45941 o		44964 I 44947 5 44930 8	26390 3 26410 0 26429 7	43963 1	27562 8 27582 8 27602 9 27622 9 27643 0	43003 8	28817 8 28838 3	420530	25 24 23 22 21
40 41 42 43	24148 6 24167 6 24186 6 24205 5	45906 9 45889 8 45872 8 45855 8	25297 5	44897 6 44881 0 44864 4 44847 9	26469 I 26488 8 26508 5 26528 3	43914 5 43898 4 43882 2 43866 1	27663 I 27683 2 27703 3 27723 4	42956 5 42940 7 42924 9 42909 2	28879 1 28899 6 28920 1 28940 5	42022 3 42006 9 41991 5 41976 2	20 19 18 17 16
44 45 46 47 48	24243 5 24262 5 24281 5 24300 5	45821 7 45804 7 45787 7 45770 7	25394 3 25413 6 25433 0 25452 4	44814 7 44798 2 44781 6 44765 1	26567 7 26587 5 26607 3 2662 7 0	43833 8 43817 6 43801 5 43785 4	27763 6 27783 7 27803 8 27824 0	42877 7 42862 0 42846 3 42830 5	28981 5 29001 9 29022 4 29042 9	41945 5 41930 1 41914 8 41899 5	15 14 13 12
49 50 51 52	24319 5 24338 5 24357 5 24376 6	45753 8 45736 8 45719 8 45702 9	25471 8 25491 2 25510 6 25530 0 25549 4	4474 ⁸ 5 4473 ² 0 447 ¹ 5 5 44699 0	26646 8 26666 6 26686 3 26706 1	43769 3 43753 2 43737 1 43721 0	27844 I 27864 3 27884 4	42814 8 42799 1 42783 4 42767 7	29063 4 29083 9 29104 4 29125 0	41884 2 41868 8 41853 5 41838 2 41822 9	10 9 8
53 54 55 56 57 58 59 60	24414 6 24433 7 24452 8 24471 8	45669 0 45652 0 45635 1 45618 2	25568 8 25588 3 25607 7 25627 2	44665 9 44649 4 44633 0 44616 5	26745 7 26765 5 26785 3 26805 1	43688 8 43672 7 43656 7 43640 6	27944 9 27965 1 27985 2 28005 4	42736 4 42720 7 42705 0 42689 4	29166 0 29186 5 29207 1 29227 6	41807 6 41792 4 41777 1 41761 8	7 6 5 4 3 2
58 59 60	24490 9 24510 0 24529 0	45601 3 45584 4 45567 5	25646 6 25666 I	44600 0	26825 0 26844 8	43624 5	28025 6 28045 8 28066 0	42673 7 42658 I	29248 2 29268 8	41746 5 41731 3	2 I 0
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	49°	319°	48°	318°	47°	317°	46°	316°	45°	315°	

	4	5°	4	6°	4	7 °	4	8°	4	9°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	29309 9 29330 5	41716 0 41700 8 41685 5 41670 3 41655 1	30576 o 30597 o	40797 3 40782 4 40767 6	31821 4 31842 7 31864 0	39915 5	33108 6 33130 2 33151 8	39054 5	344160	38227 3 38213 4 38199 6 38185 7 38171 9	60 59 58 57 56
5 6 7 8 9	29392 2 29412 8 29433 4	41639 9 41624 6 41609 4 41594 2	30638 9 30659 8 30680 8	4°737 9 4°723 ° 4°7°8 2 4°693 3	31906 6 31927 9 31949 2 31970 5	39857 5 39843 0 39828 5 39814 0	33195 I 33216 7 33238 4 33260 I	38997 8 38983 6 38969 5	345°3 9 345°5 9 34547 9	38158 1 38144 2 38130 4 38116 6 38102 8	55 54 53 52 51
10 11 12 13 14	29495 3 29515 9 29536 6	41563 9 41548 7 41533 5	30743 7	40663 7 40648 9 40634 1 40619 3	32013 2 32034 5 32055 9 32077 2	39785 0 39770 5	33303 4 33325 1 33346 8 33368 4	38927 I 38912 9 38898 8 38884 7 38870 6	34613 9 34635 9 34657 9	38089 0 38075 2 38061 4 38047 6 38033 8	50 49 48 47 46
15 16 17 18	29598 5 29619 2 29639 9 29660 5	41488 0 41472 8 41457 7	30848 7 30869 7 30890 7 30911 8	405 ⁸ 9 7 40574 9 40560 1	32119 9 32141 3 32162 7 32184 0	39712 8 39698 3	33411 8 33433 5 33455 2	388 56 5 388 42 4 388 28 3 388 14 2 388 00 1	34724 0 34746 I 34768 I 34790 2 34812 2	38020 0 38006 2 37992 4 37978 7 37964 9	45 44 43 42 41
20 21 22 23 24	29701 9 29722 6 29743 3	41412 3 41397 2 41382 1 41366 9		40515 8 40501 0 40486 3 40471 5	32226 8 32248 2 32269 6	39640 6 39626 2	33520 4 33542 1 33563 9	38786 0 38772 0 38757 9	34 ⁸ 34 3 34 ⁸ 56 3	37951 2 37937 4 37923 7 37909 9 37896 2	40 39 38 37 36
25 26 27 28 29	29805 4 29826 1 29846 9	41336 7 41321 7 41306 6 41291 5	31059 I 31080 2 31101 3 31122 4 31143 4	40442 0 40427 3 40412 6 40397 9	32333 8 32355 2 32376 7	39568 7 39554 3 39539 9 39525 5 39511 2	33629 1 33650 9 33672 7	387157	34944 7 34966 8 34988 9	37882 5 37868 7 37855 0 37841 3 37827 6	35 34 33 32 31
30 31 32 33 34	29909 I 29929 8	41261 4 41246 3 41231 2 41216 2	31164 5	40368 5 40353 8 40339 1 40324 4	32441 0 32462 4 32483 9	39496 8 39482 4 39468 1 39453 8 39439 4	33738 o 33759 8	38645 5 38631 5 38617 5 38603 5 38589 5	35°55 2 35°77 3 35°99 4 35121 6	37813 9 37800 2 37786 5 37772 8 37759 1	30 29 28 27 26
35 36 37 38 39	30012 9 30033 7 30054 5	411861 411711 411561 411410	31270 I 31291 2 31312 4 31333 5	40295 0 40280 4	32548 3 32569 8 32591 2 32612 7	39425 I 39410 8 39396 5 39382 I 39367 8	33847 ° 33868 8	38575 5	35165 9 35188 0 35210 2 35232 3	37745 4 37731 8 37718 1 37704 4 37690 8	25 24 23 22 21
40 41 42 43 44	301377	410660	31397 0 31418 2	401778	32655 7 32677 2 32698 7 32720 3	39353 5 39339 2 39324 9 39310 7		38505 6 38491 6 38477 7 38463 7	35276 7 35298 8 35321 0 35343 2	37677 I 37663 5 37649 8 37636 2 37622 6	20 19 18 17 16
45 46 47 48 49	30241 8	41021 1 41006 2 40991 2	31481 7 31502 9 31524 1 31545 3 31566 5	40134 0 40119 4 40104 8	32784 9 32806 4	39267 8 39253 6 39239 3	34087 3 34109 2 34131 0	38421 9 38407 9	35409 8 35432 0 35454 2	37608 9 37595 3 37581 7 37568 1 37554 5	15 14 13 12
50 51 52 53 54	30387 8 30408 7	40946 4 40931 4 40916 5 40901 6	31587 7 31608 9 31630 2 31651 4 31672 6	40061 0 40046 4 40031 9	32892 6 32914 2 32935 8 32957 3	39196 6 39182 3	34218 6 34240 6	38352 3 38338 4 38324 5 38310 6	35520 9 35543 1 35565 4 35587 6	3754° 9 37527 3 37513 7 375° 1 37486 5	10 9 8 7 6
55 56 57 58 59 60	30492 3	40871 8 40856 9 40842 0 40827 1	31693 9 31715 1 31736 4 31757 6 31778 9 31800 2	39988 2 39973 6 39959 1 39944 6	33022 I 33043 7 33065 3	391113	34306 3 34328 3 34350 2 34372 I	38282 8 38268 9	35632 I 35654 4 35676 7 35699 0	37473 ° 37459 4 37445 8 37432 3 37418 7 374°5 2	5 4 3 2 1
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	44°	314°	43°	313°	42°	312°	41°	31 1°	40°	310°	

	5	o°	5	r°	5	2°	53	3°	5-	4°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	35721 2 35743 5 35765 8 35788 1 35810 4	37405 2 37391 6 37378 1 37364 6 37351 0	37068 0 37090 6 37113 2 37135 8 37158 4	36601 6 36588 3 36575 1 36561 9 36548 6	38456 8 38479 7 38502 6	35789 9	39841 7 39865 0 39888 2	35°47 3 35°34 6 35°21 9 35°°9 3 34996 6		34295 3 34282 9 34270 5 34258 2 34245 8	60 59 58 57 56
56 78 9	35832 7 35855 0	37337 5	37181 1 37203 7	36535 4 36522 2	38548 5 38571 5 38594 4 38617 4	35751 I 35738 2	39934 7 39958 0 39981 2 40004 5	34984 0 34971 3	41339 2 41362 8	34233 4 34221 0	55 54 53 52 51
10 11 12 13 14	35944 3 35966 7 35989 0 36011 4 36033 7	37270 0 37256 5	37 ² 94 3 373 ¹ 7 0 373 ³ 9 6 37 ³ 6 ² 3 37 ³ 8 ⁵ 0		38663 3 38686 3	35686 5 35673 6 35660 7 35647 8	40051 1 40074 4 40097 6	34920 8 34908 2 34895 6 34882 9	41457 1 41480 6 41504 2 41527 8	34171 6 34159 2 34146 9 34134 5	50 49 48 47 46
15 16 17 18	36056 1 36078 5 36100 8 36123 2 36145 6	37202 6 37189 1 37175 6 37162 2	374°7 7 3743° 3 37453° 37475 7 37498 4	36403 5	38778 3 38801 3	35622 1 35609 2 35596 3 35583 5	40167 5 40190 8 40214 2 40237 5 40260 8	34857 7 34845 1 34832 5 34820 0	41598 6	34122 2 34109 9 34097 5 34085 2 34072 9 34060 6	45 44 43 42 41
20 21 22 23 24	36168 0 36190 4 36212 8 36235 2 36257 6	37135 3 37121 8 37108 4 37095 0 37081 5	37521 1 37543 9 37566 6 37589 3 37612 0	36337 7 36324 6 36311 4	38893 3 38916 4 38939 4	35557 7 35544 9 35532 0 35519 2	40284 1 40307 5 40330 8	34794 8 34782 2	41693 1	34048 3 34036 0	40 39 38 37 36
25 26 27 28 29	36280 0 36302 4 36324 9 36347 3 36369 7	37068 I 37054 7 37041 3	37634 8 37657 5 37680 3 37703 0 37725 8	36272 0 36258 9	39008 5 39031 6	35493 5 35480 7 35467 9 35455 0	40400 9	34732 0 34719 4 34706 9	41811 4 41835 0	33986 8 33974 5 33962 2 33949 9	35 34 33 32 31
30 31 32 33 34	36392 2 36414 6 36437 1 36459 5 36482 0	37001 I 36987 7	37748 5 37771 3 37794 1 37816 9 37839 6	36206 5 36193 4	39123 9 39146 9 39170 0 39193 1 39216 2	35429 4 35416 6 35403 8 35391 0	40517 7 40541 1	34669 2 34656 7 34644 2	41929 7 41953 4 41977 1 42000 8	33925 4 33913 1 33900 9 33888 6	30 29 28 27 26
35 36 37 38 39	36504 5 36526 9 36549 4 36571 9 36594 4	36934 2 36920 8 36907 5 36894 1	37862 4 37885 2 37908 0 37930 8 37953 6	36141 1 36128 0 36114 9 36101 9 36088 8	39239 3 39262 4 39285 5 39308 6 39331 8	35352 6 35339 9 35327 I	40634 7 40658 1 40681 5 40704 9 40728 4	34594 I 3458 I 6 34569 I	42048 2 42071 9 42095 6 42119 3 42143 0	33851 9 33839 7 33827 4	25 24 23 22 21
40 41 42 43 44	36684 4		37976 5 37990 3 38022 I 38044 9 38067 8	360627	39378 0 39401 2 39424 3	35288 8 35276 0 35263 3	40751 8 40775 2 40798 7 40822 1 40845 6	34531 7 34519 2 34506 7	42190 5 42214 2 42238 0	33790 8 33778 6 33766 3	20 19 18 17 16
45 46 47 48 49	36729 5 36752 0 36774 5 36797 1	36800 8 36787 5 36774 1 36760 8	38090 6 38113 5 38136 3 38159 2 38182 0	36010 6 35997 6 35984 6 35971 6	39470 6 39493 8 39516 9	35237 8 35225 1 35212 3 35199 6	40892 5 40916 0	34481 8 34469 3 34456 9 34444 4	42285 5 42309 2 42333 0 42356 8	33729 7 33717 5 33705 4	15 14 13 12
50 51 52 53 54	36842 2 36864 7 36887 3 36909 8	36734 2	38204 9 38227 8 38250 6	35945 6 35932 6 35919 6 35906 6	39586 4 39609 6 39632 8	35174 2 35161 5 35148 8 35136 1	40986 4 41009 9 41033 4 41056 9 41080 4	34407 I 34394 6 34382 2	42475 7	33681 0 33668 8 33656 7	10 9 8 7 6
55 56 57 58 59 60	36955 0 36977 6 37000 2 37022 8 37045 4	36667 8 36654 6 36641 3 36628 1 36614 8	383193 383422 383651 383880 384109	35880 6 35867 6 35854 7 35841 7 35828 8	397°2 4 39725 6 39748 8 39772 ° 39795 3	35110 7 35098 0 35085 3 35072 6 35059 9	41103 9 41127 4 41150 9 41174 4 41197 9	34357 4 34344 9 34332 5 34320 I 34307 7	42523 3 42547 1 42570 9 42594 7 42618 5	33620 2 33608 0 33595 9 33583 7 33571 6	5 4 3 2 1
00	37°68°° Alt.	Hour	384 33 9 Alt.	Hour	39818 5 Alt.	35°47 3 Hour Angle	41221 5 ————————————————————————————————————	Hour Angle	42642 4 Alt.	Hour Angle	0
	39°	Angle 309°	38°	Angle 308°	37°	307°	36°	306°	35°	305°	_

	5.	5°	5	6°	5	7°	5	8°	5	9°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	42642 4 42666 2 42690 0 42713 9 42737 7	33547 3 33535 2 33523 I	44080 7 44104 8 44129 0 44153 1 44177.2	32827 2	45536 I 45560 5 45584 9 45609 3 45633 7	32133 7 32122 1 32110 5 32098 8 32087 2	47008 I 47032 7 47057 4 47082 I 47106 8	31442 9 31431 5 31420 1 31408 7 31397 3	48521 1 48546 1	30766 I 30755 0 30743 8 30732 6 3072I 5	60 59 58 57 56
5 6 7 8 9	42761 6 42785 4 42809 3 42833 1 42857 0	33474 6 33462 5	44201 3 44225 5 44249 6 44273 8 44297 9	32756 o 32744 2	45658 1 45682 6 45707 0 45731 4 45755 8	32052 4	47131 5 47156 2 47180 9 47205 6 47230 3		48620 9 48645 9 48670 8 48695 8 48720 8	30710 3 30699 2 30688 1 30676 9 30665 8	55 54 53 52 51
10 11 12 13 14	42880 9 42904 8 42928 6 42952 5 42976 4	33402 I 33390 O	44322 I 44346 3 44370 4 44394 6 44418 8	32685 0 32673 2	45804 7 45829 2 45853 6 45878 1	32006 0 31994 4 31982 8 31971 2	47279 7 47304 4 47329 I 47353 9	31306 4 31295 1 31283 7	4 ⁸ 795 7 4 ⁸⁸ 20 7 4 ⁸⁸ 45 7	306102	50 49 48 47 46
15 16 17 18 19	43072 0 43096 0	33377 9 33365 8 33353 8 33341 7 33329 7 33317 6	44515 6 44539 8		45951 5 45976 0 46000 4	31959 7 31948 1 31936 5 31925 0 31913 4 31901 8	47428 1	31272 4 31261 1 31249 7 31238 4 31227 1 31215 7	48895 7 48920 7 48945 7 48970 7	30599 I 30588 0 30576 9 30565 8 30554 7 30543 6	45 44 43 42 41 40
21 22 23 24 25	43143 8	33305 6 33293 5 33281 5 33269 5	44588 2 44612 4 44636 6 44660 8	32590 5 32578 7	46049 4 46073 9	31890 3 31878 7 31867 2 31855 7	47527 I 4755I 9	31204 4 31193 1 31181 8	49020 8 49045 8 49070 8 49095 9	30532 5 30521 4 30510 3 30499 3	39 38 37 36 35
26 27 28 29 30	43263 5 43287 5 43311 4 43335 4 43359 4	33245 4 33233 4 33221 4 33209 4	447093	32531 6	46171 9 46196 5	318326	476510	31147 9 31136 6 31125 3 31114 0	49145 9 49171 0 49196 0	30477 I	34 33 32 31 30
31 32 33 34		33185 3	448306	32472 8 32461 0 32449 3 32437 6 32425 8	46294 6	31775 0 31763 5 31752 0 31740 5 31729 0	47774 9 47799 8 47824 6 47849 4 47874 2	31091 5 31080 2 31068 9 31057 7	49271 2 49296 3 49321 4	30421 8 30410 8 30399 7 30388 7	29 28 27 26 25
35 36 37 38 39 40		33125 4 33113 4 33101 4 33089 5 33077 5	44951 9 44976 2 45000 5 45024 8	32414 1 32402 4 32390 6 32378 9 32367 2	46466 4 46491 0	31717 5 31706 0 31694 5 31683 0		31023 9 31012 7 31001 4	49421 7 49446 8	30366 6 30355 6 30344 6 30333 6 30322 5	24 23 22 21 20
41 42 43 44 45	43 ⁶ 95 5 43719 5	33053 6 33041 6 33029 7 33017 7	45146 4 45170 7	32343 8 32332 I 32320 4 32308 7	46589 3 46613 9 46638 5	31648 6 31637 2 31625 7 31614 2	48097 8 48122 7	30967 7 30956 5 30945 2 30934 0	49547 2 49572 3 49597 5 49622 6	30311 5 30300 5 30289 5 30278 5 30267 5	19 18 17 16
46 47 48 49 50	43743 6 43767 6 43791 7 43815 7 43839 8	33005 8 32993 9 32981 9 32970 0 32958 1	45195 0 45219 3 45243 7 45268 0	32297 0 32285 3 32273 6 32261 9 32250 2	46663 1 46687 8 46712 4 46737 0 46761 6	31602 8 31591 3 31579 9 31568 5	48147 5 48172 4 48197 3 48222 2 48247 1	30922 8 30911 6 30900 4 30889 2 30878 0	49 ⁶ 47 7 49 ⁶ 72 9 49 ⁶ 98 0 49723 1 49748 3	30256 5 30245 5 30234 6 30223 6	14 13 12 11
51 52 53 54 55	43887 9	32922 3 32910 4 32898 5	453898 454142	32226 9 32215 2 32203 6 32191 9	46810 9 46835 5 46860 1 46884 8	31534 2 31522 7 31511 3 31499 9	48296 9 48321 8 48346 7 48371 6	30844 4 30833 2 30822 0	49798 6 49823 8 49848 9 49874 1	30179 7 30168 7	98 76 54
55 56 57 58 59 60	44008 4 44032 5 44056 6	32851 0 32839 1	454 ⁶² 9 454 ⁸ 7 3 455 ¹¹ 7	32168 6 32157 0 32145 3 32133 7	46934 1 46958 7 46983 4	31477 1 31465 7 31454 3 31442 9	48421 4 48446 3 48471 3	30766 1	49924 4 49949 6 49974 8	30146 8 30135 8 30124 9 30113 9 30103 0	5 4 3 2 1 0
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	34°	304°	33°	303°	32°	302°	31°	301°	30°	300°	

1,				ı°	0.	2°	6	3°	6.	4	
	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3	50000 0 50025 2 50050 4 50075 6 50100 8	30081 I 30070 2	51519 0 51544 5 51569 9 51595 4	29431 7 29421 0	53052 8 53078 5 53104 2 53129 9	28795 0 28784 5	54600 9 54626 9 54652 8 54678 7 54704 6	28181 2 28170 9 28160 6	56162 9 56189 9 56215 2 56241 3 56267 5	27579 0 27568 9 27558 8 27548 7 27538 6	60 59 58 57 56
4 5 6 7 8	50126 0 50151 2 50176 4 50201 7	30048 3 30037 4 30026 5	51620 8 51646 3 51671 8 51697 2 51722 7	29399 5 29388 8 29378 1	53155 6 53181 3 53207 0 53232 7 53258 4	28763 5 28753 1 28742 6	54730 6 54756 5 54782 5 54808 4	28140 0 28129 7 28119 4	56293 7 56319 8 56346 0 56372 2	27528 5 27518 4	55 54 53 52
9 10 11 12	50226 9 50252 I 50277 4 50302 6	29993 8 29982 9 29972 0		29356 7 29346 I 29335 4 29324 7	53361 3	28711 I 28700 6 28690 2	54834 4 54860 3 54886 3 54912 2	28088 6 28078 3 28068 0	56398 3 56424 5 56450 7 56476 9	27488 2 27478 I 27468 0 27458 0	51 50 49 48
13 14 15 16 17	50327 8 50353 1 50378 3 50403 6 50428 9	29939 3 29928 4	51850 1 51875 6 51901 1 51926 6 51952 1	29303 3 29292 7 29282 0 29271 3	53387 1 53412 8 53438 5 53464 3 53490 0	28658 8 28648 3 28637 9	54964 2 54990 2 55016 1 55042 1	28047 5 28037 2 28027 0 28016 7	56503 1 56529 3 56555 5 56581 7 56607 9	27447 9 27437 8 27427 8 27417 7 27407 6	47 46 45 44 43
18 19 20 21 22	50454 I 50479 4 50504 7 50529 9 50555 2	29874 I	51977 6 52003 2 52028 7 52054 2 52079 7		53515 8 53541 5 53567 3 53593 1 53618 8	28616 9 28606 5 28596 1	55068 1 55094 1 55120 1 55146 1 55172 1	27996 2	56634 1 56660 3 56686 5 56712 7 56739 0	27397 6 27387 5 27377 5 27367 5 27357 4	42 41 40 39 38
23 24 25 26	50580 5 50605 8 50631 1 50656 4	29852 3 29841 5 29830 6 29819 8	52105 3 52130 8 52156 4 52181 9	29207 4 29196 8 29186 1 29175 5	53644 6 53670 4 53696 2 53722 0	28575 2 28564 8 28554 3 28543 9	55198 I 55224 I 55250 I 55276 I	27955 3 27945 I 27934 8 27924 6	56765 2 56791 4 56817 7 56843 9	27347 4 27337 4 27327 3 27317 3	37 36 35 34
27 28 29 30 31	50681 7 50707 0 50732 3 50757 6 50783 0	29798 I 29787 3 29776 4	52207 4 52233 0 52258 6 52284 I 52309 7		53747 7 53773 5 53799 3 53825 1 53850 9	28523 I 28512 7 28502 2	55302 I 55328 2 55354 2 55380 2 55406 2	27914 4 27904 2 27894 0 27883 8 27873 6	56870 1 56896 4 56922 6 56948 9 56975 1	273°7 3 27297 3 27287 2 27277 2 27267 2	33 32 31 30 29
32 33 34 35	50808 3 50833 6 50858 9 50884 3		52335 3 52360 8	29111 8 29101 2	53876 7 53902 6 53928 4 53954 2	28481 4 28471 0	55432 3 55458 3 55484 4 55510 4	27863 4 27853 2 27843 0 27832 8	57001 4 57027 7 57053 9 57080 2	27257 2 27247 2 27237 2 27227 2	28 27 26 25
36 37 38 39	50909 6 50935 0 50960 3 50985 7	29700 7 29689 9 29679 I	52437 6 52463 2 52488 8 52514 4	29069 4 29058 8 29048 2 29037 6	53980 0 54005 8 54031 7 54057 5	28429 5 28419 1 28408 7	55562 5 55588 6 55 ⁶ 14 7	27822 6 27812 4 27802 2 27792 0 27781 9	57106 5 57132 8 57159 0 57185 3 57211 6	27187 3	24 23 22 21 20
40 41 42 43 44	51011 0 51036 4 51061 7 51087 1 51112 5	29657 5 29646 7 29635 9 29625 I	52540 0 52565 6 52591 2 52616 8 52642 4	29005 9 28995 3 28984 7	54135 0 54160 9 54186 7	28377 6 28367 2 28356 8	55640 7 55666 8 55692 9 55719 0 55745 0	27771 7 27761 5 27751 3	57237 9 57264 2 57290 5 57316 8	27167 3 27157 3 27147 4 27137 4	19 18 17 16
45 46 47 48 49	51137 9 51163 3 51188 6 51214 0 51239 4	29603 6 29592 8 29582 I	52668 0 52693 7 52719 3 52744 9 52770 6	28963 6 28953 0 28942 5	54212 6 54238 5 54264 3 54290 2 54316 1	28336 I 28325 8 28315 4	55771 1 55797 2 55823 3 55849 4 55875 5	27731 0 27720 9 27710 7 27700 6 27690 4	57343 I 573 ⁶ 9 4 57395 7 57422 I 5744 ⁸ 4	27127 4- 27117 5 27107 5 27097 6 27087 6	15 14 13 12 11
50 51 52 53 54	51264 8 51290 2 51315 6 51341 0	29560 5 29549 8 29539 0 29528 3	52796 2 52821 8 52847 5 52873 1	28921 4 28910 8 28900 3 28889 7	54342 0 54367 8 54393 7 54419 6	28294 7 28284 4 28274 I 28263 7	55901 6 55927 7 55953 8	27680 3 27670 1 27660 0 27649 9 27639 7	57474 7 57501 0 57527 4 57553 7 57580 1	27077 7	10 9 8 7 6
55 56 57 58 59 60	51366 5 51391 9 51417 3 51442 7 51468 2	29506 8 29496 0 29485 3 29474 6	52924 5 52950 1 52975 8 53001 5	28879 2 28868 7 28858 1 28847 6 28837 1	54445 5 54471 4 54497 3 54523 2 54549 1	28222 4 28212 I	56032 2 56058 3 56084 5 56110 6	27629 6 27619 5 27609 4 27599 3	57606 4 57632 7 57659 1 57685 4	27028 0 27018 0 27008 1 26998 2	5 4 3 2
59 60	51493 6 51519 0		53 ⁰²⁷ 2 53 ⁰⁵² 8	28826 6 28816 I Hour	54600 9	28201 8 28191 5 Hour	56136 7 56162 9	27589 I 27579 O Hour	57711 8 57738 2	26988 3 26978 4 ————————————————————————————————————	0
	Alt. 29°	Hour Angle	Alt. 28°	Angle 298°	Alt. 27°	Angle 297°	Alt. 26°	Angle 296°	Alt. 25°	Angle 295°	,

	6	5°	6	6°	6	7°	6	8°	6	9°	
′	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	57738 2 57764 5 57790 9 57817 3 57843 7	26978 3 26968 4 26958 5 26948 6 26938 7	59352 9 59379 5	26389 I 26379 4 26369 7 26360 0 26350 2		25811 1 25801 5 25792 0 25782 4 25772 9	62539 3 62566 3 62593 3 62620 3 62647 2	25243 8 25234 5 25225 1 25215 8 25206 4	64163 2 64190 4 64217 5 64244 7 64271 9	24687 2 24678 0 24668 8 24659 6 24650 5	60 59 58 57 56
5 6 7 8 9	57870 0 57896 4 57922 8 57949 2 57975 6	26928 8 26918 9 26909 0 26899 1 26889 2	59459 2 59485 8 59512 4 59539 \circ	26340 5 26330 8 26321 1 26311 4 26301 7	61060 8 61087 6 61114 4 61141 2 61168 0	25763 4 25753 8 25744 3 25734 8 25725 3	62674 2 62701 2 62728 2 62755 2 62782 2	25197 0 25187 7 25178 4 25169 0 25159 7	64326 2 64353 4	24641 3 24632 1 24622 9 24613 8 24604 6	55 54 53 52 51
10 11 12 13 14	58002 0 58028 4 58054 8 58081 2 58107 6	26879 4 26869 5 26859 6 26849 7 26839 8	59592 2 59618 9 59645 5 59672 1 59698 7	26292 0 26282 3 26272 6 26262 9 26253 3	611948 612216 612484 612753 613021	256967	62836 2 62863 2 62890 2	25150 3 25141 0 25131 7 25122 3 25113 0		24595 4 24586 3 24577 I 24568 0 24558 8	50 49 48 47 46
15 16 17 18 19	58134 0 58160 4 58186 9 58213 3 58239 7	26830 0 26820 1 26810 2 26800 4 26790 5	59725 3 59752 0 59778 6 59805 2 59831 9	26243 6 26233 9 26224 2 26214 5 26204 9	61328 9 61355 7 61382 6 61409 4 61436 2	25649 2 25639 8	62971 3 62998 3	25103 7 25094 4 25085 1 25075 7 25066 4		24549 7 24540 5 24531 4 24522 2 24513 1	45 44 43 42 41
20 21 22 23 24	58266 1 58292 6 58319 0 58345 5 58371 9	26780 7 26770 8 26761 0 26751 1 26741 3	59858 5 59885 1 59911 8 59938 4 59965 1	26195 2 26185 5 26175 9 26166 2 261 5 6 6	61463 1 61489 9 61516 8 61543 6 61570 5	25620 8 25611 3 25601 8 25592 3 25582 9	63106 4 63133 5 63160 5	25°57 1 25°47 8 25°38 5 25°29 2 25°19 9	64706 9 64734 2 64761 4 64788 6 64815 8	24504 0 24494 8 24485 7 24476 6 24467 4	40 39 38 37 36
25 26 27 28 29	58398 4 58424 8 58451 3 58477 7 58504 2	26731 5 26721 6 26711 8 26702 0 26692 1	59991 7 60018 4 60045 1 60071 7 60098 4	26146 9 26137 3 26127 6 26118 0 26108 3	61597 3 61624 2 61651 0 61677 9 61704 8	25573 4 25563 9 25554 5 25545 0 25535 6	63241 6 63268 7 63295 7	25010 6 25001 3 24992 1 24982 8 24973 5	64843 I 64870 3 64897 5 64924 8 64952 0	24458 3 24449 2 24440 I 2443I 0 2442I 9	35 34 33 32 31
30 31 32 33 34	58530 7 58557 1 58583 6 58610 1 58636 6	26682 3 26672 5 26662 7 26652 9 26643 I	60125 1 60151 8 60178 4 60205 1 60231 8	26098 7 26089 1 26079 4 26069 8 26060 2	61731 7 61758 5 61785 4 61812 3 61839 2	25526 1 25516 7 25507 2 25497 8 25488 3		24964 2 24954 9 24945 7 24936 4 24927 I	64979 3 65006 5 65033 8 65061 0 65088 3	24412 8 24403 7 24394 6 24385 5 24376 4	30 29 28 27 26
35 36 37 38 39	58663 1 58689 6 58716 0 58742 5 58769 0	26633 3 26623 5 26613 7 26603 9 26594 I	60285 2 60311 9 60338 6 60365 3	26050 6 26041 0 26031 3 26021 7 26012 1	1131	25478 9 25469 4 25460 0 25450 6 25441 I	635394	24917 9 24908 6 24899 3 24890 1 24880 8	65115 5 65142 8 65170 1 65197 3 65224 6	24367 3 24358 2 24349 I 24340 0 24330 9	25 24 23 22 21
40 41 42 43 44	58795 5 58822 0 58848 6 58875 1 58901 6	26584 3 26574 5 26564 7 26554 9 26545 1	60418 7 60445 4 60472 2 60498 9	26002 5 25992 9 25983 3 25973 7 25964 1	62027 5 62054 4 62081 3 62108 2	253940	63702 0 63729 I	24834 6	65251 9 65279 1 65306 4 65333 7 65361 0	24321 8 24312 8 24303 7 24294 6 24285 6	20 19 18 17 16
45 46 47 48 49	58981 2 59007 7 59034 2	26515 8 26506 1 26496 3	60552 3 60579 1 60605 8 60632 5	25945 0 25935 4 25925 8 25916 2	62162 1 62189 0 62215 9 62242 9	25375 2 25365 8 25356 4 25347 0	63783 3 63810 4 63837 5 63864 7	24825 4 24816 1 24806 9 24797 7 24788 5	65442 9 65470 2 65497 5	24276 5 24267 4 24258 4 24249 3 24240 3	15 14 13 12 11
50 51 52 53 54	59166 9	26486 5 26476 8 26467 0 26457 3 26447 5	60686 0 60712 8 60739 5 60766 3	25906 6 25897 I 25887 5 25877 9 25868 4	62296 7 62323 7 62350 6 62377 6	25337 6 25328 2 25318 8 25309 5 25300 1	63918 9 63946 0 63973 2 64000 3		65552 I 65579 4 65606 7 65634 0	24231 2 24222 2 24213 1 24204 1 24195 0	9 8 7 6
55 56 57 58 59 60	59193 5 59220 1 59246 6 59273 2 59299 8 59326 3	26437 8 26428 I 26418 3 26408 6 26398 9 26389 I	608198 608466 608733 609001	25858 8 25849 2 25839 7 25830 1 25820 6 25811 1	62431 5 62458 4 62485 4 62512 4	25271 9	64054 6 64081 7 64108 9 64136 0	24733 2 24724 0 24714 8 24705 6 24696 4 24687 2	65716 o 65743 3	24186 0 24177 0 24167 9 24158 9 24149 9 24140 9	5 4 3 2 1 0
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	
	24°	294°	23°	293°	22°	292°	21°	291°	20°	290°	

	7	0°	7	ı°	7:	2°	7.	3°	7	4°	
	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 I 2 3	65798 0 65825 3 65852 7 65880 0	24140 9 24131 9 24122 8 24113 8	67443 2 67470 7 67498 2 67525 7	23604 6 23595 7 23586 9 23578 0	691260	23078 I 23069 4 23060 7 23052 I	70790 6 70818 5	22544 2	72436 3 72464 2 72492 2 72520 2	22053 7 22045 3 22036 9 22028 6	60 59 58
4 5 6	65907 3 65934 7 65962 0	24104 8 24095 8 24086 8	67553 2 67580 7 67608 3	23569 2 23560 4 23551 5	69209 0 69236 7 69264 3	23043 4 23034 7 23026 0	70874 I 7090I 9 70929 8	22527 I 22518 6 22510 I	72548 1 72576 1 72604 1	22020 2 22011 8 22003 4	57 56 55 54
7 8 9 10	65989 4 66016 7 66044 1 66071 5	24077 8 24068 8 24059 8 24050 8	67635 8 67663 3 67690 8 67718 4	23542 7 23533 8 23525 0 23516 2	69292 0 69319 7 69347 4 69375 1	23008 7	71013 3	22484 5 22476 0	72660 0 72688 0 72716 0	21995 1 21986 7 21978 4 21970 0	53 52 51 50
11 12 13 14	66098 8 66126 2 66153 6 66180 9	24041 8 24032 8 24023 8 24014 8	67745 9 67773 4 67801 0 67828 5	23507 4 23498 5 23489 7 23480 9	69402 8 69430 5 69458 2 69485 9	22982 7 22974 0 22965 3 22956 7	710968 711247	22467 5 22459 0 22450 5 22442 0	72772 0	21961 6 21953 3 21944 9 21936 6	49 48 47 46
15 16 17 18	66208 3 66235 7 66263 1 66290 5	24005 9 23996 9 23987 9 23978 9	67856 0 67883 6 67911 1 67938 7	23472 I 23463 3 23454 4 23445 6	69513 6 69541 3 69569 0 69596 7	22922 1	71208 2 71236 1 71263 9	22416 5 22408 0	72856 0 72883 9 72911 9 72940 0	21928 2 21919 9 21911 6 21903 2	45 44 43 42
20 21 22 23	66317 9 66345 2 66372 6 66400 0 66427 4	23970 0 23961 0 23952 0 23943 I 23934 I	67966 3 67993 8 68021 4 68048 9 68076 5	23436 8 23428 0 23419 2 23410 4 23401 6	69624 4 69652 1 69679 8 69707 6 69735 3	22913 4 22904 8 22896 1 22887 5 22878 9	712918 713197 713475 713754 714033	22391 0	72968 0 72996 0 73024 0 73052 0 73080 0	21894 9 21886 6 21878 2 21869 9 21861 6	41 40 39 38 37
24 25 26 27	66454 8 66482 2 66509 7 66537 I	23925 2 23916 2 23907 3 23898 3	68104 1 68131 6 68159 2 68186 8	23392 8 23384 I 23375 3 23366 5	69763 0 69790 7 69818 5 69846 2	22870 2 22861 6 22853 0 22844 4	71431 2 71459 0 71486 9 71514 8	22357 I 22348 6 22340 2 2233I 7	73108 0 73136 0 73164 1 73192 1	21853 2 21844 9 21836 6 21828 3	37 36 35 34 33
28 29 30 31 32	66564 5 66591 9 66619 3 66646 7 66674 2	23889 4 23880 4 23871 5 23862 6 23853 6	68214 4 68241 9 68269 5 68297 1 68324 7	23357 7 23348 9 23340 2 23331 4 23322 6	69874 0 69901 7 69929 4 69957 2 69984 9	22835 7 22827 1 22818 5 22809 9 22801 3	' - '	22323 2 22314 8 22306 3 22297 9 22289 4		21820 0 21811 7 21803 4 21795 1 21786 8	32 31 30 29 28
33 34 35	66701 6 66729 0 66756 4	23844 7 23835 8 23826 8	68 352 3 68 379 9 68 407 5 68 435 1	23313 8 23305 1 23296 3	700127 700404 700682	22792 7 22784 I 22775 5	71682 1 71710 0 71737 9 71765 8	22280 9 22272 5 22264 I	73360 3 73388 3 73416 3	21778 5 21770 2 21761 9 21753 6	27 26 25 24
36 37 38 39	66783 9 66811 3 66838 8 66866 2 66893 7		68462 7 68490 3 68517 9	23287 6 23278 8 23270 0 23261 3	70095 9 70123 7 70151 4 70179 2 70207 0		71793 8 71793 8 71821 7 71849 6	22255 6 22247 2 22238 7 22230 3 22221 9	73472 4 73500 5 73528 5	21745 3 21737 0 21728 7 21720 4	23 22 21 20
40 41 42 43 44	66921 1 66948 6 66976 0 67003 5	² 3773 3 ² 3764 4 ² 3755 5	68545 5 68573 1 68600 7 68628 4 68656 0	23252 5 23243 8 23235 I 23226 3 23217 6	70234 7 70262 5 70290 3 70318 I	22723 9 22715 3 22706 7	71905 4 71933 3 71961 2 71989 2	22213 4 22205 0 22196 6	73584 6	21712 I 21703 9 21695 6 21687 3	19 18 17 16
45 46 47 48	67030 9 67058 4 67085 9 67113 3	23728 8 23719 9 23711 1	68683 6 68711 2 68738 9 68766 5	23200 I 2319I 4 23182 7	70373 6 70401 4 70429 2	22681 0 22672 4 22663 9	72017 1 72045 0 72073 0 72100 9	22171 3 22162 9 22154 5	73696 9 73724 9 73753 0 73781 1	21679 0 21670 8 21662 5 21654 2	14 13 12
50 51 52 53 54	67140 8 67168 3 67195 8 67223 2 67250 7	23693 3 23684 4 23675 5 23666 7	68794 I 6882I 8 68849 4 68877 I 68904 7	23147 8 23139 1	70457 0 70484 8 70512 6 70540 4 70568 2	22646 7 22638 2 22629 6 22621 1	72128 8 72156 8 72184 7 72212 6 72240 6	22137 6 22129 2 22120 8 22112 4	73865 3 73893 4 73921 5	21646 0 21637 7 21629 5 21621 2 21613 0	11 10 9 8 7 6
54 55 56 57 58 59 60	67278 2 67305 7 67333 2 67360 7 67388 2	23657 8 23648 9 23640 0 23631 2 23622 3		23121 6 23112 9 23104 2		22604 0 22595 4 22586 9	72268 5 72296 5 72324 4 72352 4 72380 3	22104 0 22095 6 22087 2 22078 9 22070 5	73949 5 73977 6 74005 7 74033 8 74061 9	21596 5 21588 2 21580 0 21571 8	54321
59 60	67415 7 67443 2	23613 5 23604 6	69070 6 69098 3	230868	7°735° 7°7628	22569 8	72408 3 72436 3	22062 I 22053 7	74090 0 74118 I	21563 5 21555 3	0
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	,
	19°	289°	18°	288°	17°	287°	16°	286°	15°	285°	

	7.	5°	7	6°	7:	7°	78	3°	7	9°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	74118 1 74146 2 74174 3 74202 4 74230 5	21547 I 21538 8 21530 6	75807 8 75836 0 75864 3 75892 5 75920 7	21049 6 21041 6	77533 2	20569 2	79237 3	20089 4	80919 1 80947 7 80976 2 81004 8 81033 3	19648 9 19641 3 19633 6 19626 0 19618 3	60 59 58 57 56
56 78 9	74258 6 74286 7 74314 8 74342 9 74371 1	21514 2 21505 9 21497 7 21489 5	75949 ° 75977 2 76005 4 76033 7 76061 9	1	77646 6 77675 0 77703 3 77731 7	20545 4 20537 4	79351 1 79379 6 79408 0 79436 5	20073 8 20066 I 20058 3 20050 5	81061 9 81090 5	19610 7 19603 0 19595 4 19587 7 19580 1	55 54 53 52 51
10 11 12 13	74399 ² 744 ² 7 3 74455 4 744 ⁸ 3 5	21473 I 21464 9 21456 7 21448 5	76090 2 76118 4 76146 6 76174 9 76203 2	20985 I 20977 0 20969 0	77788 4 77816 8 77845 1 77873 5 77901 9	20505 8 20497 8 20489 9	79493 4 79521 9 79550 4 79578 9 79607 3	20034 9 20027 2 20019 4 20011 6	812047 812333	19572 4 19564 8 19557 2 19549 5 19541 9	50 49 48 47 46
14 15 16 17 18	74511 7 74539 8 74567 9 74596 1 74624 2 74652 3	21432 I 21423 9 21415 7 21407 5	76231 4 76259 7 76287 9 76316 2 76344 4	20944 8 20936 8 20928 7 20920 7	7793° 3 77958 6	20466 2 20458 3 20450 4	79635 8 79664 3 79692 8 79721 3	19996 1 19988 3 19980 5 19972 8		19534 3 19526 6 19519 0 19511 4 19503 8	45 44 43 42 41
20 21 22 23 24	74680 5 74708 6 74736 8 74764 9	21391 1 21383 0 21374 8 21366 6	76372 7 76401 0 76429 2 76457 5 76485 8	20904 6 20896 6 20888 5 20880 5	78072 I 78100 5 78128 9 78157 3 78185 7	20426 7 20418 8 20410 9 20403 0		19957 3 19949 5 19941 8 19934 0		19496 1 19488 5 19480 9 19473 3 19465 7	40 39 38 37 36
25 26 27 28 29	74821 2 74849 4 74877 5 74905 7 74933 8	21350 3 21342 1 21333 9 21325 8	76514 1 76542 3 76570 6 76598 9 76627 2	20864 4 20856 4 20848 4 20840 4	78214 1 78242 5 78270 8 78299 2 78327 6	20387 3 20379 4 20371 5 20363 6	79920 7 79949 2 79977 7 80006 2 80034 7	19918 5 19910 8 19903 1 19895 3		19458 1 19450 5	35 34 33 32 31
30 31 32 33 34	74962 0 74990 2 75018 3 75046 5 75074 7	21309 4 21301 3 21293 1	76655 5 76683 7 76712 0 76740 3	20824 3 20816 3 20808 3 20800 3		20347 9 20340 0 20332 1 20324 3	80063 2 80091 7 80120 2	19879 9 19872 1 19864 4 19856 7		19420 I 19412 5 19404 9 19397 3 19389 7	30 29 28 27 26
35 36 37 38 39	75102 8 75131 0 75159 2 75187 4 75215 5	21268 7 21260 5 21252 4	76796 9 76825 2	20776 3 20768 3 20760 3	78498 1 78526 5 78554 9 78583 3 78611 7	20300 7 20292 8 20285 0	80205 7 80234 3 80262 8 80291 3 80319 8	19833 5	81919 5 81948 1 81976 7 82005 3 82033 9	19382 1 19374 6 19367 0 19359 4 19351 8	25 24 23 22 21
40 41 42 43 44	75243 7 75271 9 75300 1 75328 3 75356 5	21219 9 21211 7 21203 6	76938 4 76966 7 76995 0 77023 3 77051 6	20736 4 20728 4	78640 1 78668 5 78697 0 78725 4 78753 8	20261 4 20253 6	80376 9 80405 4 80433 9	19787 2	82062 5 82091 2 82119 8 82148 4 82177 0	19344 3 19336 7 19329 1 19321 5 19314 0	20 19 18 17 16
45 46 47 48 49	753 ⁸ 4 7 754 ¹² 9 7544 ¹ 1 754 ⁶ 9 3	21187 3 21179 2 21171 1 21163 0	77080 0	20696 5 20688 5 20680 5	78782 2 78810 7 78839 1 78867 5	20230 I 20222 3 20214 4 20206 6	80491 0 80519 5 80548 0 80576 6 80605 1	19756 4 19748 8 19741 1	82234 3 82262 9 82291 5	19298 9 19291 3 19283 7	15 14 13 12
50 51 52 53 54	75553 9 75582 1 75610 3	21138 7 21130 6 21122 5 21114 4	77221 6 77249 9 77278 2 77306 5 77334 9	20656 6 20648 6 20640 7 20632 7	78924 4 78952 8 78981 3 79009 7 79038 1	20190 9 20183 1 20175 3 20167 5	80633 6 80662 2 80690 7	197257 19718 0 19710 3 19702 6	82348 8 82377 4 82406 0 82434 7	19268 6 19261 1 19253 5 19246 0	10 9 8 7 6
55 56 57 58 59 60	75666 7 75694 9 75723 1 75751 4 75779 6 75807 8	21098 2 21090 1 21082 0 21073 9	77363 2 77391 5 77419 9 77448 2 7747 ⁶ 5 775°4 9	20616 8 20608 9 20600 9 20593 0	79095 0 79123 5	20136 2 20128 4 20120 6	80776 3 80804 9 80833 4 80862 0 80890 5 80919 1	19679 6 19671 9 19664 3 19656 6	82549 2	19230 9 19223 4 19215 8 19208 3 19200 8 19193 3	5 4 3 2 1
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	
	14.	284°	13°	283°	12°	282°	II°	281°	IO°	280°	1

	80	o°	81	c°	82	2°	8	3°	8.	4°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	82635 2 82663 8 82692 5 82721 1 82749 8		84356 5 84385 3 84414 0 84442 7 84471 5	18738 2 18730 8 18723 4	86082 7 86111 5 86140 3 86169 1 86197 9	18298 4 18291 2 18283 9	87841 9 87870 8 87899 7	17873 5 17866 4 17859 3 17852 1 17845 0	89633 9	17448 9 17441 9 17434 9 17427 9 17420 9	60 59 58 57 56
56 78 9	82778 4 82807 1 82835 7 82864 4 82893 1	19155 6 19148 1 19140 6 19133 1	84500 2 84529 0 84557 7 84586 4 84615 2	18708 6 18701 2 18693 8 18686 5	86226 7 86255 5 86284 4	18269 4 18262 1 18254 9 18247 6	87957 4 87986 3 88015 2 88044 1	17837 9 17830 7 17823 6 17816 5	89691 8 89720 7 89749 7 89778 6 89807 5	17413 9 17406 9 17399 9 17392 9 17385 9	55 54 53 52 51
10 11 12 13	82921 7 82950 4 82979 0 83007 7 83036 4	19118 1 19110 6 19103 1 19095 6	84643 9 84672 7 84701 4 84730 2 84758 9	18671 7 18664 3 18657 0 18649 6	86370 8 86399 6 86428 4	18233 2 18225 9 18218 7 18211 4	88101 8 88130 7 88159 6 88188 5	17802 3 17795 I	89836 5 89865 4 89894 4 89923 3 89952 2	17378 9 17371 9 17364 9 17357 9	50 49 48 47 46
14 15 16 17 18	83065 0 83093 7 83122 4 83151 1	19080 6 19073 1 19065 6 19058 1	84787 7 84816 4 84845 2 84873 9 84902 7	18634 9 18627 5 18620 1	86514 9 86543 7 86572 6	18197 0 18189 7 18182 5	88246 3 88275 1 88304 0 88332 9	17766 7 17759 6 17752 5 17745 4 17738 3	89981 2 90010 1 90039 1 90068 0	17343 9 17336 9 17329 9 17323 0 17316 0	45 44 43 42 41
20 21 22 23	83179 7 83208 4 83237 1 83265 8 83294 4	19043 I 19035 7 19028 2 19020 7	84931 4 84960 2 84988 9 850 17 7	18598 1 18590 7 18583 4 18576 0	86659 0 8668 7 9	18160 8 18153 6 18146 4 18139 1	88390 7 88419 6 88448 5 88477 4	17731 2 17724 1 17717 0 17709 9 17702 8	90125 9 90154 9 90183 8 90212 8	17309 0 17302 0 17295 1 17288 1 17281 1	40 39 38 37 36
24 25 26 27 28	83323 I 8335I 8 83380 5 83409 2 83437 9	18983 3	85046 5 85075 2 85104 0 85132 8 85161 5 85190 3	18561 3 18554 0 18546 7 18539 3	86803 2 86832 0 86860 9	18124 7 18117 5 18110 3	88535 2 88564 1 88593 0 88621 9	17695 7 17688 6 17681 5 17674 5 17667 4	90270 7	17274 2 17267 2 17260 2 17253 3 17246 3	35 34 33 32 31
30 31 32 33	83466 5 83495 2 83523 9 83552 6 83581 3 83610 0	18968 4 18961 0 18953 5 18946 0	85219 1 85247 8 85276 6 85305 4 85334 1	18524 7 18517 3 18510 0 18502 7	86947 4 86976 2	18088 7 18081 5 18074 3 18067 1 18059 9	88679 7 88708 6 88 7 37 5	17660 3	90415 4 90444 4 90473 3 90502 3 90531 2	17239 4 17232 4 17225 5 17218 5 17211 6	30 29 28 27 26
34 35 36 37 38	83638 7 83667 4 83696 1 83724 8	18931 1 18923 7 18916 2 18908 8	85362 9 85391 7 85420 5 85449 2 85478 0	18488 0 18480 7 18473 4 18466 1	87091 6 87120 4	18052 7 18045 5 18038 3 18031 1	88824 2 88853 I	17624 9 17617 9	90560 2 90589 2 90618 1	17204 6 17197 7 17190 7 17183 8	25 24 23 22 21
39 40 41 42 43	838109 838396 838683	18893 9 18886 5 18879 0 18871 6	85506 8 85535 6 85564 4 85593 2 85621 9	18451 5 18444 2 18436 8 18429 5	87235 8 87264 7 87293 5 87322 4 87351 2	180168 180096 180024 179952	88968 7	17589 6 17582 6 17575 5 17568 5	90705 0 90734 0 90762 9 90791 9	17169 9 17163 0 17156 1	20 19 18 17 16
46 47 48	83925 7 83954 4 83983 2 84011 9	18856 7 18849 3 18841 9 18834 5	85650 7 85679 5 85708 3 85737 1 85765 9	18414 9 18407 6 18400 4 18393 1	87380 1 87409 0 87437 8 87466 7	17980 9 17973 7 17966 5 17959 4		17554 4 17547 3 17540 3 17533 2	90849 8 90878 8	17135 3 17128 4 17121 4	15 14 13 12
50 51 52 53 54	84069 3 84098 0 84126 7 84155 5	18819 6 18812 2 18804 8 18707 4	85794 7 85823 5 85852 3 85881 1 85909 9	18378 5 18371 2 18363 9 18356 6	87524 4 87553 3 87582 1 87611 0	17945 0 17937 9 17930 7 17923 6	89257 9 89286 8 89315 7 89344 7	17519 2 17512 1 17505 1 17498 1	909947 910236 910526 910816	17100 7 17093 8 17086 9	10 9 8 7 6
55 56 57 58 59 60	84212 9 84241 6 84270 4 84299 1 84327 8	18782 6 18775 2 18767 8 18760 4 18753 0	85938 7 85967 5 85996 3 86025 1 86053 9	18342 I 18334 8 18327 5 18320 2 18313 0	87668 7 8769 7 6 87726 4 87755 3 87784 2	17909 3 17902 1 17895 0 17887 8 17880 7	89402 5 89431 4 89460 4 89489 3 89518 2	17484 0 17477 0 17470 0 17462 9 17455 9	91226 5 91255 4	17059 3 17052 4 17045 5 17038 6	5 4 3 2 1
66	84356 5		86082 7	18305 7 Hour	87813 1	Hour	89547 I ————————————————————————————————————	Hour	91284 4 Alt.	Hour	0
	Alt.	Angle 279°	Alt.	Angle 278°	Alt.	Angle 277°	6°	Angle 276°	5°	Angle 2.75°	'

	8	5°	8	6°	8	7°	8	8°	8	9°	
,	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	Sum or Diff.	Hour Angle	
0 1 2 3 4	91284 4 91313 4 91342 4 91371 4 91400 3	17031 7 17024 8 17017 9 17011 0 17004 1	93082 4	16621 7 16614 9 16608 1 16601 4 16594 6	94766 4 94795 4 94824 5 94853 5 94882 6	16218 8 16212 1 16205 5 16198 8 16192 2	96510 1 96539 1 96568 2 96597 3 96626 3	15822 9 15816 3 15809 8 15803 3 15796 7	98254 8 98283 8 98312 9 98342 0 98371 1	15433 8 15427 4 15421 0 15414 5 15408 1	60 59 58 57 56
5 6 7 8 9	91429 3 91458 3 91487 3 91516 3	16997 2 16990 3 16983 5	93169 4 93198 5 93227 5 93256 5 93285 5	16587 8 16581 1 16574 3 16567 5 16560 8	94911 6 94940 7 94969 8 94998 8 95027 9	16185 5 16178 9 16172 2 16165 6	96655 4 96684 5 96713 6 96742 6	15790 2 15783 7 15777 1 15770 6 15764 1	98400 2 98429 3 98458 3 98487 4	15401 7 15395 3 15388 9 15382 5 15376 0	55 54 53 52 51
10 11 12 13	91574 2 91603 2 91632 2 91661 2 91660 2	16962 8 16956 0 16949 1	93314 6 93343 6 93372 6 93401 6 93430 7	16554 0 16547 3 16540 5 16533 8	95056 9 95086 0 95115 0	16152 3 16145 7 16139 0 16132 4 16125 8		15757 6 15751 0 15744 5	98545 6	15369 6 15363 2 15356 8 15350 4 15344 0	50 49 48 47 46
14 15 16 17 18	91719 2 91748 2 91777 2 91806 1 91835 1	16928 5 16921 6 16914 8 16907 9	93459 7 93488 7 93517 7 93546 8 93575 8	16520 3 16513 5 16506 8 16500 1 16493 3	95202 2 95231 2 95260 3 95289 3 95318 4	16119 2 16112 5 16105 9 16099 3	96946 1 96975 2	15725 0 15718 5 15712 0 15705 4 15698 9	98691 0 98720 1 98749 2 98778 3	15337 6 15331 2 15324 8 15318 4 15312 0	45 44 43 42 41
20 21 22 23 24	91864 1 91893 1 91922 1 91951 1 91980 1	16894 2 16887 3 16880 5 16873 6	93604 8 93633 9 93662 9 93691 9	16486 6	95347 5 95376 5 95405 6 95434 6 95463 7	16086 0 16079 4 16072 8 16066 2		15692 4 15685 9 15679 4	98836 5 98865 6 98894 6 98923 7 98952 8	15305 6 15299 2 15292 9 15286 5 15280 1	40 39 38 37 36
25 26 27 28 29	92009 I 92038 I 92067 I 92096 I 92125 I	16860 o 16853 I	937500	16452 9 16446 2 16439 5 16432 8 16426 1	95492 8 95521 8 95550 9 95579 9 95609 0	16053 0 16046 4 16039 8 16033 2 16026 6	97236 9 97266 0	15659 9	98981 9 99011 0 99040 1 99069 2	152737	35 34 33 32 31
30 31 32 33 34	92154 I 92183 I 92212 I 9224I I 92270 I	16825 8	93895 I 93924 2 93953 2 93982 2 94011 3	16419 3 16412 6 16405 9 16399 2 16392 5	95638 I 95667 I	16020 0 16013 4 16006 8 16000 2 15993 6	97382 3 97411 4 97440 5 97469 5 97498 6	15627 5 15621 0 15614 5 15608 1 15601 6	991 27 3 99156 4	15241 8 15235 4 15229 1 15222 7 15216 4	30 29 28 27 26
35 36 37 38 39	92299 I 92328 I 92357 I 92386 I 92415 I	16791 6 16784 8 16778 0 16771 2 16764 3	94040 3 94069 4 94098 4 94127 4 94156 5	16385 8 16379 1 16372 4 16365 7	95783 4 95812 4 95841 5	15987 0 15980 4 15973 8 15967 2 15960 7	97527 7 97556 8 97585 9	15595 I 15588 6 15582 2 15575 7 15569 2	992 72 8 99301 9	15210 0 15203 6 15197 3 15190 9 15184 5	25 24 23 22 21
40 41 42 43 44	92444 I 92473 I 92502 I 9253I I 92560 I	16757 5 16750 7	94185 5 94214 6 94243 6 94272 6 94301 7	16352 3 16345 6 16338 9	95928 7	15954 I 15947 5 15940 9 15934 3 15927 8	97673 I 97702 2	15562 8 15556 3 15549 8 15543 4 15536 9	99418 2 99447 3 99476 4 99505 5	15178 2 15171 8 15165 5 15159 1 15152 8	20 19 18 17 16
45 46 47 48 49	92589 1 92618 2 92647 2	16723 5 16716 7 16709 9 16703 1	943598	16318 8 16312 2 16305 5 16298 8	96132 1 96161 2	15921 2 15914 6 15908 1	97818 5 97847 6 97876 7 97905 8	15530 4 15524 0 15517 5	99563 7 99592 8 99621 8 99650 9	15146 5 15140 1 15133 8	15 14 13 12
50 51 52 53 54	92734 2 92763 2 92792 2 92821 2 92850 3	16689 5 16682 7 16675 9 16669 1	94475 9	16285 4 16278 8 16272 1 16265 4	96219 3 96248 4 96277 5 96306 6	15888 4 15881 8 15875 3 15868 7	97963 9 97993 0 98022 1 98051 2 98080 3	15498 2 15491 7 15485 3 15478 9	99709 I 99738 2 99767 3 99796 4	15114 8 15108 4 15102 1 15095 8 15089 4	10 9 8 7 6
55 56 57 58 59 60	92879 3 92908 3 92937 3 92966 3 92995 3 93024 3	16648 8 16642 0 16635 2 16628 4	94621 2 94650 2 94679 3 94708 3 94737 4 94766 4	16252 I 16245 4 16238 8 16232 I 16225 4 16218 8	96364 7 96393 8 96422 8 96451 9 96481 0	15855 6 15849 1 15842 5	98109 3 98138 4 98167 5 98196 6 98225 7		99854 6 99883 6 99912 7 99941 8	15083 1 15076 8 15070 5 15064 1 15057 8 15051 5	543210
	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	Alt.	Hour Angle	
	4°	274°	3°	273°	2 °	272°	I°	271°	o°	270°	′

,					Hour	Angle	• .				
	90°,	91°	92°	93°	94°	95°	96°	97°	98°	99°	
0 1 2 3 4	15051 5 15045 2 15038 9 15032 6 15026 2	14663 4 14657 2 14651 0	14288 3 14282 2	13931 8 13925 8 13919 8	13581 4 13575 5 13569 6 13563 7	13231 1 13225 3 13219 6 13213 8	12887 0 12881 3 12875 6 12869 9	12548 8 1254 3 2 12537 6 12532 0	12211 0 12205 5 12200 1		60 59 58 57 56
5 6 7 8 9	15019 9 15013 6 15007 3 15001 0 14994 7		14257 8	13895 9 13889 9	13546 1 13540 2 13534 3	13202 2 13196 4 13190 7 13184 9	12852 9 12847 2 12841 5	12509 7 12504 2	12189 1 12183 6 12178 1 12172 7	11868 5 11863 1 11857 7 11852 3 11847 0	55 54 53 52 51
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15 16 17 18 19 20	14950 7 14944 4 14938 1 14931 8	14576 7 14570 5 14564 4 14558 2	14209 2 14203 2 14197 1 14191 0	13848 I 13842 I 13836 2 13830 2 13824 2	13493 2 13487 4 13481 5 13475 6 13469 8	13144 5 13138 8 13133 0 13127 2 13121 5	12801 9 12 79 6 2 12 7 90 5 12 7 84 9	12465 2 12459 6 12454 1 12448 5	12134 4 12128 9 12123 4 12118 0	11809 3 11804 0 11798 6 11793 2 11787 9	44 43 42 41 40
21 22 23 24 25	14913 0 14906 7 14900 4	14545 8 14539 7 14533 5 14527 3 14521 2	14178 9 14172 8 14166 8 14160 7 14154 6	13812 3 13806 4 13800 4 13794 5	13458 1 13452 2 13446 4 13440 5		12767 9 12762 3 12756 6 12751 0	12426 3 12420 7 12415 2	12101 6 12096 1 12090 7 12085 2	117718	39 38 37 36 35
26 27 28 29 30			14148 6 14142 5 14136 5 14130 4	13782 6		13064 0	12739 7 12734 1 12728 4 12722 8	12409 6 12404 1 12398 6 12393 0 12387 5	12074 3	11755 7 11750 4 11745 0 11739 7	34 33 32 31 30
31 32 33 34	14856 6 14850 3 14844 1 14837 8 14831 5	14484 2 14478 1 14471 9 14465 8	14118 3 14112 3 14106 3 14100 2	13758 8 13752 9 13746 9	13405 5 13399 6 13393 8	13058 3 13052 6 13046 8 13041 1	12717 I 12711 5 12705 9 12700 2	12381 9 12376 4	12041 7	11729 0 11723 6 11718 3	29 28 27 26 25
35 36 37 38 39	14825 3 14819 0 14812 8 14806 6	14453 5 14447 4 14441 2 14435 1	14088 1 14082 1 14076 1 14070 0	13729 1 13723 2 13717 3 13711 3	13376 3 13370 5 13364 7 13358 8	13029 6 13023 9 13018 2 13012 5	12689 0 12683 4 12677 7 12672 1	12354 3 12348 7 12343 2 12337 7	12025 4	11702 3	24 23 22 21 20
40 41 42 43 44	14794 1 14787 8 14781 6 14775 3	14422 8 14416 7 14410 6 14404 4	14058 0 14052 0 14045 9 14039 9	13699 5 13693 6	13347 2 13341 4 13335 6 13329 7	13001 0 12995 3 12989 6 12983 9	12660 9 12655 2 12649 6 12644 0	12326 6 12321 1 12315 6 12310 1	11998 2 11992 8 11987 4 11982 0	11675 6 11670 3 11664 9 11659 6	19 18 17 16
45 46 47 48 49	14762 9 14756 6 14750 4 14744 2	14379 9 14373 8	14027 9 14021 9 14015 8 14009 8	13669 9 13664 0 13658 1 13652 2	13318 1 13312 3 13306 5 13300 7	12972 4 12966 7 12961 0	12632 8 12627 2 12621 6 12616 0	12299 0 12293 5 12288 0 12282 5	11971 1 11965 7 11960 3	11649 0 11643 6 11638 3 11633 0	14 13 12
50 51 52 53 54	14731 7 14725 5 14719 3 14713 1	14355 4	13997 8 13991 8 13985 8 13979 8	13640 3 13634 4 13628 5 13622 6	13289 1 13283 3 13277 5 13271 7	12943 9	12604 7 12599 1 12593 5 12587 9	12271 5 12266 0 12260 5 12255 0	11944 1 11938 7 11933 3 11927 8	11622 4 11617 1 11611 7 11606 4	9 8 7 6
55 56 57 58 59 60	14700 6 14694 4	14331 0 14324 9 14318 8	13967 8 13961 8 13955 8 13949 8	136108	13260 1 13254 3 13248 5	12915 4 12909 7 12904 0 12898 3	12576 8 12571 2 12565 6 12560 0	12244 0 12238 5 12233 0 12227 5	11917 0 11911 6 11906 2 11900 8	11595 8 11590 5 11585 2 11579 9	5 4 3 2 1 0
	269°	268°	267°	266°	265°	264°	263°	262°	261°	260°	,
					Hour	Angle	•		-		

,	Hour Angle 100° 101° 102° 103° 104° 105° 106° 107° 108° 109°											
	100°	IOI°	102°	103°	104°	105°	106°	107°	108°	109°		
0 1 2 3 4	11574 6 11569 3 11564 0 11558 7 11553 4	11259 4 11254 2 11249 0 11243 8 11238 6	10949 7 10944 6 10939 5 10934 4 10929 3	10635 5	10346 8 10341 9 10336 9 10332 0 10327 1	10053 3 10048 5 10043 6 10038 8 10034 0	9765 I 9760 4 9755 6 9750 9 9746 I	9482 I 9477 5 9472 8 9468 I 9463 4	9204 2 9199 7 9195 1 9190 5 9185 9	8931 4 8926 9 8922 4 8917 9 8913 4	60 59 58 57 56	
5 6 7 8 9	11548 1 11542 8 11537 5 11532 3 11527 0	11233 4 11228 2 11223 0 11217 8 11212 6	10919 1 10914 0 10908 9 10903 8	10615 4 10610 4 10605 4 10600 4	10322 I 10317 2 10312 3 10307 4 10302 4	100098	9741 4 9736 6 9731 9 9727 1 9722 4	9458 8 9454 1 9449 4 9444 8 9440 1	9181 3 9176 7 9172 1 9167 6 9163 0	8908 9 8904 4 8899 9 8895 4 8890 9	55 54 53 52 51	
10 11 12 13 14	115217 115164 115111 115058 115006		10888 5 10883 4 10878 3	10595 4 10590 4 10585 4 10580 4 10575 4	10297 5 10292 6 10287 7 10282 8 10277 8	10004 9 10000 1 9995 3 9990 4 9985 6 9980 8	9717 6 9712 9 9708 1 9703 4 9698 6	9435 5 9430 8 9426 1 9421 5 9416 8	9158 4 9153 8 9149 3 9144 7 9140 1 9135 6	8886 4 8881 9 8877 4 8872 9 8868 5 8864 0	50 49 48 47 46	
15 16 17 18 19	11495 3 11490 0 11484 7 11479 5 11474 2 11468 9	11181 5 11176 3 11171 1 11165 9 11160 7	108528	10570 4 10565 4 10560 4 10555 4 10550 4 10545 4	10272 9 10268 0 10263 1 10258 2 10253 3 10248 4	9976 0 9971 1 9966 3 9961 5	9693 9 9689 2 9684 4 9679 7 9675 0	9412 2 9407 5 9402 9 9398 2 9393 6 9388 9	9131 0 9126 4 9121 9 9117 3	8859 5 8855 0 8850 5 8846 0	45 44 43 42 41 40	
20 21 22 23 24 25	11463 6 11458 4 11453 1 11447 8	11155 4 11150 4 11145 2 11140 0 11134 9	10842 7 10837 6 10832 5 10827 4	10545 4 10540 4 10535 4 10530 4 10525 4	10243 5 10238 6 10233 7 10228 8	9930 7 9951 9 9947 1 9942 2 9937 4	9665 5 9660 8 9656 0 9651 3	9384 3 9379 6 9375 0 9370 4	9108 2 9103 6 9099 1 9094 5	8837 I 8832 6 8828 I 8823 7	39 38 37 36 35	
25 26 27 28 29 30	11437 3 11432 1 11426 8 11421 6	11124 5 11119 4 11114 2 11109 0	10817 3 10812 2 10807 1 10802 0	10515 4 10510 4 10505 5 10500 5	10219 0 10214 1 10209 2 10204 3	9927 8 9923 0 9918 2 9913 4 9908 6	9641 9 9637 1 9632 4 9627 7	9361 1 9356 4 9351 8 9347 2 9342 5	9085 4 9080 8 9076 3 9071 7	8814 7 8810 3 8805 8 8801 3	34 33 32 31 30	
31 32 33 34 35	11411 0 11405 8 11400 5 11395 3	11038 7 11093 6 11088 4 11083 2	10791 9 10786 8 10781 8 10776 7	10490 5 10485 5 10480 6 10475 6	10194 5 10189 6 10184 7 10179 8	9903 8 9899 0 9894 2 9889 4 9884 6	9618 3 9613 6 9608 8 9604 1	9337 9 9333 3 9328 7 9324 0	9062 6 9058 1 9053 6 9049 0	8792 4 8787 9 8783 5 8779 0	29 28 27 26 25	
35 36 37 38 39 40	11384 8 11379 6 11374 3 11369 1	11072 9 11067 8 11062 6 11057 5	10766 6 10761 5 10756 5 10751 4	10465 7 10460 7 10455 7 10450 7	10170 1 10165 2 10160 3 10155 4	9879 8 9875 0 9870 2 9865 4	9594 7 9590 0 9585 3 9580 6	9314 8 9310 2 9305 5 9300 9 9296 3	9039 9 9035 4 9030 9 9026 3	8770 I 8765 6 8761 2 8756 7 8752 3	24 23 22 21 20	
41 42 43 44	11358 6 11353 4 11348 1 11342 9	11047 2 11042 1 11036 9 11031 8	10741 3 10736 2 10731 2	10440 8 10435 9 10430 9 10425 9	10145 7 10140 8 10135 9 10131 1	9855 8 9851 0	9571 2 9566 5 9561 8 9557 1	9291 7 9287 1 9282 5 9277 8	9017 3 9012 7 9008 2 9003 7 8999 1	8747 8 8743 4 8738 9 8734 5 8730 0	19 18 17 16	
45 46 47 48 49 50	11332 4 11327 2 11322 0	11021 5 11016 4 11011 2 11006 1	10716 1 10711 0 10706 0 10700 9	10416 0 10411 1 10406 1 10401 2	10121 3 10116 5 10111 6 10106 7	9831 9 9827 1 9822 4 9817 6	9547 7 9543 0 9538 3 9533 6	9268 6 9264 0 9259 4 9254 8	8994 6 8990 1 8985 6 8981 0	8725 6 8721 2 8716 7 8712 3 8707 8	14 13 12 11	
51 52 53 54	11306 3 11301 1 11295 9 11290 7	10995 8 10990 7 10985 6 10980 5	10690 8 10685 8 10680 8	10391 3 10386 3 10381 4 10376 4	10097 0	9808 0 9803 3 9798 5 9793 7		9245 6 9241 0 9236 4 9231 8	8972 0 8967 5 8963 0 8958 5 8953 9	8703 4 8699 0 8694 5 8690 1	9 8 7 6	
55 56 57 58 59 60	11280 2 11275 0 11269 8 11264 6	10970 2 10965 1 10960 0	10665 7 10660 6 10655 6 10650 6	10366 5 10361 6 10356 7	10072 7	9784 2 9779 4 9774 7 9769 9	9500 8 9500 8 9496 2 9491 5 9486 8 9482 1	9227 2 9222 6 9218 0 9213 4 9208 8 9204 2	8949 4 8944 9 8940 4 8935 9 8931 4	8681 3 8676 8 8672 4 8668 0 8663 5	5 4 3 2 1 0	
	259°	258°	257°	256°	255°	254°	253°	252°	251°	250°	,	
					Hour	Angle	•					

,					Hour	Angle					
	110°	III°	112°	113°	114°	115°	116°	11 7 °	118°	119°	
0	8663 5	8400 6	8142 6	7889 3	7640 9	7397 I	7158 0	6923 4	6693 4	6468 0	60
1	8659 1	8396 3	8138 3	7885 2	7636 8	7393 I	7154 0	6919 6	6689 6	6464 2	59
2	8654 7	8392 0	8134 1	7881 0	7632 7	7389 0	7150 1	6915 7	6685 9	6460 5	58
3	8650 3	8387 6	8129 8	7876 8	7628 6	7385 0	7146 1	6911 8	6682 1	6456 8	57
4	8645 9	8383 3	8125 5	7872 6	7624 5	7381 0	7142 2	6907 9	6678 3	6453 I	56
56 78 9	8641 5 8637 0 8632 6 8628 2 8623 8	8378 9 8374 6 8370 3 8365 9 8361 6	8121 3 8117 0 8112 8 8108 5 8104 3	7868 5 7864 3 7860 1 7855 9 7851 8	7620 4 7616 3 7612 2 7608 1 7604 0	7377 ° 7373 ° 7368 9 7364 9 7360 9	7138 2 7134 3 7130 4 7126 4 7122 5	6904 I 6900 2 6896 4 6892 5 6888 6	6674 5 6670 7 6666 9 6663 1 6659 3	6449 4 6445 7 6441 9 6438 2 6434 5	55 54 53 52 51
10	8619 4	8357 3	8100 0	7847 6	7599 9	7356 9	7118 5	6884 8	6655 5	6430 8	50
11	8615 0	8353 0	8095 8	7843 4	7595 8	7352 9	7114 6	6880 9	6651 8	6427 1	49
12	8610 6	8348 6	8091 5	7839 3	7591 7	7348 9	7110 7	6877 1	6648 0	6423 4	48
13	8606 2	8344 3	8087 3	7835 1	7587 6	7344 9	7106 8	6873 2	6644 2	6419 7	47
14	8601 8	8340 0	8083 1	7830 9	7583 6	7340 9	7102 8	6869 4	6640 4	6416 0	46
15	8597 4	8335 7	8078 8	7826 8	7579 5 7575 4 757 ¹ 3 7567 2 7563 2	7336 9	7098 9	6865 5	6636 7	6412 3	45
16	8593 0	8331 3	8074 6	7822 6		7332 9	7095 0	6861 7	6632 9	6408 6	44
17	8588 6	8327 0	8070 3	7818 5		7328 9	7091 0	6857 8	6629 1	6404 9	43
18	8584 2	8322 7	8066 1	7814 3		7324 9	7087 1	6854 0	6625 3	6401 2	42
19	8579 8	8318 4	8061 9	7810 1		7320 9	7083 2	6850 1	6621 6	6397 5	41
20	8575 4	8314 I	8057 6	7806 0	7559 I	7316 9	7°79 3	6846 3	6617 8	6393 8	40
21	8571 0	8309 8	8053 4	7801 8	7555 °	7312 9	7°75 4	6842 4	6614 0	6390 1	39
22	8566 6	8305 4	8049 2	7797 7	755° 9	7308 9	7°71 4	6838 6	6610 2	6386 4	38
23	8562 2	8301 I	8044 9	7793 5	7546 9	7304 9	7°67 5	6834 7	6606 5	6382 7	37
24	8557 8	8296 8	8040 7	7789 4	7542 8	7300 9	7°63 6	6830 9	6602 7	6379 0	36
25	8553 4	8292 5	8036 5	7785 2	7538 7	7296 9	7°59 7	6827 0	6598 9	6375 3	35
26	8549 0	8288 2	8032 3	7781 1	7534 6	7292 9	7°55 8	6823 2	6595 2	6371 6	34
27	8544 6	8283 9	8028 0	7776 9	7530 6	7288 9	7°51 9	6819 4	6591 4	6368 0	33
28	8540 2	8279 6	8023 8	7772 8	7526 5	7284 9	7°47 9	6815 5	6587 7	6364 3	32
29	8535 9	8275 3	8019 6	7768 7	7522 4	7280 9	7°44 °	6811 7	6583 9	6360 6	31
30	8531 5	8271 0	80154	77 ⁶ 4 5	7518 4	7276 9	7040 I	6807 9	6580 I	6356 9	30
31	8527 1	8266 7	80111	77 ⁶ 0 4	7514 3	7273 0	7036 2	6804 0	6576 4	6353 2	29
32	8522 7	8262 4	80069	775 ⁶ 2	7510 3	7269 0	7032 3	6800 2	6572 6	6349 5	28
33	8518 3	8258 1	80027	775 ² 1	7506 2	7265 0	7028 4	6796 4	6568 9	6345 8	27
34	8514 0	8253 8	79985	774 ⁸ 0	7502 1	7261 0	7024 5	6792 5	6565 I	6342 2	26
35	8509 6	8249 5	7994 3	7743 8	7498 I	7257 ° 7253 ° 7249 1 7245 1 7241 1	7020 6	6788 7	6561 4	6338 5	25
36	8505 2	8245 2	7990 1	7739 7	7494 °		7016 7	6784 9	6557 6	6334 8	24
37	8500 8	8240 9	7985 9	7735 6	749° °		7012 8	6781 1	6553 9	6331 1	23
38	8496 5	8236 6	7981 6	7731 4	7485 9		7008 9	6777 2	6550 1	6327 5	22
39	8492 1	8232 4	7977 4	7727 3	7481 9		7005 0	6773 4	6546 4	6323 8	21
40	8487 7	8228 1	7973 2	7723 2	7477 8	7237 I	7001 1	6769 6	6542 6	6320 I	20
41	8483 4	8223 8	7969 0	7719 0	7473 8	7233 2	6997 2	6765 8	6538 9	6316 4	19
42	8479 0	8219 5	7964 8	7714 9	74 ⁶ 9 7	7229 2	6993 3	6762 0	6535 1	6312 8	18
43	8474 6	8215 2	7960 6	7710 8	74 ⁶ 5 7	7225 2	6989 4	6758 1	6531 4	6309 I	17
44	8470 3	8210 9	7956 4	7706 7	74 ⁶ 1 6	722I 3	6985 5	6754 3	6527 7	6305 4	16
45	8465 9	8206 6	7952 2	7702 5	7457 6	7217 3	6981 6	6750 5	6523 9	6301 8	15
46	8461 5	8202 4	7948 0	7698 4	7453 5	7213 3	6977 7	6746 7	6520 2	6298 1	14
47	8457 2	8198 1	7943 8	7694 3	7449 5	7209 4	6973 9	6742 9	6516 4	6294 4	13
48	8452 8	8193 8	7939 6	7690 2	7445 5	7205 4	6970 0	6739 1	6512 7	6290 8	12
49	8448 5	8189 5	7935 4	7686 1	7441 4	7201 5	6966 1	6735 3	6509 0	6287 1	11
50	8444 I	8185 3	7931 2	7681 9	7437 4	7197 5	6962 2	6731 5	6505 2	6283 5	10
51	8439 8	8181 0	7927 0	7677 8	7433 3	7193 5	6958 3	6727 6	6501 5	6279 8	9
52	8435 4	8176 7	7922 8	7673 7	7429 3	7189 6	6954 4	6723 8	6497 8	6276 2	8
53	8431 I	8172 4	7918 6	7669 6	7425 3	7185 6	6950 6	6720 0	6494 0	6272 5	7
54	8426 7	8168 2	7914 4	7665 5	7421 2	7181 7	6946 7	6716 2	6490 3	6268 8	6
55 56 57 58 59 60	8422 4 8418 0 8413 7 8409 3 8405 0 8400 6	8163 9 8159 6 8155 4 8151 1 8146 8 8142 6	7910 3 7906 1 7901 9 7897 7 7893 5 7889 3	7661 4 7657 3 7653 2 7649 1 7645 0 7640 9	7417 2 7413 2 7409 2 7405 1 7401 1 7397 1	7177 7 7173 7 7169 8 7165 8 7161 9 7158 0	6942 8 6938 9 6935 0 6931 2 6927 3 6923 4	6712 4 6708 6 6704 8 6701 0 6697 2 6693 4	6486 6 6482 9 6479 1 6475 4 6471 7 6468 0	6265 2 6261 5 6257 9 6254 2 6250 6 6246 9	5 4 3 2 1
	249°	7397 7397 7397 7397 7397 7397 7397 7397									
		· · · · · ·				Angle					1

					Hour	Angle					
′	120°	121°	122°	123°	124°	125°	126°	127°	128°	129°	
0 1 2 3 4	6246 9 6243 3 6239 6 6236 0 6232 4	6030 3 6026 7 6023 2 6019 6 6016 0	5818 I 5814 6 5811 I 5807 6 5804 I	5610 I 5606 7 5603 3 5599 9 5596 4	5406 5 5403 I 5399 8 5396 4 5393 I	5207 I 5203 8 5200 5 5197 2 5194 0	5011 9 5008 7 5005 5 5002 3 4999 0	4820 9 4817 7 4814 6 4811 4 4808 3	4634 0 4630 9 4627 8 4624 7 4621 7	4451 2 4448 2 4445 2 4442 1 4439 1	60 59 58 57 56
56 78 9	6228 7 6225 1 6221 4 6217 8 6214 2 6210 5	6012 5 6008 9 6005 3 6001 8 5998 2 5994 6	5800 6 5797 1 5793 6 5790 1 5786 6 5783 1	5593 0 5589 6 5586 2 5582 8 5579 3	5389 7 5386 4 5383 0 5379 7 5376 3	5190 7 5187 4 5184 1 5180 8 5177 6	4995 8 4992 6 4989 4 4986 2 4983 0 4979 8	4805 I 4802 0 4798 9 4795 7 4792 6 4789 4	4618 6 4615 5 4612 4 4609 4 4606 3	4436 I 4433 I 4430 I 4427 I 4424 I	55 54 53 52 51 50
11 12 13 14	6206 9 6203 3 6199 6 6196 0	5994 0 5991 1 5987 5 5984 0 5980 4	5779 6 5776 1 5772 7 5769 2	55/5 9 55/72 5 55/69 1 55/65 7 55/62 3 55/58 8	5369 6 5366 3 5362 9 5359 6 5356 3	51/4 3 5171 0 5167 7 5164 5 5161 2	4976 6 4973 4 4970 2 4967 0 4963 8	4786 3 4783 2 4780 0 4776 9 4773 8	4597 I 4594 0 4591 0 4587 9	4418 I 4415 I 4412 I 4409 I	49 48 47 46 45
15 16 17 18 19 20	6188 7 6185 1 6181 5 6177 9 6174 2	5973 3 5969 7 5966 2 5962 6	5762 2 5758 7 5755 2 5751 8 5748 3	5555 4 5552 0 5548 6 5545 2 5541 8	535 ² 9 5349 6 5346 2 534 ² 9 5339 6	5154 6 5151 4 5148 1 5144 8 5141 6	4960 6 4957 4 4954 2 4951 0 4947 8	4770 6 4767 5 4764 4 4761 3 4758 1	4584 8 4581 8 4578 7 4575 7 4572 6	4403 I 4400 I 4397 I 4394 I 4391 I	44 43 42 41 40
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	239°	238°	237°	236°	235°	234°	233°	232°	231°	230°	
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0 1 2 3 4	4272 4 4269 5 4266 5 4263 6 4260 7	4°97 7 4°94 8 4°92 ° 4°89 1 4°86 2	3927 ° 3924 2 3921 4 3918 6 3915 7	37 ⁶ 0 2 37 ⁵ 7 5 37 ⁵ 4 7 37 ⁵ 2 0 37 ⁴ 9 2	3597 4 3594 7 3592 0 3589 4 3586 7	3438 5 3435 8 3433 2 3430 6 3428 0	3283 4 3280 9 3278 3 3275 8 3273 2	3132 2 3129 7 3127 2 3124 8 3122 3	2984 8 2982 4 2980 0 2977 6 2975 I	2841 2 2838 9 2836 5 2834 2 2831 8	60 59 57 57 56
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	229°	228°	227°	226°	225°	224°	223°	222°	221°	220°	
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	Hour Angle										
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1	2699 1	2563 1	2430 8	2302 2	2177 3	2056 I	1938 4	1824 4	1714 0	1607 2	
2	2696 8	2560 9	2428 6	2300 I	2175 3	2054 I	1936 5	1822 6	1712 2	1605 4	
3	2694 5	2558 6	2426 5	2298 0	2173 2	2052 I	1934 6	1820 7	1710 4	1603 7	
4	2692 2	2556 4	2424 3	2295 9	2171 2	2050 I	1932 7	1818 8	1708 6	1601 9	
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	2687 6	2551 9	2420 0	2291 7	2167 I	2046 I	1928 8	1815 1	1705 0	1598 5	54
	2685 4	2549 7	2417 8	2289 6	2165 0	2044 I	1926 9	1813 2	1703 2	1596 7	53
	2683 I	2547 5	2415 6	2287 5	2163 0	2042 I	1925 0	1811 4	1701 4	1595 0	52
	2680 8	2545 3	2413 5	2285 4	2160 9	2040 2	1923 0	1809 5	1699 6	1593 2	51
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14	2669 3	2534 I	2402 6	2274 9	2150 7	2030 3	1913 4	1800 2	1690 6	1584 5	46
15	2667 I	2531 9	2400 5	2272 8	2148 7	2028 3	1911 5	1798 4	1688 8	1582 8	45
16	2664 8	2529 7	2398 3	2270 7	2146 7	2026 3	1909 6	1796 5	1687 0	1581 0	44
17	2662 5	2527 5	2396 2	2268 6	2144 6	2024 3	1907 7	1794 6	1685 2	1579 3	43
18	2660 2	2525 2	2394 0	2266 5	2142 6	2022 4	1905 8	1792 8	1683 4	1577 6	42
19	2657 9	2523 0	23919	2264 4	2140 6	2020 4	1903 9	1790 9	1681 6	1575 8	41
20	2655 6	2520 8	2389 7	2262 3	2138 5	2018 4	1901 9	1789 1	1679 8	1574 1	40
21	2653 4	2518 6	2387 5	2260 2	2136 5	2016 4	1900 0	1787 2	1678 0	1572 4	39
22	2651 1	2516 4	2385 4	2258 I	2134 5	2014 5	1898 1	1785 4	1676 2	1570 6	38
23	2648 8	2514 2	2383 2	2256 0	2132 4	2012 5	1896 2	1783 5	1674 4	1568 9	37
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	219°	218°	217°	216°	215°	214°	213°	212°	211°	210°	
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		Hour Angle										
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١		150°	151°	152°	153°	154°	155°	156°	157°	158°	159°	
I	0	1505 6 1503 9	1405 8	1309 6 1308 0	12168	1127 6	1041 8	959 6 958 2	880 7 879 4	805 3 804 I	733 4 732 2	60 50
ı	3	1502 2 1500 5	1402 6	1306 4	12138	11247	1039 0	956 9 955 5	878 2 876 9	802 9 801 7	731 0	59 58 57 56
ı	4	1498 9	1399 3	1303 3	12108	11218	1036 3	954 2 952 9	875 6 874 3	800 4 799 2	728 7	
ı	5 6 7	1495 5	1396 1	1300 2	1207 8	1118 9	1033 5	951 5	873 0 871 8	798 0	726 5	55 54
ŀ	7 8 9	1492 1	1392 8	1297 0	1204 7	11160	1030 7	948 9	870 5 869 2	795 6	725 2 724 I	53 52
	10	1488 7	13896	12939	12017	11131	1027 9	947 5 946 2	867 9	794 3 793 I	722 9	51 50
	11	1487 1 1485 4	1387 9	1292 3	11987	11116	1026 5	944 9 943 5	866 7 865 4	791 9 79° 7	720 6	49 48
I	13	1483 7	1384 7	1289 2	1197 2	11087	1023 7	942 2 940 9	864 1 862 8	789 5 788 2	718 2	47 46
	15 16	1480 3 1478 7	1381 4	1286 1	1194 2	11058	1021 0	939 5 938 2	861 6 860 3	787 ° 785 8	715 9 714 8	45 44
	17 18	1477 0 1475 3	1378 2	12830	11912	11030	1018 2 1016 8	936 9 935 5	859 o 857 8	784 6 783 4	7136	43
	19 20	1473 6	1375 0	12798	1188 2	1100 1	10154	934 2	856 5	782 2	711 3	41
	2I 22	1472 0 1470 3 1468 6	1373 4	12767	11852	1097 2	10140	932 9 931 6	855 2 854 0	7810	710 2	40 39 38
	23 24	1467 0	1370 1	1275 2	11837	1095 8	1009 9	930 3	852 7 851 4 850 2	778 6	707 9	38 37 36
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	30 31	1455 3 1453 6	1357 3 1355 7	12628	11718	1084 3	1000 3 998 9	9197 9184	842 6 841 4	768 9 767 7	698 7 697 6	30 29
i	32 33	14520	1354 1	1259 7	11688	1081 4	997 5 996 2	917 1	840 I 838 8	766 5 765 3	696 4 695 3	28 27
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	50 51	1422 2	1325 4	1232 1	1142 2	1055 9	973 ° 971 7	892 3	8177	745 I 744 °	676 0 674 9	9
	52 53	1418 9	1322 2	1229 0	1139 3	1053 1	970 3 969 0	891 0 889 7 888 5	815 2 814 0 812 7	742 8 741 6	673 8 672 7	7 6
	54	14157	1319 1	12260	1136 4	1050 3	967 6 966 3	887 2	8127	74° 4 739 3	670 4	
	56 57	14124	1315 9	1222 9 1221 4	1133 4	1047 5 1046 1	964 9 963 6	885 9 884 6	8103	73 ⁸ 1 73 ⁶ 9	669 3 668 2	5 4 3 2
	55 56 57 58 59 60	1409 1	1312 7 1311 2	12199	1130 5	1044 7	962 2 960 9	883 3 882 0	807 8 806 6	735 7 734 6	667 I 666 o	1
	60	1405 8	1309 6	12168	11276	10418	959 6	880 7	805 3	733 4	664 9	0
		209°	208°	207°	206°	205°	204°	203°	202°	201°	200°	
					1	Hour	Angle					1
	!	Hour Angle										

,	Hour Angle										
	160°	161°	162°	163°	164°	165°	166°	167°	168°	169°	
0	664 9	599 7	538 o	479 7	424 7	373 ¹	324 9	280 I	238 6	200 4	60
1	663 7	598 7	537 o	478 7	423 8	37 ² ³	324 2	279 4	237 9	199 8	59
2	662 6	597 6	536 o	477 8	422 9	37 ¹ ⁵	323 4	278 6	237 2	199 2	58
3	661 5	596 6	535 o	476 9	422 I	37 ⁰ ⁷	322 6	277 9	236 6	198 6	57
4	660 4	595 5	534 o	475 9	421 2	369 ⁸	321 8	277 2	235 9	198 0	56
5 6 7 8 9	659 3 658 2 657 1 656 0 654 9	594 5 593 4 592 4 591 3 590 3	533 ° 532 ° 531 ° 53° ° 529 °	475 ° 474 ° 473 I 472 2 47I 2	420 3 419 4 418 5 417 7 416 8	369 0 368 2 367 4 366 5 365 7	321 1 320 3 319 5 318 8 318 0	276 5 275 8 275 1 274 3 273 6	235 3 234 6 233 9 233 3 232 6	197 4 196 8 196 2 195 6	55 54 53 52 51
10	653 8	589 2	528 0	47° 3	415 9	364 9	317 2	272 9	232 0	194 4	50
11	652 7	588 2	527 I	469 4	415 0	364 1	316 5	272 2	231 3	193 8	49
12	651 6	587 1	526 I	468 4	414 1	363 2	315 7	271 5	230 7	193 2	48
13	650 5	586 1	525 I	467 5	413 3	362 4	314 9	270 8	230 0	192 6	47
14	649 4	585 0	524 I	466 6	412 4	361 6	314 2	270 1	229 4	192 0	46
15	648 3	584 0	523 I	465 6	411 5	360 8	313 4	269 4	228 7	191 4	45
16	647 2	582 9	522 I	464 7	410 6	360 0	312 6	268 7	228 1	190 8	44
17	646 1	581 9	521 I	463 8	409 8	359 1	311 9	268 0	227 4	190 2	43
18	645 0	580 9	520 2	462 8	408 9	358 3	311 1	267 3	226 8	189 6	42
19	643 9	579 8	519 2	461 9	408 0	357 5	310 4	266 6	226 1	189 0	41
20	642 8	578 8	518 2	461 0	407 2	356 7	309 6	265 9	225 5	188 4	40
21	641 7	577 7	517 2	460 1	406 3	355 9	308 9	265 2	224 8	187 8	39
22	640 6	576 7	516 2	459 1	405 4	355 1	308 1	264 5	224 2	187 2	38
23	639 5	575 7	515 3	458 2	404 6	354 3	307 3	263 8	223 5	186 7	37
24	638 4	574 6	514 3	457 3	403 7	353 5	306 6	263 I	222 9	186 1	36
25	637 3	573 6	513 3	456 4	402 8	352 7	305 8	262 4	222 3	185 5	35
26	636 2	572 6	512 3	455 4	402 0	351 8	305 1	261 7	221 6	184 9	34
27	635 1	571 5	511 3	454 5	401 1	351 0	304 3	261 0	221 0	184 3	33
28	634 0	570 5	510 4	453 6	400 2	350 2	303 6	260 3	220 3	183 7	32
29	633 0	569 5	509 4	452 7	399 4	349 4	302 8	259 6	219 7	183 2	31
30	631 9	568 4	508 4	451 8	398 5	348 6	302 I	258 9	219 I	182 6	30
31	630 8	567 4	507 5	450 9	397 7	347 8	301 3	258 2	218 4	182 0	29
32	629 7	566 4	506 5	449 9	396 8	347 0	300 6	257 5	217 8	181 4	28
33	628 6	565 4	505 5	449 0	395 9	346 2	299 8	256 8	217 2	180 8	27
34	627 5	564 3	504 5	448 1	395 1	345 4	299 I	256 1	216 5	180 3	26
35 36 37 38 39	626 5 625 4 624 3 623 2 622 I	563 3 562 3 561 3 560 2 559 2	503 6 502 6 501 6 500 7 499 7	447 ² 446 3 445 4 444 5 443 6	394 2 393 4 392 5 391 7 390 8	344 6 343 8 343 0 342 2 341 4	298 4 297 6 296 9 296 1 295 4	255 5 254 8 254 I 253 4 252 7	215 9 215 3 214 6 214 0 213 4	179 7 179 1 178 5 178 0	25 24 23 22 21
40	621 1	558 2	498 7	442 7	390 0	340 6	294 7	252 0	212 8	176 8	20
41	620 0	557 2	497 8	441 8	389 1	339 8	293 9	251 3	212 1	176 2	19
42	618 9	556 2	496 8	440 9	388 3	339 0	293 2	250 7	211 5	175 7	18
43	617 8	555 2	495 9	440 0	387 4	338 3	292 4	250 0	210 9	175 1	17
44	616 8	554 I	494 9	439 0	386 6	337 5	291 7	249 3	210 3	174 5	16
45	615 7	553 I	493 9	438 I	385 7	336 7	291 0	248 6	209 6	174 0	15
46	614 6	552 I	493 0	437 2	384 9	335 9	290 2	248 0	209 0	173 4	14
47	613 6	551 I	492 0	436 3	384 0	335 1	289 5	247 3	208 4	172 8	13
48	612 5	550 I	491 1	435 4	383 2	334 3	288 8	246 6	207 8	172 3	12
49	611 4	549 I	490 1	434 5	382 3	333 5	288 0	245 9	207 I	171 7	11
50 51 52 53 54	610 3 609 3 608 2 607 2 606 1	548 I 547 ° 546 ° 545 ° 544 °	489 2 488 2 487 3 486 3 485 4	433 6 432 8 431 9 431 0 430 I	38 i 5 38 o 7 37 9 8 37 9 0 37 8 i	33 ² 7 33 ² 0 33 ¹ 2 33 ⁰ 4 329 6	287 3 286 6 285 9 285 1 284 4	245 3 244 6 243 9 243 2 242 6	206 5 205 9 205 3 204 7 204 I	171 1 170 6 170 0 169 5 168 9	98 76
55 56 57 58 59 60	605 0 604 0 602 9 601 8 600 8	543 ° 542 ° 541 ° 549 ° 539 ° 538 ° 538 °	484 4 483 5 482 5 481 6 480 6 479 7	429 2 428 3 427 4 426 5 425 6 424 7	377 3 376 5 375 6 374 8 374 0 373 1	328 8 328 0 327 3 326 5 325 7 324 9	283 7 283 0 282 2 281 5 280 8 280 1	241 9 241 2 240 6 239 9 239 2 238 6	203 5 202 8 202 2 201 6 201 0 200 4	168 4 167 8 167 2 166 7 166 0 165 6	5 4 3 2 1 0
	199°	198°	197°	196°	195°	194°	193°	192°	191°	190°	
						Angle	***				'

,	Hour Angle										
	170°	171°	172°	173°	174°	175°	176°	177°	178°	179°	
0 1 2 3 4	165 6 165 0 164 5 163 9 163 4	134 I 133 6 133 I 132 6 132 I	105 9 105 5 105 0 104 6 104 2	81 1 80 7 80 3 79 9 79 5	59 6 59 2 58 9 58 6 58 2	41 4 41 1 40 8 40 5 40 3	26 5 26 2 26 0 25 8 25 6	14 9 14 7 14 6 14 4 14 2	6 6 6 5 6 4 6 3 6 2	1 7 1 6 1 5 1 5	60 59 58 57 56
56 78 9	162 8 162 3 161 7 161 2 160 6	131 6 131 1 130 6 130 1 129 6	103 7 103 3 102 9 102 4 102 0	79 2 78 8 78 4 78 0 77 6	57 9 57 6 57 3 56 9 56 6	40 0 39 7 39 4 39 2 38 9	25 4 25 2 24 9 24 7 24 5	14 I 13 9 13 7 13 6 13 4	6 1 6 0 5 9 5 8 5 7	I 4 I 3 I 3 I 2 I 2	55 54 53 52 51
10 11 12 13 14	160 1 159 6 159 0 158 5 157 9	129 2 128 7 128 2 127 7 127 2	101 6 101 1 100 7 100 3 99 8	77 3 76 9 76 5 76 1 75 8	56 3 56 0 55 7 55 3 55 0	38 6 38 4 38 1 37 8 37 6	24 3 24 1 23 9 23 7 23 5	13 3 13 1 13 0 12 8 12 7	5 6 5 5 5 4 5 3 5 2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	50 49 48 47 46
15 16 17 18	157 4 156 9 156 3 155 8	126 7 126 2 125 8 125 3 124 8	99 4 99 0 98 5 98 1 97 7	75 4 75 0 74 6 74 3 73 9	54 7 54 4 54 1 53 7 53 4	37 3 37 1 36 8 36 5 36 3	23 3 23 1 22 8 22 6 22 4	12 5 12 4 12 2 12 1 11 9	5 I 5 0 4 9 4 8 4 7	09 09 09 08	45 44 43 42 41
20 21 22 23 24	154 7 154 2 153 6 153 1 152 6	124 3 123 8 123 4 122 9 122 4	97 3 96 8 96 4 96 0 95 6	73 5 73 2 72 8 72 4 72 I	53 I 52 8 52 5 52 2 51 9	36 0 35 8 35 5 35 3 35 0	22 2 22 0 21 8 21 6 21 4	11 8 11 6 11 5 11 3	4 6 4 5 4 4 4 3 4 2	07 07 07 06 06	40 39 38 37 36
25 26 27 28 29	152 I 151 5 151 0 150 5 149 9	121 9 121 5 121 0 120 5 120 1	95 2 94 7 94 3 93 9 93 5	71 7 71 3 71 0 70 6 70 3	51 6 51 3 51 0 5° 7 5° 3	34 7 34 5 34 2 34 0 33 7	21 2 21 0 20 8 20 6 20 5	11 0 10 9 10 8 10 6	4 I 4 I 4 0 3 9 3 8	06 05 05 05	35 34 33 32 31
30 31 32 33 34	149 4 148 9 148 4 147 8	119 6 119 1 118 7 118 2	93 I 92 7 92 3 91 8 91 4	69 9 69 5 69 2 68 8 68 5	50 0 49 7 49 4 49 1 48 8	33 5 33 2 33 0 32 8 32 5	20 3 20 1 19 9 19 7	10 3 10 2 10 1 9 9 9 8	3 7 3 6 3 6 3 5 3 4	0 4 0 4 0 4 0 3 0 3	30 29 28 27 26
35 36 37 38 39	146 8 146 3 145 8 145 2 144 7	117 3 116 8 116 3 115 9	91 0 90 6 90 2 89 8 89 4	68 I 67 8 67 4 67 I 66 7	48 5 48 2 47 9 47 6 47 3	32 3 32 0 31 8 31 5 31 3	19 3 19 1 18 9 18 7 18 6	97 95 94 93	3 3 3 2 3 2 3 1 3 0	0 3 0 3 0 2 0 2 0 2	25 24 23 22 21
40 41 42 43 44	144 2 143 7 143 2 142 7 142 2	114 9 114 5 114 0 113 6 113 1	89 0 88 6 88 2 87 8 87 4	66 4 66 0 65 7 65 3 65 0	47 I 46 8 46 5 46 2 45 9	31 1 30 8 30 6 30 4 30 1	18 4 18 2 18 0 17 8 17 6	9 0 8 9 8 7 8 6 8 5	2 9 2 9 2 8 2 7 2 7	0 2 0 2 0 I 0 I	20 19 18 17 16
45 46 47 48 49	141 6 141 1 140 6 140 1 139 6	112 7 112 2 111 7 111 3 110 8	87 0 86 6 86 2 85 8 85 4	64 6 64 3 63 9 63 6 63 3	45 6 45 3 45 0 44 7 44 4	29 9 29 6 29 4 29 2 28 9	17 5 17 3 17 1 16 9 16 8	8 4 8 2 8 1 8 0 7 9	2 6 2 5 2 4 2 4 2 3	01 01 01 01 01	15 14 13 12
50 51 52 53 54	139 I 138 6 138 I 137 6	110 4 109 9 109 5 109 0 108 6	85 0 84 6 84 2 83 8 83 4	62 9 62 6 62 2 61 9 61 6	44 2 43 9 43 6 43 3 43 0	28 7 28 5 28 3 28 0 27 8	16 6 16 4 16 2 16 1 15 9	7 8 7 6 7 5 7 4 7 3	2 3 2 2 2 I 2 I 2 O	00	10 9 8 7 6
55 56 57 58 59 60	136 6 136 1 135 6 135 1 134 6	108 1 107 7 107 3 106 8 106 4	830 826 822 819 815 811	61 2 60 9 60 6 60 2 59 9	42 7 42 5 42 2 41 9 41 6	27 6 27 4 27 1 26 9 26 7 26 5	15 7 15 6 15 4 15 2 15 1 14 9	7 ² 7 ¹ 6 9 6 8 6 7 6 6	1 9 1 9 1 8 1 8 1 7	00	5 4 3 2 1
	134 ¹	188°	187°	186°	185°	184°	183°	182°	181°	180°	_
	189° 188° 187° 186° 185° 184° 183° 182° 181° 180° Hour Angle										

A FEW VALUABLE OPINIONS.

RIVISTA MARITTIMA ITALIANA, February 1910. BIBLIOGRAFIA.

"Il procedimento del de Aquino è ingegnosissimo, poichè, spezzando in due triangoli sferici rettangoli il noto triangolo SPZ, conducendo l'arco normale all'arco PZ, dà una serie di relazioni ben note, che abilmente utilizzate, per mezzo di una tavola di altezza ad azimut e tavole ausiliarie (pagg. 3-128), rende il conttegio pratico così semplice ed esatto per le esigenze nautiche da destare in verità meraviglia."— E. MILLOSEVICH, Director of the Observatory of Kome, Italy.

ALMIRANTE GARCIA MANSILLA, DETERMINACIÓN DEL PUNTO EN LA MAR, BUENOS AIRES, 1910.

"Sea como fuera, debo mencionar en primer término y con especial satisfacción, las tablas de Altura y Azimut, del señor Radler de Aquino por ser, sin duda alguna, la mejor solución del problema que yo conozco."—From Paper read before the Congreso Científico Internacional held at Buenos Aires, 1910.

ANNALEN DER HYDROGRAPHIE UND MARITIMEN METEOROLOGIE, *November* 1910.

RADLER DE AQUINO: Altitude and azimuth tables for facilitating the determination of lines of position and geographical position at sea. The simplest and readiest in solution. Spherical traverse tables for solving all problems of navigation. 8vo. 128 pp. London, 1910. J. D. Potter, and Rio de Janeiro, 1910. Radler de Aquino. Preis 10s. 6d.

Die Höhen- und Azimut-Tafeln des Leutnants RADLER DE AQUINO der brasilianischen Kriegs-Marine liefern ein recht bequemes Hilfsmittel, um die für Anwendung der Marcq St. Hilaireschen Methode notwendigen Berechnungen der Höhe und des Azimuts ohne logarithmische Rechnung durchzuführen. Durch Zerlegung des Poldreiecks in zwei rechtwinklige sphärische Dreiecke (durch Fällen eines Lots vom Gestirnsort auf den Meridian) wird ermöglicht, dass die Lösung der Haupt-aufgaben der nautischen Astronomie mit den Tafeln nach einheitlicher Methode zu erreichen ist. Um die Höhe und das Azimut eines Gestirns zu finden, geht man mit der Abweichung und dem Stundenwinkel in die Tafel und entnimmt zunächst Näherungswerte zweier Hilfsgrössen (a und b). Mit diesen findet man durch nochmaligen Eingang den der Abweichung entsprechenden Wert von b und aus diesem den Wert eines Stundenwinkels, der anstatt des aus der gegissten Länge hergeleiteten Stundenwinkels benutzt wird. Das gefundene b und die zweckentsprechend geändert Breite geben Höhe und Azimut, die also nicht für den gegissten Ort, sondern für einen Hilfspunkt gelten. Es ist jedoch nach den in den Tafeln gegebenen Anweisungen nur mit wenig Mehrarbeit verknüpft, wenn man Höhe und Azimut für das gegisste Besteck ermitteln will. Die Tafeln lassen sich, wie in der Gebrauchsanweisung ausführlich auseinander gesetzt wird, auch zur Lösung anderer Aufgaben der nautischen Astronomie mit Vorteil verwenden. So lässt sich mit den Tafeln leicht ermitteln, wenn Höhe und Azimut eines Gestirnes beobachtet sind, zu welchem Gestirne diese Grössen gehören. Auch die Ermittlung des Zeit- und des Zeithöhen-Azimuts, der Amplitude und der Höhe eines Gestirns im Ersten Vertikal usw. lässt an Bequemlichkeit nichts zu wünschen übrig, so dass sich diese Tafeln bald Freunde unter den Nautikern erwerben werden, die Höhenberechnungen ohne Benutzung der Logarithmentafeln bevorzugen. Sk.

NAUTICAL MAGAZINE, February 1910.

"Whether or no any marked simplification results from the use of the new processes is a point which the navigator may easily determine for himself, but we have no hesitation in endorsing the verdict of the Hydrographer of the U.S. Navy, that 'the plan of the work is sound in principle and scientific in conception.' The central idea is distinctly original, and the work forms an interesting addition to the literature of Nautical Astronomy."

"Altogether the book is a remarkable triumph of ingenuity, and does credit to designer and printer and publisher."—Rev. WILLIAM HALL, R.N., in the Nautical Magazine for November, 1910, page 486.

BRAZILIAN NAVY OFFICIAL OPINIONS

PARECERES OFFICIAES.

Cópia.—Ministerio da Marinha. Estado Maior da Armada. Em 15 de setembro de 1910.—Ao Sr. Vice-almirante Ministro da Marinha. Passo ás vossas mãos com os presentes papeis o parecer apresentado pelo capitão-tenente Augusto Cesar Burlamaqui, membro da commissão nomeada pelo capitão de mar e guerra João Baptista das Neves, commandante do encouraçado Minas Geraes, para estudar o trabalho apresentado pelo capitão-tenente Radler de Aquino, intitulado Altitude and Azimuth Tables. Não só pela leitura do referido parecer, como pela opinião daquelle commandante, que diz que o uso dessas taboas tornou-se generalisado a bordo durante a longa commissão emprehendida pelo mesmo encouraçado, do porto de Newcastle-on-Tyne ao desta Capital, facto este que demonstra a sua utilidade e o modo facil e pratico do seu emprego, podereis verificar que o trabalho desse intelligente e operoso official é digno de ser adoptado, pois torna de extrema facilidade o traçado da recta de posição e resolve com um grau de precisão acceitavel para a navegação um numeroso grupo de problemas. Saude e fraternidade. (Assignado) H. PINHEIRO GUEDES, Vice-almirante, Chefe do Estado Maior da Armada.

Cópia.—Commando do encouraçado *Minas Geraes*. Rio de Janeiro, 9 de setembro de 1910. N. 264.—Sr. Contra-Almirante Commandante da Divisão de Encouraçados. Cumpre-me enviar-vos o parecer apresentado pelo Sr. capitão-tenente Augusto Cesar Burlamaqui sobre o trabalho intitulado *Altitude and Azimuth Tables*, do Sr. capitão tenente Radler de Aquino. Tendo apparecido este trabalho antes da partida deste encouraçado do porto de Newcastle, nomeei uma commissão de tres officiaes do navio para dar parecer sobre o seu valor e utilidade; esta commissão era composta dos Srs. capitães-tenentes Augusto Cesar Burlamaqui, Alfredo Dodsworth e Leopoldo Nobrega Moreira. Pela leitura do parecer, podereis verificar a opinião favoravel da commissão, cabendo pela minha parte accrescentar que o uso dessas taboas tornou-se generalisado a bordo durante a commissão, facto este que demonstra a sua utilidade e o modo facil e pratico do seu emprego. Estas taboas representam mais um importante trabalho dado á publicidade pelo seu illustre e operoso autor. Saude e fraternidade. João Baptista das Neves, capitão de mar e guerra.

Ilha Grande, 10 de abril de 1910.—Passo ás vossas mãos o parecer elaborado pela commissão por vós nomeada para emittir juizo sobre o trabalho da lavra do Sr. capitão-tenente Radler de Aquino, intitulado Altitude and Azimuth Tables. Em abono das referidas taboas do estudioso official da nossa marinha de guerra vem a longa commissão desempenhada pelo couraçado Minas Geraes, sob o vosso commando, durante a qual foram verificados á saciedade os magnificos resultados fornecidos pelas taboas em comparação com os varios processos utilizados a bordo para o mesmo fim. O methodo Marcq, hoje definitivamente adoptado, encontra no inestimavel livro do Sr. capitão-tenente Radler de Aquino a sua resolução simples, rapida e segura, tornando de extrema facilidade o traçado da recta de posição e resolvendo com um gráo de precisão acceitavel para a navegação um numeroso grupo de pro-Julgo que as taboas de 360 paginas, que o Sr. capitão-tenente Radler de Aquino promette publicar, facilitarão de modo tal o calculo das coordenadas da posição do navio, que affirmo esperar o mais favoravel acolhimento por todos os que se interessam pelos progressos da navegação. - Augusto Cesar Burlamaqui, capitãotenente, instructor de navegação. Ao Sr. capitão de mar e guerra commandante do couraçado Minas Geraes, João Baptista das Neves.

OTHER WORKS OF THE AUTHOR NOT MENTIONED IN THESE TABLES

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ALTITUDE TABLES.		,
Computed for Intervals of Four Minutes between the Parallels of Latitude 31° and 60° and Parallels of Declination 0° and 24°, designed for the Determination of the Position Line at all Hour Angles without Logarithmic Computation, by Frederick Ball, M.A. (late Scholar of Exeter College, Oxford), Chaplain and Naval	g.	a.
Instructor in His Majesty's Fleet	15	0
Ditto, ditto, between the Parallels of Latitude 0° and 30° and Parallels of Declination 0° and 24°	15	0
Ditto, ditto, between the Parallels of Latitude 24° and 60° and Parallels of Declination 24° and 60°	15	0
These Tables are so arranged for working by the New Navigation that only one correct has to be applied to the altitude taken direct from the book. The entire logarith work is replaced by a single subtraction and the application of the correction. conjunction with the Nautical Almanac all the usual problems of Navigation are so	imic In	; i
The Tables have been adopted for use in the Japanese Navy.		
New Log and Versine Altitude Tables (Reprinted from the 2nd Edition of	10	6
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The Landfall of Columbus on his First Voyage to America, with a Translation of The Baron Bonnefoux's History of his previous life, also a Chart showing his Track from the Landfall to Cuba, and an outline of his subsequent voyages, by Capt. A. B. Becher, R.N. (1856)		C
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